

# Microwave adsorption of core–shell structured $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$ composites

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**Abstract** Polyaniline polymer-coated MnTi-substituted strontium hexaferrite ( $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$ ,  $x = 1.0, 1.5, 2.0$ ) composites were synthesized by the oxidative chemical polymerization of aniline in the presence of ammonium peroxydisulfate. The structure and morphologies of the products were characterized by X-ray diffraction, FT-IR, TGA, SEM, and TEM. In the magnetization for the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$  composites, it was found that the saturation magnetization ( $M_s$ ) and coercivity ( $H_c$ ) decreased after polyaniline coating. The composite under an applied magnetic field exhibited hysteretic loops of ferromagnetic behavior, such as high saturation magnetization ( $M_s = 12.1\text{--}1.9$  emu/g) and coercivity ( $H_c = 0.919\text{--}0.084$  kG). The composite specimens of core–shell  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$  and thermal plastic resin had a band-width microwave absorption due to the reflection losses from  $-15$  to  $-35$  dB at frequencies between 18 and 40 GHz as observed by a high-frequency network analyzer.

## Introduction

M-type hexaferrites have a large intrinsic magnetic anisotropy field, and the variation of this field is caused by  $\text{Sr}^{2+}$  and  $\text{Fe}^{3+}$  ions being substituted by extrinsic metallic ions. As a result, the applications of M-type hexaferrites in both microwave resonant and microwave non-resonant devices are very important [1]. Such types of M-type hexaferrites have also continued to be of great interest for both the applications of microwave absorbers and the protectoral materials of electromagnetic interference (EMI) on electronic and communication equipment [2, 3]. The M-type hexaferrites are advantageous because of their high permeability and high resonant frequency.  $\text{Ba}(\text{MnTi})_{1.6}\text{Fe}_{8.8}\text{O}_{19}$  shows a strong microwave absorption within the frequency range of 8.0–12.0 GHz [4].

Many different methods of producing ferrites have been developed thus far. Such methods include, the dry method, the hydrothermal reaction [5–7], chemical coprecipitation [8–11], aerosol pyrolysis [12], the sol–gel technique [13–16], the glass crystallization method [7, 17, 18], low temperature combustion synthesis (LCS) [19, 20], and aqueous combustion synthesis (ACS) [21–23]. An ideal method to make hexaferrites should include a facile operation and low calcination temperature, and it should be energy-efficient and have a short reaction time. In addition, ultra-fine powder particles with narrow particle size distribution, excellent chemical homogeneity, and single magnetic domain are all required for ideal strontium M-type hexaferrite (Sr-M) resulting powders. The LCS method was used to synthesize  $\text{Ba}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  hexaferrites [24]. The ACS method has not only the advantages described above but also the benefit that the wet sol–gels containing the proper amount of  $\text{H}_2\text{O}$  can be ignited directly and the thermal explosion

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self-propagating combustion will be completed in a short time. The particle size distribution of the as-burnt powder was found to be between 30 and 50 nm; therefore, the ACS method was used for the preparation of Sr-M hexaferrites in the research presented here.

Conductive polyaniline has attracted much attention because of its potential applications in various fields, such as molecular electronics, chemical sensor, EMI shielding, antistatic coatings, rechargeable batteries, corrosion inhibitors, and microwave absorbing materials [25–29]. It is well known that conducting polymers can effectively shield electromagnetic waves generated by an electric source, whereas electromagnetic waves from a magnetic source can be effectively shielded only by magnetic materials [30, 31]. Thus, incorporation of magnetic constituents and conducting polymeric materials opens new possibilities for the achieving good shielding for various electromagnetic sources.

Until now, many reports have focused on selecting the hexaferrite as the magnetic component in polyaniline-based composites; see, e.g., [32–34]. Additionally, our laboratory has previously described a successful PANI/SrFe<sub>12</sub>O<sub>19</sub> and Sr(ZnZr)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>/PANI synthesis using the chemical polymerization method [35, 36]. To our knowledge, there are no other existing reports on studies related to modifying the magnetic properties of conducting polyaniline coating and strontium manganese titanium hexaferrites composites (Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>/PANI) with our method.

In this study, electromagnetic functionalized Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>/PANI composites were synthesized by the oxidative chemical polymerization of aniline in the presence of ammonium peroxydisulfate (APS). The Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub> particles were the magnetic cores obtained using the ACS method in the glycine–metal nitrate sol–gel system, and polyaniline (PANI) was the conducting shell. The samples were characterized by various experimental techniques, and the magnetization properties of the composites were investigated. The absorption of microwaves and the *relatively* complex permittivity and permeability of the composite powders were also investigated.

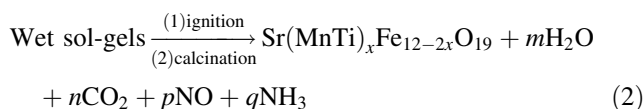
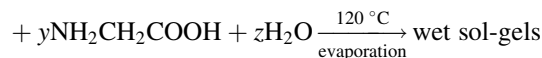
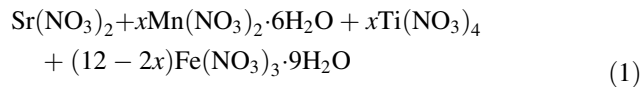
## Experimental

### Materials

Aniline was distilled twice under reduced pressure and stored below 0 °C. Citric acid, ammonia, HCl, Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, Sr(NO<sub>3</sub>)<sub>2</sub>, Mn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, NH<sub>2</sub>CH<sub>2</sub>COOH, Ti(NO<sub>3</sub>)<sub>4</sub>, and (NH<sub>4</sub>)<sub>2</sub>S<sub>2</sub>O<sub>8</sub> (APS) were all of analytical purity and used without further purification.

### Preparation of Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub> hexaferrite particles

M-type hexaferrites of Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>, where  $x = 0, 1.0, 1.5,$  and  $2.0,$  were synthesized using ACS in a glycine–metal nitrates system. The reaction equations of the ACS method for the preparation of hexaferrites and the formation of gaseous species [16] in these reactions can be described simply by the following:



The mole ratios of all starting metal nitrates in the reactions were controlled depending on the composition of the desired materials. We defined  $R$  as the molar ratio of glycine to the nitrate ions in the precursor solution. According to our experimental observation and the proposed ACS by Varma and coworkers [24], the value of  $R$  was fixed at 0.75 in all synthetic reactions to obtain the thermal explosion self-propagation combustion.

Using Eq. 3, the stoichiometric amount of metal nitrates were dissolved completely in 50 mL of deionized water to obtain aqueous solution I. Solution II was prepared by dissolving an appropriate amount of glycine into 50 mL of deionized water. Solutions I and II were further mixed to form a homogeneous transparent aqueous solution. Ammonium hydroxide (mass percent 28) was then added to the mixed solution to adjust the pH value. The mixed solutions were then heated in oil-bath at 120 °C for 1.5 h to evaporate approximately 50% of the water until high viscosity, wet sol–gels were formed. Finally, the wet sol–gels were ignited in an air atmosphere and the thermal explosion self-propagation combustion reactions were accomplished. The ash produced after combustion was deep reddish-brown and voluminous. The as-burnt powders were the precursors of M-type strontium hexaferrites. Furthermore, the M-type of cation-substituted strontium manganese titanium hexaferrites (Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>) were obtained after annealing the as-burnt powders at different temperatures for 2 h.

### Polymerization of Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>/PANI composites

The core–shell structure materials of Sr(MnTi)<sub>x</sub>Fe<sub>12–2x</sub>O<sub>19</sub>/PANI, where  $x = 0, 1.0, 1.5,$  and  $2.0,$  were prepared by

oxidative chemical polymerization of aniline on the surface of 10 g Sr-ferrite powders that had been suspended in 50-mL aqueous solution containing the surface active agent APS. To improve the contacts between ferrites and anilines in aqueous solution, Sr-ferrite powder was dispersed in deionized water by ultrasonic waves with an oscillation frequency of 42 kHz for 30 min before polymerization. The monomer solution for polymerization was created by mixing aniline and HCl in 100-mL deionized water. The molar ratio of aniline to HCl in solution was 1:3 and the concentration of aniline in solution was 0.033 M. The required amount of aniline aqueous solution was added drop by drop to each flask containing the suspended Sr-ferrite solution; the polymerization was allowed to proceed at temperature between 0 and 5 °C under mechanical stirring for 3 h. After the solid core-shell particles were formed, the solid products were collected and washed with methanol and deionized with water several times sequentially. Finally, the products were dried in a vacuum oven at 100 °C for 24 h.

### Characterization

The XRD patterns of the samples were collected using powder X-ray diffraction (XRD) (Siemens D5000X) with Cu K $\alpha$  radiation ( $\lambda = 0.15418$  nm). Fourier transmission infrared (FTIR) spectra were recorded on a TENSOR 27 spectrometer (Varian) in the range of 400–4000 cm $^{-1}$  using KBr pellets. Thermogravimetric analysis (TGA, PERKIN-ELMER) was used to measure the thermal decomposition behavior of the 1200 °C Sr(MnTi) $_x$ Fe $_{12-2x}$ O $_{19}$ /PANI powders. The heating rate was 10 °C/min, and the flow rate of air in the thermal property measurements was 10 mL/min. The morphology was characterized by a JSM-6390 scanning electron microscope (SEM) and JEOL2000-EX 2 transmission electron microscope (TEM). Magnetic measurements were carried out at room temperature using a vibrating sample magnetometer (VSM, Lake Shore, model 7400) with a maximum magnetic field of 15 kG. The specimens for microwave adsorption testing were prepared by homogeneously mixing the 60 wt% composite powders with 40 wt% thermal plastic resin (TPR), utilizing a high-heat machine (Molding Test Press Tester 0–150 kg/cm $^2$ , 0–400 °C, HT-8122B) to manufacture microwave absorption-films (155 mm  $\times$  155 mm  $\times$  2.0 mm) at temperatures of approximately 150–175 °C (stress design 10–30 kg/cm $^2$ , 15 min). A high-frequency network analyzer (Vector Network Analyzer HP8722ES) was used to measure the reflection loss (RL) of electromagnetic radiation of the polyaniline-TPR, Sr(MnTi) $_x$ Fe $_{12-2x}$ O $_{19}$ -TPR, Sr(MnTi) $_x$ Fe $_{12-2x}$ O $_{19}$ /PANI-TPR composite materials. The RL curves were calculated from the complex relative

permeability and permittivity at a given frequency and absorber thickness with the following equations:

$$Z_{in} = \sqrt{\frac{\mu_\gamma}{\epsilon_\gamma}} \tanh \left[ \left( j \frac{2\pi}{\lambda} \right) d \sqrt{\mu_\gamma \epsilon_\gamma} \right] \quad (3)$$

$$\Gamma = \frac{Z_{in} - 1}{Z_{in} + 1} \quad (4)$$

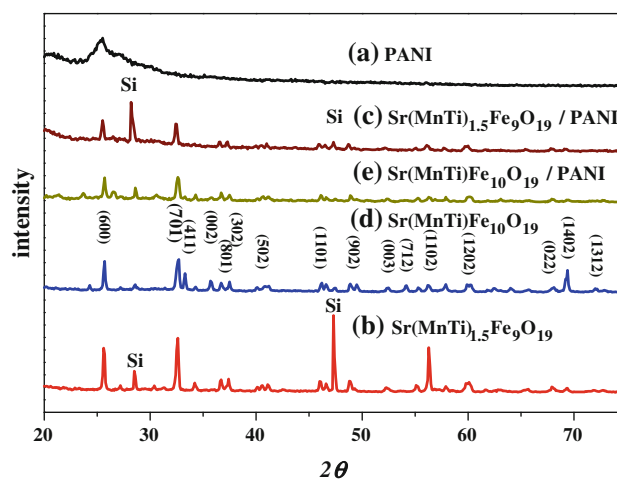
$$RL(\text{dB}) = 20 \times \log|\Gamma| \quad (5)$$

where  $\lambda$  is the frequency,  $d$  is the thickness of the absorber,  $j$  is the condition of vacuum,  $\epsilon_\gamma$  and  $\mu_\gamma$  are the relative complex permeability and permittivity, respectively, of the absorber medium,  $\Gamma$  is the reflection parameter,  $Z_0$  the impedance of air, and  $Z_{in}$  is the input impedance of the absorber [37].

## Results and discussions

### X-ray powder diffraction

The XRD patterns of Sr(MnTi) $_x$ Fe $_{12-2x}$ O $_{19}$  and Sr(MnTi) $_x$ Fe $_{12-2x}$ O $_{19}$ /PANI composite nanoparticles and PANI are shown in Fig. 1. As shown in Fig. 1b and d, respectively, the crystal structures of Sr(MnTi) $_{1.5}$ Fe $_8$ O $_{19}$  and Sr(MnTi)Fe $_{10}$ O $_{19}$  annealed at 1200 °C for 2 h were determined by the powder X-ray diffraction technique. The X-ray diffraction patterns of Sr(MnTi)Fe $_{10}$ O $_{19}$  particles present the M-type structure, and the XRD spectra showed the diffraction peaks similar to hexagonal SrFe $_{12}$ O $_{19}$  (110), (107), (114), (203), (205), (206), (0014), (304), (221), and (404), which were all observed in each curve [38]. The lattice constant  $a$  of Sr(MnTi)Fe $_{10}$ O $_{19}$  is 5.88–5.90 Å. A typical XRD pattern of polyaniline shows one broad



**Fig. 1** XRD patterns of (a) PANI, (b) Sr(MnTi) $_{1.5}$ Fe $_9$ O $_{19}$  particles, (c) Sr(MnTi) $_{1.5}$ Fe $_9$ O $_{19}$ /PANI composite, (d) Sr(MnTi)Fe $_{10}$ O $_{19}$ , and (e) Sr(MnTi)Fe $_{10}$ O $_{19}$ /PANI composite

diffraction peak centered at  $2\theta = 25.51^\circ$  (see Fig. 1a), which can be ascribed to the periodicity parallel and is perpendicular to the polymer chains [39]. Figure 1c and e shows the values of the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$ /PANI composite, which contains the characteristic peaks of PANI and  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 1.0, 1.5$ ), including the peaks at  $2\theta = 25.62^\circ, 32.52^\circ, 33.43^\circ, 35.72^\circ, 36.76^\circ, 37.57^\circ, 40.88^\circ, 46.04^\circ, 48.91^\circ, 52.35^\circ, 56.25^\circ, 60.15^\circ, 68.29^\circ, 69.33^\circ, 72.08^\circ, \text{ and } 74.48^\circ$ . These results indicated that the structure of the core materials is a hexagonal structure, and the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$ /PANI core-shell composites were obtained.

FTIR spectral analysis

The FTIR spectra of the  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$ ,  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$ /PANI composites and PANI sample without  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  core-particles under the same conditions are shown in Fig. 2. It is observed in Fig. 2c that there is a peak at  $1388$  and  $1647\text{ cm}^{-1}$ , corresponding to vibrations of  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  in each curve. The characteristic peaks of PANI occur at  $1110, 1237, 1291, 1486, 1565, \text{ and } 805\text{ cm}^{-1}$ . The peaks at  $1565$  and  $1486\text{ cm}^{-1}$  are attributed to the characteristic C=C stretching of the quinoid and benzenoid rings, and the peaks at  $1291$  and  $1237\text{ cm}^{-1}$  correspond to N–H bending and asymmetric C–N stretching modes of the benzenoid ring, which were also observed in each curve of Fig. 2b. The peak near  $1110\text{ cm}^{-1}$  is associated with vibrational modes of N=Q=N (Q refers to the quinonic-type rings), indicating that PANI was formed in our sample. The peak at  $805\text{ cm}^{-1}$  is attributed to the out-of-plane deformation vibration of the *p*-disubstituted benzene ring.

The absorption peaks of the  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$ /PANI composite shifted to  $1119, 1298, 1396, \text{ and } 1475\text{ cm}^{-1}$  (see

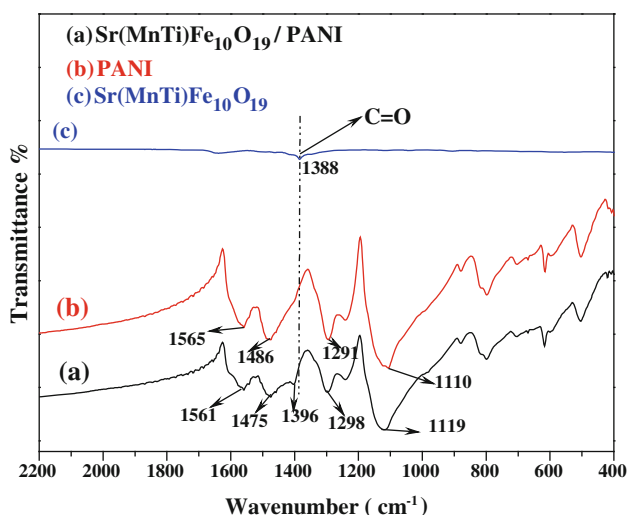


Fig. 2 FT-IR spectra prepared with different (a)  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$ /PANI composite, (b) PANI, and (c)  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$

Fig. 2a). The absorption peak of the composite with  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$ /PANI is approximately  $8\text{ cm}^{-1}$  shifted, compared to that of the pure PANI. These results indicate the good quality of the coating of  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  particle with PANI in the composite.

Thermogravimetric analysis measurements

TGA curves of the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 1.0, 1.5, 2.0$ ) dry sol-gels (Fig. 3) show that there are two steps of primary weight loss, which occur at temperature between  $150\text{--}250^\circ\text{C}$  and  $250\text{--}350^\circ\text{C}$ . A weight loss in the first step of approximately  $20\text{--}25\%$  was considered to be due to the oxidation reduction of  $\text{NO}_3^-$  ions and the free glycine molecules that did not link to the metal ions. Approximately  $25\text{--}30\%$  of weight loss in the second step corresponded to the decomposition reactions or oxidation-reduction reactions of the nitrate ions and liganded glycine molecules. Approximately  $2\text{--}5\%$  of weight loss occurred at temperature between  $350$  and  $600^\circ\text{C}$ . The third step of weight loss was considered to be the oxidation reaction of the residual carbon atoms in the surface of the ashes.

The TGA curve of  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 1.0, 1.5, 2.0$ ), annealed at  $1200^\circ\text{C}$ , and PANI composites in Fig. 4a shows  $100\%$  PANI. Approximately  $10\%$  weight loss occurred at temperatures between  $0$  and  $150^\circ\text{C}$ , which was due to vaporization of water in polyaniline. Figure 4a also indicates that pure PANI material will undergo a redox reaction or decomposition initially at around  $150^\circ\text{C}$ . PANI has the greatest weight loss ( $\sim 96.7\%$ ) at temperatures between  $250$  and  $600^\circ\text{C}$ . Figure 4b–d shows that the starting decomposition temperature of PANI depends on the amount of  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$ , which is the shell material of the core-shell hexagonal ferrites. In the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 1.0, 1.5, 2.0$ ) and PANI core-shell structure composites approximately  $71.1\text{--}26.5\%$

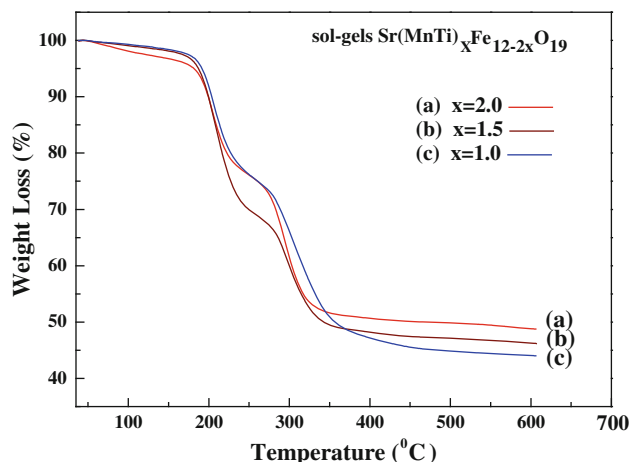
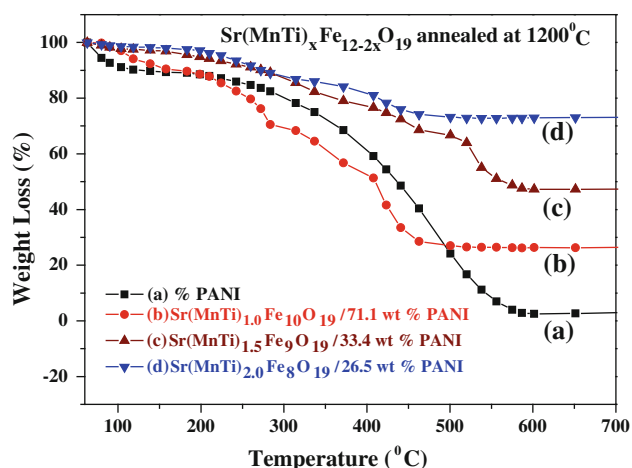


Fig. 3 TGA curves of the dry  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  sol-gels



**Fig. 4** TGA curves of  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$ . (a) 100% PANI, (b)  $\text{Sr}(\text{MnTi})_{1.0}\text{Fe}_{10}\text{O}_{19}/71.1$  wt% PANI, (c)  $\text{Sr}(\text{MnTi})_{1.5}\text{Fe}_9\text{O}_{19}/33.4$  wt% PANI, and (d)  $\text{Sr}(\text{MnTi})_{2.0}\text{Fe}_8\text{O}_{19}/26.5$  wt% PANI

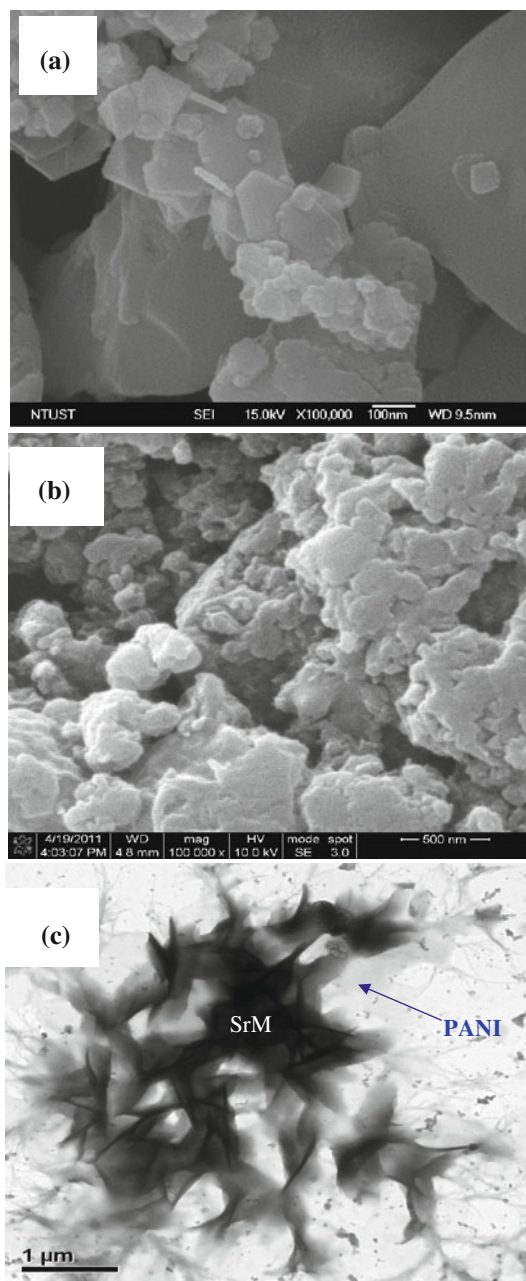
PANI materials of weight loss occurs at a temperature between 350 and 500 °C. This variation in initial decomposition temperature occurs because the more the hexagonal ferrite, the stronger the strontium manganese titanium hexaferrites/polyaniline composites' structure. It is obvious that the more strontium manganese titanium hexaferrites/PANI hybrid, the more remnant weight percent there is after decomposition at 600 °C.

#### SEM and TEM observations

The SEM micrograph diameter of the hexagonal  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  powders were found to increase, distributed in the range of 50–250 nm (Fig. 5a) after heat treatment at 1200 °C for 2 h. Figure 5b shows the SEM image of the core-shell  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$  composites. The image indicates that the core-shell are coated by polyaniline and form spherical coral-like particles, which have diameters around 100–500 nm and are connected by the polymer. To investigate the detailed structure of  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$  core-shell samples, TEM was performed. The  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$  powder composites were dissolved with *N*-methyl-2-pyrrolidone (NMP), which is a good dissociation solvent for PANI. Figure 5c shows the  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  particles coated by the PANI layer and indicates that the  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  particles are imbedded in the PANI matrix. The black region shows the  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  particles, and the gray colored shell is PANI in the composite, due to the different electron penetrability.

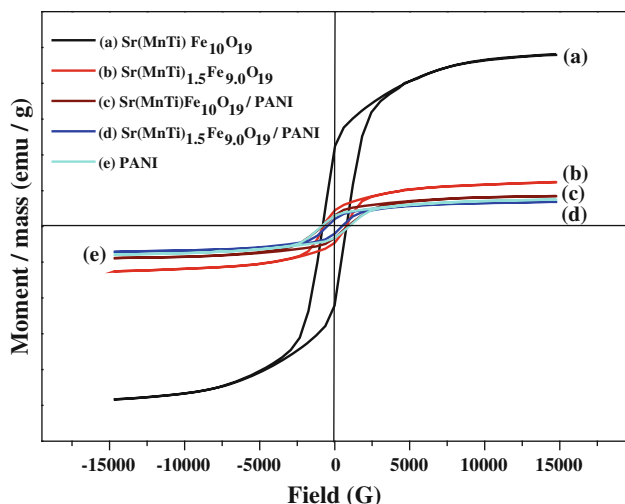
#### Magnetic properties

The magnetic hysteresis loop measurements of  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  annealed at 1200 °C are shown in Fig. 6, along



**Fig. 5** SEM images of **a**  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  particles, **b**  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$  composites. TEM images of **c**  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$  composite

with the area of the magnetic hysteresis loop of the powder  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}$  (Fig. 6a). The saturation magnetization ( $M_s$ ), remanence magnetization ( $M_r$ ), and coercivity ( $H_c$ ) of this specimen are 12.06 emu/g, 0.81 emu/g, and 0.805 kG, respectively. Figure 6b–d shows the hysteresis loops of the  $\text{Sr}(\text{MnTi})_{1.5}\text{Fe}_9\text{O}_{19}$  as well as  $\text{Sr}(\text{MnTi})\text{Fe}_{10}\text{O}_{19}/\text{PANI}$ ,  $\text{Sr}(\text{MnTi})_{1.5}\text{Fe}_9\text{O}_{19}/\text{PANI}$  composites, and the pure PANI at room temperature. It is observed that the saturation magnetization ( $M_s$ ), coercivity ( $H_c$ ), and remanence magnetization ( $M_r$ ) values for  $\text{Sr}(\text{MnTi})_{1.5}\text{Fe}_9\text{O}_{19}$  and PANI

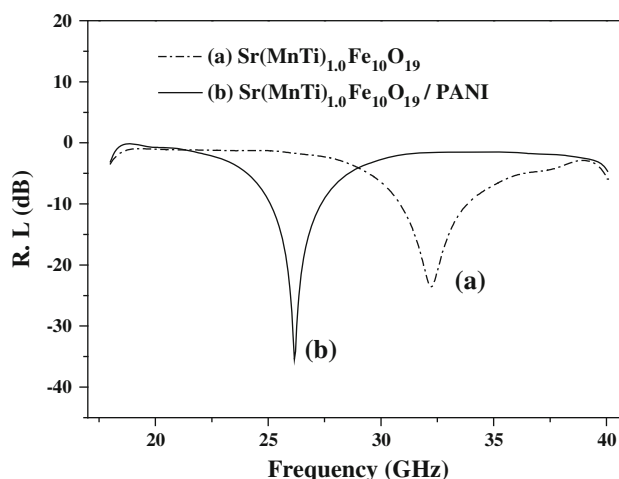


**Fig. 6** Hysteresis loops of (a) Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub> particles, (b) Sr(MnTi)<sub>1.5</sub>Fe<sub>9.0</sub>O<sub>19</sub> particles, (c) Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub>/PANI, (d) Sr(MnTi)<sub>1.5</sub>Fe<sub>9.0</sub>O<sub>19</sub>/PANI composite, and (e) PANI

are  $M_s = 2.16, 3.12$  emu/g,  $H_c = 0.086, 0.75$  kG, and  $M_r = 0.81, 1.12$  emu/g (Fig. 6b, e). In contrast, the Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub>/PANI and Sr(MnTi)<sub>1.5</sub>Fe<sub>9.0</sub>O<sub>19</sub>/PANI composites under an applied magnetic field exhibit a clear hysteretic behavior. As seen in Fig. 6c and d, the  $M_s = 1.92, 1.74$  emu/g, and  $H_c = 0.92, 0.51$  kG are lower than those of pure Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub> particles. When pure Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub> particles were coated with PANI (Fig. 6d), the values of  $M_s$ ,  $H_c$ , and  $M_r$  all decreased with increasing PANI values, and contraction of the hysteresis loop area is seen. These results show that the pure Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub> particle cores are responsible for the magnetic behavior of the pure Sr(MnTi)Fe<sub>10</sub>O<sub>19</sub>/PANI composites. According to the equation  $M_s = \phi m_s$ ,  $M_s$  is related to the volume fraction of the particles ( $\phi$ ) and the saturation moment of a single particle ( $m_s$ ) [40]. It can be assumed that the  $M_s$  of the Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub>/PANI composite depends mainly on the volume fraction of the magnetic hexaferrite particles, due to the contribution of the non-magnetic PANI coating layer to the total magnetization, resulting in a decrease in the saturation magnetization. The magnetic properties observed for magnetic particles are a combination of many anisotropy mechanisms. An effective anisotropy constant ( $K$ ) could be obtained by adding the bulk anisotropy and surface contributions, and the following expression has been used to account for  $K$  [41]:

$$K = K_b + (6/d)K_s \tag{6}$$

where  $K_b$  is the bulk magnetocrystalline anisotropy,  $K_s$  is the surface anisotropy, and  $d$  is the particle diameter.  $K_s$  is usually the maximum for free surfaces and is reduced by solid coverage. The decrease in  $K_s$  resulting from the



**Fig. 7** The microwave absorption RL of (a) Sr(MnTi)<sub>1.0</sub>Fe<sub>10</sub>O<sub>19</sub> and (b) Sr(MnTi)<sub>1.0</sub>Fe<sub>10</sub>O<sub>19</sub>/PANI composites

particle coverage by the PANI reduces the effective magnetocrystalline anisotropy ( $K$ ) and therefore decreases  $H_c$ .

### Microwave absorption

A high-frequency network analyzer (Vector Network Analyzer HP8722ES) was used to examine the reflectivities of the pure ferrites and the core-shell ferrites. Figure 7 and Table 1 show the characteristic absorption of materials at frequencies between 18.0 and 40.0 GHz. It was found that the conductivity of PANI coated on the Sr-M dramatically affects the microwave absorption of the materials. Composite specimens comprising the PANI, Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub>, core-shell Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub>/PANI materials, and a TPR demonstrated a microwave absorbing band-wide between 26.0 and 38.0 GHz, where reflections observed on a network analyzer lost  $-15.7$  to  $-35.5$  dB.

### Conclusion

A Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub>/PANI core-shell composite was successfully synthesized by the facile oxidative chemical

**Table 1** Microwave absorption of Sr(MnTi)<sub>x</sub>Fe<sub>12-2x</sub>O<sub>19</sub>/PANI composites

Samples	Frequency (GHz)	Reflection (dB)	Thickness (mm)
Sr(MnTi) <sub>1.0</sub> Fe <sub>10</sub> O <sub>19</sub>	32.21	-23.5	2.0
Sr(MnTi) <sub>1.5</sub> Fe <sub>9.0</sub> O <sub>19</sub>	26.65	-15.7	2.0
Sr(MnTi) <sub>2.0</sub> Fe <sub>8.0</sub> O <sub>19</sub>	28.08	-15.9	2.0
Sr(MnTi) <sub>1.0</sub> Fe <sub>10</sub> O <sub>19</sub> /PANI	26.17	-35.5	2.0
Sr(MnTi) <sub>1.5</sub> Fe <sub>9.0</sub> O <sub>19</sub> /PANI	37.94	-17.8	2.0
Sr(MnTi) <sub>2.0</sub> Fe <sub>8.0</sub> O <sub>19</sub> /PANI	32.50	-31.5	2.0

polymerization of aniline in the presence of  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 0, 1.0, 1.5, 2.0$ ) particles. The core-shell structure of the  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI}$  composite was characterized by XRD, FT-IR, TGA, SEM, and TEM. The intrinsic magnetic hysteresis loop measurements revealed that the  $M_s$  and  $H_c$  decreased with the polyaniline content. The core-shell  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI-TPR}$  materials have stronger absorption for microwave between 18.0 and 40.0 GHz than pure hexagonal ferrite,  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}\text{-TPR}$ . A nearly 40% band-width range of RL peaks below  $-20$  dB at frequencies between 25.0 and 37.8 GHz was observed in the core-shell  $\text{Sr}(\text{MnTi})_x\text{Fe}_{12-2x}\text{O}_{19}/\text{PANI-TPR}$  composite. Improvement in the adsorption performance may be attributed to the relative permittivity change induced by the exchange coupling interaction between the conducting polymer and the magnetic materials.

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