

Transesterification of Methyl Acetate with *n*-Butanol Catalyzed by Single and Mixed Ionic Liquids

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Abstract Several acidic ionic liquids (ILs) with different cations and anions were used as catalysts in the transesterification of methyl acetate with *n*-butanol. The IL [omim][PF₆] can enhance the catalytic activity of the partially soluble IL catalyst. The kinetics for the transesterification using the catalysts [HSO₃bmim][p-TS] and [HSO₃bmim][OTF] were measured. The ideal homogeneous model and the nonideal homogeneous (NIH) model were used to correlate the kinetic data. The NIH model was more reliable to describe the reaction rate. *Graphical Abstract*



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Abbreviations

IL	Ionic liquid
MRD	Mean relative deviation
BuOH	<i>n</i> -Butanol
MeOAc	Methyl acetate
[HSO ₃ bmim][Cl]	1-Sulfobutyl-3-methylimidazolium chloride
[HSO ₃ bmim][OTF]	1-Sulfobutyl-3-methylimidazolium trifluoromethanesulfonate
[HSO ₃ bmim][p-TS]	1-Sulfobutyl -3-methylimidazolium tosylate
[HSO3bpy][OTF]	N-sulfobutylpyridinium
	trifluoromethanesulfonate
[HSO3bHim][HSO4]	1-Sulfobutylimidazolium
	hydrogensulfate
[omim][PF ₆]	1-Octyl-3-methylimidazolium
	hexafluorophosphate

Variables

- r^0 Initial reaction rate (mol/(L min))
- *r* Reaction rate (mol/(L min))
- *c* Mole concentration (mol/L)
- *E* Constant defined in Eq 2
- *c_{cat}* Mole concentration of ionic liquid catalysts (mol/L)
- k_+ Forward reaction rate constant (L²/(min mol²))
- k_{-} Backward reaction rate constant (L²/(min mol²))
- k^0_{\perp} Arrhenius pre-exponential factors (L²/(min mol²))
- k^0 Arrhenius pre-exponential factors (L²/(min mol²))
- E_{A+} Activation energy of forward reaction (kJ/mol)
- E_{A-} Activation energy of backward reaction (kJ/mol)
- *V* Volume of the reaction mixture (L)

- *R* General gas constant, 8.314 kJ/(mol K)
- *N* Total number of experimental data
- *v* Stoichiometric coefficient
- x Mole fraction
- ρ Molar density of reaction mixture (mol/L)
- t Time (min)

Greek Letters

- α Activity
- γ Activity coefficient

Superscripts and Subscripts

- 0 Standard state/conditions
- + Forward reaction
- Backward reaction
- cal Catalyst
- calc Calculated value
- exp Experimental value

1 Introduction

Transesterification, as a method to produce useful esters via the catalytic reaction of aliphatic esters and alcohols, has been widely used in chemical industry [1-3]. An important application of transesterification is to transform methyl acetate with *n*-butanol to *n*-butyl acetate and methanol [4, 5]. Methyl acetate is a by-product in poly(vinyl alcohol) (PVA) process and its application in chemical industry is limited, but butyl acetate is a widely used chemical for manufacturing paint, varnish and coating materials [6], and methanol is a feed stock for PVA, so the transesterification process is a good choice to deal with methyl acetate. Transesterification is a catalytic reaction, and the commonly used catalysts are solid heterogeneous catalysts such as acidic ion-exchange resins [7, 8], heteropolyacids [9] and molecular sieves [10]. Nevertheless, these catalysts have some drawbacks, such as easy deactivation, high mass transfer resistance and especially difficult installation in a reactive distillation column, which restrain their practical applications [11].

To overcome the above problems, many researchers began to use ionic liquids (ILs) as catalysts because of their advantages over the traditional catalysts, such as negligible vapor pressure, wide liquid range, high catalytic activity and thermal stability [12, 13]. For example, comparing with acidic ion-exchange resin, the IL possesses high thermal stability and catalytic activity. Moreover, the IL is also easy to be used and has no mass transfer problems. So far, ILs have been successfully utilized in laboratory for some transesterification reactions [14–16]. For example, Qureshi et al. have used a halogen free Bronsted acidic IL N-methyl-2-pyrrolidone hydrogen sulfate as catalyst for the transesterification of β -ketoesters with alcohols and found the IL shows high catalytic activity and reusability with high yields of the desired products [17]. Kuschnerow et al. have carried out a continuous IL-catalyzed transesterification of butanol with ethyl acetate to produce ethanol and butyl acetate and they found the ILs did not show a relevant loss of activity after 1000 h of reaction [18]. Peng et al. have catalyzed the transesterification of methyl acetate and ethanol by 4-(3-methyl-1-imidazolio)-1-butanesulfonic acid triflate and 4-(3-methyl-1-imidazolio)-1-butanesulfonic acid hydrogen sulfate respectively and measured the reaction kinetics [19, 20]. Wang et al. have synthesized five acidic imidazolium ILs as catalysts for the preparation of sec-butanol via the transesterification of sec-butyl acetate (SBAC) with methanol and a high conversion of the SBAC of 97.72 % was obtained by the reactive distillation in the presence of 1-(3-sulfopropyl)-3-methylimidazolium hydrogen sulfate [21]. However, published information about the effects of cations or anions on the transesterification is still limited and to the best of our knowledge, there is no research work on transesterification catalyzed by mixed ILs.

To describe the reaction rate of the transesterification of methyl acetate and *n*-butanol, different kinetic models were applied by researchers. Bozek-Winkler et al. have used two kinetic models, namely, the pseudohomogeneous and the Langmuir-Hinshelwood model to describe the kinetic for the transesterification of methyl acetate and n-butanol catalyzed by ion-exchange resin Amberlyst 15 [22]. Jimenez et al. have also applied pseudohomogeneous model to describe the kinetic of the transesterification of methyl acetate and n-butanol using acid ion-exchange resin as catalyst [23]. But the transesterification catalyzed by ILs is different from that catalyzed by acidic ion-exchange resin, because the former is homogenous and the latter is heterogeneous. Cui et al. have proposed two kinetic models, the ideal homogeneous (IH) model and the nonideal homogeneous (NIH) model, for the transesterification of methyl acetate and *n*-butanol catalyzed by an acidic IL [24].

In this paper, the effects of cations ($[HSO_3bmim]^+$, $[HSO_3bpy]^+$) and anions (Cl⁻, $[p-TS]^-$ and $[OTF]^-$) on the catalytic performance of ILs in the transesterification of methyl acetate with *n*-butanol were investigated. The effects of mixed IL catalysts on the transesterification reaction were also studied. Furthermore, the kinetics of the transesterification catalyzed by $[HSO_3bmim][p-TS]$ and $[HSO_3bmim][OTF]$ were measured and correlated by IH model and NIH model, respectively.

2 Experimental Section

2.1 Materials

2.1.1 Chemicals

n-Butanol and methanol was purchased by Kewei Chemical Reagents Co., Tianjin, China. Methyl acetate and *n*butyl acetate was obtained from Guangfu Chemical Reagents Co., Tianjin, China. The purities of these chemicals were greater than 0.997 (mass fraction) as confirmed by gas chromatography and used without additional purification.

2.1.2 Catalyst

All the ILs used in the experiments including 1-sulfobutyl-3-methylimidazolium trifluoromethanesulfonate [HSO₃ bmim][OTF], 1-sulfobutyl-3-methylimidazolium chloride [HSO₃bmim][Cl], 1-sulfobutyl-3-methylimidazolium tosylate [HSO₃bmim][p-TS], N-sulfobutylpyridinium trifluoromethanesulfonate [HSO₃bpy][OTF] and 1-octyl-3methylimidazolium hexafluorophosphate [omim][PF₆] were supplied by Chengjie Chemical Reagents Co., Shanghai, China, with a minimum mass fraction of 0.99 (confirmed by liquid chromatography) and the mass fraction of water in ILs was less than 0.0001 (confirmed by Karl Fischer titration). Therefore, the ILs were used without further purification.

2.2 Apparatus and Procedure

All experiments were carried out in a 100 mL round-bottom flask equipped with a reflux condenser which was utilized to avoid any loss of volatile compounds. A mechanical agitator was used to mix the solution in the flask. The flask was put in a thermostatic water bath. All the temperatures were measured by a calibrated thermometer to an accuracy of ± 0.01 K.

Catalyst and *n*-butanol were added in the flask and heated by thermostatic water bath, while methyl acetate was preheated in a separate vessel in the same water bath. When the temperatures of methyl acetate and solution in the flask reached the desired value, methyl acetate was added to the flask, and the reaction started. Liquid samples of 1 μ L were taken with a syringe at regular intervals and analyzed by gas chromatograph (GC).

For convenience in description, we set the basic reaction conditions as a catalyst concentration of 0.183 mol/L, reaction temperature 315 K, agitation speed 250 rpm and an initial molar ratio of *n*-butanol to methyl acetate 1:1.

2.3 Sample Analysis

All the samples were analyzed by a gas chromatograph equipped with a FID detector and a capillary column SE-30 (50 m \times 0.32 mm \times 0.25 µm). The temperatures of injector, detector and column were set 473.15, 493.15, 343.15 K, respectively. The flow rates of nitrogen, hydrogen and air are 30, 30, 300 mL/min, respectively. To prevent ILs from passing into the GC column, a porous ceramics trap was located in the middle section of the glass tube in injector.

2.4 UV–Vis Determination of Acidity of Ionic Liquid Catalysts

A series of ethanol solutions of 4-Nitroaniline (used as indicator) of different concentrations ranging from 0.01885 to 0.05792 mM were prepared. The absorbance of these solutions was measured by Shimadzu UV-1800 spectroscopy at 300–500 nm. Several ethanol solutions containing ILs (75 mM) and 4-Nitroaniline (0.05792 mM) were also prepared to measure the absorbance, then a Hammett function was used to calculate the acidity of these acidic ILs [25–27].

3 Results and Discussion

As all chemicals were water free, the by-products caused by side reaction hydrolysis are less than 0.01 wt % which is confirmed by gas chromatography, so the side reaction caused by hydrolysis can be neglected. Similar results were also reported in the literature [23]. Therefore, the selectivity of the products for the transesterification of methyl acetate and *n*-butanol is close to 1.

3.1 Acidity of ILs

Peng et al. have studied the mechanism of the transesterification of methyl acetate and ethanol catalyzed by [HSO₃bmim][OTF] [19]. Cui et al. have studied the kinetics of the transesterification of methyl acetate and *n*butanol with [HSO₃bHim][HSO₄] [24]. Rodriguez et al. have catalyzed the transesterification of methyl acetate and isobutanol using NaHSO₄ [28]. Based on their work, the reaction mechanism of methyl acetate and *n*-butanol catalyzed by IL can be described in Fig. 1, taking IL catalyst [HSO₃bmim][OTF] as example.

As shown in Fig. 1, the transesterification was catalyzed by proton produced by IL catalyst. Therefore, the ability to provide protons (acidity) is an essential property of acidic IL catalyst.



Fig. 1 Reaction mechanism for the transesterification of methyl acetate and n-butanol

The acidity of an IL can be calculated by the Hammett function (H_0) :

$$H_0 = pK(I)_{aq} + \left(\log\frac{[I]_S}{[IH]_S^+}\right)$$
(1)

where $pK(I)_{aq}$ is the pK_a value of the indicator referred to an aqueous solution (0.99 for 4-Nitroaniline); $[IH]_S^+$ and $[I]_s$ are the molar concentrations of the protonated and unprotonated forms of the indicator in the acidic ILs.

There is a good linear relationship between the concentration of 4-Nitroaniline and absorbance (see Fig. 2), which indicates the concentration of indicator between 0.01885 and 0.05792 mM follows Beer–Lambert Law. The maximal absorbance of the unprotonated form of



Fig. 2 The relationship of absorbance of 4-nitroaniline and its concentration

4-Nitroaniline is observed at 375 nm and the results of Hammett acidity of acidic ILs were listed in Table 1. The acidity order is as follows: $[HSO_3bHim][HSO_4] > [HSO_3$ bmim][p-TS] > $[HSO_3bmim][OTF] > [HSO_3bpy][OTF] >$ $[HSO_3bmim][C1]$. It is obvious that the cations and anions of ILs have significant influences on their acidity which is an important factor of catalytic performance on the transesterification reaction.

3.2 Effects of Single Ionic Liquid Catalyst Structure on Transesterification

The transesterification of *n*-butanol and methyl acetate with several IL catalysts were conducted to investigate the effects of IL catalyst structure. The catalysts we used are all well dissolved in the reaction mixture at basic reaction conditions except [HSO₃bmim][Cl]. The results are illustrated in Fig. 3. Cui et al. has used [HSO₃bHim][HSO₄] to catalyze the transesterification [24] and the results are also shown in Fig. 3 for comparison. It is obvious that the reaction rates are in an increasing order of [HSO₃bHim] [HSO₄] > [HSO₃bmim][p-TS] > [HSO₃bmim][OTF] \approx

Table 1 Hammett acidity function (H_0) values of different ILs

Entry	IL	A _{max}	[I] _s (%)	$[\mathrm{IH}^+]_{\mathrm{s}}(\%)$	H_0
1	-	0.945	100	0	-
2	[HSO3bHim][HSO4]	0.524	55.218	44.782	1.080
3	[HSO3bmim][p-TS]	0.581	61.276	38.724	1.189
4	[HSO3bmim][OTF]	0.619	65.315	34.685	1.265
5	[HSO3bpy][OTF]	0.666	70.311	29.689	1.364
6	[HSO3bmim[Cl]	0.702	74.138	25.863	1.447



Fig. 3 Effects of anions in ionic liquid catalysts on the transesterification of n-butanol and methyl acetate at basic reaction conditions

 $[HSO_3bpy][OTF] > [HSO_3bmim][Cl], which is generally in$ line with the acidity order described above. The catalyst activity of [HSO₃bmim][Cl] is the smallest, because its acidity is the lowest and it is partially dissolved in the reaction mixture. The ILs [HSO₃bmim][p-TS], [HSO₃ bmim][OTF] and [HSO₃bmim][Cl] have the same cation but different anions, and their acidity and catalyst activity are in the same order, so in such a case the acidity of acidic IL is affected by different anions, which results in different catalytic activities. However, when we compare the imidazolium ring-based IL [HSO3bmim][OTF] and pyridinium ringbased IL [HSO₃bpy][OTF], their catalytic activity are nearly the same though the acidity of [HSO3bmim][OTF] is stronger than that of [HSO₃bpy][OTF]. In such a case, the acidity is influenced by different heterocyclic rings in cations, but the catalyst activity is not affected by them. Therefore, the acidity characterized by Hammett function (H_0) is a rough indicator for catalytic activity of the IL catalyst.

3.3 Transesterification Catalyzed by Mixed Ionic Liquids

As mentioned above, The IL [HSO₃bmim][Cl] cannot be well dissolved in the reaction mixture at basic reaction conditions, so we use a hydrophobic IL [omim][PF₆] to enhance its solubility in the reaction mixture. The IL [omim][PF₆] has no catalytic activity, because it cannot provide protons to catalyze the transesterification (as shown in Fig. 1). This is also confirmed by reaction tests. The IL [omim][PF₆] can be well dissolved in both esters and [HSO₃bmim][Cl], so it was mixed with [HSO₃bmim][Cl] and added to the reaction system to enhance the solubility of [HSO₃bmim][Cl]. To investigate the behavior of mixed IL catalysts, experiments were also carried out using the mixed ILs of [HSO₃bmim][p-TS] + [omim][PF₆] at basic reaction conditions. The molar ratios of $[omim][PF_6]$ to IL catalysts are varied from 1:1 to 3:1 and the experimental results are shown in Figs. 4 and 5. Figure 4 indicates that the reaction rate with a molar ratio of [omim][PF₆] to [HSO₃bmim][Cl] 1:1 is almost the same as that of without $[omim][PF_6]$. However, the reaction rate increases obviously with the molar ratio of [omim][PF₆] to [HSO₃bmim][Cl] 3:1. The IL $[omim][PF_6]$ has two opposite effects: it can enhance the solubility of IL catalyst in reaction system and it can also dilute the IL catalyst. When a small amount of $[omim][PF_6]$ (molar ratio of [omim][PF₆] to [HSO₃bmim][Cl] 1:1) is added, only a small amount of extra catalyst [HSO3 bmim][Cl] dissolves further in the reaction mixture and it is also diluted by [omim][PF₆] meanwhile. The two effects are both not obvious, so the reaction rate is nearly unchanged. When a large amount of $[omim][PF_6]$ is added (molar ratio of [omim][PF₆] to [HSO₃bmim][Cl] 3:1), all of the catalyst [HSO₃bmim][Cl] dissolves in the reaction mixture, and the extra dissolved catalyst plays the main role even though it is diluted by [omim][PF₆], so the reaction rate increases. Therefore, the solubility of IL catalyst in the reaction mixture is another important factor that determines the catalytic activity except acidity for the partial dissolved catalyst. However, when we carried out the transesterification with $[HSO_3bmim][p-TS] + [omim][PF_6]$ as catalyst, the reaction rate decreases with the addition of $[omim][PF_6]$ (see Fig. 5). Since catalyst [HSO₃bmim][p-TS] is totally dissolved in the reaction system, when [omim][PF₆] is added, the catalyst is diluted by [omim][PF₆], and the reaction rate slows down.

Therefore, if a Bronsted acidic IL catalyst such as $[HSO_3bmim][CL]$ is partially dissolved in the transesterification reaction system, its solubility can be enhanced by another IL such as $[omim][PF_6]$, and the reaction rate



Fig. 4 Effects of the molar ratios of $[\text{omim}][\text{PF}_6]$ to $[\text{HSO}_3 \text{ bmim}][\text{Cl}]$ on the transesterification of *n*-butanol and methyl acetate at basic reaction conditions



Fig. 5 Effects of the molar ratios of $[\text{omim}][\text{PF}_6]$ to $[\text{HSO}_3\text{bmim}][\text{p-TS}]$ on the transesterification of *n*-butanol and methyl acetate at basic reaction conditions

can be improved. However, for a totally dissolved Bronsted acidic IL catalyst ([HSO₃bmim][p-TS]), the reaction rate cannot be enhanced by the mixed catalyst ([HSO₃bmim][p-TS] + [omim][PF₆]).

In summary, among all the catalysts discussed above, the strong acidic IL [HSO₃bHim][HSO₄] has the best performance for the transesterification reaction, but the study of IL mixture provides a method of improving the performance of those catalysts such as [HSO₃bmim][Cl] that cannot be well dissolved in reaction mixture.

3.4 Reaction Kinetics

In this section, the reaction temperatures were in a range of 310.15-325.15 K, the initial molar ratios of *n*-butanol to methyl acetate were 0.5–2 and the catalyst concentrations were 0.122 mol/L to 0.305 mol/L. Since the catalyst [HSO₃bmim][Cl] cannot be well dissolved in the reaction mixture, it is not utilized in this section, and the catalysts used are [HSO₃bmim][OTF] and [HSO₃bmim][p-TS]. When we studied the effects of the operational parameters, only one parameter was varied and the other reaction conditions were the same as those of basic reaction conditions.

3.4.1 Effects of the Initial Reactant Molar Ratio

For convenience to investigate the effects of initial molar ratio of *n*-butanol to methyl acetate $(R^0_{B/M})$, we set the methanol concentration as the objective function. Because the transesterification is a chemical equilibrium reaction, it is obvious that the conversion of methyl acetate increases with $R^0_{B/M}$, but the concentration of product such as methanol in the reaction mixture varies differently. As shown in Fig. 6a, the biggest methanol concentration is obtained at $R_{B/M}^0 = 1$ for both of the catalysts, because $R_{B/M}^0$ in such cases is equal to the ratio of stoichiometric coefficients of corresponding reactants. When the initial reactant molar ratio $R_{B/M}^0$ is 0.5 and 2, the mole fractions of methanol in the reaction mixture are equal, but the mole density of the reaction mixture of $R_{B/M}^0 = 2$ is less than that of $R_{B/M}^0 = 0.5$, because the density of *n*-butanol is less than methyl acetate. Therefore, methanol concentration of $R_{B/M}^0 = 2$ is less than that of $R_{B/M}^0 = 0.5$.

3.4.2 Effects of Reaction Temperature

Experiments using $[HSO_3bmim][OTF]$ and $[HSO_3bmim][p-TS]$ as catalysts were carried out to investigate the effects of reaction temperature. Figure 6b shows obviously that for both of the two catalysts, reaction rates increase rapidly with reaction temperature. However, the equilibrium conversions of methyl acetate only change a little in the investigated temperature range. Similar results have been reported in the literature [29, 30]. The reason is that the heat of reaction for this transesterification reaction is small, the equilibrium constant depends only slightly on temperature.

3.4.3 Effects of Catalyst Concentration

Catalyst concentration is an important factor that affects the reaction rate. Figure 6c illustrates that the transesterification reaction rate increases with the catalyst concentration for both of the catalysts, but for the chemical equilibrium constant, the same value was obtained. In addition, the initial reaction rates in the presence of [HSO₃ bmim][OTF] and [HSO₃bmim][p-TS] were calculated at the starting point of the reaction and proposed to be a linear function of the catalyst loading (see Fig. 7). It can be expressed as:

$$r^{0} = \frac{1}{v_{i}} \left(\frac{dc_{i}}{dt}\right)_{t=0} = Ec_{cat}$$
⁽²⁾

where r^0 is the initial rate of transesterification reaction, mol/(L min); v_i is the stoichiometric coefficient of component *i*; c_i is the mole concentration of component *i*, mol/ L; c_{cat} is the mole concentration of catalyst, mol/L; *E* is constant.

The constant *E* is obtained from the slope of the best fitted line in Fig. 7, and the values are 0.165 min⁻¹ for [HSO₃bmim][OTF] and 0.185 min⁻¹ for [HSO₃bmim][p-TS], respectively.



Fig. 6 Influence of the initial reactant molar ratio (**a**), reaction temperature (**b**), and the catalyst concentration (**c**) on the conversion of MeOAc at basic reaction conditions. Solid symbol, experimental data for [HSO₃bmim][OTF]; Open symbol, experimental data for [HSO₃bmim][p-TS]



Fig. 7 Initial reaction rate versus catalyst concentration at 315.15 K

3.4.4 Kinetic Model

Peng et al. has studied the kinetics of the transesterification of methyl acetate and ethanol catalyzed by $[HSO_3 bmim][OTF]$ and used the IH model and NIH model to describe the reaction rate [19]. The mechanisms of the two transesterification reactions are similar. Therefore, the expressions for IH model and NIH model are also used in this work:

IH

$$r = \frac{1}{V} \frac{1}{v_i} \frac{dn_i}{dt} = \rho^2 c_{cat} (k_+ x_{BuOH} x_{MeOAc} - k_- x_{MeOH} x_{BuOAc})$$
(3)

NIH

$$r = \frac{1}{V} \frac{1}{v_i} \frac{dn_i}{dt} = \rho^2 c_{cat} (k_+ a_{BuOH} a_{MeOAc} - k_- a_{MeOH} a_{BuOAc})$$
(4)

where *V* is volume of the reaction mixture, L; n_i is moles of component *i*, mol; ρ is the molar density which can be considered as constant during the reaction process, mol/L; $\alpha_i (= \gamma_i x_i)$ is the activity of component *i*, while γ_i and x_i are the activity coefficient and molar fractions respectively. The activity coefficient γ_i is calculated by the UNIQUAC model and the parameters needed are obtained from the literature reported [22, 24]. k_+ and k_- are forward and backward reaction rate constants respectively, which can be calculated by Arrhenius equations:

$$k_{+} = k_{+}^{0} \exp(\frac{-E_{A+}}{RT})$$
(5)

$$k_{-} = k_{-}^{0} \exp(\frac{-E_{A-}}{RT})$$
(6)

where k_{+}^{0} and k_{-}^{0} are pre-exponential factors and E_{A+} and E_{A-} are activation energies.

The kinetic parameters were estimated by minimizing the objective function of mean relative deviation (MRD) between the calculated and experimental mole fractions of methyl acetate, using all of the experimental data in the above sections.

$$MRD = \frac{1}{N} \left(\sum_{i=1}^{N} \left| \frac{x_{MeOAC,cal,i} - x_{MeOAC,exp,i}}{x_{MeOAC,exp,i}} \right| \right)$$
(7)

where N is the total number of data points.

The correlated results were summarized in Table 2. It is clear that the mean relative deviations of the IH model are larger than those of the NIH model, which indicates NIH model is more accurately than IH model. Bozek-Winkler et al. [22] have used pseudohomogeneous model to describe the reaction kinetics for the transesterification of methyl acetate and *n*-butanol catalyzed by ion-exchange resin and the active energies E_{A+} , E_{A-} are 40.89 and 40.85 kJ/mol. Cui et al. [24] have applied a NIH model to describe the same reaction catalyzed by an acidic IL and the active energies E_{A+} , E_{A-} are 36.26 and 36.02 kJ/mol. The active energies we correlated in Table 2 are very similar, which indicates that the transesterification is catalyzed by H⁺ whether the catalyst is acidic ion-exchange resin or acidic IL. Therefore, the catalytic activities are mainly indicated by the pre-exponential factors of forward and backward reactions when the active energies are quite similar. So the relationship between the measured acidity and pre-exponential factors of forward and backward reactions can be applied to predict the reaction kinetics if the acidity of the catalyst is determined. As shown in Fig. 8a, b, the relationship can be fitted by quadratic functions, and the correlated equations are, re $k_{+}^{0} = -428,338H_{0}^{2} + 1042,130H_{0} - 620,157$ spectively, and $k_{-}^{0} = -757,336H_{0}^{2} + 1815,940H_{0} - 1072,650.$

Substitution of the values of kinetic parameters shown in Table 2 into NIH model gives the reaction rate equation: For catalyst [HSO₃bmim][OTF]:

 Table 2 Kinetic parameters for the reaction rate equation



Fig. 8 The relationship between the acidity and pre-exponential factors of forward and backward reactions: **a** forward reaction, **b** backward reaction

$$r_{MeOAc} = -\frac{1}{V} \frac{dn_{MeOAc}}{dt} = \rho^2 c_{cat}$$

$$\times \left(12,698 \exp\left(\frac{-4618.2}{T}\right) a_{MeOAc} a_{BuOH} \right)$$

$$-12,603 \exp\left(\frac{-4649.4}{T}\right) a_{BuOAc} a_{MeOH} \right)$$
(8)

Face 2 Knette parameters for the reaction rate equation									
Catalyst	Kinetic model	Forward reaction		Backward reaction		MRD			
		k_{+}^{0} (L ² /(min mol ²))	E_{A+} (kJ/mol)	k_{-}^{0} (L ² /(min mol ²))	E_{A-} (kJ/mol)				
[HSO3bmim][OTF]	NIH	12698 ± 2790	38.4 ± 0.577	12603 ± 7400	38.66 ± 1.565	1.01×10^{-2}			
	IH	9982.6 ± 2923	37.6 ± 0.716	9927 ± 7920	38.41 ± 1.88	1.62×10^{-2}			
[HSO3bmim][p-TS]	NIH	13383 ± 5030	37.8 ± 0.989	15838 ± 6640	38.40 ± 2.76	2.50×10^{-2}			
	IH	10082 ± 5826	36.9 ± 1.20	10183 ± 6851	37.69 ± 3.27	3.21×10^{-2}			

For catalyst [HSO₃bmim][p-TS]:

$$r_{MeOAc} = -\frac{1}{V} \frac{dn_{MeOAc}}{dt} = \rho^2 c_{cat}$$

$$\times \left(13,383 \exp\left(\frac{-4547.5}{T}\right) a_{MeOAc} a_{BuOH} \right)$$

$$-15,838 \exp\left(\frac{-4628.6}{T}\right) a_{BuOAc} a_{MeOH} \right)$$
(9)

The conversion of methyl acetate and the concentration of methanol in the reaction mixture can be calculated by the equations:

$$\frac{dX_{MeOAc}}{dt} = \frac{1}{\rho x_{MeOAc}^0} r_{MeOAc} \tag{10}$$

$$\frac{dc_{MeOH}}{dt} = r_{MeOAc} \tag{11}$$

The calculated results were plotted in Fig. 6a–c. It is obvious to find that the calculated results agree well with the experimental results, which indicates the NIH model can reliably describe the kinetics of transesterification of *n*-butanol and methyl acetate catalyzed by [HSO₃ bmim][OTF] or [HSO₃bmim][p-TS].

4 Conclusions

Several acidic ILs with different cations or anions were used as catalysts for the transesterification of methyl acetate with *n*-butanol and the results show that the catalytic activities of these IL catalysts differ greatly. The acidity of ILs is influenced by cations and anions. The acidity of acidic ILs with same catalytic cation is affected by different anions, which results in different catalytic activities of the IL catalysts. The acidity of acidic ILs with same anion and different catalytic cations (containing imidazolium or pyridinium ring) is affected by different heterocyclic rings in cations, but the catalyst activities are hardly influenced by the heterocyclic rings. The performance of partially soluble catalyst [HSO₃bmim][CL] can be enhanced by $[omim][PF_6]$ in mixed ILs. The kinetic behavior of the transesterification catalyzed by [HSO₃ bmim][OTF] and [HSO3bmim][p-TS] was studied experimentally. Two different kinetic models, IH and NIH, were applied to correlate the reaction kinetics. The NIH model was found to describe the reaction rate reliably and the correlated results agree well with those of experimental.

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