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Experimental observations of 3D fow alterations by vegetation under oscillatory fows

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Abstract

This study presents observations from a series of experiments on an oscillatory tunnel, using a three-dimensional, volumetric particle image velocimetry system to investigate the efect of a single plant morphology on fow alterations. Three synthetic plants, mimicking three species representative of riverine, tidal, and coastal vegetation communities are investigated under various combinations of wave period and orbital excursion. The study allows to investigate the temporal and spatial distribution of the velocity feld past the submerged plants with high spatial resolution. It shows that even a detailed characterization of plant morphology, represented by obstructed area or patch porosity, is not enough to accurately parameterize variations in instantaneous velocity, turbulent kinetic energy, bed shear stresses, and coherent fow structures. The study shows that bending and swaying of the plant generates eddies at multiple scales, at various locations and orientations with respect to the stem, branches, and leaves, which may be overlooked with point measurements or even 2D PIV, and can signifcantly enhance or dampen forces at the bed driving sediment transport processes in sparse vegetation patches.

Keywords Vegetation · Oscillatory fow · Volumetric PIV · Turbulence · Bed shear stress

1 Introduction

Restoration and conservation for aquatic ecosystems exposed to wave action rely on accurate understanding of aquatic vegetation—fow interactions [\[20,](#page-26-0) [27](#page-26-1)]. Such interactions impact ecosystems directly and indirectly through various mechanisms. For example, turbulence levels inside and around vegetated patches determine erosion/deposition patterns [[61](#page-27-0), [62\]](#page-28-0), while sediment transport affects water quality and physicochemical characteristics of the substrata. These dynamics impact biota and alter ecological functions [\[35\]](#page-27-1). In consequence, relationships among biotic and abiotic components of aquatic ecosystems challenge restoration and conservation efforts [[8,](#page-25-0) [45](#page-27-2)]. Temporal and spatial variability also

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adds complexity of these processes in habitats subject to oscillatory fows, such as estuar-ies, nearshore, and offshore regions [[19](#page-26-2), [24](#page-26-3)].

Plant morphology, defned as the spatial distribution of biomass and geometric features [[4\]](#page-25-1), difers from simplifed shapes in nature. Morphological structures (leaves, branches, stems) impose heterogeneous resistance upon the fow in terms of irregular blockage and biomechanical resistance [\[49\]](#page-27-3) altering flow organization and turbulence statistics. For example, Albayrak et al. [[5](#page-25-2)] found that turbulence scales are strongly associated with morphological structures of the plant and its biomechanical properties. Parameters such as frontal area, volumetric biomass, number of shoots per plane area, mean stem-to-stem separation, fexibility, and submergence, allow for characterization of plant morphology in context of vegetation—fow interactions [\[4,](#page-25-1) [40,](#page-27-4) [42\]](#page-27-5). Velocity felds, drag, and turbulence structure become highly afected by these morphological parameters. Vertical velocity gradients and vertical secondary fows develop as a consequence of vegetation obstruction. Vegetation density and distribution defne strength, degree of velocity infection, and spatial heterogeneity of velocity felds [\[12,](#page-26-4) [31](#page-26-5), [34](#page-26-6)]. Drag varies across morphological scales: leaves, stems, shoots, and vegetated patches [\[5,](#page-25-2) [56](#page-27-6), [63\]](#page-28-1). Henry et al. [\[19\]](#page-26-2) point out that understanding reciprocity between complexity of biomorphological features and fow is a key factor to accurately represent drag. Vegetation density, plant fexibility, and submergence, determine levels of turbulence inside and around the canopy [[46](#page-27-7), [53](#page-27-8)]. The combination of hydraulic and canopy morphology determines wake-turbulence production near the bed, afecting deposition/erosion rates within and around the patch. Balance between vegetation-drag and shear fow above the canopy varies signifcantly between rigid and fexible vegetation and defnes in-canopy turbulence [[52](#page-27-9), [55\]](#page-27-10). As fexible vegetation aligns with the fow and reduces vegetation-drag, they allow higher in-canopy velocity and hence higher wake-production near the bed [[2](#page-25-3)]. Furthermore, solid volume fraction and submergence infuence vertical and horizontal distribution of turbulent kinetic energy, as the fow becomes highly three-dimensional. Zhang et al. [[71](#page-28-2)] found that near-bed turbulence increases with volumetric solid fraction in oscillatory fows when wave excursion-to-plant spacing ratio is greater than 0.5. Because emergent canopies span across the whole flow depth, they transform wave-scale turbulence into stem-scale turbulence as the waves travel through [[52](#page-27-9)], developing a nonuniform spatial turbulence distribution in the direction of the traveling waves [[60\]](#page-27-11). On the other hand, studies like Ghisalberti and Schlosser [[14](#page-26-7)] and Abdolahpour et al. [[1\]](#page-25-4), show that submerged canopies produce fow structure and turbulence variability characterized by above-canopy, shear, and in-canopy fow. Plant morphology thus clearly becomes a valuable component to understand vegetation—hydrodynamic interactions and their implications in their ecosystem.

Even though aquatic vegetation develops three-dimensional fow features inside and around the canopy, most studies in oscillatory fows over vegetated beds rely on pointwise and two-dimensional approaches. Computational cost of 3D modeling and instrument capabilities limit detailed analysis of instantaneous three-dimensional velocity felds. Current 1D and 2D experimental approaches have been useful to investigate certain processes: fow resistance, wave attenuation and energy dissipation. For instance, Acoustic Doppler Velocimeters (ADV) have been extensively used to study fow structure, turbulence, and wave attenuation in laboratory settings [[3,](#page-25-5) [53\]](#page-27-8) and feld studies [\[40,](#page-27-4) [54](#page-27-12)] in combination with sediment transport estimation [\[55,](#page-27-10) [65](#page-28-3)]; and arrays of single-point gauge for water surface elevation [[6,](#page-25-6) [30,](#page-26-8) [67\]](#page-28-4). On the other hand, studies like Tinoco and Cowen [\[63\]](#page-28-1) and Hansen and Reinderbach [[17](#page-26-9)] have implemented Particle Image Velocimetry (PIV) as a two-dimensional approach to characterize hydrodynamic response under diferent morphological characteristics, in laboratory and feld, respectively, which allows to capture certain fow structures when lateral uniformity can be relatively ensured [\[14\]](#page-26-7). Due to the limitation of 3D experimental data availability, even three-dimensional numerical simulation depends on point-wise measurements for calibration and validation. For example, Maza et al. [[36](#page-27-13), [37](#page-27-14)] studied wave attenuation and propagation using 3D simulations, validating their models using water surface gauge from experiments. Capturing three dimensionality of vegetated fows under oscillatory conditions is thus needed to better understand these complex vegetation—hydrodynamic interactions [\[10,](#page-26-10) [29](#page-26-11)].

Simplified models allow us to efficiently evaluate the role of specific vegetation parameters in fow-canopy interactions. Studies like Luhar and Nepf [[32](#page-26-12)], Garcia and Lopez. [[12](#page-26-4)], and Nepf [\[41\]](#page-27-15) have contributed to the fundamental understanding of these interactions. Unfortunately, oversimplifcation may misrepresent spatial organization of the fow, wake development [\[7](#page-25-7)], and lead to underestimation of sediment transport rates [[22](#page-26-13)]. Accurate representation and quantifcation of plant morphology is important to accurately simulate fow velocity, sediment transport, and drag forces for specifc species. To improve our understanding of fow-vegetation interaction for complex plant morphologies under oscillatory fows, we investigate experimentally how vegetation morphology of a single plant afects fow structure and turbulence statistics under oscillatory fow conditions. We use a novel Volumetric Particle Velocimetry technique (3D-PIV) to capture instantaneous and averaged three-dimensional (3D), three-component (3C) velocity felds. Thus, we provide three-dimensional fow organization, turbulence, and coherent structures produced by vegetation as a function of its 3D morphology. This study improves our understanding on aquatic vegetation—fow interaction in habitats exposed to oscillatory fows and its implication on ecosystem altering processes such as enhanced mixing and sediment transport.

2 Materials and methodology

2.1 Experimental setup

Figure [1](#page-2-0) shows an illustration of the experimental setup. A U-shaped oscillatory tunnel, 0.203 m-wide, 0.254 m-high, and 4.0 m-long, with a 1.52 m-long testing section, is used to impose sinusoidal cross-sectional uniform fows over a single plant. It is provided with a piston-actuator system controlled through a LabView script that allows a maximum stroke of 0.10m and minimum oscillation period of 3.0 s. The tunnel has smooth transparent acrylic walls, allowing for studies on boundary layer and coherent structures; e.g., [\[38,](#page-27-16) [39](#page-27-17)].

Fig. 1 Experimental setup: oscillatory 203×254 mm-cross section tunnel and 3D PIV system

Table 1 Summary of fow conditions as a combination of oscillation amplitude *A* and period *T*. Maximum volumetric averaged velocity U_{∞} and *Re* for the non-vegetated cases are shown (See Sect. [3.2](#page-9-0) for details)

Figure [2](#page-3-0) represents the piston position and corresponding velocity with respect to the plant, as it moves away from $(0^{\circ} - 180^{\circ})$ and towards the plant $(180^{\circ} - 360^{\circ})$.

3D-PIV measurements are taken with a TSI V3V system (TSI, Inc). It uses a coplanar array of 3 PowerView, $4MP$ (2048 \times 2048), 180 fps cameras, and an Nd:YAG, 100 mJ, 532 nm, 100 Hz, dual cavity PIV laser to measure instantaneous 3D, 3C velocity felds at a fixed $12x12x10$ *cm*³ space, at a maximum sampling frequency of 100 Hz, with a 2 mm-spatial resolution. A detailed description of the technique can be found in Pothos et al. [[51](#page-27-18)]. This novel technique has been used in ecohydraulic investigations of swimming mechanisms; e.g., [[11](#page-26-14), [26,](#page-26-15) [28](#page-26-16)], but not yet in vegetated fows. Six fow conditions are assessed as a combination of three stroke amplitudes, *A*, and four periods, *T*, as indicated in Table [1](#page-3-1). Sampling rate for the V3V system is selected such that 16 instantaneous velocity felds are measured within one wave period. Single and fexible plants are placed at the centerline of the tunnel $(y = 0 \text{ mm})$ and at 197 mm in the *x*-direction away from the center of the measuring volume $(x = 0 \text{ mm})$. It guarantees that the deflected stems of the plants will not interfere with the laser illumination of the measuring volume.

Figure [3](#page-4-0) shows an example of the available data, with the phase averaged longitudinal velocity, U_{θ} , at a given phase ($\theta = 225^{\circ}$), for flow condition A in the presence of a single seagrass-type plant. While only four planes are shown to ease visualization, the system provides the same spatial and temporal resolution for any horizontal and vertical plane within the sampling volume. Such a capability becomes important for irregular plant morphologies (as is the case for the present study), and randomly distributed vegetation arrays

(the focus of a future study), where fow structure and thus mixing and sediment transport patterns depend on spatial arrangement and geometry of the vegetation.

2.2 Synthetic vegetation

Three plant morphologies are evaluated: (a) 'seagrass', characterized by fat, elongated, blade-shaped leaves; (b) 'leafy', characterized by ascending stems with rounded and fat leaves running along each stem; and (c) 'spikey', showing needle-like leaves, arranged in crown-shaped foliage (Figs. [4,](#page-4-1) [5](#page-5-0)). Plastic surrogates are used to represent these morphologies, made of the same plastic material but distinct shapes. Material density ρ is 840 kg m⁻³ and Young's modulus *E* is 5.33 × 10⁷ Pa. These two intrinsic properties of the material are true for each morphological element of the plant (stems, leaves, branches). These values agree with biomechanical properties of aquatic vegetation

Fig. 4 Synthetic plants representing: **a** 'seagrass', **b** 'leafy', and **c** 'spikey' morphologies, their respective stem morphology (**d**–**f**) and their leaf morphology (**g**–**h**)

Fig. 5 Synthetic plants representing: **a** 'seagrass', **b** 'leafy', and **c** 'spikey' morphologies. They show frontal area contours variation under fow condition A. Top insets show raw images from submersed camera. Lower plots **d**–**f** present an example of frontal area variation under flow condition A

 $(\rho = 664.17 - 1032.34 \text{ kg m}^{-3} [66]$ $(\rho = 664.17 - 1032.34 \text{ kg m}^{-3} [66]$ and $E = 5.56 \times 10^6 - 1.99 \times 10^8 \text{ Pa} [48]$ $E = 5.56 \times 10^6 - 1.99 \times 10^8 \text{ Pa} [48]$) and fall within the range of values used in previous studies to replicate aquatic vegetation-fow interaction ($\rho = 670 - 920 \text{ kg m}^{-3}$ and $E = 5.0 \times 10^5 - 2.4 \times 10^9 \text{ Pa}$) e.g., [\[2](#page-25-3), [13](#page-26-17), [32\]](#page-26-12). Flexural strength is defned as the product between Youngs modulus *E* and the second moment of the cross-sectional area *I* perpendicular to the force [\[4](#page-25-1)]. Table [2](#page-5-1) summarizes fexural strength of the tested models considering cross-sectional geometry of their stems.

Seagrass plant is formed by 5 leaves, 195 mm-long, 1.72 mm-thick, and 21.5 mmwide. Leafy plant consists of 4 ascending branches 144 mm-long with approximately 23 leaves 1.72 mm-thick and 13.5 mm-wide. Spikey plant is formed by 3 branches 164 mm-long with 22 crown-shaped arrays of spikes. Spikey shoots are fan-shaped leaves with 1.02 mm-diameter spikes that branch out from large into smaller spikes; with their lengths ranging from 23.3 to 2.7 mm. Species like like *Zostera* subgenus *Zosterella*, *Thalassia*, and *Posidonia* fall under Seagrass type of morphology [[25\]](#page-26-18). Leafy morphology includes species with environmental interest such as *Micranthemum umbrosum* sp., *Elodea candensis*, *Hyrophila polysperma*, and *Cedamine lyrata*. *Cabomba aquatica*,

Cabomba coraliniana, *Ceratophyllum echinatum* A. Gray, and *Limnophila indica* are just a few examples of Spikey morphology.

Frontal area is calculated from videos taken with a submerged camera (GoPro Hero4- Black) downstream of each plant at 30 fps (30 Hz) under each fow condition prior to velocity measurements. 8.3 MP-frames from video recordings are extracted at the sampling frequency shown in Table [1.](#page-3-1) Since fps from the camera is signifcantly higher than sampling frequencies, we are able to match precisely the velocity measurements with the pictures of vegetation frontal area. Figure [5](#page-5-0) illustrates the frontal contour variation of these morphologies from 0° to 180°. The top insets show a raw image from the downstream camera, and bottom insets show an example of the frontal area profle for one of the fow conditions investigated, to be discussed in next section.

2.3 Method of analysis

Longitudinal, lateral, and vertical coordinates are defned as *x*, *y*, and *z* axis, respectively; with their corresponding velocity components *u*, *v*, and *w*. Instantaneous velocity is decom-posed according to Eq. [1](#page-6-0); where u is instantaneous velocity, U_c is time-averaged velocity, U_{θ} is phase-averaged velocity, and u' is the turbulent fluctuation [\[43,](#page-27-20) [64\]](#page-28-6). Phase-averaged velocity is computed following Eq. [2](#page-6-1), where *N* is the total number of measured oscillations and ω is angular velocity [[21](#page-26-19), [23\]](#page-26-20).

$$
u = U_c + U_\theta + u'
$$
 (1)

$$
U_{\theta} = \frac{1}{N} \sum_{n=1}^{N} [u(x, y, z, \omega(t + nT)) - U_c]
$$
 (2)

Spatial-averaging is denoted by angle brackets ⟨⟩. Equations [3a](#page-6-2), [3b](#page-6-3) and [3c](#page-6-4) presents examples of the averaging schemes of *u* to average over *y* to obtain a single vertical *xz* plane ([3a\)](#page-6-2), average over *x* and *y* to obtain a single vertical profle ([3b](#page-6-3)), and average over *x*, *y*, and *z* to obtain a volumetric average, i.e., a single bulk value representative of the fow conditions. Notice that subscripts indicate coordinates over which averaging took place. N_x , N_y , and *Nz* are total points along coordinates *x*, *y*, and *z*, respectively. Same scheme applies for all other possible vertical and horizontal planes and profles within the sampling volume (see Fig. 3).

$$
\langle u \rangle_{\mathbf{y}} = \frac{1}{N_{\mathbf{y}}} \sum_{j=1}^{N_{\mathbf{y}}} u(x_i, y_j, z_k, \omega t)
$$
 (3a)

$$
\langle u \rangle_{xy} = \frac{1}{N_x N_y} \sum_{i=1}^{N_x} \sum_{j=1}^{N_y} u(x_i, y_j, z_k, \omega t)
$$
 (3b)

$$
\langle u \rangle_{xyz} = \frac{1}{N_x N_y N_z} \sum_{i=1}^{N_x} \sum_{j=1}^{N_y} \sum_{k=1}^{N_z} u(x_i, y_j, z_k, \omega t); \tag{3c}
$$

Phase-averaged turbulence kinetic energy (TKE_{θ}) is computed according to Eq. [4](#page-7-0) [\[50\]](#page-27-21).

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$$
TKE_{\theta} = \frac{1}{2} \sqrt{(u'^2)_{\theta} + (v'^2)_{\theta} + (w'^2)_{\theta}}
$$
(4)

3 Results and discussion

3.1 Vegetation frontal area

Figures [6](#page-7-1) and [7](#page-8-0) present the vertical variation of phase-averaged frontal area at $\theta = 0^{\circ}$, 90[°], and 270° for the three plant types. We explore the effect of changing period while keeping a constant oscillation excursion ($A = 54$ mm with *T* varying from 3.2 to 10 s in Fig. [6\)](#page-7-1), and

Fig. 6 Vertical profile of normalized phase-averaged frontal obstructed area at three phases, $\theta = 0$ [°], 90[°], and 270◦. Blue line: leafy, orange line: seagrass, green line: spikey. Depth is normalized by tunnel height *H*, frontal area normalized by tunnel width *W*. Cases with constant $A = 54$ mm are shown

Fig. 7 Vertical profile of normalized phase-averaged frontal obstructed area at three phases, $\theta = 0$ [°], 90[°], and 270◦. Blue line: leafy, orange line: seagrass, green line: spikey. Depth is normalized by tunnel height *H*, frontal area normalized by tunnel width *W*. Cases with constant $T = 5$ s are shown

the effect of varying excursion while keeping a constant period ($T = 5$ s with A varying from 54 to 14 mm in Fig. [7\)](#page-8-0). Normalized frontal area is calculated as the fraction of tunnel width obstructed by the plant, l_f/W ; where $l_f(z)$ is cumulative length of actual tunnel width obstructed by a plant at elevation z (see Fig. 5 for reference).

Spikey and leafy cases show similarities in their frontal area distribution, while seagrass is signifcantly diferent. Frontal area profles of spikey and leafy cases show small-scale variations (a zig-zag pattern) and are more uniformly distributed along the height of the plant, as the clumps and crowns (Fig. [5\)](#page-5-0) are more uniformly distributed along the plant length. Seagrass frontal area profles are smoother due to the blade-shape of their leaves, and present two peaks due to diferent leaves positioned at diferent heights. Frontal area profles respond more dynamically to shorter oscillation periods, but they are less sensitive

to variations on oscillation excursion. In flow C (Fig. $6g-i$ $6g-i$), frontal area profiles do not show any evident change over a deceleration-acceleration cycle; whereas a more dynamic change is observed under flow condition A (Fig. $6a-c$ $6a-c$). Since rearrangement of vegetation canopy is associated with passive and active interactions to reduce drag [\[5](#page-25-2)], the observed plant alignment is a relevant parameter to predict the impact of vegetation on fow.

3.2 Flow structure: spatial organization

3.2.1 Velocity

Table [1](#page-3-1) shows a summary of maximum velocity U_{∞} and Reynolds number (Re = $U_{\infty}A/\nu$) for non-vegetated cases. U_{∞} corresponds to the maximum absolute value of the longitudinal, volumetric-, phase-averaged velocity (see Eq. [5](#page-9-1)).

$$
U_{\infty} = \max\left(\left| \langle U_{\theta} \rangle_{xyz} \right| \right) \tag{5}
$$

A time average of the longitudinal velocity over several periods shows a non-zero underlying current *Uc*. This velocity is attributed to remaining momentum after the piston changes direction.

Figure [8](#page-10-0) shows velocity felds over the vertical *x*–*z* plane at the centerline of the tunnel ($y = 0$ mm), for case B ($T = 5$ s, $A = 54$ mm) for all three plants. Flow is predominantly aligned in the x-direction and negative as phase $\theta = 270^\circ$ corresponds to the negative-velocity peak. Longitudinal velocity is consistently uniform in the *x*-direction. A clear boundary layer is noticed with low near-bed velocities growing until reaching outer fow speeds above $z = 20$ mm. Velocity vectors are clearly aligned in the longitudinal direction for the non-vegetated case, but they show clear variations as fow moves past the plant, with larger vertical component clearly noticed around $z = 100$ mm at the regions closest to the plant.

As a single plant, there is a low impact on the average longitudinal velocity feld (as is the case with very sparse canopies), but the interactions of the oscillatory fow with the moving plant clearly alter the 3D structure of the fow, as noticed by the larger lateral velocities identifed in Fig. [8](#page-10-0) past the plants. The diferent plant morphologies force fuid parcels to move laterally generating shedding vortices at multiple scales. Keulegan–Carpenter number ($KC = U_{\infty}T/L$, where *L* is the stem-shoot width) ranges from 11 to 19 for these morphologies; which results in additional asymmetric shedding vortices according to Guilmineau and Queutey [\[15\]](#page-26-21). Apparent size of these eddies varies as a function of plant geometry. Areas of organized fow scale with leaf size and crown-shaped leaves of leafy and spikey morphologies, respectively (20 mm and 10 mm). For seagrass with blade-shape, long, and flexible leaves, a smaller effect on lateral velocity is expected under uniform flow conditions [\[5](#page-25-2)], but bending of the plant under oscillatory conditions creates a clear 3D fow. Such heterogeneity of lateral velocity can enhance lateral dispersion, both as a function of vegetation density [[58](#page-27-22)] and as a function of plant morphology.

Figures [9](#page-11-0) and [10](#page-12-0) present phase-averaged velocity felds in horizontal *x* − *y* planes at $z = 2$ mm (near the bottom, Fig. 9), and at $z = 100$ $z = 100$ $z = 100$ mm (Fig. 10) as the piston accelerates towards the plant ($\theta = 225$ °). Horizontal in-plane velocity vectors and magnitudes of vertical velocities represented by the colormap near the bed (Fig. [9](#page-11-0)) show areas of large negative and positive vertical velocity, coupled with local perturbations of U_{θ} and V_{θ} , which are more prevalent and with higher intensities in vegetated cases.

Fig. 8 Phase-averaged velocity field at vertical x –*z* plane at $y = 0$ mm under flow condition B, $T = 5$ s and $A = 54$ mm

Longitudinal velocities are smaller at this near-bed location (see Fig. [8](#page-10-0)), such that the vertical and lateral component can be more signifcant to determine bed efects (total stress and efect on sediment transport). In accelerating phases, low-velocity fuid parcels are moved upward from the bottom (ejections) and high-velocity fuid parcels are transported downward from higher elevations (sweeps) $[21, 23, 64]$ $[21, 23, 64]$ $[21, 23, 64]$ $[21, 23, 64]$ $[21, 23, 64]$. The bed thus becomes subject to vortices set by the plant morphology as they are swept towards the bed. The detected fow spatial organization can infuence patterns of near-bottom sediment transport and bedform development.

Fig. 9 Phase-averaged velocity field at a horizontal $x - y$ plane at $z = 2$ mm under flow condition B, $T = 5$ s and $A = 54$ mm

In Fig. [10](#page-12-0), the longitudinal velocity component is prevalent. However, large average fuctuations are noticed in the proximity of plant locations, with a more noticeable velocity divergence for seagrass and spikey plants. While stifness is not a controlled parameter in this experiment; the morphology and freedom to deform to align with the fow induces anisotropic fow organizations at a diferent degree for each plant type.

Figure [11](#page-13-0) shows longitudinal velocity, time averaged over several periods, on a vertical *y* − *z* plane, perpendicular to wave propagation, at a location $x = -1$ mm, to identify patterns in the underlying current U_c . Underlying current is defined here as the resulting

Fig. 10 Phase-averaged velocity field at a horizontal x –*y* plane at $z = 100$ mm under flow condition B, $T = 5$ s and $A = 54$ mm

fow after time-averaging the velocity felds over a certain number of oscillation periods. While this non-zero value can be driven by small asymmetries in the piston motion driving the fow, the structure and patterns noticed in Fig. [11](#page-13-0) highlight the diferences created by the obstructions, and are akin to efects observed in other oscillatory tunnels and wave flumes. See for example; Tinoco and Coco [[61](#page-27-0)], and Luhar and Nepf [\[32\]](#page-26-12). Further volumetric-averaging of U_c shows that the net longitudinal velocity is practically negligible $(O(10^{-3} \text{ m s}^{-1}))$, thus ensuring continuity is being satisfied. U_c varies around ±0.01 m s[−]¹ , with strong fuctuations in the presence of vegetation. In the no vegetation

Fig. 11 Longitudinal velocity distribution of underlying flow at $x = -1$ mm. Oscillation period and stroke amplitude are 5 s and 54 mm, respectively. Black lines over the surface correspond to longitudinal velocity profles

case, it contributes to approximately 8 % of the maximum outer velocity U_{∞} and causes *A* to become larger than half of the piston stroke by a similar proportion (see Table [1\)](#page-3-1). Positive and negative peaks of longitudinal velocity increase progressively in seagrass, leafy, and spikey morphologies. Velocity feld also shows some concavity along the centerline of the tunnel ($y \approx 0$ mm) for leafy and spikey plants, a behavior associated with lateral and vertical wakes behind the plants.

To better understand the changes in velocity for diferent plant species, we look at how the plants bend with the fow, using side-view recordings and identifying their maximum excursions on both directions for all flow conditions (Fig. [12](#page-14-0)), as they experience displacement in the positive x-direction (between 0°–180°), and in the negative x-direction (between 180° and 360°). Lateral displacements range from 4.9 to 105.1 mm. It is noticed that: (a) Not all stems and blades experience the same range of motion, specially noticed for the seagrass case, where the one blade bent the most towards the negative x-direction barely moved throughout the full oscillation (noticed by the overlap between shaded profles), while other blades (seagrass) and stems (spikey and leafy) rotate almost 90◦ in an *x*–*z* plane during one period (cases A and B, Fig. [12\)](#page-14-0); and (b) Looking closely at both Figures [5](#page-5-0) and [12](#page-14-0) we notice spikey and leafy plants sway mostly around the y-axis within vertical *x*–*z* planes, while seagrass experiences more signifcant rotation around the *z*-axis, with blades changing orientation with respect to the flow at different phases, in contrast with expected streamlining under unidirectional conditions.

These two observations show that a static plant morphology can inform us of the scale of the expected eddies, but a dynamic analysis and bending observations are critical to identify their orientation and location. As plants reach their maximum excursion towards either the negative or positive x-direction, they get closer to the bed, potentially increasing their efect on near-bed velocities, shear stress, and thus their efect on sediment transport.

Fig. 12 Lateral displacement range for the three species at all flow conditions. Positive x displacement (blue) between 0 and 180. Negative *x* displacement (red) between 180 and 360. Excursion length, *L*exc, is represented in top-right subplot

Figure [12](#page-14-0) shows that plant excursions are mostly dependent on maximum speed (see Table [1\)](#page-3-1) rather than *A* or *T* alone. Keeping the same $A = 54$ mm while changing $T = 3.2$ s (A), 5.0 s (B), and 10.0 s (C), results in a decrease in maximum velocity from 99 to 37 mm/s, yielding large plant excursions for A and minimum motion for C. Keeping the same $T = 5$ s while varying $A = 54$ mm (B), 25 mm (D), and 14 mm (F), results in reduction of maximum velocity from 66 mm/s (B) to 15.6 mm/s (F), and thus barely noticeable motion in F. This pattern is also evident in cases C, D, and E, with chosen combinations of *T* and *A* that yield similar maximum speeds (32.5–37.7 mm/s) and show almost identical plant excursions.

Drag force (F_D) acting on flexible vegetation depends on the relative velocity between flow and plant. This is conceptualized by Zeller et al. [\[70\]](#page-28-7) using the maximum plant excursion L_{exc} and oscillation excursion *A* ($KC_{\text{exc}} = A/L_{\text{exc}}$, see Fig. [12](#page-14-0)). Drag coefficient C_D follows a power-law relationship with Keulegan–Carpenter KC_{exc} number when wake development scales with *A* and obstruction scales with L_{exc} ($C_D \propto (A/L_{\text{exc}})^{-1.7}$) [\[70\]](#page-28-7). Cauchy number *Ca* measures the ratio between drag and rigidity-restoring forces [[33](#page-26-22)]. This balance indicates how prone fexible vegetation is to streamline or stay upright under certain fow conditions. The relative strength of drag force with respect to plant rigidity (rigidity force F_R), expressed in Eq. [6,](#page-15-0) depends on the maximum velocity by a power of 2; where ρ_w is water density, A_f is stem frontal area, and *l* is stem length. Therefore, the larger weighted contribution to drag coming from *U* with respect to *A* makes plant excursion more dependent on maximum velocity than oscillation excursion or period alone. Furthermore, the ratio between oscillation excursion and plant size becomes a limiting factor for fow-vegetation behavior and turbulence production. Luhar and Nepf [[32](#page-26-12)] explain that fow-vegetation interaction resemble steady unidirectional behavior at the limit where *A* is larger enough than vegetation length *l*. Inertia forces from the plant acting upon the fow may be neglected because the relative velocity between fow and vegetation is similar to the fow velocity itself. Investigating Vogel number efects on velocity skewness, Pan et al. [[47](#page-27-23)] found that more negative Vogel number (associated with increasing A/L_{exc}) correlates with peaks in longitudinal and vertical velocity skewness (strong sweeps) that penetrates into near-bed elevations. Such efect can potentially enhance resuspension and favor mass exchange with above-canopy regions.

$$
Ca = \frac{F_D}{F_R} = \frac{C_D U_{\infty}^2 \rho_w A_f}{2} \frac{l^2}{EI}
$$
 (6)

$$
B = \frac{F_B}{F_R} = g(\rho_w - \rho_v) V_{\text{stem}} \frac{l^2}{EI}
$$
 (7)

Buoyancy parameter, *B*, is a dimensionless parameter that measures the relative contribution between buoyancy- and rigidity-restoring forces [\[2](#page-25-3)]. It is defned in Eq. [7](#page-15-1) as the ratio between buoyancy and rigidity forces (F_B/F_R) ; where ρ_ν is the density of the plants, *g* is gravitational acceleration, and V_{stem} is stem volume. Figure [13](#page-16-0) presents the *Ca* variation with respect to *B* and KC_{exc} . Drag (and thus *Ca*) increases with maximum flow velocity and buoyancy coefficient *B*. Higher buoyancy contributes to keep stems upright longer, resulting in shorter plant excursions (smaller KC_{exc}). In contrast, a weaker impact of *A* is seen in flow C and E of Fig. [13.](#page-16-0) While both have the same maximum velocity, drag force is stronger in flow E ($A = 0.05$ m) than in flow C ($A = 0.01$ m) by almost an order

Fig. 13 Cauchy number, *Ca*, as function of buoyancy coefficient, *B*, and Keulegan–Carpenter number based on plant excursion, KC_{exc} , at all flow conditions

of magnitude. Data also show that canopy morphology afects the balance between drag, buoyancy, and rigidity forces. Even though all synthetic plants used in this work are made out of the same material, second moment of inertia *I*, stem volume, and frontal area, are necessarily function of vegetation geometry.

3.2.2 Velocity defect profles

The efect of plant morphology is investigated by looking at the normalized velocity defect profles, calculated from Eq. [8,](#page-16-1) where "veg" and "no veg" denote vegetated and no vegetated conditions, respectively.

$$
\Delta U_{xy}(z,\omega t) = \left[U_{xy}(z,\omega t) \right]_{\text{veg}} - \left[U_{xy}(z,\omega t) \right]_{\text{no veg}}
$$
(8)

Results are shown in Figs. [14](#page-17-0) and [15](#page-18-0). An additional case with a single rigid cylinder, with diameter of 11.3 mm was conducted for comparison at all fow conditions. Profles of longitudinal phase-averaged velocity show a decrease in the presence of vegetation for the phases presented in Figs. [14](#page-17-0) and [15](#page-18-0). The efect of vegetation decreases with increasing *T* (i.e., when reducing maximum velocities). Velocity defect past the plants becomes more sensitive to *A* variation than to *T* variation. Diferences between longitudinal velocity defect profiles at phases 90° and 270° are attributed to the relative location of the measuring volume with respect to the vegetation and the fow direction. Over negative-velocity phases, the measuring volume is located at the wake zone of the vegetation (see Figs. [1,](#page-2-0) [2](#page-3-0)). While, it is found "upstream" of the plants over the positive-velocity phases. Although no consistent $\Delta \langle U_{\theta} \rangle_{xy}$ pattern based only on plant morphology is found, it is noticed that the profles of velocity defect for the leafy and spikey cases resemble the general trend of their frontal area profles, with a zig-zag small-scale fuctuation in both frontal area and velocity profles. Overall, the spikey case presents a larger efect on longitudinal velocity, almost on par with the rigid cylinder, in particular for the higher velocity cases (A and B).

Fig. 14 Profles of longitudinal velocity defect. Blue line: leafy, orange line: seagrass, green line: spikey, red line: cylinder. Flow conditions A, B, and C where $A = 54$ mm

3.2.3 Vorticity

Since the plants generate eddies at multiple scales, and their changing orientation and position (Figs. [5,](#page-5-0) [12](#page-14-0)) yields eddies on various planes, we conduct an analysis of vorticity to identify their net effect. Figure [16](#page-19-0) presents iso-surfaces of phase-averaged vorticity with respect to the y-axis, ω_y , under flow B at accelerating phase $\theta = 225^\circ$. The iso-surfaces are integrated with *x*–*z* planes color maps at $y = -20$ mm and $y = 20$ mm.

The 3D vorticity captures tubular coherent structures described frst by [[9](#page-26-23)] and later studied by [[38](#page-27-16)]. Previous lacking of 3D measurements limited experimental identifcation and description of these structures [\[38\]](#page-27-16). Results from the non-vegetated case agree with Mujal et al.'s experiments [[38](#page-27-16)]: tubular coherent structures form at early accelerating phases and are ejected half-way of the accelerating phases; at which point new coherent

Fig. 15 Profles of longitudinal velocity defect. Blue line: leafy, orange line: seagrass, green line: spikey, red line: cylinder. Flow conditions B, D, and F where $T = 5.0$ s

structures start developing close to the wall (Fig. [16\)](#page-19-0). The non-vegetated case shows this tubular surfaced uniformly aligned near the bed, which contrast with the patterns observed past the three plant types, where production and ejection of elongated vortices prevails. The tubular coherent structures become segmented by the plant morphology (stem, blades, leaves, and/or needles) over the negative-velocity phases. Figure [16](#page-19-0) shows a more irregular, highly 3D vorticity feld, with smaller length scale structures for the case of spikey and leafy cases, as expected due to the prevalence of crowns and small leaves for such morphologies in comparison with the long, smooth blades of the seagrass type. Such shorter tubular coherent fow structures generated by the plants with a broader distribution within the water column, in contrast with the near-bed long structures creating a nearly 2D scenario from a fat bed, can alter the spatial development of bedforms under oscillatory fows in presence of fexible vegetation. Tubular vortex in oscillatory boundary layer fows cause

Fig. 16 Iso-surface of lateral component of vorticity $\omega_y = 5 \text{ s}^{-1}$ under flow condition B, $T = 5 \text{ s}$ and *A* = 54 mm. Two *x*–*z* planes show color maps of ω ^{*y*} at $y = -20$ mm and $y = 20$ mm

sediment entrainment as they resemble size and strength of vortex shedding over wave ripples [[18](#page-26-24)].

3.2.4 Shear stress

Figure [17](#page-20-0) presents variation of phase-averaged bed shear stress as a function of phase θ and lateral coordinates *y* for all three plants, for the maximum and minimum orbital velocities: case A (U_{∞} = 99.0 mm/s), B (U_{∞} = 66 mm/s), and F (U_{∞} = 15.6 mm/s). Since log-law velocity conditions do not fully develop over a complete oscillation [\[21\]](#page-26-19), spatial distribution of τ_b is estimated by the momentum deficit between the outer and the boundary layer velocity [[39](#page-27-17)] (Eq. [9\)](#page-19-1). Bed shear stress corresponds to the estimated shear at our closest measurement to the bottom ($z = 2$ mm). It is later normalized by ρU_{∞}^2 from each case. Fig-ure [17](#page-20-0) shows the estimated bed shear stress along the *y*-axis at $z = 2$ mm and $x = 40$ mm for each phase.

$$
\frac{\tau(\theta, z)}{\rho} = \int_{z}^{\infty} \frac{\partial \left[U_{\infty}(\theta) - U_{\theta}(\theta, z) \right]}{\partial t} dz
$$
\n(9)

The highest phase-averaged shear stress occurs near 160° and 337.5°, following a approx-imate 65°-phase lag behind the top speeds at 90° and 270°. Hansen and Reidenbach [[16](#page-26-25)] found that bed shear stress is signifcantly reduced in the presence of patches of vegetation. Yang et al. [\[68\]](#page-28-8) developed a predictor for bead shear stress in arrays of rigid vegetation

Fig. 17 Transverse spatial distribution of phase-averaged bed shear stress., $\tau_{b\theta}/(\rho U_{\infty})$ (1), past the plant, for flow conditions A ($A = 54$ mm, $T = 3.2$ s, $U_{\infty} = 99.0$ mm s⁻¹), B ($A = 54$ mm, $T = 5.0$ s, $U_{\infty} = 66.0$ mm s⁻¹), and F ($A = 14$ mm, $T = 5.0$ s, $U_{\infty} = 15.6$ mm s⁻¹), for all plants studied

using an efective friction velocity that depends on the dampened velocity within the array and either a drag coefficient for the bare bed or the individual plant diameter. As we focus on a single vegetation element, these type of predictors do not directly apply, as we look at how the bending and orientation of the plants can afect stresses locally, and there is not an array dense enough to dampen velocities as in [[16](#page-26-25), [68](#page-28-8)]. From Fig. [12](#page-14-0) for all cases, and Fig. [5](#page-5-0) for case A, we notice the displacement of the three plants under fows A, B, and F. From 180 \degree to 360 \degree the plant bends in the direction of wave propagation (negative *x*), with stems and blades getting closer to the bed toward the measured volume. From 0° to 180◦, the blades move towards the positive *x* direction, away of the measured volume. The closer proximity of blades and stems to the bed around 270◦ coupled with the lateral movement of the blades can result in asymmetric effects on the stress distribution. Lateral variations of bed stress with respect to the non-vegetated case are more evident for seagrass and leafy types, consistent with the wider range of motion in the *y*-direction, as seen in Fig. [5](#page-5-0), whereas the spikey case, which motion is more constrained to the *x*–*z* plane, shows a more uniformly distributed stress in the transverse, *y*-direction.

Figure [17](#page-20-0) provides a clear picture of the distributed stresses and efect of a single plant due to stems and bed orientation (Fig. [5](#page-5-0)) and proximity to the bed (Fig. [12](#page-14-0)), but does not show the changes in magnitude of these stresses. Taking transects from plots in Fig. [17](#page-20-0) at $y = -20$ mm, $y = 0$ mm, and $y = 20$ mm along the full cycle, Fig. [18](#page-21-0) shows the

Fig. 18 Phase-averaged bed shear stress as function of phase along $y = -20$ mm, $y = 0$ mm, and $y = 20$ mm for the three plants investigated, for flow conditions A, B, and F

phase-averaged bed shear stress evolution, as a function of phase, at these three transverse locations. Figure [18](#page-21-0) shows more clearly the decrease in mean bed shear stress in the vegetated cases, as well as the asymmetry between $y = -20$ mm and $y = +20$ mm data seen in Fig. [17](#page-20-0)

Plant morphology efect on bed shear stress heterogeneity is stronger in fows with low velocity. Higher variability in bed shear stress is found in fow F, where all plants had very limited range of motions. The degree of velocity alteration becomes more sensitive to plant morphology in low-velocity fows as they are easily disrupted by the vegetation. Leafy case has the greatest impact on bed shear stress distribution compared to the non-vegetated cases. This plant morphology has the shortest plant excursion in fow F and intermediate buoyancy coefficient B among the three morphologies. Thus, bed shear stress heterogeneity comes from flow separation that take place from a nearly steady standing plant rather than a swaying one.

The impact on bed shear stress variability as a function phase is higher in vortex shedding from a relatively static plant than from fow separated at swaying branches. The earlier will be able to strike the bottom mainly at peak-velocity phases where L_{exc} is the longest and if plant excursions scales with the canopy height. Note in flow A negative-bed shear stress increasings at $\theta = 270^{\circ}$, where plant excursion and oscillation excursion are

the maximum ($A = 54$ mm and $L_{\text{exc}} = 94$ and 105 mm). This may be attributed to flow separating from the defected plant and disrupting the near-bottom velocity distribution i.e. altering bed shear stress distribution. Pan et al. [\[47\]](#page-27-23) explain that larger plant excursion leads to strong vortex shedding towards to bed. Later quadrant analysis shows sudden increase of Q1 events at 270° corresponding to events that move low momentum flow from lower elevation to higher elevations in the negative-velocity part of the oscillation and coinciding with potentially fow separated from defected branches.

We notice that the heterogeneity of the plant morphology, and its behavior as it sways in response to the fow, can create areas of stress that difer from spatially averaged estimates, and can bias estimation of sediment transport.

3.3 Turbulence

3.3.1 Phase‑spatial development of TKE

Phase-averaged values allow us to estimate mean efects on bed stresses, but do not provide enough information regarding large instantaneous bursts and turbulent features. Figure [19](#page-22-0) presents phase-variation of the near-bed turbulent kinetic energy (TKE) distribution in the *y*-direction past the plant. The inset in Fig. [19](#page-22-0) shows the region over which TKE is averaged in *x* and *z*. Vegetation density (above-ground biomass per unit area) has been found positively correlated with TKE [[44](#page-27-24)]. Studies on arrays of rigid cylinders showing a clear increase of TKE as array density increases [\[61,](#page-27-0) [62\]](#page-28-0), but fexible vegetation canopies are associated with a reduction in TKE; e.g., [\[52,](#page-27-9) [55](#page-27-10)]. Our single-plant cases represent an

Fig. 19 Transverse distribution of phase-averaged TKE at $z = 2$ mm, past the plant as shown in the inset, for flow condition B, $T = 5$ s and $A = 54$ mm, for all plant types studied

extremely sparse condition, where near-bed TKE is enhanced not by the combined TKE generated by an array, but by fow perturbations generated by a single swaying plant. The variations in TKE are consistent with Tempest et al. [[59](#page-27-25)], who pointed out that high TKE and local scouring is found in salt marsh canopies around isolated plants or small vegetation patches.

Our data show that: (a) a clear increase in TKE driven by the presence of the diferent plants, (b) higher TKE levels for spikey and leafy morphology, larger than the generated by the smoother blades from seagrass, (c) a more widely transversely distributed TKE for the leafy plant compared with the spikey plant, corresponding to the lateral, y-direction, incursions of the leafy morphology, whereas the spikey plant remains mostly constrained in an *x*–*z* plane, (d) higher values are seen for the range 180°–360° than 0°–180°, corresponding to the range on which the plant sways towards the sampling volume, and (e) a maximum found for the spikey case around $y = 0$ mm, $\theta = 225^{\circ} - 270^{\circ}$, corresponding to the spikey stems getting the closest to the bed within the sampling volume during the maximum fow speed than the other plant types. These observations highlight the need to consider not only the frontal area of plant elements, but their location and orientation at diferent phases of the fow, to improve prediction schemes of velocity and shear stress in order to more accurately estimate sediment transport.

3.3.2 Quadrant events distribution

Figure [20](#page-24-0) presents relative frequency of instantaneous turbulent events (represented by combinations of *u'* and *w'*), defined as the ratio between the number of events N_q taking place in the quadrant q (1, 2, 3, or 4) and the total number of events in all quadrants $(N_T = N_1 + N_2 + N_3 + N_4)$ at the $x - y$ plane located at $z = 10$ mm and bounded between $x = 30$ mm and 40 mm. In contrast to phase-averaged velocities, we find that velocity fluctuations are more sensitive to laser refection from the bottom. Vertical elevation equal to 10 mm is the closest *z* elevation where refections do not introduce excessive noise in velocity fuctuations. Clear patterns of turbulent events are found at this near-bottom elevation. Following a typical quadrant analysis, we examine the occurrence of sweeps $(u' > 0$, $w' < 0$, Quadrant 4), ejections ($u' < 0$, $w' > 0$, Quadrant 2), outward interactions ($u' > 0$, $w' > 0$, Quadrant 1), and inward interactions ($u' < 0$, $w' < 0$, Quadrant 3). The number of events identifed for each quadrant, divided by the total number of events recorded, yield the percentages shown in Fig. [20](#page-24-0). Flow is dominated by outward and sweeps events over the positive-velocity phases, while over the negative-velocity phases, inward and ejection events dominate. Vegetation enhance the occurrence of the (u', w') fluctuation events. Yang and Choi [[69](#page-28-9)] found that sweep interactions are more frequent in vegetated fows near the bottom. An increasing frequency of fuctuation events near the bottom suggest higher potential for sediment resuspension [[57](#page-27-26)]. By combining sweep-outward and ejection-inward interactions, turbulent fuctuations can pick sediment particles up at the bottom and bring them into suspension. Even for a single plant, a clear increase in prevalence of these turbulent events is noticed in comparison with the non-vegetated scenario. Frequency of these instantaneous turbulent events varies with plant morphology. We notice a larger efect by spikey and leafy morphologies, which for the present study have a wider range of motion during a wave period, have multiple scales at which wakes can be generated (spines/leaves, crowns, stems) and reach a closer proximity to the bed when swaying towards the sampling volume, in contrast with the smoother blades of the seagrass type. Even if the seagrass would show a larger frontal area when considering all blades, the

Fig. 20 Proportion of (u', w') events occurring at each quadrant of the $u' - w'$ plane at $z = 10$ mm, past the plant as shown in the inset, for flow condition B, $T = 5$ s and $A = 54$ mm, for all plant types studied

alignment with respect to the fow allows for a smaller efect in TKE generation than the thinner, more complex geometry of the spikey and leafy plants.

4 Conclusions

Studies on aquatic vegetation often characterize the efect of vegetation patches in terms of their porosity, frontal area, height, submergence ratio, and population density. Such parameters are used to classify them as "sparse" or "dense" arrays, a designation that specifes whether they can prevent or enhance bed stresses and thus sediment transport within the patches. Our study explored the lowest end of vegetation density, conducted with a single submerged plant, to explore the efect of three diferent plant morphologies, representative of vegetation on riverine, tidal, and coastal conditions. The study, using a 3D-volumetric PIV system, found diferences among the three vegetation species in the recorded magnitude, as well as temporal and spatial distributions, of bed shear stresses, turbulent kinetic energy, and instantaneous turbulent events. Such changes were associated not only with the plant morphology (blades, leaves, or needles), but also the relative position and orientation with respect to the flow, as different plants can sway around their x , y , or z axis throughout the oscillation period depending on their morphology, with some species bending to a closer proximity to the bed, allowing for blade- and leave-scale eddies from the prone branches to interact with the bed. Even though this study do not seek to formulate a sediment transport relationship, it suggests that, at the limit of extreme sparse fexible canopy, morphology and biomechanical characteristics infuence the local near-bed turbulence and surrounding fow structure under oscillatory conditions. Studies have shown that sparse vegetation have little impact on the bulk fow structure, acting only as fow roughness and producing turbulence at the stem-scale in unidirectional settings. This works explores further into how even a single fexible plant, as it bends with the fow, can locally alter fow organization and turbulence, enough to alter bed shear stress and instantaneous turbulent events to potentially enhance sediment transport even within the sparsest fexible canopies. Our study also shows that such an efect can be quantifed by identifying correlations between oscillation period and plant excursion with morphological parameters of the vegetation. In addition, we show that characterizing plants with a single porosity or plant density parameter can neglect signifcant instantaneous turbulent events, such that the range of motion of the plant under study must be considered to quantify a range of stress and turbulence values that can be generated even within very sparse patches of vegetation, in order to improve predictions of erosion and deposition patterns within them.

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