ORIGINAL ARTICLE

Diagnostics and energetics of the topographic Rossby waves generated by a typhoon propagating over the ocean with a continental shelf slope

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Abstract

The dynamics of the subinertial response when a typhoon propagates over the ocean with a sloping bottom topography is investigated by carrying out a set of idealized numerical experiments. At least two diferent topographic Rossby waves (TRWs) are identifed at the same along-slope wavenumber and two diferent subinertial frequencies in the wavenumber– frequency spectra. The diagnostics of vorticity balance demonstrates that the bottom pressure torque plays an important role in both the generation and propagation of TRWs. Two sets of sensitivity experiments show that the spatial structure of the typhoon is a "decisive" parameter in determining the along-slope wavenumber as well as the corresponding frequencies; the along-slope wavenumber of a TRW is frst determined as a response to the typhoon-induced perturbation, and the corresponding frequencies are then determined so as to satisfy the theoretical TRW dispersion relationship. The amplitude of TRWs, in contrast, are controlled by both the typhoon radius as well as the typhoon traveling speed. For typhoons with a large radius or slow traveling speed, the resulting TRWs can be comparable to or more energetic than the near-inertial waves. This indicates that the TRWs might play an important role in inducing the near-bottom mixing along the shelf slope by using energy supplied from typhoon winds.

Keywords Topographic Rossby waves · Typhoon radius · Typhoon traveling speed · Vorticity balance · Continental shelf slope · Bottom pressure torque

1 Introduction

Most previous studies of the oceanic responses to travelling typhoons have focused on the generation and propagation of near-inertial waves (NIWs) (e.g., Gill [1984](#page-8-0); Niwa and Hibiya [1997](#page-9-0); Tada et al. [2018\)](#page-9-1), with little attention paid to subinertial waves. Recently, however, several observations have successfully captured the generation of subinertial waves in response to typhoon passages. A group of subinertial waves with a period of 2–5 days, for example,

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was observed after a hurricane traveled over the northeastern Gulf of Mexico (Teague et al. [2007](#page-9-2)). Based on an oceanic observing system in the northern Arabian Sea, Wang et al. [\(2012](#page-9-3)) observed subinertial waves with a period of 12.7 days after the passage of tropical cyclone "Gonu". Igeta et al. ([2011](#page-8-1)) also observed strong subinertial motions together with near-inertial oscillations off the eastern coast of Japan after a typhoon passage.

Topographic Rossby waves (TRWs) are representative subinertial motions resulting from the conservation of potential vorticity. They are trapped near the topography and propagate with shallower (deeper) water on their right in the northern (southern) hemisphere (Gill [1982\)](#page-8-2). The observational evidence of TRWs has been widely presented over continental shelf slopes (Thompson and Luyten [1976;](#page-9-4) Pickart [1995](#page-9-5); Oey and Lee [2002](#page-9-6); Jensen et al. [2013](#page-9-7); Rivas [2017\)](#page-9-8) and mid-ocean ridges (Miller et al. [1996](#page-9-9); Wang et al. [2012](#page-9-3)).

The generation of TRWs requires that a fluid parcel is shoved in the cross-slope direction. The conservation of potential vorticity then makes the fuid gain cyclonic (anticyclonic) relative vorticity when it is shoved onto deeper (shallower) topography. Typhoons can be an efective way to shove the fuid parcel when they travel over the sloping ocean bottom.

By solving a two-dimensional eigenvalue problem, Wang and Mooers [\(1976](#page-9-10)) showed the theoretical cross-slope structure of subinertial TRWs in the continuously stratifed ocean. It was found that the density stratifcation has an important efect on the TRW modal structure: the TRWs are bottomtrapped over the shelf slope when the local baroclinic radius of deformation is larger than the shelf width, suggesting the possibility that they can create an efficient energy pathway toward the deep ocean to induce strong mixing near the ocean bottom. This is quite diferent from the NIWs which cannot penetrate into the deep ocean due to their low vertical group velocities (Furuichi et al. [2008](#page-8-3)). Indeed, there is increasing evidence that the TRWs play a very important role in ocean mixing processes by concentrating their energy on the ocean bottom and dissipating it efficiently (Tanaka et al. [2010](#page-9-11); Damerell et al. [2012\)](#page-8-4).

However, there still remain some key questions regarding typhoon-generated TRWs: which term in the vorticity equation is responsible for the generation and propagation of TRWs, how do the properties and energetics of the generated TRWs depend on the typhoon parameters, and what controls the relative amplitudes of the TRWs with respect to the NIWs?

The western North Pacifc Ocean is the most active tropical cyclone basin in the world's oceans (Emanuel [2005](#page-8-5)). In this study, we analyze the generation and propagation of TRWs when typhoons travel over the ocean with a sloping bottom topography. For this purpose, we carry out idealized numerical experiments in which a typhoon is assumed to propagate perpendicular to the isobaths of the ocean with simplifed sloping bottom topography and a typical density stratifcation, both representative of the East China Sea (ECS). Section [2](#page-2-0) describes the numerical setting. A standard case of numerical simulation is analyzed in Sect. [3](#page-3-0). Section [4](#page-7-0) includes the discussions of the vorticity balance, the sensitivity of TRW properties to typhoon parameters, and the relative amplitudes of the TRWs with respect to the NIWs. Conclusions are presented in Sect. [5](#page-7-0).

2 Numerical setting

Numerical experiments were carried out using the Massachusetts Institute of Technology General Circulation Model which solves the free surface Boussinesq equations under the hydrostatic approximation. The model domain is 3000 km in both the zonal (*X*) and meridional (*Y*) directions, with a grid resolution of 5 km (Fig. [1](#page-1-0)a). There are 43 vertical levels with the interval varying from 10 m near the ocean surface

Fig. 1 a The model domain. The water depth increases from 200 to 2000 m eastward. The *gray solid lines* running north–south indicate the isobaths (every 400 m from 400 to 2000 m). The frequency analysis in Fig. [2](#page-2-1) is carried out along the eight *short black solid lines*. The *four red squares* denote the positions where vorticity diagnostics in Fig. [6](#page-5-0) is carried out. The *gray dashed arrow* denotes the track of the typhoon traveling westward perpendicular to the shelf slope. A snapshot of the wind stress feld with a radius of 240 km is superposed on the track. **b** A zoomed cross-sectional view of the sloping bottom topography

to 100 m at the bottom. The bottom topography only varies in the zonal direction with a shallow region (200 m in depth) westward and a deep region (2000 m in depth) eastward, connected by a slope centered at $x = 1125$ $x = 1125$ $x = 1125$ km (Fig. 1b). The gradient of the model shelf slope (0.02) is set to be close to the typical value of the ECS shelf slope.

In this study, we employ the β -plane approximation with the Coriolis parameter $f=3.1\times10^{-5}$ s⁻¹ at the south boundary of the domain and $\beta = 2.1 \times 10^{-11}$ m⁻¹ s⁻¹. The vertical viscosity and difusivity are calculated using the K-profle parameterization scheme (Large et al. [1994](#page-9-12)). The background vertical viscosity (A_z) and diffusivity (K_z) are assumed to be 10^{-4} m² s⁻¹ and 10^{-5} m² s⁻¹, respectively, whereas the background horizontal viscosity (A_H) and diffusivity (K_H) are assumed to be $10^2 \text{ m}^2 \text{ s}^{-1}$ and $10 \text{ m}^2 \text{ s}^{-1}$, respectively. A no-slip boundary condition is employed, and the bottom stress is parameterized using the quadratic law with a constant drag coefficient $C_d = 2.5 \times 10^{-3}$.

The model is initialized with a horizontally homogeneous and vertically stratifed temperature feld. We frst obtain the profles of temperature and salinity by horizontally averaging the summer and autumn mean data obtained from the World Ocean Atlas 2013 in the ECS shelf slope region (118–128°E, 22–28°N). The transport equation of salinity is closed in the model, but the employed temperature feld is derived from the profles of both temperature and salinity to refect the efects of salinity on the stratifcation.

The model is initially at rest and forced with an idealized hurricane-type wind stress feld that propagates westward with a constant speed. To prevent artificial wave reflections, sponge layers are assumed along the four open boundaries where the velocities are gradually decreased to zero toward the boundaries. The wind forcing is constructed following Price [\(1983\)](#page-9-13), which has an axisymmetric wind stress feld with a constant inflow angle of 17°. The maximum tangential wind stress is set to be 2.5 N m^{-2} . In the control experiment, the typhoon has a radius of 240 km with a traveling speed of 5 m s^{-1}. To investigate the response of TRWs to the change of typhoon parameters, we carry out a series of sensitivity experiments. The basic setting of the simulations remains the same as that in the control experiment, and only the radius and traveling speed of the typhoon are changed. The results of these sensitivity experiments are presented in Sect. [5.](#page-7-0)

3 Model results

The depth-averaged power spectra of current velocity in the frequency domain are frst examined (Fig. [2](#page-2-1)). They show marked peaks at the inertial frequency (f_0) , the inertial frequency at the latitude of the typhoon track) and its harmonics $(2f_0$ and $3f_0$) both over the flat and shelf slope regions. The spectral peaks at the inertial harmonics are in agreement with the numerical results of Niwa and Hibiya [\(1997](#page-9-0)), suggesting that these are induced by nonlinear interactions between high-vertical-mode NIWs. In addition to the inertial and inertial harmonic waves, there are two distinct subinertial peaks at $\omega \approx 0.2 f_0$ and 0.8 f_0 found only over the shelf slope region (Fig. [2](#page-2-1)b). For simplicity, we hereafter call these two subinertial waves subf1 $(0.8f_0)$ and subf2 $(0.2f_0)$, respectively.

Figure [3](#page-3-1) shows the time evolution of the bandpassed velocity along the shelf slope. Both subf1 and subf2 propagate southward with the shallow water on their right. As denoted by the black arrows in Fig. [3c](#page-3-1), d, the phase speeds of subf1 and subf2 are estimated to be 4.9 and 1.8 m s⁻¹, respectively. To further interpret the subinertial response over the shelf slope, we employ a linearized model for a continuously stratifed Boussinesq ocean with the same shelf slope as used in the simulation. Although this model was originally derived to study the coastal trapped waves (Wang and Mooers [1976;](#page-9-10) Brink [1982\)](#page-8-6), it is also applicable to the waves generated over the continental shelf slopes. In terms

Fig. 2 Depth-averaged power spectra of the numerically obtained current velocity in the **a** fat and **b** shelf slope regions. *Diferent lines in each panel* represent the results along the four zonal sec-tions shown in Fig. [1.](#page-1-0) f_0 is the inertial frequency at the latitude of the typhoon track. Two *black arrows* denote the two subinertial frequency peaks

of the pressure perturbation, $P \sim e^{i(\omega t + ly)}$, the governing equation for the waves can be written as

$$
\frac{\partial^2 P}{\partial x^2} - l^2 P + (f^2 - \omega^2) \frac{\partial}{\partial z} \left(\frac{1}{N^2} \frac{\partial P}{\partial z} \right) = 0
$$
 (1)

where *l* is the wavenumber in the *y* direction, *f* is the Coriolis frequency, and N^2 is the squared buoyancy frequency. The boundary conditions for the trapped waves consist of (1) free surface boundary, (2) no flow through the solid bottom, (3) no disturbances far offshore, and (4) no normal flow at the coast. The governing equation (Eq. [1](#page-2-2)) together with these boundary conditions form a two-dimensional eigenvalue problem. In solving this eigenvalue problem, we exploited the code presented by Brink ([2006;](#page-8-7) see also [http://www.](http://www.whoi.edu/page.do?pid=23361) [whoi.edu/page.do?pid=23361](http://www.whoi.edu/page.do?pid=23361)).

The existence of the frst two-mode TRWs, at least, can be recognized as the subinertial frequency spectral peaks on the dispersion curves at nearly the same along-slope wavenumber of ~ 2×10^{-6} cpm (Fig. [4\)](#page-3-2). Figure [5](#page-4-0)c, d shows the numerically obtained along-slope velocity felds at 500 km southward from the typhoon track associated with subf1 and subf2, respectively, which are confned near the sloping bottom due to the presence of stratifcation (Wang and Mooers [1976;](#page-9-10) Tanaka et al. [2010\)](#page-9-11) and correspond very well to the theoretical cross-slope structures of mode 1 and mode 2 TRWs shown in Fig. [5](#page-4-0)a, b, respectively. Putting all the obtained results together, we can conclude that these

Fig. 3 Time variations of the numerically obtained zonal (**a**, **b**) and meridional (**c**, **d**) velocity components at the bottom along $X = 1150$ km. The water depth is 1550 m. The velocities of subf1 (\mathbf{a} ,

c) and subf2 (**b**, **d**) are bandpassed 0.55–0.9 f_0 and 0.05–0.5 f_0 , respectively. The *black arrows* denote the phase propagation

Fig. 4 Meridional (along-slope) wavenumber–frequency spectra of the numerically obtained horizontal kinetic energy near the bottom along $aX = 1100$ km and $bX = 1150$ km. Note that these are created by calculating the meridional wavenumber spectrum for each frequency band horizontal kinetic energy. The three *lines* represent the

subinertial motions generated by the traveling typhoon are associated with the mode 1 and mode 2 TRWs propagating along the shelf slope.

theoretical dispersion curves of the frst three mode TRWs obtained by solving the eigenvalue problem (Eq. [1\)](#page-2-2). Here, *l*>0 represents the southward propagation. The other half of spectra with $l < 0$ are not shown because of their negligible values

4 Discussion

4.1 Vorticity balance

The generation mechanism of TRWs can be explained in terms of the conservation of potential vorticity $\left(\frac{f+\zeta}{H}\right)$ over the sloping

Fig. 5 *Upper panels* cross-slope distribution of the theoretically predicted along-shelf velocity associated with **a** mode 1 and **b** mode 2 TRW. The frequencies are set to be $0.8f_0$ and $0.2f_0$ in solving the eigenvalue problem for mode 1 and mode 2 TRWs, respectively. The contour units are arbitrary. *Lower panels* cross-slope distribu-

bottom (Gill [1982\)](#page-8-2). When the continental shelf slope is steep enough to dominate the potential vorticity balance, the crossisobath motions cause the stretching or shrinking of the water column, creating the cyclonic or anti-cyclonic motion. To quantitatively examine the role of each term in the generation and propagation of the TRW, the depth-integrated vorticity balance is diagnosed. By depth-integrating the momentum equations and then taking the curl of them, we can derive the depth-integrated vorticity equation as

$$
\frac{\partial \zeta}{\partial t} - \frac{\partial \eta}{\partial t} \operatorname{curl}(u, v)|_{\eta} \n= -\beta V + \frac{1}{\rho_0} J(p_b, H) - \operatorname{curl} \left[\int_{-H}^{\eta} (\mathcal{A}(u), \mathcal{A}(v)) \mathrm{d}z \right] \n+ \operatorname{curl} \left[\int_{-H}^{\eta} (\mathcal{V}_h(u), \mathcal{V}_h(v)) \mathrm{d}z \right] + \operatorname{curl} \frac{\tau_s}{\rho_0} - \operatorname{curl} \frac{\tau_b}{\rho_0}
$$
\n(2)

tion of the amplitude (*color*) and phase (*contours*) of the numerically obtained along-slope velocity along *Y*=−500 km associated with **c** subf1 and **d** subf2, which are bandpassed $0.55-0.9f_0$ and $0.05-0.5f_0$, respectively

where two operators are defined as $J(A, B) = \frac{\partial A}{\partial x}$ $\frac{\partial B}{\partial y} - \frac{\partial A}{\partial y}$ ∂B and curl(C) = $\frac{\partial C_y}{\partial x} - \frac{\partial C_x}{\partial y}$, *u* and *v* are the calculated eastward and northward velocities, respectively, $\zeta = \frac{\partial V}{\partial x} - \frac{\partial U}{\partial y}$ is the vorticity of depth-integrated velocity U and V , η is the sea surface height, H is the water depth, ρ_0 is the reference water density, p_b is the bottom pressure, operators A and V_h denote the advection and the horizontal viscosity, respectively, and $\tau_s = (\tau_{sx}, \tau_{sy})$ and $\tau_b = (\tau_{bx}, \tau_{by})$ are the wind stress and the bottom stress, respectively. The terms on the right-hand side represent the beta efect, the bottom pressure torque, the curl of the horizontal momentum advection, the curl of the horizontal viscosity, and the curl of the wind and bottom stresses. The bottom pressure torque term is induced by the pressure diference along the isobaths and is the only term related to the bottom topography (Mertz and Wright [1992](#page-9-14)).

The ratio of the second to the frst term on the left-hand side is very small $\left(\frac{\sim \Delta \eta}{H}\right)$, so that the tendency of the depth-integrated vorticity $(\frac{\partial \zeta}{\partial t})$ is balanced by the six terms on the righthand side.

Figure [6](#page-5-0) shows the time series of the diagnosed vorticity balance. In the fat region, subinertial motions are generated under the typhoon track, and the balance is mainly between the wind stress (curl $\frac{\tau_s}{\rho_0}$) and subinertial tendency $(\frac{\partial \zeta}{\partial t})$ (Fig. [6a](#page-5-0)). However, no corresponding subinertial signal can be detected 300 km southward from the typhoon track, namely, out of the typhoon radius (Fig. [6](#page-5-0)d). This means that the subinertial wave generated under the typhoon track in the fat region is a kind of forced wave and cannot freely propagate out of the direct efect of the typhoon.

As the typhoon approaches the shelf slope region, the bottom pressure torque comes into balance (Fig. [6b](#page-5-0), c). Under the typhoon track, the dominant vorticity balance becomes mainly among the subinertial tendency, the wind stress, and the bottom pressure torque. The subinertial wave can freely propagate out of the wind forcing region (Fig. [6](#page-5-0)e, f) where the subinertial tendency is primarily balanced by the bottom pressure torque.

The above analysis shows that the bottom pressure torque
 $\left(\begin{array}{cc} 1 & I(n-H) \end{array}\right)$ plays a grueial role in both the generation and $\frac{1}{\rho_0}J(p_b, H)$) plays a crucial role in both the generation and propagation of TRWs. In the presence of sloping topography, the pressure force from the topography into the ocean has a horizontal component. When this horizontal component changes along the isobaths, the diference can create the "twisting force" on the overlying fuid (Jackson et al. [2006\)](#page-9-15). For the question discussed here, disturbances induced by the approaching typhoon is the original reason that causes the change of the density feld and then the bottom pressure feld along the isobaths.

4.2 The sensitivity of TRW properties to typhoon parameters

In this section, we demonstrate how the TRW response (i.e., the frequency/along-slope wavenumber and intensity) is controlled by the typhoon parameters (radius and traveling

Fig. 6 Time series of each term in the depth-integrated vorticity equation (Eq. [2](#page-4-1)). **a**, **b**, **d**, **e** are for subf2 (0.05–0.5 f_0) and **c** and **f** are for subf1 $(0.55-0.9f_0)$ averaged within a small square area in the flat region (**a** 1600<*X*<1610 km, −5<*Y*<5 km; **d** 1600<*X*<1610 km,

−305<*Y*<−295 km) or the slope region (**b**, **c** 1100<*X*<1110 km, −5<*Y*<5 km; **e**, **f** 1100<*X*<1110 km, −305<*Y*<−295 km). The corresponding locations are also shown in Fig. [1](#page-1-0)

speed) by carrying out two sets of sensitivity experiments. In the frst set, the typhoon traveling speed remains unchanged (5 m s^{-1}) but the typhoon radius is gradually increased from 90 to 720 km. In the second set, the typhoon radius is fxed (240 km) but the typhoon traveling speed is increased or decreased by a factor of two. The basic numerical setting (e.g., bottom topography and stratifcation) in the sensitivity experiments is otherwise the same as that in the control experiment.

Figure [7a](#page-6-0) and b show the along-slope wavenumber and frequency spectra calculated using the results from the frst set of sensitivity experiments. The along-slope wavenumber spectra are obtained by averaging the wavenumber–frequency spectra over the frequency range between $0.05f_0$ and $0.95f_0$. One robust result of the wavenumber spectra is that the wavenumber of the energy peak decreases with the increase of the typhoon radius (Fig. [7](#page-6-0)a); the along-slope wavelength $(\lambda = \frac{1}{l})$ has a positive correlation with the typhoon radius (R) , and the best linear fitting between them is $\lambda = R + 230$ km with the correlation coefficient 0.92.

The frequency of the energy peak is also correlated with the typhoon radius through the TRW dispersion relationship (Fig. [7](#page-6-0)b).

Next, the results of the second set of sensitivity experiments are examined. Unlike the frst set of sensitivity experiments, the along-slope wavenumber of the spectral peak remains constant at \sim 2×10⁻⁶ cpm with two subinertial frequency peaks fixed at $0.2f_0$ and $0.8f_0$ (Fig. [7](#page-6-0)c, d). These results indicate that it is not the traveling speed but the radius of the typhoon which has a "decisive" efect on the resulting TRW properties, such as the along-slope wavenumber and frequency. This is a new fnding because previous studies have never focused on the relationship in the spatial scale between the large-scale wind forcing and subinertial ocean currents (e.g., Brooks and Mooers [1977](#page-8-8); Miller et al. [1996](#page-9-9); Wahlin et al. [2016\)](#page-9-16).

The vertical structures of the generated TRWs, on the other hand, depend on both the typhoon radius and the typhoon traveling speed (Fig. [7](#page-6-0)c, d). Although the mode 2 TRW is generally more energetic than the mode 1 TRW,

Fig. 7 The along-slope wavenumber spectra obtained by averaging the wavenumber–frequency spectra over the frequency range between 0.05 and $0.95f_0$ (a, c) with the corresponding frequency spectra obtained by averaging over the wavenumber range between 0 and 10−5 cpm (**b**, **d**). Note that the typhoon traveling speed remains

at 5 m s^{-1} and the typhoon radius is gradually increased from 90 to 720 km in **a** and **b**, while the typhoon radius is fxed at 240 km and the typhoon traveling speed is increased from 2.5 to 10 m s−1 in **c** and **d**. Each black triangle in **a** and **c** denotes the position of the maximum value

the latter amplifes as the typhoon traveling speed increases or the typhoon radius decreases. It must be noted, however, that, in this study, the dependence of the frequency and wavenumber of the generated TRWs on the typhoon radius and the typhoon traveling speed is addressed for a special case in which a typhoon travels perpendicular to the shelf slope. Changing the propagation direction of the typhoon may induce more complicated stratifed ocean responses, which remain to be examined in the future.

4.3 Predominance of NIW or TRW

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The NIWs are usually thought to be the most dominant oceanic response to traveling typhoons (e.g., Gill [1984](#page-8-0)). However, recent studies have begun to fnd that there may also exist strong subinertial motions as a response to storms passing over the oceanic topographic slopes or ridges (Dukhovskoy et al. [2009](#page-8-9); Igeta et al. [2011](#page-8-1)). To quantitatively compare the energetics between TRWs and NIWs, we calculate the vertically integrated meridional energy fuxes given by

$$
F_y = \int_{-H}^{V} p'v' dz
$$
 (3)

where the prime ()' represents the bandpass-filtered variables for the corresponding frequency range. p' and v' are thus the hydrostatic pressure perturbation and meridional velocity fltered in frequency domain, respectively, and *z*=−*H* is the ocean bottom. Once the energy fux is integrated across a zonal section over the continental shelf slope, the cumulative integral with time can be calculated as

$$
KE = \int_{0}^{t} \int_{1000 \text{ km}}^{1250 \text{ km}} F_{y} \text{d}x \text{d}t \tag{4}
$$

where $X = 1000$ and 1250 km represent the west and east boundary of the zonal section (corresponding to the shelf slope region), respectively. Equation [4](#page-7-1) thus represents the typhoon-generated wave energy propagating in the meridional direction across the zonal section over the shelf slope.

Figure [8](#page-7-2) shows an example of the time-cumulated integral of energy fux. The results of diferent sensitivity experiments are summarized in Fig. [9.](#page-8-10) As discussed in Sect. [4.2,](#page-5-1) the typhoon radius and traveling speed both control the amplitude of TRWs. Figure [9](#page-8-10) shows that the subinertial energy can be comparable to or more than the near-inertial energy for typhoons with large radii (480 and 720 km) or a slow traveling speed (2.5 m s^{-1}) . This indicates that, under these particular conditions, TRWs can carry more energy along the shelf slope than NIWs.

Fig. 8 The cumulative integral of energy fux with time through the zonal section between *X*=1000 and 1250 km along *Y*=−240 km (240 km southward from the typhoon track) (Eq. [4\)](#page-7-1). The typhoon has a radius of 240 km and a traveling speed of 2.5 m s^{-1} . This zonal section thus locates at the southern edge of the typhoon. The results for the NIW, and mode 1 and mode 2 TRWs are calculated from the hydrostatic pressure perturbation and velocity bandpassed $0.95-1.3f_0$, 0.55–0.9 f_0 , and 0.05–0.5 f_0 , respectively. Note that the negative sign in the cumulated energy fux is omitted here

The generated wave energy is closely related to the predominant frequency of the wind stress feld. In this linear system, more energy is injected into the waves with the frequencies close to those of the predominant wind stress feld. This induces the energy peaks of the NIW and mode 1 TRW at the typhoon radii of 240 and 360 km (Fig. [9a](#page-8-10)), respectively. Since the TRWs are bottom-intensifed, they may directly change the near-bottom mixing along their path. More realistic numerical simulations are needed to document the dissipation processes of the typhoon-generated TRWs as well as their efects on the water-mass deformation and the circulation system in the ECS.

5 Conclusions

This study has focused on the subinertial waves excited by a typhoon traveling over the ocean with a continental shelf slope. The idealized numerical simulations with a simplifed sloping topography and stratifcation typical of the East China Sea have demonstrated that, in addition to the inertial waves and their inertial harmonics, subinertial waves have been excited with their energy peaks at $\omega = 0.2 f_0$ and 0.8 f_0 . These subinertial waves follow the theoretical dispersion curves of the TRWs, and at least the frst two modes can be clearly identifed to be bottom-trapped with their amplitudes increasing toward the seabed. The main conclusions are as follows:

Fig. 9 The time-cumulated zonally-integrated energy fuxes that pass the zonal sections at the southern edges of typhoons (*Y*=−*R*) until 25 f_0 (Eq. [4\)](#page-7-1). The typhoon traveling speed remains at 5 m s⁻¹ and the typhoon radius is gradually increased from 90 to 270 km in **a**, whereas the typhoon radius is fxed at 240 km and the typhoon trave-

ling speed is increased from 2.5 to 10 m s^{-1} in **b**. The corresponding predominant frequencies of different wind stress fields (ω/ω_f) are shown on the *top axes*. Note that all the negative signs in the cumulated energy fuxes are omitted here

- 1. The diagnostics of the depth-integrated vorticity balance associated with the TRWs show that the subinertial tendencies are balanced by the wind stress and the bottom pressure torque in the wind forcing region over the shelf slope, and are primarily balanced by the bottom pressure torque out of the wind forcing region. The vorticity analysis thus demonstrates the importance of the bottom pressure torque in both the generation and propagation processes of TRWs. In contrast, in the fat region, although subinertial motions are also generated immediately below the typhoon track, they remain as forced waves and no subinertial signal can be detected out of the typhoon track.
- 2. Two sets of sensitivity experiments show that the typhoon radius is a "decisive" parameter in determining the frequency and wavenumber of the generated TRWs; the along-slope wavenumber of the generated TRWs is frst determined by the typhoon radius, and the frequency is next determined so as to satisfy the dispersion relationship.
- 3. The vertical structures of the generated TRWs (such as which of the mode 1 and 2 TRWs becomes dominant) are determined by both the typhoon radius and the typhoon traveling speed. Furthermore, energetics analysis shows that for a typhoon with a large radius or slow traveling speed, the subinertial TRW can transport comparable or more energy southward than the near-inertial waves. This indicates that the TRWs might play an important role in inducing the near-bottom mixing along the shelf slope by using energy supplied from typhoon winds.

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