

In situ IV and CV characterization of Pt/n‑GaN Schottky barrier diodes irradiated by 100 MeV oxygen ions

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ABSTRACT

Pt/n-GaN Schotky diodes were fabricated on metal organic chemical vapor deposition grown epitaxial GaN thin flms. Temperature-dependent electrical characterizations current–voltage and capacitance–voltage were performed in the temperature range of 80–500 K. Barrier inhomogeneity calculations of the pristine Schotky barrier diodes were performed. Furthermore, these devices were irradiated with 100 MeV oxygen ions in fluencies ranging from 10^{10} to 10^{14} ions/cm². In situ current–voltage and capacitance–voltage measurements were performed after each fuence. The Schotky barrier height and ideality factor increased, whereas the carrier concentrations decreased with an increase in the ion fuence. The results were interpreted based on the thermionic emission model and energy loss mechanism of the ion beam in GaN.

1 Introduction

GaN-based Schotky barrier diodes (SBDs) have various technological applications in power electronics, optoelectronic devices, and space because of their unique properties such as wide bandgap, radiation hardness, high saturation velocity, and high breakdown voltage $[1, 2]$ $[1, 2]$ $[1, 2]$ $[1, 2]$ $[1, 2]$. It is essential to analyze the variation in the device parameters of the SBD, such as the ideality factor, Schottky barrier height (SBH), carrier concentration, and series resistance with temperature and ion irradiation for the sustainability of these devices working under variable temperatures and radiation harsh space applications. Metal–semiconductor (MS) contacts with large SBHs, high rectifcation efficiencies, and low reverse leakage currents are required in applications such as power rectifers and HEMTs [[3\]](#page-6-2). As specified by the Schottky–Mott model, the SBH depends on the metal work function and semiconductor electron affinity (4.1 eV for GaN) $[3-5]$ $[3-5]$ $[3-5]$. Platinum (Pt) metal is suitable for use as a Schotky contact on n-type GaN because of its high work function

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 (5.65 eV) and corrosion and oxidation resistance [[3\]](#page-6-2). There is not much literature on in situ experimental investigations of swift heavy ion (SHI) irradiation, especially for the MS interface, which is the subject of the current work. Radiation afects the properties of GaN depending on the type of radiation energy and doping [\[6](#page-6-4), [7](#page-6-5)]. According to previous reports, the production of point defects, their migration, and annihilation, as well as a few other parameters, infuence the damage mechanism in GaN at keV energies [\[7](#page-6-5), [8\]](#page-7-0). In the keV regime, ions are implanted in the near-surface region, whereas in the SHI regime (energy \geq of 1 MeV/ amu), ions reach the substrate in the epitaxial flms [[9](#page-7-1)]. As a result, controlled changes at the MS interface can be accomplished either by creating new defects or by annealing existing defects [[8,](#page-7-0) [10](#page-7-2)]. Several reports have been published on temperature-dependent current transport in Silicon and GaAs-based Schotky diodes [\[11–](#page-7-3)[13](#page-7-4)]. Variations in the ideality factor and SBH with the fluence in metal/n-GaN Schottky diodes have been reported [\[14](#page-7-5)–[17\]](#page-7-6). These results are linked to the modifcation in the interface state density at the MS contact afected by heating and defect formation caused by irradiation. Recently, temperature-dependent current–voltage (*I*–*V*) and capacitance–voltage (*C*–*V*) characteristics of Ni/n-GaN SBDs were studied by Yildirim [[18\]](#page-7-7). However, few reports on the effects of temperature and ion irradiation on Pt/GaN Schotky diodes, are available in the literature. One such report by Kumar et al. highlighted *I*–*V* characteristics and Hall effect measurements of a Pt/GaN Schottky diode at temperatures in the range of 200–380 K [\[16\]](#page-7-8).

In this study, SBDs were fabricated using Pt metal and GaN epitaxial layer on a sapphire substrate. In situ *I*–*V* and *C*–*V* characterizations of Pt/n-GaN SBDs were performed to observe the variation in electronic parameters under the infuence of varying temperatures in the range of 80–500 K and ion fuences of 100 MeV oxygen ion irradiation from 1×10^{10} to 1×10^{14} ions/cm² .

2 Experimental

GaN epitaxial layer (\sim 4 µm) used in the fabrication of the Schotky contacts were obtained by MOCVD technique *µ* grown on a c-plane sapphire substrate. Before fabrication, the GaN epitaxial layers were chemically cleaned sequentially using trichloroethylene, acetone, and isopropyl alcohol solutions in an ultrasonic bath

for 10 min each followed by rinsing with deionized (DI) water for 5 min. Immediately before metallization, the oxide contaminant was removed by dipping the samples in a HCl: $H₂O$ (1:1) solution for 1 min and then in DI water. Deposition of Pt flms of 100 nm on the n-GaN epitaxial layer was carried out using an electron beam deposition system. The base pressure of deposition was 10^{-8} mbar. For the characterization, small indium ohmic contacts were planted on the diode samples at two opposite edges via soldering. The diodes were irradiated with 100 MeV oxygen ions using the Pelletron accelerator facility available at IUAC, New Delhi. The fuences of the ion beams varied from 1×10^{10} to 1×10^{14} ions/cm². The ion beam was focused at an angle of 7° to avoid channeling. In situ *I*–*V* and *C*–*V* characterization of the diodes were performed using an Agilent Semiconductor Analyzer. Before the irradiation experiments, temperaturedependent electrical characterizations were performed at various temperatures in the range of 80–500 K by increasing the temperature by 30 K in each step using an LN2 Optistat DNV cryostat and a temperature controller (Oxford Instruments ITC503).

3 Results and discussion

3.1 *I***–***V* **characterization of Pt/GaN SBD**

The *I*–*V* characteristics were determined by varying the temperature to analyze the variations in the SBD parameters. The reverse and forward bias characteristics of the Pt/n-GaN SBD at various temperatures ranging from 80 to 500 K are shown in Fig. [1a](#page-2-0). A thermionic emission model was used to ft the experimental data [[4,](#page-6-6) [5](#page-6-3)].

$$
I = I_{\rm S} \left[\exp\left(\frac{q(V - IR_{\rm S})}{\eta k_{\rm B} T} \right) - 1 \right],\tag{1}
$$

where I_{S} , *V*, R_{S} , and η are the saturation current, bias voltage applied across the barrier, series resistance, and the ideality factor, respectively. The SBH expression is given by

$$
\phi_{\rm B} = \frac{k_{\rm B}T}{q} \ln \left(\frac{AA^* T^2}{I_{\rm S}} \right),\tag{2}
$$

where *T*, A , ϕ _B, and A^* represent the temperature of the diode, efective area of the MS contact, **Fig. 1 a** *I*–*V* characteristics of Pt/n-GaN SBD with varying temperature from 80 to 500 K, **b** variation of measured SBH and ideality factor with the temperature (based on *I*–*V*), **c** *C*–*V* curves of Pt/n-GaN SBD and inset shows $1/C^2$ vs. *V* curves for reverse bias voltage at a varying temperature in the range 80–500 K, and **d** variation of SBH and carrier concentration vs. temperature of Pt/n-GaN SBD (based on *C*–*V*)

barrier height, and the efective Richardson constant, respectively.

Using the above thermionic emission equation, the ideality factor *η* was calculated using the slope of the linear fit to the *I*–*V* characteristics between $log(I)$ and *V* in the forward bias region. The intercept of the linear ft on the *y*-axis was expressed as the saturation current [[19\]](#page-7-9). The SBH was calculated using Eq. ([2\)](#page-1-0). The series resistance was calculated from the forward *I*–*V* characteristics using the Cheung and Cheung method [[20\]](#page-7-10). The diode parameters are listed in Table [1](#page-3-0) and the changes in the SBH and *η* with temperature are shown in Fig. [1b](#page-2-0). Ideality factor decreased from 5.5 to 1.24, while SBH increased from 0.17 to 0.81 eV, when temperature increased from 80 to 350 K. The increased value of η at lower temperatures indicates a deviation in the current transport from thermionic emission in the SBD [[21](#page-7-11)]. This deviation might have occurred because of the presence of other current transport phenomena, such as tunneling and feld emission [\[16](#page-7-8)]. At elevated temperatures, *η* improved and found to be 1.16 at 410 K. This means that the factor responsible for current transport, that is tunneling/ feld emission, decreased with increasing temperature. Another important parameter is SBH, which is related to the electric feld developed at the MS junction. It also increased with increasing temperature. The calculated experimental data for the series resistance displayed in Table [1](#page-3-0) show that it decreases with increasing temperature.

3.2 *C***–***V* **characterization of Pt/GaN SBD**

The *C*–*V* measurement of a SBD is dependent on temperature and is an important aspect of interest that can clarify the Fermi energy, built-in voltage, carrier concentration, and SBH. The variation in the capacitance of SBD can be expressed as follows [[4,](#page-6-6) [5\]](#page-6-3),

$$
C = \sqrt{\frac{q\epsilon_s \epsilon_0 A^2 N_D}{2(V_{bi} + V)}} = \frac{\epsilon_S}{w'},
$$
\n(3)

where *q* is the electronic charge, ε_0 is the permittivity of free space, ε _s is the dielectric constant, *A* is the cross-sectional area of the contact, $V_{\rm bi}$ is the built-in voltage, and N_D is the carrier concentration. The capacitance of the diode was measured at 1 MHz. The *C*–*V* characteristic curves of the Pt/n-GaN SBD at various temperatures in the range of 80–500 K are shown in Fig. [1](#page-2-0)c. The carrier concentration was calculated using the slope obtained from the graph between $1/C^2$ and *V* according to the following equation as

Table 1 Calculated Schottky parameters with varying temperatures in the range of 80–500 K of Pt/n-GaN SBD from temperature dependent *I*–*V* and *C*–*V* analysis

$$
N_{\rm D} = \left(\frac{2V}{q\epsilon_{\rm S}A^2 \times \text{slope}}\right) = \frac{2V}{q\epsilon_{\rm S}A^2 \frac{\text{d}(C^{-2})}{\text{d}(V)}}\tag{4}
$$

and SBH related to built-in potential can be determined from the following equation

$$
\phi_{\rm ap} = \text{Intercept} * q \epsilon_{\rm S} A^2 \frac{N_{\rm d}}{2} + \left(\frac{kT}{q}\right) \ln\left(\frac{N_{\rm c}}{N_{\rm d}}\right). \tag{5}
$$

 here Intercept is the intercept on the *y*-axis in the curve plotted between $1/C^2$ and V , and N_C is the effective charge state concentration in the conduction band. The parameters determined from the *C*–*V* analysis are listed in Table [1](#page-3-0) and shown in Fig. [1d](#page-2-0). It can be seen from the data that there is an increment in carrier concentration from 1.05×10^{17} to 8.67×10^{17} cm⁻³ and in SBH from 0.22 eV to 1.06 eV as temperature increases from 80 to 500 K.

This type of dependence of the SBH on temperature is generally described in terms of the energy band gap of semiconductors, which can fuctuate with temperature. Nevertheless, in an actual Schottky diode, the temperature coefficient of the energy bandgap is often considerably diferent from that of the SBH. Many reports have specifed various distinct causes for such non-ideal behaviors. Werner and Gütler reported that this type of behavior arises from Schotky barrier inhomogeneity [\[18](#page-7-7), [22](#page-7-12)[–24](#page-7-13)] present at the interface [\[25\]](#page-7-14). This inhomogeneity arises because of many factors, such as the diode fabrication process, material preparation, surface defect density, and local increase in the electric field, which can also cause a local reduction in the SBH. Consequently, the transport current became inhomogeneous. The ideality factor *η* greater than one in the *I*–*V* curves results from the shape and location of the peaks in the potential barriers which are dependent on the bias voltage. Using the weighted data of the Gaussian distribution across all patches and the thermionic emission current expression with each value of SBH, the total current can be obtained in SBDs. The model indicates that the perceived SBH is consistently less than the barrier distribution' mean value and is given by the following equations [\[22](#page-7-12), [26\]](#page-7-15).

$$
\phi_{\rm ap} = \phi_{\rm bo} - \frac{q\sigma_{\rm SO}^2}{2kT}.\tag{6}
$$

here ϕ_{an} is the apparent SBH calculated in the forward region of the diode, and σ_{so} is the standard deviation of the SBH distribution at zero bias and the barrier homogeneity measure with negligible temperature dependence. ϕ_{bo} is the mean SBH at zero bias. By plotting the graph between ϕ_{ap} and $1/2kT$, we obtained the value of $\sigma_{\rm so}^2$ from the slope and $\phi_{\rm bo}$ from the intercept. The variation in *η* is given as

$$
(\eta^{-1} - 1) = -\rho_2 - (9\rho_3/2kT). \tag{7}
$$

The non-dependence of *η* on the bias requires a linear dependence of SBH and the square of the standard deviation on the bias voltage. Parameters ρ_2 and ρ_3 are the voltage coefficients of the mean SBH and the standard deviation square, respectively. Details of the calculations can be found elsewhere [[17](#page-7-6)]. Three sets of $\sigma_{\rm so}^2$, $\phi_{\rm bo}$, ρ_{2} , and ρ_{3} in the temperature ranges of 80–140 K, 170–260 K, and 290–500 K are shown in Fig. [2a](#page-4-0). The linearity of the graph depicts adherence to the barrier inhomogeneity model.

Similarly, for the Richardson plot, the modifed saturation current equation is given as

$$
\ln\left(\frac{I_0}{T^2}\right) - \frac{q^2 \sigma_{\rm so}^2}{2k^2 T^2} = \ln\left(AA^{**}\right) - \left(\frac{q\phi_{\rm bo}}{kT}\right). \tag{8}
$$

Using the above expression, a modifed Richardson plot was obtained by ploting the LHS of the equation as a function of 1/kT. Using linear fting, the modifed Richardson constant was determined from the intercept and ϕ_{bo} from the slope [[27](#page-7-16)]. Theoretically, for n-GaN, A^{**} is 26.4 $A/(cm^2K^2)$. Three plots were obtained for three values of $\sigma_{\rm so}^2$, and thus three different Richardson constants and SBH were obtained for three temperature ranges (80–140 K, 170–260 K, and 290–500 K), as listed in Table [2](#page-4-1) and are shown in Fig. [2](#page-4-0)b [[16\]](#page-7-8). When moving from the low-temperature range to the high-temperature range, the value of the Richardson constant also approached the theoretical value. These types of SBDs with large barrier heights are suitable for many power electronic applications.

3.3 Ion irradiation efect on Pt/GaN SBD

The samples were then irradiated at 300 K with 100 MeV oxygen ions using a Pelletron accelerator

Table 2 Calculated mean SBH, Richardson's constant from the barrier inhomogeneity model

Temperature range (K)	Mean SBH (eV)	Richardson's constant (A) cm^2K^2
$80 - 140$	0.496	47.97
$170 - 260$	0.99	39.49
290-500	1.584	30.12

. at IUAC, New Delhi. The *I*–*V* and *C*–*V* data were obtained at 300 K for ion fluencies ranging from 1×10^{10} to 1×10^{14} ions/cm². The analysis of the SBH and ideality factor was repeated using Eqs. $(1-5)$ $(1-5)$ $(1-5)$, as explained above. An increase in the SBH and a decrease in *η* with increasing ion fluence were observed as shown in Fig. [3](#page-5-0)a. The parameters determined from the *I*–*V* analysis of the irradiated samples are listed in Table [3](#page-5-1).

C–*V* data were obtained for the irradiated sample, and the carrier concentration was determined from the slope, whereas the SBH was obtained from the intercept of the $1/C^2$ vs. voltage (*V*) curves at diferent fuences. The changes in the carrier concentration and SBH with the fuence are shown in Fig. [3b](#page-5-0). It was observed that SBH increased while the carrier concentration decreased with an increase in the ion fuence. The increase in the ideality factor and decrease in the carrier concentration with an increase in fuence can be easily understood because the ion beam is expected to cause damage at the MS interface as well as the bulk of GaN. However, most reported irradiation investigations with heavier

Fig. 2 a Variation of SBH (square symbol) and $\eta^{-1} - 1$ (triangle symbol) vs. 1/2kT curve (triangle symbol) of Pt/n-GaN SBD, **b** modifed Richardson plot of $\left[\ln\left(\frac{I_0}{T^2}\right) - \frac{\dot{q}^2 \sigma_{so}^2}{2k^2 T^2}\right]$ *vs* $\frac{1}{kT}$. Three plots were obtained for three values $\sigma_{\rm so}^2$ as represented by the symbols triangle, circle, and square for given temperature ranges (80– 140 K, 170–260 K, and 290–500 K), respectively

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Table 3 Calculated parameters of irradiated Pt/n-GaN SBD from *I*–*V* and *C*–*V* characteristics.

The blank spaces in this table indicate the unavailability of results due to the presence of noise in the system

ions (200 MeV Ag and 150 MeV Au) in GaN devices showed a decrease in the SBH values after irradiation [[28](#page-7-17)[–31\]](#page-7-18). The present SBH trend can only be understood by considering the oxygen ion-GaN interaction mechanism in detail. When an ion enters a material, it loses energy via two mechanisms electronic energy loss (S_E) and nuclear energy loss (S_N) . For oxygen ions (100 MeV), the former loss mechanism is dominant in epitaxial GaN thin films $(5 \mu m)$ thick). The nuclear energy loss process dominates only at the end of the ion range, which is in the sapphire region in the present samples. Because of this energy transfer, the GaN latice temperature spikes for a very short duration. However, the maximum latice temperature reached for the 100 MeV oxygen ion is ∼ 530 K, which is signifcantly lower than the melting point of GaN (2773 K) [[32](#page-7-19)]. Thus, no local melting or permanent cluster/track formation occurred

for oxygen ions in the present case. Furthermore, a simple SRIM/TRIM calculation for 100 MeV oxygen ions in GaN showed that each oxygen ion created approx. 9.5 vacancies. This shows that small point defects were still produced, which might contribute to the electrically active defect states (charge trap levels and scatering centers) in the bandgap. As a result, the carrier concentration and conductivity of GaN decreased with increasing fuence, as observed in our case. The measured value of SBH (φ_{av}) is given as the diference between the ideal barrier height (*φ*b) *and* Schotky barrier lowering factor (*Δφ*b), that is, φ_{ap} *=* φ_b −Δ φ_b . Factor Δ φ_b depends on the carrier (dopant) concentration of the sample (α (N_D^+)^{1/4}) [[5](#page-6-3), [28](#page-7-17), [29](#page-7-20)]. The decrease in N_D^+ with irradiation fluences results in a reduced $\Delta\varphi_{\rm b}$ factor, and hence, an increased value of SBH at higher fuence values. At higher fuences, the accumulated defects degrade

device properties by providing leakage paths, and alternate transport mechanisms. The increased value of the ideality factor is a clear indication of the presence of a non-thermionic emission current transport mechanism. For GaN-based SBDs irradiated by heavier ions (Ag and Au), defect accumulation and device degradation begin at much lower fuences because the energy transferred to the latice per ion is much larger [\[30–](#page-7-21)[33](#page-7-22)].

4 Conclusion

Pt/n-GaN Schottky diodes were fabricated and investigated using temperature-dependent *I*–*V* and *C*–*V* measurements. An increase in the SBH and a reduction in the ideality factor were observed, whereas the series resistance decreased with increasing temperature. Barrier inhomogeneity was observed in the samples, as the diode samples exhibited diferent mean barrier heights under diferent temperature regimes. The Richardson's constant was found to be close to the theoretical value of 26.4 $A/cm² K²$ in the temperature range of 290–500 K. In situ irradiation studies of the device with oxygen ions (100 MeV) showed that the SBH enhanced in both the *C*–*V* and *I*–*V* analysis as the fuence of irradiation increased. The ideality factor and carrier concentration determined from the *C*–*V* analysis decreased with increasing fuence. A beter understanding of the defect evolution in GaN-based devices in harsh environments with high temperatures and radiation is necessary for potential low-earth satellite applications. Further studies with diferent ion types and energies are required to fully understand the mechanism and predict device behavior and lifetime for such applications.

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Author contributions

NK: performed the electrical measurements, analyzed the results, and wrote the manuscript. AK: planned the investigation, performed the in situ measurements, and helped in writing the manuscript. RP: and RB: helped with analysis and manuscript review. RM and KA: provided assistance in situ measurements. FC and DK: provided mentorship and revised the manuscript.

Data availability

Data supporting the fndings of this manuscript are available from the corresponding author upon reasonable request.

Declarations

Conflict of interest I, corresponding author, declare that we have no known competing fnancial interests or personal relationships that could have appeared to infuence the work reported in this paper.

Ethical approval The study was approved by the Ethics Commitee of Inter University Accelrator Centre (IUAC), New Delhi, India. There was not done any experiment involving humans and animals.

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