

# Structure and property of lead-free (K,Na)NbO<sub>3</sub>–(Bi<sub>1/2</sub>Na<sub>1/2</sub>) ZrO<sub>3</sub>–CaTiO<sub>3</sub> piezoelectric ceramics

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#### Abstract

Simultaneous improvement of piezoelectricity and temperature stability is vital for developing high-performance KNNbased lead-free materials. Here, effects of CaTiO<sub>3</sub> on phase structure, piezoelectricity and temperature stability of (1 - x) $[0.95(K_{0.5}Na_{0.5})NbO_3-0.05(Bi_{0.5}Na_{0.5})ZrO_3]-xCaTiO_3-0.2\%MnO_2$  ceramics were studied. It was found that the orthorhombic-tetragonal phase transition temperature can be gradually decreased by increasing CaTiO<sub>3</sub> content. Particularly, the improved strain temperature stability (strain varied < 15% when measurement temperature reaches 110 °C) and enhanced electrical properties ( $d_{33} \sim 296$  pC/N and strain ~ 0.14%) can be observed in the ceramics with x = 0.02. Therefore, shifting the  $T_{O-T}$  below room temperature is an effective way to promote temperature stability and electrical properties of KNNbased piezoelectric materials.

## 1 Introduction

Since  $Pb(Zr,Ti)O_3$  (PZT) was reported as a ferroelectric solid solution in 1952, numerous researches have been conducted because of excellent piezoelectricity and high Curie temperature [1–4]. However, the lead oxide content in lead-based ceramics is about 60%, which can cause great harm to the environment and human health [5, 6]. With the improvement of science and technology, the awareness of environmental protection has gradually increased, and countries like the European Union, Japan and China have successively enacted laws that restrict or inhibit the use of harmful materials such as lead [6, 7]. Therefore, developing lead-free piezoelectric materials that can replace PZT-based piezoceramics has great social-economic significance.

Lead-free piezoceramics can be mainly divided into three types, including bismuth layer structure, tungsten bronze structure and perovskite structure [5]. Bismuth layer ceramics belong to strontium perovskite structure and are suitable for applications in high temperature and high frequency fields, but have a low piezoelectric performance; Tungsten bronze structure ceramics possess a high spontaneous polarization, high Curie temperature and a large optical

☑ Jiagang Wu wujiagang0208@163.com; msewujg@scu.edu.cn nonlinearity, which can be used in electro optical crystals, but those ceramics are hardly sintered into dense ceramics and not easily polarized; Perovskite structure ceramics have attracted more and more attentions due to their excellent performance, which is one of the hot topics in the field of lead-free piezoelectric ceramics [5, 6]. Currently, perovskite-type lead-free piezoelectric ceramics mainly have three types: BaTiO<sub>3</sub>, Bi<sub>0.5</sub>Na<sub>0.5</sub>TiO<sub>3</sub> and K<sub>0.5</sub>Na<sub>0.5</sub>NbO<sub>3</sub> [8-10]. Furthermore, Bismuth (BiFeO<sub>3</sub>), one of the leadfree materials, is a multiferroic material with a distorted rhombohedral perovskite structure [11]. BiFeO<sub>3</sub> has a high remanent polarization and high Curie temperature, but the volatilization of Bi and the valence fluctuations of Fe ions in the high temperature sintering process can induce the structure loose and high leakage current [12, 13]. Lots of researches have been carried out to ameliorate the drawbacks as well improve electrical properties, including the adulteration of various ions and the addition of ABO<sub>3</sub>-type perovskites [14-16]. BaTiO<sub>3</sub>-based ceramics are the first lead-free piezoelectric ceramics to be discovered, but the low Curie temperature and high sintering temperature limit its applications. Bi<sub>0.5</sub>Na<sub>0.5</sub>TiO<sub>3</sub> ceramics have large remanent polarization. Although the improvements in energy storage performance, piezoelectricity and temperature stability have been realized through constructing binary and ternary compounds by doping ions or other perovskites [17–20], the existence of depolarization temperature seriously limits its development. KNN ceramics were invented

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in 1959 [1, 10]. Currently, piezoelectric properties of KNN based ceramics can be effectively enhanced by constructing phase boundaries and optimizing experimental conditions [21–28]. Besides, By introducing local structural heterogeneity, the averaged free energy profile of a ferroelectric is possible to be further flattened and thus high piezoelectricity can be achieved [29–31]. However, the temperature stability of electrical properties is often degraded [32–36]. Previously, it was thought that the addition of CaTiO<sub>3</sub> can shift the  $T_{O-T}$  of KNN-based ceramics, and then the stability of electrical properties can be improved [37]. Unfortunately, the stability enhancement is achieved at the expense of piezoelectricity [37, 38]. Therefore, how to achieve the balanced development of piezoelectric properties and temperature stability of the ceramics is a critical consideration for us. Thus, we expect to obtain the  $(1 - x)[0.95(K_{0.5}Na_{0.5})]$ NbO<sub>3</sub>-0.05(Bi<sub>0.5</sub>Na<sub>0.5</sub>)ZrO<sub>3</sub>]-xCaTiO<sub>3</sub>-0.2%MnO<sub>2</sub> ceramics with good piezoelectricity and large usage temperature range by adding CaTiO<sub>3</sub>. Through the composition design, we realize the enhancement of both temperature stability and piezoelectric properties by modifying the CT contents. In addition, the underlying physical mechanisms have been illuminated.

### 2 Experimental process

The  $(1 - x)[0.95(K_{0.5}Na_{0.5})NbO_3 - 0.05(Bi_{0.5}Na_{0.5})]$  $ZrO_{3}$ ] - x C a T i O<sub>3</sub> - 0.2 % M n O<sub>2</sub> [(1 \_ (KNN-BNZ)-xCT-MnO<sub>2</sub>] ceramics were prepared by the convention solid-state method using  $K_2CO_3$ , Na<sub>2</sub>CO<sub>3</sub>, Nb<sub>2</sub>O<sub>5</sub>, Bi<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub>, CaCO<sub>3</sub>, TiO<sub>2</sub> and MnO<sub>2</sub> as raw materials. An excess 0.2 wt% MnO2 was added as

a sintering aid to improve densification of the ceramics during the sintering process. These raw materials were weighed and ball milled with ethanol for 24 h. Then, the evenly mixed pastes were dried using a heating lamp and calcined at 850 °C for 6 h. After that, these powders were mixed with 8% PVA binder and pressed into small disks with 10 mm in diameter. After removing the binder by heating the pellets at 850 °C for 2 h, the disks were sintered at 1080-1120 °C for 3 h. Subsequently, the both sides of the sintered ceramics were covered with silver and the samples were fired at 600 °C for 10 min for measuring their electrical properties. Finally, all the specimens were polarized at room temperature in the silicon oil bath under a dc field of 3 kV/mm for 20 min.

The phase structure of the ceramics was tested by X-ray diffraction (Bruker D8 Advanced XRD, Bruker AXS Inc., Madison, WI, CuKa). The sintered sample was triturated into powders, and a high-resolution X-ray diffraction (X' Pert Pro MPD (DY 120 PANalytical, Netherlands)) was used to collect the XRD data of the powders for the Rietveld refinement, and then the Maud software was used for data fitting. The surface microstructure of the ceramics was characterized by a scanning electron microscope (JSM-7500, Japan). The temperature dependence of  $\varepsilon_r$  and tan $\delta$  were measured by LCR analyzer (HP 4980, Agilent, U.S.A.). A TF-2000 was used to measure the P-E hysteresis loops, electric field-induced strain and unipolar strain of the samples at 10 Hz. A quasi-static  $d_{33}$  meter (ZJ-3 A, China) and an impedance analyzer (HP 4194 A) were used to test the  $d_{33}$ and  $k_{\rm P}$ , respectively.



MnO<sub>2</sub> ceramics



Fig. 2  $\varepsilon_r$  of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics with  $\sim -150$  °C -200 °C, measured at f=100 kHz

## 3 Results and discussion

Figure 1a shows the XRD patterns of the ceramics, measured at room temperature and  $2\theta = 20^{\circ}-60^{\circ}$ . As shown in Fig. 1a, a pure perovskite structure is shown and no secondary phase can be observed in the all ceramics, indicating that BNZ, CaTiO<sub>3</sub> and MnO<sub>2</sub> have completely entered into the KNN matrix and formed a stable solid solution. To characterize the phase structure of all the ceramics clearly, we conduct the expended XRD patterns in the 2 $\theta$  range of 44°-47°, as shown in Fig. 1b. We can see from Fig. 1b that there are two separated peaks at  $2\theta = 45^{\circ}-46^{\circ}$  when x = 0-0.03. The diffraction peak



**Fig. 3** a Rietveld refinement of XRD results with x = 0.02, b Enlarged Rietveld refinement of XRD patterns with x = 0.02

of high angle is clearly stronger than that of low angle, imaging the existence of tetragonal phase [39].

For further analyzing the phase evolution of the ceramics, we measured the temperature dependence of dielectric constant of all the samples, as shown in Fig. 2. The  $T_{\rm O-T}$  of the ceramics gradually decreases from 50 °C to - 29 °C as the CT content increases, indicating that the doping of Ca<sup>2+</sup> ions can significantly decrease the  $T_{O-T}$ of the ceramics far below the room temperature. So the ceramics with x = 0.02 ( $T_{O-T} \sim -7$  °C) can be considered as a pure T phase at room temperature. To further investigate the phase structure of the ceramics, the XRD pattern of the ceramic with x = 0.02 in powder form was measured. Figure 3a, b show the Rietveld refinement and the enlarged Rietveld refinement, respectively. Table 1 lists the detailed refinement results. The original XRD data well matched the fitting data, and a low  $R_w$  (4.84%) as well a low Sig (1.56) value can be observed in the fitting process, illustrating that we chose the decent phase structure mode for the ceramic (x = 0.02). Besides, the XRD results of the Rietveld refinement also confirm the existence of T phase with x = 0.02. The ceramics with x = 0.04 - 0.05 should be T-pseudo cubic coexistence phase, according to the XRD patterns (Fig. 1),  $d_{33}$  curves (Fig. 6) and P-E loops (Fig. 7). However, the T-pseudo phase boundary is restrained with the further increase of CT contents (x = 0.04 - 0.05), and becoming a diffused peak because of the decreased grain size, as shown in Figs. 2g, h and 4a [40]. In addition, the phase diagram of the  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics can be established according to the temperature dependence of  $\varepsilon_r$  in Figs. 2 and 4a, as shown in Fig. 4b. It can be seen that  $T_{O-T}$  and  $T_C$  drop with increasing CT contents. Finally, we can give the phase structure of the ceramics by the XRD patterns, the  $\varepsilon_r - T$  curves and the Rietveld

**Table 1** Rietveld refinement ofXRD results with x = 0.02

x (phase)	e) Cell parameters				Content (%)	Rw (%)	Sig
	a (Å)	b (Å)	c (Å)	$\alpha(=\gamma=\beta)$ (°)			
0.02 (T)	3.9715	3.9715	4.0080	90	100 (P4mm)	4.84	1.56

**Fig. 4** a  $\varepsilon_r$  of (1 - x)(KNN–BNZ)–xCT–MnO<sub>2</sub> ceramics from room temperature to 450 °C, measured at f=100 kHz, **b** phase diagram



refinement: O–T for  $0 \le x \le 0.015$ , T for x = 0.02-0.03 and T-pseudo cubic for x = 0.04-0.05.

Figure 5 shows the SEM micrographs procured from the surface of the sintered samples. We can see that most of grains are rectangular. Besides, it can be found that the addition of CT inhibits the growth of the grains in the ceramics. Furthermore, it is filled with small ungrown grains in the ceramics with x = 0.04, indicating that the excessive doping of CT contents will enrich at the grain boundary and impede the transmission of particles during the sintering process, hindering the growth of grains and forming small grains [24]. In addition, the refinement of grain in certain degree will inhibit the reversal of domain structure, thus reducing the piezoelectricity of ceramics.



Fig. 5 SEM images of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics with **a** x=0, **b** x=0.01, **c** x=0.02, **d** x=0.04

Figure 6a and b show the piezoelectric constant  $(d_{33})$ , electromechanical coupling factor  $(k_p)$ , dielectric constant  $(\epsilon_r)$  and dielectric loss (tan  $\delta$ ) of the ceramics as a function of CT contents, respectively. Previous researches have shown that piezoceramics can obtain large piezoelectric properties at the boundary of multiphase coexistence, owing to its easy domain switching



**Fig. 6 a**  $d_{33}$  and  $k_p$  of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics as a function of CT contents, **b**  $\varepsilon_r$  and tan  $\delta$  of  $(1 - x)(KNN-BNZ) - xCT - MnO_2$  ceramics as a function of CT contents, measured at room temperature and f = 100 kHz



Fig. 7 a, b P-E loops of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics as a function of CT content, measured at room temperature and f=10 Hz, c, d Electric field-induced strain curves



**Fig. 8** a Unipolar strain curves of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics as a function of CT content, measured at room temperature and f=10 Hz; b Unipolar strain ( $S_{uni}$ ) and  $d_{33}^*$  of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics varying with CT content

and easy polarization [22, 23]. Therefore, from Fig. 6a, we can see that the ceramics with O–T phase boundary (x=0-0.01) have a relatively larger piezoelectric properties of  $d_{33} = 329-355$  pC/N and  $k_p = 0.44-0.49$ . In contrast, the ceramics with  $x \ge 0.04$  possess an inferior  $d_{33}$ due to the formation of the pseudo cubic phase. Previously, a low  $d_{33}$  of ~ 210 pC/N can be found in the KNNbased ceramics by introducing CT, due to the involvement of T phase [37]. However, a higher  $d_{33}$  of 261–296 pC/N can be observed in this work, which is attributed to composition modification. As shown in Fig. 6b, the dielectric constant increases firstly and then drops down quickly. And the dielectric loss slightly fluctuates with the variation of CT contents.

Figure 7a shows the composition dependence of P-E loops of the ceramics. We can see that all the ceramics have typical P-E loops. Moreover, the remnant polarization  $(P_r)$  and the coercive field  $(E_C)$  as a function of CT contents are



**Fig.9 a** Temperature dependent unipolar strain of  $(1 - x)(KNN-BNZ)-xCT-MnO_2$  ceramics measured at room temperature and f=10 Hz, **b** Temperature dependence of normalized strain  $(d_{33}^* = S_{max}/E_{max})$  for this work (x=0.02)

shown in Fig. 7b.  $P_r$  and  $E_C$  exhibit a similar trend because of the phase evolution of the samples. Besides,  $P_r$  and  $E_C$ show a downward trend after the first rise, with x=0.01, x=0.02 highest, respectively. Figure 7c gives the electric field-induced strain behavior of the ceramics. We can see that all the samples possess symmetry typical butterfly shape strain curves. As shown in Fig. 7d, the positive strain decreases gradually while the negative strain increases as the CT rises, indicating that the  $\Delta S$  ( $\Delta S = |S_{pos} - S_{neg}|$ ) descends with rising CT content. Figure 8a shows the unipolar strain curves of the ceramics. In order to clearly identify the composition dependence of unipolar strain, we portrayed the max unipolar strain and the converse piezoelectric constant of the ceramics, as shown in Fig. 8b. It can be seen that the  $S_{uni}$  and the  $d_{33}^*$  almost show a similar trend.

The temperature stability of the piezoelectricity of the ceramics is vital for the practical applications [6, 35]. Figure 9a shows the temperature stability of the unipolar strain with x = 0.02. To clearly characterize the temperature dependence strain of the ceramics, we give the curve of normalized strain changing with temperature for this work, as shown in Fig. 9b. It is observed that normalized strain decreases linearly when the temperature increases from room temperature to 130 °C. Generally, the piezoelectricity is attributed to intrinsic and extrinsic contributions; the former is affected by lattice deformations, and the latter is influenced by domain wall motions, which is sensitive to external conditions (e.g. electric field, measurement temperature) [41, 42]. Normally, normalized strain reflects both components. Therefore, the declined normalized strain may

be related to the electric field-induced phase transition and the external ambient temperature. Furthermore, strain changes in < 10% within temperature range of 30–80 °C for this work, indicating that the ceramics possess a relatively good temperature stability.

## 4 Conclusion

We have obtained a kind of KNN-based lead-free ceramics possessing a relatively large piezoelectricity and good temperature stability.  $T_{O-T}$  of the ceramics decreases from 50 °C to -29 °C within the range of  $0 \le x \le 0.03$ , resulting in the  $T_{O-T}$  far below room temperature, and at the same time, obtaining a relatively high piezoelectricity ( $d_{33} = 261-355$ pC/N) and good temperature stability (e.g., unipolar strain varied less than 15% at T=30-110 °C). We believe that our research can promote the development of KNN-based lead free ceramics.

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