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Mechanochemical-assisted production of 5hydroxymethylfurfural from high concentration of cellulose

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Abstract Direct production of the platform chemical 5-hydroxymethylfurfural (5-HMF) from cellulose is challenging due to the rigid structure of cellulose. Herein, 5-HMF was effectively obtained from cellulose with high loading concentrations (> 20 wt.%) via an Al₂(SO₄)₃-assisted mechanochemical method. The Al₂(SO₄)₃ not only acted as catalyst for its Lewis and Brønsted acidity, but also assisted the disruption of the hydrogen bonds among cellulose molecules during ball milling pretreatment. The particle size and crystallinity of the cellulose greatly decreased after Al₂(SO₄)₃-assisted ball milling pretreatment. The effects of various factors, including the organic solvent, reaction temperature and time, catalyst dose, and substrate concentration, on the yield of 5-HMF from cellulose were studied. A yield of 5-HMF up to 43.5% was obtained from cellulose via the developed mechanochemical-assisted method. A 36.1% yield of 5-HMF was retained when the initial cellulose loading concentration was as high as 21.6 wt.%. The green and efficient mechanochemical-assisted method was applicable to the efficient coproduction of 5-HMF and furfural from several waste biomass feedstocks.

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Graphic abstract



Keywords Ball milling · Metal salt · Lignocellulose · 5-Hydroxymethylfurfural · Biomass

Introduction

With the gradual depletion of fossil energy resources, attention has increasingly focused on sustainable production of chemicals and fuels from renewable biomass (Saha and Abu-Omar 2014). Among the variety of biomass-derived chemicals, 5-hydrox-ymethylfurfural (5-HMF) has attracted much attention because of its importance as a platform chemical and listing as a top ten bio-based chemical by the U.S. Department of Energy (Werpy et al. 2004). For instance, 5-HMF can be converted to 2,5-furandicar-boxylic acid, 2,5-diformylfuran, ethoxymethyl furfural, furfuryl alcohol, and dimethylfuran (Kubota and Choi 2018; Li et al. 2016; Wang and Chen 2016; Zhu et al. 2018), which are substitutes for petroleum-based chemicals (Yu and Tsang 2017).

To date, considerable efforts have been devoted to the production of 5-HMF from biomass. An excellent 5-HMF yield can be obtained using fructose and glucose as the feedstock (Elsayed et al. 2018; Ma et al. 2017; Martínez et al. 2017; Qi et al. 2009, 2012b). For example, up to 88.1% yield of 5-HMF was produced from fructose with carbonaceous microspheres in our previous study (Qi et al. 2015). However, the cost is high because of the low abundances of fructose and glucose in nature (Yan et al. 2019). Moreover, the use of edible sugars creates competition with food production. Compared with glucose and fructose, cellulose is more readily available and is the most abundant and renewable biomass resource on the earth (Qiu and Hu 2013). Cellulose is a biopolymer composed of β -(1-4)-linked glucose units. Cellulose can be translated into various kinds of valuable chemicals including 5-HMF. Undoubtedly, cellulose is an ideal feedstock for sustainable production of 5-HMF. However, the high crystallinity and three-dimensional hydrogen-bonding network of cellulose make it difficult to convert (Hu et al. 2016; Huang et al. 2018). Therefore, direct production of 5-HMF from cellulose is still challenging.

Pretreatment is considered as an efficient way to gain higher product yield from cellulose by disrupting the highly crystalline structure of cellulose so that catalyst can easily access the cellulose (Parveen Kumar et al. 2009). Currently, numerous strategies, including physical, chemical, and biological methods, have been developed to pretreat cellulosic biomass (Hendriks and Zeeman 2009). Each method has its advantages but still suffers from some problems. For instance, strong acids (H₂SO₄) or bases (KOH) used for biomass pretreatment are equipment corrosion. They need to be removed from the biomass before the next step (Chimentão et al. 2014). Biological pretreatment of cellulose is efficient, but they are expensive, thermal instable and lengthy. Ionic liquids showed excellent performance for cellulose pretreatment under mild conditions (Endo et al. 2017). Unfortunately, high cost of ionic liquids hinders its industry application.

Mechanical techniques including ball milling are green, simple, and efficient methods that have been applied in many fields such as extractive metallurgy and materials engineering medicine (Howard et al. 2018; James et al. 2012; Lin et al. 2017). Mechanical ball milling also showed great potential for the pretreatment of cellulosic biomass (Jiang et al. 2019; Ling et al. 2019; Mattonai et al. 2018; Zhang et al. 2019). The crystallinity of cellulose could be reduced after ball milling treatment and thus improving the accessibility for catalysts to reach reactive sites in the cellulose (Qi et al. 2019; Qiu et al. 2018; Su et al. 2017). No chemicals or harsh conditions are required for ball milling process. More importantly, ball milling pretreated cellulose could be directly used for the subsequent reactions. However, the drawback of ball milling pretreatment is its high energy consumption, which hinders scaling of this method to industrial requirements. To solve this problem, researchers have tried to combine techniques such as acid (Boissou et al. 2015), liquid nitrogen (Shen et al. 2019), or microwave irradiation treatments with ball milling to pretreat cellulosic biomass. These methods halve the ball milling time and reduce the energy consumption. The pretreatment efficiency is also improved with coupled pretreatment strategies.

In this work, as shown in Scheme 1, a metal salt $(Al_2(SO_4)_3)$ was used to assist ball milling pretreatment of cellulose for efficient production of 5-HMF in a biphasic solvent system. Metal salts show potential for the pretreatment of cellulosic materials because they can disrupt hydrogen bonds of cellulose (Thulluri et al. 2013; Zhang et al. 2019). Compared with other chemicals, metal salts cause less equipment corrosion and are more environmentally friendly. In addition, the metal salt of $Al_2(SO_4)_3$ can be used in situ as a catalyst to convert cellulose into 5-HMF because of its Lewis and Brønsted acidity. The conversion reaction was performed in a water/ γ -valerolactone (GVL) biphasic solvent system, in which the formed 5-HMF in aqueous solution could be immediately extracted to GVL phase. Results show that high yields of 5-HMF could be obtained from high concentrations of cellulose (> 20 wt.%) and several lignocellulosic feedstocks via the developed $Al_2(SO_4)_3$ based mechanochemical method.

Experimental

Materials

Cellulose, $Al_2(SO_4)_3$, γ -valerolactone (GVL), tetrahydrofuran (THF), toluene, methyl isobutyl ketone (MIBK), *n*-butyl alcohol (BA), and *n*-hexanol (HA) were purchased from Aladdin Chemistry Co., Ltd (Shanghai, China). 5-HMF standard was obtained from ANPEL Laboratory Technologies Inc. (Shanghai, China).

Corn straw (35.1% cellulose and 20.2% hemicellulose) and rice straw (33.7% cellulose and 18.1% hemicellulose) were collected from a farm (Xiangtan, China). Cow dung (27.2% cellulose and 17.2% hemicellulose) was collected from a local cattle farm (Tianjin, China). Poplar sawdust (26.0% cellulose and 22.1% hemicellulose) was provided by a local wood factory (Tianjin, China). The contents of cellulose and hemicellulose in the biomasses were determined by the NREL standard method (NREL 2004).

Mechanochemical-assisted production of 5-HMF from biomass

The procedures for 5-HMF production from cellulose were showed in Scheme 1. Cellulose was first pretreated by $Al_2(SO_4)_3$ -assisted ball milling (BM-Al pretreatment). Typically, 972 mg cellulose and



Scheme 1 Schematic for mechanochemical-assisted production of 5-HMF from cellulose

342 mg $Al_2(SO_4)_3$ were added to a 50-mL stainless bowl and milled by a planetary ball mill (PM 100, Retsch) at 350 rpm for 4 h with a 10 min pause after every 30 min of milling. The mass (g) ratio of sample to stainless steel balls (ø 1 cm) was 1:100. The obtained mixtures were used directly for catalytic reactions. 131.4 mg of the mixture containing 97.2 mg cellulose and 34.2 mg Al₂(SO₄)₃ was added to a 50-mL sealed Teflon vessel containing 389 mg of NaCl, 2 mL of water, and 8 mL of GVL. The homogeneous mixture of water and GVL turned into biphasic solvent after the addition of NaCl. The produced 5-HMF in aqueous phase can be continuously extracted into GVL phase (Pagán-Torres et al. 2012). The reactor was charged with 1 MPa He to prevent the evaporation of water. The catalytic reaction was performed at desired temperature for a given time. At the end of reaction, the reactor was cooled immediately with cold water. The obtained mixture was filtered and the filtrate was analysed by UPLC. The sole ball milling (BM) pretreated cellulose was used as control in this work. The process was the same as that described above but without the addition $Al_2(SO_4)_3$.

Analysis of products

Products were analysed by a Waters UPLC apparatus with refractive index (RI) detector and a SHODEX SH1011 column. The eluent was 5 mM H_2SO_4 with a flowing rate of 0.5 mL min⁻¹. The yields of 5-HMF was calculated as follows:

$$5 - \text{HMF} (\text{mol}\%) = \frac{\text{mole of } 5 - \text{HMF produced}}{\text{mole of glucose unit in cellulose}} \times 100$$

Furfural (mol%) =
$$\frac{\text{mole of furfural produced}}{\text{mole of xylose unit in hemicellulose}} \times 100$$

Characterization of the cellulose

The raw cellulose (untreated), BM-pretreated cellulose, and BM-Al-pretreated cellulose were characterized by X-ray powder diffraction (XRD, Bruker D8 advance, Germany), scanning electron microscopy (SEM, Hitachi SU-8010, Japan), gel permeation chromatography (GPC), and particle size distribution analysis. XRD patterns were recorded from 5° to 60°. Before characterization, the BM-Al-pretreated cellulose was washed with 50 mL distilled water for three times to remove the $Al_2(SO_4)_3$ and then dried at 80 °C for 12 h. The crystallinity index (CrI) was calculated using the following formula (Segal et al. 1959; Azubuike et al. 2012):

$$CrI(\%) = \frac{I_{002} - I_{am}}{I_{002}} \times 100\%$$
(3)

where I_{002} is the maximum intensity of the peak (002) lattice diffraction (at 22.6° for cellulose I, and 21.6° for cellulose II), and I_{am} is the intensity of diffraction attributed to amorphous cellulose (at 16°).

Particle size distribution analysis was performed with a Mastersizer 2000 laser granulometer (Malvern Panalytical, UK). GPC was performed on chromatography system (Waters 2414) using RI detector and Agilent PLGEL 5- μ m MIXED-C column. DMF was used as mobile phase with a flowing rate of 1 mL min⁻¹. The polystyrene was used as a standard. Py-FTIR was performed on Thermo Nicolet 380 FT-IR spectrometer. The Al₂(SO₄)₃ sample was evacuated at 350 °C for 60 min. Then, the sample was exposed to pyridine vapour at room temperature for another 60 min. After that, the sample was outgassed at 150 and 350 °C. The concentrations of Lewis acid and Brønsted sites were calculated from the area of the absorption band at 1544 and 1450 cm⁻¹, respectively.

Results and discussion

(1)

(2)

Characterization of the cellulose samples

The morphologies of the cellulose samples before and after pretreatment were observed by SEM at different magnifications (Fig. 1). The untreated raw cellulose had a smooth and dense surface with an intact structure (Fig. 1a). However, the surface became rough after BM pretreatment and cracks were observed (Fig. 1c). Compared with BM pretreatment, the BM-Al pretreatment caused greater destruction of cellulose and more cracks appeared in the surface of the cellulose (Fig. 1e). At lower magnification (Fig. 1b, d, and f), it



Fig. 1 SEM images of cellulose samples pretreated by different methods: **a** and **b** no treatment, **c** and **d** BM pretreatment, and **e** and **f** BM-Al pretreatment

is obvious that the cellulose particle size greatly decreased after both BM and BM-Al pretreatments.

The particle size distributions of the three cellulose samples were further analyzed using a Mastersizer 2000 laser granulometer (Fig. 2). The untreated cellulose showed a broad peak with an average particle size of 56.4 μ m. This peak became narrower after both BM and BM-Al pretreatment, which indicated that the mechanical ball milling process made the cellulose particles more uniform. The observed remarkable decrease in the average particle size of the cellulose after pretreatment (Fig. 2) was in accordance with that observed from the SEM images (Fig. 1). The average



Fig. 2 Particle size distributions of cellulose pretreated by different methods

particle size of BM-Al-pretreated cellulose (22.4 μ m) was smaller than that of BM-pretreated cellulose (28.3 μ m). Therefore, the Al₂(SO₄)₃ enhanced the efficiency of mechanical ball milling for destroying the rigid structure of cellulose. This is useful because cellulose with a smaller particle size will have better contact with catalysts.

Crystallinity and molecular weight [MW] are considered as two important factors influencing cellulose conversion efficiency (Lee et al. 2017; Liu et al. 2018). Therefore, XRD and MW of cellulose samples were investigated in this work. The untreated cellulose showed peaks at $2\theta = 14.8^{\circ}$, 16.2° , 22.6° , and 34.9° (Fig. 3a), corresponding to the 1-10, 110, 002, and 004 planes of cellulose I (French 2014), respectively. After BM pretreatment, the sample had the same XRD pattern of cellulose I as the untreated cellulose, but the peaks showed lower intensities. Interestingly, the XRD pattern of cellulose changed after BM-Al pretreatment, and new peaks were observed at $2\theta = 20.1^{\circ}$ and 21.6° attirbuting to cellulose II (French 2014). The CrI values for the untreated cellulose, the BM treated cellulose, and the BM-Al treated cellulose were 77.1%, 48.1%, and 43.4%, respectively. Therefore, mechanical ball milling could significantly decrease the crystallinity of cellulose, especially in the presence of $Al_2(SO_4)_3$. During pretreatment of cellulose by BM-Al, the $Al_2(SO_4)_3$ entered into the



Fig. 3 XRD spectra (a) and molecular weights (b) of cellulose samples pretreated by different methods

crystalline region of the cellulose and could break the cellulose hydrogen bonds, which enhanced the destruction of the cellulose crystal structure (Sen et al. 2013).

The MW value of the untreated cellulose was measured to be 33537 by GPC (Fig. 3b), and this value greatly decreased to 26825 after BM pretreatment. The MW of BM-Al-pretreated cellulose (26578) was almost the same as that of BM-pretreated cellulose. Therefore, the presence of $Al_2(SO_4)_3$ during the BM process did not facilitate the decrease in the molecular weight of cellulose, but promoted the reduction of particle size and crystallinity of cellulose.

Mechanochemical-assisted production of 5-HMF from cellulose

After pretreatment of cellulose with BM-Al, the samples containing cellulose and $Al_2(SO_4)_3$ was directly hydrolyzed by $Al_2(SO_4)_3$ in situ without a washing process. As a control, untreated cellulose and BM-treated cellulose were also used to produce 5-HMF in the same way, except that $Al_2(SO_4)_3$ was added afterwards. The yields of 5-HMF from cellulose were determined for the different pretreatment methods (Fig. 4). It was obvious that both BM and BM-Al pretreatment increased the yield of 5-HMF. For the untreated cellulose, the yield of 5-HMF was very low when the reaction time was below 40 min. The maximum yield of 5-HMF (33.4%) was obtained at 70 min. After sole BM pretreatment, the maximum yield of 5-HMF increased to 39.8% within 70 min. The maximum 5-HMF yield further increased to 44.6% at 50 min after BM-Al pretreatment. Therefore,



Fig. 4 Yields of 5-HMF from cellulose after different pretreatment methods. Conditions: cellulose, 97.2 mg; $Al_2(SO_4)_3$, 34.2 mg; NaCl, 389.6 mg; water, 2 mL; GVL, 8 mL; and temperature, 165 °C

BM-Al-pretreated cellulose was more readily converted into 5-HMF than sole BM-pretreated cellulose. This can be explained by the changes in the cellulose structure after the different pretreatment methods. As discussed above, mechanical milling greatly decreased the particle size and CrI of cellulose. Compared with BM treatment, BM-Al pretreatment could more effectively destroy the rigid structure of cellulose, thus leading to high yield of 5-HMF.

Optimization of reaction conditions

Solvent plays an important role in the catalytic production of 5-HMF from lignocellulosic biomass (Saha and Abu-Omar 2014). Generally, 5-HMF was unstable in aqueous solution. Nowadays, 5-HMF is usually produced in biphasic reaction systems

containing both aqueous solution and organic solvent. Water is used as reaction phase for catalytic conversion of biomass to 5-HMF. Organic solvent is used as an extracting phase for continuous extraction of 5-HMF from water to the organic phase, thus reducing the decomposition of 5-HMF in aqueous solution. NaCl is normally added into the aqueous solution to promote the in situ extraction of 5-HMF from aqueous to organic phase by salting-out effect (Chen et al. 2016). Another advantage of biphasic system is easy recycling of aqueous phase containing catalysts. In this work, extraction efficiency of different organic solvents (i.e., GVL, THF, n-butyl alcohol (BA), toluene, *n*-hexanol (HA), and methyl isobutyl ketone (MIBK)) for 5-HMF from aqueous solution was studied. A 10 mg sample of 5-HMF was dissolved in 1 mL of water containing 200 mg of NaCl. Then, 4 mL of one of the above organic solvents was added. After stirring vigorously for 1 h, the concentrations of 5-HMF in both the aqueous and organic layers were measured. As shown in Fig. 5a, among these solvents, GVL gave the highest extraction efficiency, and 96.6% of the 5-HMF was extracted from the water. Although THF also had a high extraction efficiency for 5-HMF (95.3%), it is poisonous and harmful. By comparison, GVL is a green solvent that has low toxicity, is readily available, and is produced from biomass (Molleti et al. 2017). Thus, a mixture of GVL and water was selected as a green biphasic solvent system to produce 5-HMF from cellulose.

Next, the effect of GVL/H_2O ratio on the yield of 5-HMF was investigated. In sole water solution, the

5-HMF yield was only 13.2% (Fig. 5b). It was because 5-HMF is unstable in water and easily decomposes to form by-products such as levulinic acid (Xu et al. 2018). Herein, 12.1% yield of levulinic acid was detected in pure water system. When GVL was added to the aqueous phase and its content gradually increased, the total yield of 5-HMF increased accordingly. A biphasic solvent formed after introduction of GVL, and the 5-HMF in the aqueous phase could be immediately in situ extracted into the GVL. Because 5-HMF is stable in GVL, its decomposition was suppressed. Continuous extraction of 5-HMF to GVL shifts the equilibrium to the product side thus improving the conversion efficiency. Maximum yield of 5-HMF (44.9%) was obtained when ratio of GVL/ H₂O was 8:2 (Fig. 5b). In pure GVL phase, the 5-HMF yield was only 5.8%. In this case, the limited solubility of $Al_2(SO_4)_3$ in GVL may prevent it from well contacting with the solid cellulose. GVL/H_2O (8:2) was used as reaction solvent in the following experiments and the yield of 5-HMF was calculated from the GVL phase.

The effect of the reaction temperature and catalyst dose on the yield of 5-HMF from BM-Al pretreated cellulose were also investigated (Fig. 6). The yield of 5-HMF increased gradually when the temperature was increased from 145 °C to 165 °C (Fig. 6a). The maximum yield of 5-HMF (44.1%) was obtained at 165 °C. However, when the reaction temperature was increased further to 175 °C, the yield of 5-HMF decreased to 38.1%. The drop in the yield can be attributed to the occurrence of undesired side reactions



Fig. 5 a Influence of the organic solvent on the extraction of 5-HMF from water. Conditions: 5-HMF standard, 10 mg; NaCl, 200 mg; water, 1 mL; organic solvent, 4 mL. **b** Effect of the



GVL/H₂O ratio on the yield of 5-HMF from BM-Al treated cellulose. Conditions: cellulose, 97.2 mg; $Al_2(SO_4)_3$, 34.2 mg; NaCl, 389.6 mg; temperature, 165 °C; and reaction time, 50 min



Fig. 6 a Effect of the reaction temperature on the yield of 5-HMF. Conditions: cellulose, 97.2 mg; $Al_2(SO_4)_3$, 34.2 mg; NaCl, 389.6 mg; water, 2 mL; GVL, 8 mL; and time, 50 min.

such as polymerization of 5-HMF with glucose or fructose to form humins (Chen et al. 2016), which can be confirmed by the deep black color observed after reaction at higher temperature (inset in Fig. 6a).

Influence of the catalyst dosage on the yield of 5-HMF was evaluated. The initial amount of cellulose was fixed at 97.2 mg. It can be seen from Fig. 6b that 5-HMF was not detected in the absence of $Al_2(SO_4)_3$. With the addition of $Al_2(SO_4)_3$, the yield of 5-HMF increased remarkably, demonstrating good catalytic activity of $Al_2(SO_4)_3$. Previous studies showed that after dissolution in aqueous solution, the metal salt undergoes hydrolysis to provide H⁺ as Brønsted acidic sites (Choudhary et al. 2013; Wrigstedt et al. 2015). The complex of $[Al(OH)_2(aq)]^+$ serving as Lewis acid promoted the isomerization of glucose to fructose (Tang et al. 2016). The amounts of Brønsted acid sites and Lewis acid sites of Al₂(SO₄)₃ calculated from Py-FTIR measurement at 150 °C were 94.5 µmol/g and 44.4 µmol/g, respectively. It is known that catalysts containing both Brønsted acid and Lewis acid sites facilitate production of 5-HMF from cellulose, where glucose isomerization to fructose was catalysed by Lewis acid and cellulose hydrolysis to glucose and fructose dehydration to 5-HMF were favorable by Brønsted acid. Therefore, the high catalytic efficiency of $Al_2(SO_4)_3$ could be attributed to its Brønsted acidic and Lewis acidic sites.

A maximum yield of 5-HMF (42.7%) was obtained when the catalyst/cellulose ratio was 8:24. When the catalyst/cellulose ratio was increased to 16:24, the yield of 5-HMF decreased. The reason for the yield decrease caused by more catalyst addition can be



(**b**) 50

b Effect of the catalyst dose on the yield of 5-HMF. Conditions: cellulose, 97.2 mg; NaCl, 389.6 mg; water, 2 mL; GVL, 8 mL; temperature, 165 °C; and time, 50 min

attributed to excess active sites provided by $Al_2(SO_4)_3$ in the system, which would also accelerate side reactions (Elsayed et al. 2018).

It is necessary to evaluate the tolerance of a catalytic system to high feedstock concentrations since it is important for its practical applications. Generally, the product yield greatly decreases with increases in the cellulose concentration because higher feedstock concentration may not only result in the insufficient of the catalytic sites, but also promote the occurrence of undesired side reactions, especially the formation of humins by polymerization (Qi et al. 2012a; Xu et al. 2018). In this work, the effect of the cellulose concentration on mechanochemical-assisted production of 5-HMF was investigated. A high yield of 5-HMF (43.5%) was obtained when the initial concentration of cellulose was 4.9 wt.% (Table 1). With increases in the cellulose concentration, the maximum yield of 5-HMF decreased slightly. However, a 36.1% yield of 5-HMF could still be obtained when the initial cellulose concentration was up to 21.6 wt.%. Mechanical milling could effectively decrease the particle size and CrI of cellulose. Besides, with the assistance of ball milling, the catalyst has better contact with cellulose ensuring high efficiency of the catalyst even with high loading of substrate. This result is outstanding, especially considering the insolubility of cellulose in water.

Table 1 Effect of the cellulose concentration on the yield of 5-HMF	Cellulose concentration (wt.%)	Reaction time (min)	5-HMF yield (%)
	4.9	30	33.4
		40	40.0
		50	43.5
		60	42.1
		70	38.6
	10.8	20	14.7
		40	31.1
		60	38.8
		80	28.9
	21.6	20	15.7
		40	36.1
		60	30.7
	32.4	40	21.3
Condition: Al ₂ (SO ₄) ₃ , 34.2 mg; NaCl, 389.6 mg; water, 2 mL GVL, 8 mL; and temperature, 165 °C. Cellulose concentrations were calculated based on the mass of water		60	22.2
		80	21.3
	43.2	40	17.9
		60	18.6
		80	19.6
		100	18.9

Application for 5-HMF production from real waste biomass

The move from cellulose to real waste biomass is considered as a promising trend for the application of a catalytic systems (Yang et al. 2017). In this work, the developed method was applied to the production of 5-HMF and furfural from several lignocellulosic biomasses such as corn straw, rice straw, poplar sawdust, and cow dung. High furfural yields (> 50%) were produced from all four kinds of biomasses (Fig. 7). Furfural is an important platform chemical that is produced by the hydrolysis and dehydration of the hemicellulose fraction in lignocellulosic biomass. In addition to furfural, 5-HMF was also obtained from the corn straw, rice straw, poplar powder, and cow dung biomasses with yields of 29.8, 34.7, 65.7, and 35.3%, respectively. From the above results, it can be concluded that the developed green BM-Al pretreatment method was applicable to the efficient coproduction of 5-HMF and furfural from biomass feedstocks.



Fig. 7 Yields of 5-HMF and furfural from different waste biomasses in the developed catalytic system. Condition: biomass substrate, 97.2 mg; $Al_2(SO_4)_3$, 34.2 mg (0.1 mmol); NaCl, 389.6 mg; water, 2 mL; GVL, 8 mL; temperature, 165 °C; and time, 50 min

Conclusions

High value-added chemical 5-HMF was produced directly from cellulose and agricultural wastes in a high yield via a mechanochemical-assisted process in the presence of $Al_2(SO_4)_3$. The $Al_2(SO_4)_3$ not only acted as a catalyst for degradation of cellulose but also assisted disruption of the hydrogen bonds in cellulose during BM pretreatment. A 36.1% yield of 5-HMF was obtained when the initial cellulose loading concentration was as high as 21.6%. The particle size

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