Effect of $Bi₂O₃$ doping on the dielectric properties of medium-temperature sintering $BaTiO₃$ -based X8R ceramics

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Abstract Medium-temperature sintering X8R ceramics were fabricated based on $BaTiO₃$ -based ceramics with $Bi₂O₃$ additives. The effects of sintering aids $Bi₂O₃$ on crystalline structure and electrical properties of $BaTiO₃$ based ceramics were investigated. The sinterability of $BaTiO₃$ ceramics was significantly improved by adding $Bi₂O₃$, whose densification sintering temperature reduced from 1,260 to 1,130 °C. However, the dielectric constant (e) of BaTiO₃-based ceramics doped with $Bi₂O₃$ was decreased dramatically. Both low ε phase $Bi₄Ti₃O₁₂$ and the decrease of the tetragonality (c/a ratio), which are demonstrated by XRD pattern, are resulted in the decrease of ε . The ε of samples doped with 5.5 wt% Bi₂O₃ was higher than the other doped samples. The substitution of Bi^{3+} for the Ba^{2+} in BaTiO₃ resulted in the increase of electrovalence (from $+2$ to $+3$) of A-site ion, so the attractive force between A and B (Ti^{4+}) sites becomes stronger. Thus Ti^{4+} 's polarization enhances, then ε was increased to some extent. The X8R BaTiO₃-based ceramics could be sintered at as low as $1,130$ °C by doping 5.5 wt% $Bi₂O₃$ additives into the BaTiO₃-based ceramics, with a ε greater than 2,430 at 25 $^{\circ}$ C, dielectric loss lower than 1.3 % and temperature coefficient of capacitance $\lt \pm 15$ % $(-55-150$ °C).

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1 Introduction

Because of temperature-stable dielectric behaviors (temperature coefficient of capacitance TCC less than ± 15 % over the temperature range from -55 to 150 °C), X8R multilayer ceramic capacitors have been widely used for harsh conditions, such as the engine electronic control unit (ECU), programmed fuel injection (PGMFI), and anti-lock brake system (ABS) [[1\]](#page-4-0). These modules are subjected to high temperature above 130 °C. TCC equals to $(C - C_{25})/$ C_{25} , where C and C_{25} represent the capacitance value at measuring temperature and at 25° C respectively. Currently, the development of X8R MLCCs has been focused on the BaTiO₃-based ceramics.

Barium titanate (BaTiO₃) is a well-known material for EIA X8R capacitors. However, dielectric constant e of pure $BaTiO₃$ ceramics shows noticeable changes as the temperature changes, particularly when approaching the Curie temperature (Tc about 125 °C). Thus, BaTiO₃ is modified with different additives to increase the Tc and obtain smooth TCC. Another requirement for X8R MLCCs is the cofiring of dielectric ceramics with low-cost electrode. The sintering temperature of the pure $BaTiO₃$ is as high as 1,300 \degree C, so expensive electrode slurry of Pd or Pt must be used and the cost of MLCCs were increased dramatically. If the sintering temperature was lower than $1,160$ °C, the electrode slurry of Pd30Ag70 can be used and the cost of monolithic capacitors can be greatly reduced. Several approaches have been reported to reduce the sintering temperature of dielectric materials including: (1) adding low melting point compounds such as $Li₂O₃$, CuO, B₂O₃, $Bi₂O₃$ and glass [[2–5\]](#page-4-0), (2) chemical processing for smaller particle sizes of starting powders [\[6](#page-4-0)]. The second method leads to higher cost and longer processing time because of a complicated procedure. In this study, the approach of

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adding a low-melting oxide was adopted due to the ease in processing and its effectiveness in reducing sintering.

In this paper, low-melting oxide $Bi₂O₃$ was chosen as additive doped into BaTiO₃ composite. Bi₂O₃ has been proved to lower the sintering temperature effectively, meanwhile, the dielectric properties of $BaTiO₃$ composite can meet X8R requirement. The effects of $Bi₂O₃$ on the dielectric properties of $BaTiO₃$ -based ceramics were discussed.

2 Experimental procedures

2.1 Preparation of X8R ceramics

Pb $(Ti_{0.55}Sn_{0.45})O_3$ powders (synthesized according to chemical formula), BaTiO₃ (99.9 %, Aoxin, China), Nb₂O₅ (99.5 %, Fengchuan, China), $Co₂O₃(99.5 %$, Fengchuan, China) and $Bi_2O_3(99\%$, Fengchuan, China) were used as the starting materials. Samples were prepared by a conventional ceramic processing technique with powders of BaTiO₃ (calcined at 1,100 °C for 2 h), 2–3 wt% Nb₂O₅, $0.5 -2$ wt% $Co₂O₃$, 0.5–7 wt% Pb (Ti_{0.55}Sn_{0.45}) $O₃$ and x wt% Bi_2O_3 (x = 0, 3.5, 5.5, 7). The mixed powders were ball milled in deionized water for 6 h, and dried, sieved, then pressed into disks with 15 mm diameter. The disks without and with Bi_2O_3 were sintered at 1,260 and 1,130 °C for 6 h, respectively.

2.2 Measurements

The surface microstructure of sintered samples was observed with Scanning Electron Microscopy (SEM, Philips XL 30). The core–shell structure was observed with Scanning Electron Microscopy (NanoSEM430, FEI). Crystal structure of the samples were identified at room temperature using an X-ray diffractometer (XRD, Rigaku 2038X) with Cu Ka radiation ($\lambda = 0.15406$ nm) at a step width of 0.02° and a scan rate of $2^{\circ}/$ min. The lattice constants of samples were derived from XRD data by least square fit. In order to measure the sample's electrical properties, silver electrodes were attached to the surface of the sintered discs and fired at 800 °C for 15 min. ε and dielectric loss (tan δ) were measured by Agilent 4,278 Capacitance Meter at 1 kHz, with temperature range of -55 to 150 °C.

3 Results and discussion

3.1 Crystalline phases and surface microstructure

The X-ray analysis of $BaTiO₃$ -based ceramics with and without $Bi₂O₃$ was shown in Fig. 1. As shown in Fig. 1, main phase was BaTiO₃, and extra phases $Ti_{0,1}Sn_{0,9}O_2$, $Ti₉O₁₇$, TiO and PbTiO₃ were formed in both samples. Within the XRD resolution limit, the Nb and Co elements were not detected in the profile. As shown in Fig. 1b, $Bi₂O₃$ were also not detected, but new phase $Bi₄Ti₃O₁₂$ was appeared in the sample doped with 5.5 wt% $Bi₂O₃$. Doped with 5.5 wt% $Bi₂O₃$, the content of $Bi₂O₃$ exceed the solubility of Bi_2O_3 in barium titanate (about 3–5 wt% [\[7](#page-4-0)]). Surplus Bi_2O_3 reacted with dissociative TiO₂ and the new phase $Bi_4Ti_3O_{12}$ was formed. Due to the low solubility of $Bi_4Ti_3O_{12}$ in Barium titanate (less than 2.9 wt% [\[8\]](#page-4-0)), the new phase $Bi_4Ti_3O_{12}$ was detected in the Fig. 1b.

As shown in Table [1](#page-2-0), the lattice parameters and tetragonality (c/a ratio) were derived from XRD data by least square fit. Doped with 5.5 wt% $Bi₂O₃$, the tetragonality (c/a ratio) was decreased.

Figure [2](#page-2-0) shows SEM images of samples doped with different content of $Bi₂O₃$. As shown in Fig. [2a](#page-2-0), the sample doped without $Bi₂O₃$ was predominantly composed of fine grains with smooth surface and clear boundaries; although a small amount of strip grains were observed. The strip grains were formed attributed to non-ferroelectric phases, such as $Ti_{0.1}Sn_{0.9}O_2$, Ti_9O_{17} and TiO. As shown in Fig [2b](#page-2-0), the $Bi₂O₃$ mainly resides in the grain boundaries or covers the grains, so the edges of the grains were not distinct and a lot of air pores existed in the ceramics. Because the amount of $Bi₂O₃$ was small, the sintering temperature was too low to research the desired temperature for the growth of grain crystal. As shown in Fig [2](#page-2-0)c, the grains were well crystallized with smooth surface and clear boundaries. $Bi₂O₃$ addition can be dissolved in BaTiO₃ matrix, meanwhile, the grain growth was improved and the ceramics were densification; so the ceramics become quite dense and

Fig. 1 X-ray analysis of BaTiO₃-based ceramics a Bi₂O₃-free sintered at 1,260 °C. **b** Doped with 5.5 wt% Bi₂O₃ sintered at $1,130$ °C

Table 1 The lattice parameters and the tetragonality (c/a ratio) of $BaTiO₃$ -based ceramics doped without and with $Bi₂O₃$

	a (nm)	c (nm)	c/a
Doped with 0 mol % Bi_2O_3	0.3998	0.4031	1.008
Doped with 5.5 wt% Bi_2O_3	0.4012	0.4029	1.004

almost no air pore could be found. As shown in Fig 2d, the grain size was smaller as the content of $Bi₂O₃$ addition was increased. The reduction in grain size could be explained by the grain-growth-inhibiting phase at the grain boundaries. However, some large grains with a strip shape were also observed, owing to over doping of $Bi₂O₃$ (Fig. 2d).

For the sample doped with 5.5 wt% Bi_2O_3 , a fine structure in the core and a coarse structure in the shell were observed in Fig. 3, so this sample was the core–shell type. Jain [\[9](#page-4-0)] has reported that an apparent core–shell structure was observed, when BaTiO₃-based ceramics was doped with proper amount of $Bi_4Ti_3O_{12}$.

3.2 The effect of $Bi₂O₃$ additives on dielectric properties of BaTiO₃-based X8R ceramics

Calcination is an important section in fabrication process of ceramics, because the solid state reaction occurred mainly

Fig. 3 SEM images of the core–shell structure of the sample doped with 5.5 wt% $Bi₂O₃$

in calcination process. Yang et al. [[10\]](#page-4-0) found that both densification and grain growth processes rely on mass transport. The melting point of $Bi₂O₃$ was as low as 825 °C. During the sintering process, $Bi₂O₃$ were formed liquid phase due to the high sintering temperature

Fig. 2 SEM images of samples doped with different content of Bi₂O₃ a 0 wt% sintered at 1,260 °C b 3.5 wt% sintered at 1,130 °C c 5.5 wt% sintered at 1,130 °C d 7 wt% sintered at 1,130 °C

1,130 \degree C. The liquid phase enhances the ion diffusion via dissolution and reprecipitation process, and the small grains grew quickly. The densification of ceramics was accelerated, and the sintering ability of ceramics was enhanced. Hence the sintering temperature of $BaTiO₃$ based ceramics was significantly reduced from 1,260 to 1130 °C.

Figure 4a shows temperature dependence of e for $BaTiO₃$ -based ceramics doped with different content of $Bi₂O₃$. The effect of Pb (Ti_{0.55}Sn_{0.45}) $O₃$ on Tc of BaTiO₃based ceramics has been discussed in detail in Ref. [[11\]](#page-4-0) and is not of further relevance to the present work.

In an ideal cubic perovskite $BaTiO₃$ structure, the ionic radius of 12-coordinated Bi^{3+} is 0.145 nm, which is nearly comparable to the value of 0.135 nm for Ba^{2+} . Despite of three electrovalence of Bi^{3+} , Bi^{3+} substituted for A-site in $ABO₃$ structure. As shown in Eq. (1), solid state reaction might occur during the sintering process:

Fig. 4 Temperature dependence of $\bf{a} \varepsilon$, \bf{b} TCC of the BaTiO₃-based ceramics with various $Bi₂O₃$ contents

$$
xBi2O3 + BaTiO3 \to (1 - 2x)BaBa× + xVBa" + 2xBiBa*+ TiTi× + 3OO× + 3xBaO
$$
 (1)

where Ba_{Ba}^{\times} stands for a neutral barium atom on a barium site, $V_{Ba}^{''}$ for a barium vacancy with two negative charges, Bi_{Ba}^{\bullet} for a bismuth atom on barium site with one positive charge, Ti_{Ti}^{\times} for neutral titanium on a titanium site, and O_0^{\times} for a neutral oxygen atom on an oxygen site.

As shown in Fig. 4a, ε of the samples was dramatically decreased. According to Eq. 1, the appearance of V_{Ba} and Bi_{Ba} would result in the shrinkage of crystal lattice in some direction, which is demonstrated by the date in Table [1.](#page-2-0) Hence, the volume of titanium centered eight oxygen octahedrons was decreased. So the active space for Ti^{4+} was decreased, and Ti^{4+} ions were restricted to the center of oxygen octahedrons. Thus Ti^{4+} 's polarization was depressed, then e was decreased accordingly.

Zhang duanming et al. reported the equation between e and tetragonality (c/a ratio) in perovskite with $ABO₃$ structure, which can be described in the following equation:

$$
\frac{C}{\varepsilon} = T - T_0 + \frac{12\varepsilon_0(\alpha_{11}C/Q_{12}) \times (1 - c/a)}{c/a - Q_{11}/Q_{12}} + \frac{30\varepsilon_0(\alpha_{111}C/Q_{12}^2) \times (1 - c/a)^2}{(c/a - Q_{11}/Q_{12})^2}
$$
(2)

$$
\frac{(1/Q_{12}) \times (1 - c/a)}{(c/a - Q_{11}/Q_{12})} = \frac{-\alpha_{11}C + \sqrt{(\alpha_{11}C)^2 - 3\alpha_1C\alpha_{111}C}}{3\alpha_{111}C}
$$
(3)

In Eqs. (2) and (3) , C is Curie constant, T is measuring temperature, T_0 is Curie–Weiss temperature, ε_0 is vacuum permittivity, α_1 is second order dielectric stiffness, α_{11} is fourth order dielectric stiffness, α_{11} is sixth order dielectric stiffness, Q_{11} and Q_{12} are electrostrictive coefficient, all the parameters above are constant for specific material.¹

Form Eqs. (2) and (3) , Eq. (4) can be obtain.

$$
\frac{C}{\varepsilon} = T - T_0 + 12\varepsilon_0 \alpha_{11} C \times \frac{-\alpha_{11} C + \sqrt{(\alpha_{11} C)^2 - 3\alpha_1 C \alpha_{111} C}}{3\alpha_{111} C} \n+ \frac{-\alpha_{11} C + \sqrt{(\alpha_{11} C)^2 - 3\alpha_1 C \alpha_{111} C}}{3\alpha_{111} C} \n\times \frac{30\varepsilon_0 (\alpha_{111} C/Q_{12}) \times (1 - c/a)}{(c/a - Q_{11}/Q_{12})}
$$
\n(4)

 1 The list of the parameters of G (in SI units, T in kelvin) used in the calculations. For BaTiO₃: $\alpha_1(T) = 4.124 \times 105(T - 118) \text{Jm}/C^2$;
 $\alpha_{11}(T) = -2.097 \times 10^8 \text{Jm}^5/C^4$; $\alpha_{111}(T) = 1.294 \times 10^9 \text{Jm}^9/C^6$; $\alpha_{11}(T) = -2.097 \times 10^8 \text{Jm}^5/\text{C}^4; \qquad \alpha_{111}(T) = 1.294 \times 10^9 \text{Jm}^9/\text{C}^6;$
 $Q_{12} = -0.043 \text{ m}^4/\text{C}^2; Q_{11} = 0.1024 \text{ m}^4/\text{C}^2.$

 δ

$$
\frac{\delta\left(\frac{C}{\varepsilon}\right)}{\delta(c/a)} = \frac{(-\alpha_{11}C + \sqrt{(\alpha_{11}C)^2 - 3\alpha_1C\alpha_{111}C}) \times 30\varepsilon_0(\alpha_{111}C/Q_{12})}{3\alpha_{111}C} \times \frac{(Q_{11}/Q_{12} - 1)}{(c/a - Q_{11}/Q_{12})^2}
$$
(5)

The value of Eq. (5) is lower than zero, so ε was decreased with the decrease of c/a. As shown in Table [1,](#page-2-0) doped with Bi_2O_3 , the tetragonality (c/a ratio) was decreased from 1.008 to 1.004, so e of the ceramics was decreased accordingly.

Meanwhile, as the amount of $Bi₂O₃$ increasing, the new phase was detected in the XRD profile. ε of Bi₄Ti₃O₁₂ was about 127. According to Lichtenecker formula:

$$
\ln \varepsilon = x_1 \ln \varepsilon_1 + x_2 \ln \varepsilon_2 + x_3 \ln \varepsilon_3 + \dots + x_n \ln \varepsilon_n \tag{6}
$$

So, why ε was decreased when the content of $Bi_4Ti_3O_{12}$ phases was increased was explained well by Eq. (6).

 ϵ of samples doped with 5.5 wt% Bi₂O₃ was higher than the samples doped with 3.5 and 7 wt% $Bi₂O₃$. For the increase of electrovalence (from $+2$ to $+3$) of A-site ion, a residual positive charge appears (Bi_{Ba}^{\bullet}) and the attractive force between A and B (Ti^{4+}) sites becomes stronger. Thus Ti^{4+} 's polarization enhances, then ε was increased accordingly. The fine and homogeneous grains were responsible for good dielectric properties. SEM indicated that fine and homogeneous grains were observed at 25 °C with 5.5 wt% $Bi₂O₃$ additives, which also gave rise to the increase of e.

Figure [4b](#page-3-0) shows the temperature dependence of TCC of the BaTiO₃-based ceramics with various $Bi₂O₃$ contents. For BaTiO₃-based ceramics doped with 5.5 wt% Bi₂O₃, the change of ε is less than ± 9 %. Moreover, tand of four samples was lower than 2.0 % at 25 \degree C, which satisfied X8R specification.

4 Conclusions

Because of low melting point (825 °C), $Bi₂O₃$ were formed liquid phase during the sintering process. The ion diffusion was enhanced via dissolution and reprecipitation process, so the densification of ceramics was accelerated, and sintering ability of $BaTiO₃$ -based ceramics were enhanced. The sintering temperature is reduced from 1,260 to 1,130 \degree C, the electrode slurry of Pd30Ag70 can be used and the cost of monolithic capacitors was greatly reduced.

Compared with ceramic without $Bi₂O₃$, ε of BaTiO₃based ceramics doped with $Bi₂O₃$ was decreased dramatically. Ba²⁺ was substituted by Bi³⁺, Ti⁴⁺⁺'s polarization was depressed, then e was decreased accordingly. According to the equation between ε and tetragonality (c/a ratio), e was decreased with the decrease of c/a ratio. Demonstrated by the XRD pattern, c/a ratio was decreased from 1.008 to 1.004, so e of the ceramics was decreased accordingly. Meanwhile, new phase $Bi₄Ti₃O₁₂$ was detected in XRD pattern. According to Lichtenecker formula, ϵ of Bi₄Ti₃O₁₂ was as low as 127, so the ϵ was decreased. Both enhancement of Ti^{4+} 's polarization and homogeneous microstructure are attributed to the highest e among $Bi₂O₃$ doped samples.

Doped with 5.5 wt% $Bi₂O₃$, the sintering temperature of BaTiO₃-based can be reduced form 1,260 to 1,130 °C, exhibited dielectric properties: $\varepsilon_{25} \sim \approx 2430$, tan $\delta \approx$ 1.3 %, TCC $< \pm 15$ % (-55–150 °C), which satisfied X8R specification.

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References

- 1. G.-H. Chen, Mater. Sci. Mater. Electron. (2012). doi[:10.1007/](http://dx.doi.org/10.1007/s10854-012-0710-0) [s10854-012-0710-0](http://dx.doi.org/10.1007/s10854-012-0710-0)
- 2. N. Ma, J. Electroceram. 28(4), 275 (2012)
- 3. K. Yan, J. Am. Ceram. Soc. 93(11), 3823 (2010)
- 4. H. Naghib-zadeh, J. Eur. Ceram. Soc. 3(1), 31 (2010)
- 5. L. Zhou, J. Eur. Ceram. Soc. 21(4), 531 (2001)
- 6. H. Beltrán, J. Electroceram. **18**, 277 (2007)
- 7. L. Zhou, J. Am. Ceram. Soc. 82(4), 1064 (1999)
- 8. Y. Li, J. Wuhan Univ. Technol. Mater. Sci. Edit. 23, 143 (2008)
- 9. T.A. Jain, J. Eur. Ceram. Soc. 29, 2595 (2009)
- 10. K.Y.J. Yang, Alloys Compd. 458, 415 (2008)
- 11. S. Wang, Mater. Sci. Mater. Electron. 21, 1159 (2010)