

# Effect of Hydrothermal Treatment on Precipitated Iron Catalyst for Fischer–Tropsch Synthesis

Cailian Ma · Jiangan Chen

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**Abstract** Two series of Fe/Cu/K catalysts were prepared by co-precipitation (CP-xK) and by co-precipitation accompanied with hydrothermal treatment (HY-xK), respectively. The catalysts were investigated by N<sub>2</sub> adsorption, X-ray diffraction (XRD), Mössbauer effect spectroscopy (MES), scanning electron microscopy (SEM), high-resolution transmission electron microscopy (HRTEM), H<sub>2</sub> temperature-programmed reduction (H<sub>2</sub>-TPR) and thermogravimetric analysis. N<sub>2</sub> adsorption revealed that HY-xK catalysts displayed relatively low surface area, but generated additional macropore. XRD and SEM showed that HY-xK catalysts were well grown crystallite, while the CP-xK catalysts were amorphous. In addition, hydrothermal treatment remarkably influenced the growth orientation of hematite nanocrystals, resulting in the preferential exposure of the (110) plane. HRTEM also indicated that HY-1.32K was dominated by Fe<sub>2</sub>O<sub>3</sub> nanocrystals with (110) plane, and the CP-1.38K primary particle mainly exposed (104) plane. The H<sub>2</sub>-TPR profiles for the two series of catalysts were similar, though the merged and smooth peak of HY-xK catalysts possibly suggested that the component elements were more uniform. MES and XRD indicated that the catalyst after hydrothermal treatment can be easily reduced into active carbide

phases in Fischer–Tropsch synthesis (FTS) reaction. In FTS reaction, the HY-xK catalysts showed higher activity and better stability than the CP-xK catalysts given comparable K content.

**Keywords** Fischer–Tropsch synthesis · Iron-based catalyst · Hydrothermal treatment · Morphology · Stability

## 1 Introduction

Fischer–Tropsch synthesis (FTS), a well-known process to convert syngas into liquid fuels and chemicals, has been attracting great interest due to petroleum resource shrinking in the past decades [1]. Iron-based catalysts are preferred for FTS reaction due to their low cost, high activity and excellent water–gas-shift reactivity, which match the syngas from coal gasification with low H<sub>2</sub>/CO ratio [2]. Remarkably, three principal challenges come for iron-based FTS catalyst: activity, selectivity and stability [3]. At present, modification of iron-based catalyst by introducing promoters or supports, or change of the preparation methods is being explored to achieve the goal.

Among the chemical promoters, Cu can enhance the hematite reducibility. When copper oxide is reduced to metallic Cu, the crystallites provide H<sub>2</sub> dissociation sites, which spillover to iron oxides and promote its reduction at lower temperatures [4, 5]. The well-known electronic agent K in the iron-based catalysts contributes to improving the dissociative adsorption of CO [6], strengthening the bond of Fe–C by increasing the electron density on Fe while weakening Fe–H and C–O bonds; [6–8] favoring the formation of olefins and longer-chain hydrocarbon molecules [8] and the suppression of CH<sub>4</sub> formation [9, 10]; facilitating the water–gas-shift activity [11, 12] and the carburization of surface Fe

C. Ma · J. Chen (✉)  
State Key Laboratory of Coal Conversion, Institute of Coal Chemistry, Chinese Academy of Sciences,  
Taiyuan 030001, Shanxi, People's Republic of China  
e-mail: chenjl19@163.com

C. Ma  
e-mail: macailian2006@163.com

C. Ma  
University of Chinese Academy of Sciences, Beijing 100049,  
People's Republic of China

as well [13]. However, excessive K loading will break the balance between the CO dissociation and the carbon hydrogenation, leading to the deactivation of catalysts for an excessive carbon deposition [14]. So, the appropriate amount of K promoter is essential for iron catalysts.

The method of catalyst preparation also plays an important role in the physical property and catalytic performance of the catalysts [15]. Nowadays, the iron-based catalyst has been prepared by the co-precipitation [11, 16], fusion [9, 17], sol-gel [18], microemulsions [19] and so on [20–22]. It is known that during the preparation of typical iron-based FTS catalyst, the precipitate is boiled and maintains for several minutes [11, 23]. Kölbl et al. [23] reported that brief boiling of the precipitate facilitates the filtration and titrimetric standardization of the precipitant against the iron solution. In essence, this operation is a hydrothermal treatment at room pressure. In this paper, hydrothermal treatment is operating at high temperature and pressure. However, few reports refer to the iron-based catalysts prepared by co-precipitation accompanied with hydrothermal treatment. The FTS reaction is a structure sensitive reaction [24]. It is well known that hydrothermal treatment operating at elevated temperature and pressure [25] allows the synthesis material with particular morphology [26, 27]. In addition, various structures may be formed such as morphology, dispersion, phases, if different conditions of hydrothermal method are applied. These differences may affect the FTS activity, selectivity and stability of catalysts. Therefore, the effect of hydrothermal treatment on the structure of iron catalysts needs to be investigated in more detail.

In our previous studies, the CoFe nanocrystals were obtained by the hydrothermal treatment and thermal decomposition of the iron-doped cobalt carbonate hydroxide hydrate intermediate on an iron substrate, and were tested in fixed-bed reactor. From the results of characterization study demonstrate that, CoFe nanowires catalyst and nanosheets catalyst exposed distinguished crystal planes and showed different FTS performance [28].

The purpose of the present study is to investigate the catalytic performance and the changes in structure and crystal plane of precipitated iron-based catalysts which involves hydrothermal treatment, instead of being untreated to be clear of its effect. Since K promoter influences the performance greatly, Fe/Cu/K catalysts of varying K content are designed.

## 2 Experimental

### 2.1 Catalyst Preparation

The HY-xK catalysts were prepared by co-precipitation accompanied with hydrothermal treatment. In a typical

synthesis, 10 mmol of  $\text{Fe}(\text{NO}_3)_3$ , 0.53 mmol of  $\text{Cu}(\text{NO}_3)_2$  and 40 mmol of  $(\text{NH}_2)_2\text{CO}$  were dissolved in 100 mL of deionized water under stirring and then transferred into a Teflon-lined stainless steel autoclave, sealed and maintained at 110 °C for 8 h. After cooling down to the room temperature, the obtained solid product was recovered by filtration and washed with deionized water. The potassium promoter was added in a calculated amount to the precursor by impregnation with aqueous solution of  $\text{K}_2\text{CO}_3$  to give the desired K content. The final products were further dried in air at 100 °C for 10 h and then calcined at 350 °C for 6 h.

For comparison, the CP-xK catalysts were prepared by the co-precipitation method. A solution containing both 10 mmol of  $\text{Fe}(\text{NO}_3)_3$  and 0.53 mmol of  $\text{Cu}(\text{NO}_3)_2$  and a separate solution of  $\text{NH}_4\text{OH}$  ( $0.5 \text{ mol L}^{-1}$ ) were used in the precipitation processes. Under stirring, the ammonium hydroxide solution with a certain flow rate was added into the salt solution to achieve a pH value of 8.8–9.0. The precipitate was filtered, washed completely with deionized water. The potassium promoter was added in a calculated amount to the precursor by impregnation with aqueous solution of  $\text{K}_2\text{CO}_3$  to give the desired K content. The final products were further dried in air at 100 °C for 10 h and then calcined at 350 °C for 6 h.

The series catalysts prepared by co-precipitation accompanied with hydrothermal treatment are denoted as HY-xK and the series catalysts prepared by co-precipitation method are denoted as CP-xK; in both cases x denotes the wt% of  $\text{K}_2\text{O}$ .

### 2.2 Catalyst Characterization

The textural properties of catalysts were determined via  $\text{N}_2$  adsorption at  $-195.8 \text{ °C}$  with a TriStar 3000 Gas Adsorption Analyzer (Micromeritics Instrument Co., USA) and surface area was calculated using the BET method. The pore diameter was calculated by applying the Barret–Joyner–Halenda method (BJH) to the adsorption branches of the  $\text{N}_2$  isotherms. The samples were degassed at 200 °C and 6.7 Pa for 2 h prior to the measurement.

The actual composition of the catalysts was determined by inductively coupled plasma atomic emission spectroscopy (ICP-AES). To prepare the solution for elemental analysis, 2 mL of concentrated nitric acid was used to dissolve 40 mg of catalyst sample, followed by adding 2 mL of 30 wt%  $\text{H}_2\text{O}_2$ ; the solution was then diluted to 1,000 mL with deionized water.

X-ray diffraction (XRD) measurements were carried out with a D/max-RA X-ray diffractometer (Rigaku, Japan), equipped with Cu  $\text{K}\alpha$  radiation ( $\lambda = 1.5406 \text{ \AA}$ ) at 40 kV and 150 mA. The measurements were made at room temperature in the  $2\theta$  range of 10–80 °C with a scanning rate of 2 or 4  $\text{min}^{-1}$ .

The Mössbauer effect spectroscopy (MES) of catalysts was obtained on an MR-351 constant-acceleration Mössbauer spectrometer (FAST, Germany) at room temperature, using 25 mCi  $^{57}\text{Co}$  in a Pd matrix. The spectrometer was operated in a symmetric constant-acceleration mode.

The morphology of catalysts was investigated by scanning electron microscopy (SEM) (JSM-6701F, Japan). The catalysts were treated by desiccation and spray-gold.

Transmission electron microscopy (TEM) and high-resolution transmission electron microscopy (HRTEM) images of the catalysts were obtained by using a JEM 2010 microscope operating at 200 kV. The catalysts were dispersed in ethanol and mounted on a carbon foil supported on a copper grid.

$\text{H}_2$  temperature-programmed reduction ( $\text{H}_2$ -TPR) was carried out using a dynamic analyzer (Micromeritics, Model 2920). About 30 mg of catalyst was treated in 5 %  $\text{H}_2/95$  % Ar (v/v) (flow rate  $50 \text{ mL min}^{-1}$ ), and the reduction temperature was increased from room temperature to  $1,000 \text{ }^\circ\text{C}$  at a heating rate of  $10 \text{ }^\circ\text{C min}^{-1}$ . The hydrogen consumption was calibrated using the  $\text{H}_2$ -TPR of CuO (Aldrich, 99.99+ %) as the standard sample under the same conditions.

Thermogravimetric analysis (TGA) was conducted on a thermogravimetric analyzer of Setsys Evolution TGA 16/18 in nitrogen atmosphere from ambient temperature to  $650 \text{ }^\circ\text{C}$  with a heating rate of  $10 \text{ }^\circ\text{C min}^{-1}$ .

### 2.3 Reactor System

The FTS performance of the catalysts was tested in a stainless steel fixed-bed reactor with inner diameter of 12 mm loaded with 2 mL of catalyst.

The syngas ( $\text{H}_2/\text{CO} = 2$ ) was passed through a series of purification traps to remove trace amounts of iron carbonyls, water, and other impurities. The flow rate of syngas was controlled by mass flow controller (Brooks, model 5850E). The exit stream passed through a hot trap ( $130 \text{ }^\circ\text{C}$ ), a back-pressure regulator and a cold trap ( $0 \text{ }^\circ\text{C}$ ) to collect liquid products. A wet gas flow meter was used to monitor the flow rate of tail gas.

The catalyst was reduced in situ in syngas at  $290 \text{ }^\circ\text{C}$ , 0.5 MPa and  $1,000 \text{ h}^{-1}$  for 20 h. After reduction, steady-state reaction conditions were set as  $220\text{--}290 \text{ }^\circ\text{C}$ , 1.5 MPa,  $\text{H}_2/\text{CO} = 2$  and  $2,000 \text{ h}^{-1}$ .

The tail gas was analyzed online by gas chromatography (GC) (models 6890N and 4890D, Agilent) equipped with a 16-port sampling valve and two sampling loops. In one sampling loop, the hydrocarbons were analyzed with an  $\text{Al}_2\text{O}_3$  capillary column (HP-PLOT,  $30 \text{ m} \times 0.53 \text{ mm}$ ) and a flame ionization detector (FID). In the other loop,  $\text{H}_2$ ,  $\text{N}_2$ ,  $\text{CO}$ ,  $\text{CO}_2$ , and  $\text{CH}_4$  were analyzed with a Porapak Q stainless steel packed column ( $2 \text{ m} \times 3 \text{ mm}$ ), a PLOT Q packed column (HP-PLOT,  $25 \text{ m} \times 0.53 \text{ mm}$ ), a molecular sieve 5A packed column (HP-PLOT,  $30 \text{ m} \times 0.53 \text{ mm}$ ), and a TCD. The products in oil phase were analyzed off-line by GC (model 6890N, Agilent) with a quartz capillary column (DB-1,  $60 \text{ m} \times 0.25 \text{ mm}$ ) and a FID. The products in wax were analyzed offline using a gas chromatograph (6890N, Agilent, USA) with a stainless steel capillary column [UA+(HT),  $30 \text{ m} \times 0.53 \text{ mm}$ ] and a FID. Oxygenates in water were analyzed off-line using GC (model 6890N, Agilent) with a quartz capillary column (J&W DB-WAX,  $30 \text{ m} \times 0.32 \text{ mm}$ ) and a FID.

The carbon balance and mass balance were  $100 \pm 5 \%$ .

## 3 Results and Discussion

### 3.1 Textural Properties of Catalysts

The textural properties (BET surface area, pore volume and average pore diameter) and elemental compositions of the catalysts are shown in Table 1. BET surface area of all samples after hydrothermal treatment is lower than that untreated. Obviously, the catalyst surface area depends on the K content almost linearly in each series. Dry et al. [9] mentioned that the potassium could improve the agglomeration of the FeOOH precursor and further enlarge the crystallite size of  $\alpha\text{-Fe}_2\text{O}_3$  after being calcined, which would induce the decrease in surface area. In the

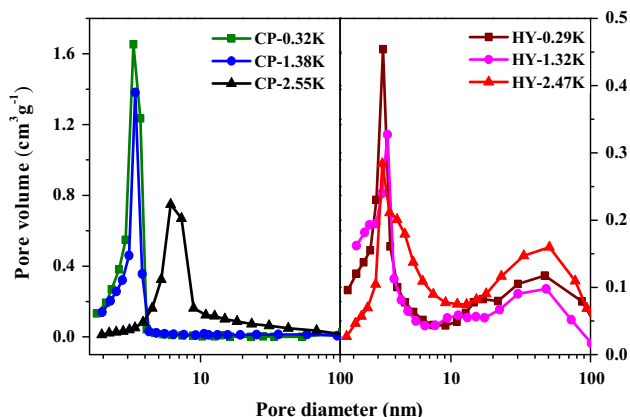
**Table 1** Physical properties of catalysts as prepared

Catalyst	Component (on mass basis) analyzed by ICP			BET results		
	Fe	Cu	K	BET surface area ( $\text{m}^2/\text{g}$ )	Pore volume ( $\text{cm}^3/\text{g}$ )	Average pore size (nm)
CP-0.32K	100	5.99	0.32	217.30	0.23	4.23
CP-1.38K	100	5.86	1.38	202.58	0.19	3.77
CP-2.55K	100	5.90	2.55	164.94	0.17	3.84
HY-0.29K	100	6.01	0.29	118.49	0.20	6.77
HY-1.32K	100	5.98	1.32	107.14	0.15	5.56
HY-2.47K	100	5.93	2.47	100.32	0.19	7.59

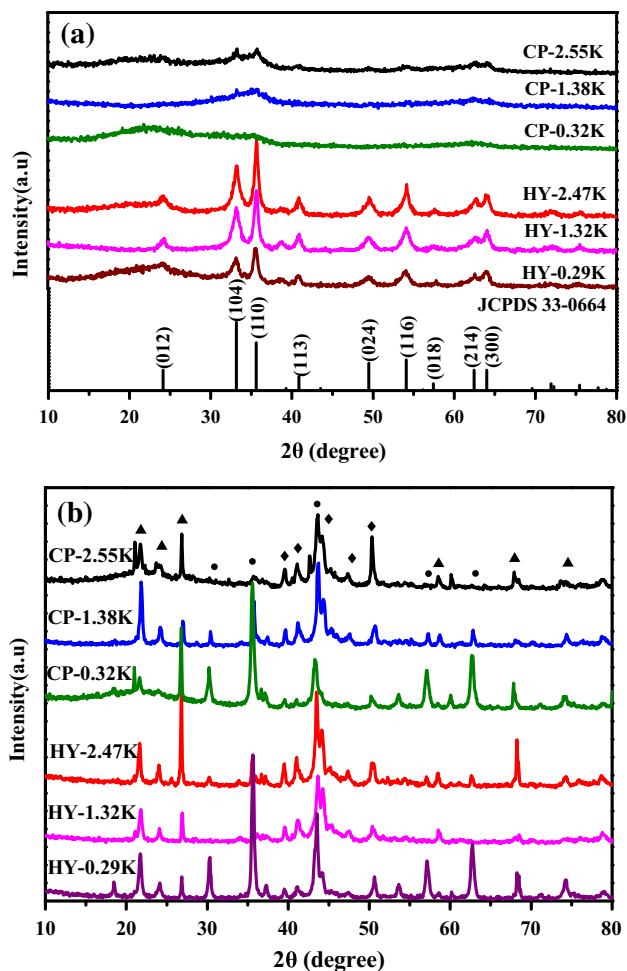
preparation of the CP-xK catalysts, the FeOOH precursor is small and the dangling hydroxyl group is rich on the surface. In contrast, the FeOOH precursor in HY-xK catalysts is large and the dangling hydroxyl group is less. The term “dangling hydroxyl group” in this paper is defined as “hydroxyl groups located on the surface of FeOOH precursors that easily lead to agglomeration of FeOOH precursors via oxygen bridge mechanism”. The pore distribution of catalysts prepared by different methods is shown in Fig. 1. CP-xK catalysts exhibit a relatively narrow pore size distribution. HY-xK catalysts show a bimodal pore distribution with maxima at 3 and 40 nm, respectively. In addition, Table 1 shows that the elemental composition of CP-xK catalysts is similar to the corresponding HY-xK catalysts, thus providing a comparison benchmark.

### 3.2 Crystallite Structure of Catalysts

XRD patterns of catalysts as-prepared with different methods are presented in Fig. 2a. The only detectable phase in the diffraction patterns of the catalysts with different preparation methods is hematite. It is obvious that the CP-xK catalysts display broad diffraction peaks at  $2\theta$  of  $35^\circ$  and  $64^\circ$ , which is the characteristic of amorphous hematite with small crystallite diameters (about 4 nm). In contrast, iron phases in HY-xK catalysts are well-crystallized hematite with sharp diffraction peaks at  $2\theta$  angle of  $24.2^\circ$ ,  $33.1^\circ$ ,  $35.6^\circ$ ,  $40.8^\circ$ ,  $49.52^\circ$ ,  $54.0^\circ$ ,  $57.6^\circ$ ,  $62.5^\circ$  and  $64.0^\circ$ . Interestingly, comparison with the standard stick pattern (JCPDS Card No. 033-0664) of pure hematite, the peak of the (110) plane is anomaly higher than that of the (104) plane. This result indicates that hydrothermal treatment remarkably influences the growth orientation of hematite nanocrystals, resulting in the preferential exposure of the (110) plane. Moreover, it is found that the intensity of  $\alpha\text{-Fe}_2\text{O}_3$  characteristic peak increases



**Fig. 1** The pore size distribution of catalysts as-prepared

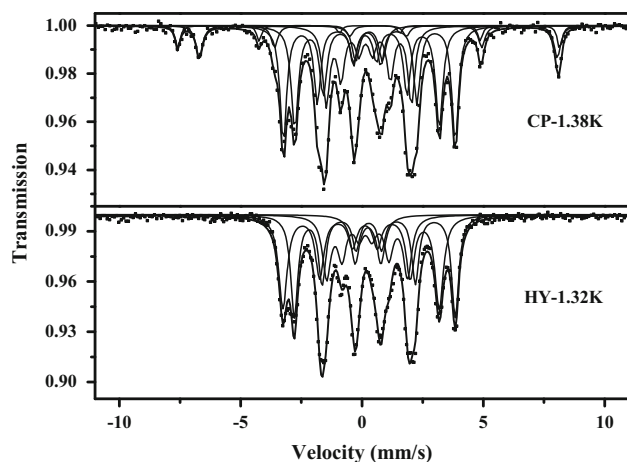


**Fig. 2** XRD pattern of catalysts: (a) as-prepared and (b) after reaction: filled triangle quartz; filled circle magnetite; filled diamond  $\text{Fe}_5\text{C}_2$

monotonously with the content of potassium for both series catalysts. In summary, the hydrothermal treatment and potassium addition promote the growth of  $\alpha\text{-Fe}_2\text{O}_3$  crystallite. This is in agreement with the decrease in the catalyst surface area.

The XRD patterns of the used catalysts are shown in Fig. 2b. There are feature lines assigned to dilute quartz in all samples. Two series of catalysts, are almost dominated by diffractions at  $2\theta$  of  $35.5^\circ$ ,  $43.1^\circ$ ,  $57.0^\circ$  and  $62.6^\circ$ , suggesting that magnetite ( $\text{Fe}_3\text{O}_4$ ) formed during FTS is highly crystallized, which is consistent with the observations by Bukur et al. [29]. It is well known that although magnetite is the most active phase for the water–gas–shift (WGS) reaction on iron-based catalysts [30], this phase is not active for FTS, as Huang et al. [31] reported that magnetite alone showed no initial activity when being exposed to syngas. The peaks at  $39.3^\circ$  and  $43.5^\circ$  are attributed to the characteristic diffraction of iron carbide ( $\chi\text{-Fe}_5\text{C}_2$ ) which is the active phase for FTS [32]. The

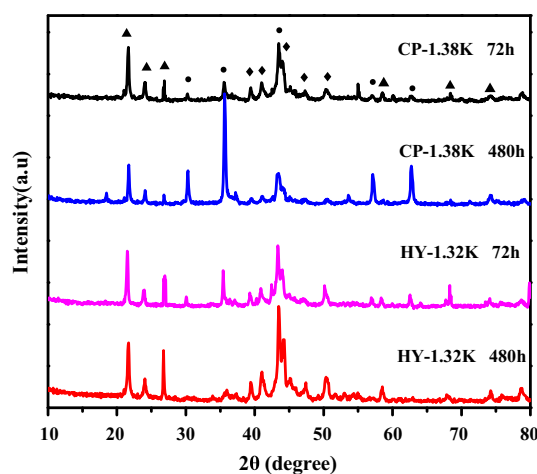
relatively stronger diffraction peak of iron carbide for the catalysts after hydrothermal treatment, compared with that for co-precipitated catalysts, conforms with the higher FTS activity of the catalysts after hydrothermal treatment. Because K has been found to be the most efficient promoter for iron-based catalysts among all of the additives studied to date, their promoting effects on the FTS performance of the two series of catalysts are also investigated in the present work aiming to improve the FTS selectivity. If the K content is similar, the iron phase is comparable for two preparation methods. In addition, the XRD patterns indicate that the diffraction peak intensities of iron carbide are enlarged and the  $\text{Fe}_3\text{O}_4$  peak decreases with the increase of K content in CP-xK catalysts. This meant that the K is helpful to stable the carbide by preventing from steam oxidation during FTS. Particularly, the peak intensity of iron carbide in HY-1.32K catalyst is higher than that of the CP-1.38K catalyst and magnetite of HY-1.32K catalyst is not detected in XRD patterns. In order to further determine iron phase compositions of catalysts, the used catalysts (CP-1.38K and HY-1.32K) were measured by MES. Figure 3 shows the Mössbauer spectra of catalysts. MES parameters of various phases and their relative contributions to spectral absorption areas are summarized in Table 2. The subspectra with Hhf in the range of 476–504 and 445–467 kOe are contributed to ferrimagnetic  $\text{Fe}_3\text{O}_4$  phases. The subspectra with 0.20 mm/s <IS <0.40 mm/s and 102 kOe <Hhf <256 kOe correspond to the stoichiometric  $\chi\text{-Fe}_5\text{C}_2$  [33]. As can be seen, the CP-1.38K catalyst is composed of  $\text{Fe}_3\text{O}_4$  and  $\chi\text{-Fe}_5\text{C}_2$ , while the HY-1.32K catalyst is only composed of  $\chi\text{-Fe}_5\text{C}_2$ . This is in agreement with XRD results. However, in HY-1.32K catalyst, content of iron carbide is higher than that in CP-1.38K catalyst. The high iron carbide content indicates that the catalyst after hydrothermal treatment can be easily reduced into active carbide phases in FTS reaction.



**Fig. 3** Mössbauer spectra of catalysts after reaction

**Table 2** Mössbauer parameters of catalysts after reaction

Catalyst	Phase	IS (mm/s)	QS (mm/s)	Hhf (kOe)	Area (%)
CP-1.38K	$\text{Fe}_3\text{O}_4$	0.30	-0.04	489	4.4
		0.67	0.01	458	8.6
	$\chi\text{-Fe}_5\text{C}_2$	0.26	0.09	220	31.1
		0.17	0.08	185	29.1
		0.22	0.13	109	21.6
(spm) $\text{Fe}^{3+}$	0.29	1.1		5.2	
HY-1.32K	$\chi\text{-Fe}_5\text{C}_2$	0.40	0.25	206	32.9
		0.04	-0.16	200	35.1
		0.18	0.07	105	22.8
	(spm) $\text{Fe}^{3+}$	0.25	1.06		9.2



**Fig. 4** XRD patterns of catalysts after different time on stream: filled triangle quartz; filled circle magnetite; filled diamond  $\text{Fe}_5\text{C}_2$

XRD patterns of catalysts after different time on stream (TOS) are presented in Fig. 4. It is found that the diffraction peak intensities of iron carbide of CP-1.38K catalyst after running 72 h are higher than that after running 480 h. However, the diffraction peak intensities of iron carbide of HY-1.32K catalyst after running 72 h are lower than that after running 480 h. It indicates that the stability of iron carbide of HY-1.32K catalyst is improved in FTS reaction. This improved stability may be ascribed to the stabilization effect caused by catalyst structure after hydrothermal treatment. Under typical FTS conditions where  $\text{H}_2\text{O}$  is present, the iron carbide can be oxidized to  $\text{Fe}_3\text{O}_4$ , leading to the deactivation of the catalysts [34]. The catalyst structure after hydrothermal treatment has broad pore size distribution and uniform particles which facilitate the diffusion of gas and mass transport. Notably,  $\text{H}_2\text{O}$  carried with gas in the FTS will be removed quickly. For the catalyst after hydrothermal treatment, the iron carbide will be slower oxidized by  $\text{H}_2\text{O}$  than that catalyst untreated. It



indicates that hydrothermal treatment improves the stability of catalyst.

### 3.3 SEM and TEM Results

The morphology and microstructure of the as-prepared CP-1.38K and HY-1.32K catalysts were elucidated by means of SEM and TEM. The SEM images of CP-1.38K and HY-1.32K catalysts are shown in Fig. 5. CP-1.38K catalyst is plane and exposes irregular facet. The images reveal that the primary particle size of CP-1.38K catalyst is small (Fig. 5a, b). This suggests that the catalyst may be composed of numerous small iron oxide particles, bound together via oxygen bridge connection (Fig. 5b). The primary particles are so close to each other that accelerate the particle sintering rate, as observed by BET. The HY-1.32K catalyst shows shale-like shape and is regular, attributed to the particle reforming after hydrothermal treatment (Fig. 5c, d). In high magnification (Fig. 5d), the HY-1.32K bulk is packed with nanoparticles. By reference to XRD, the nanoparticle is crystallite.

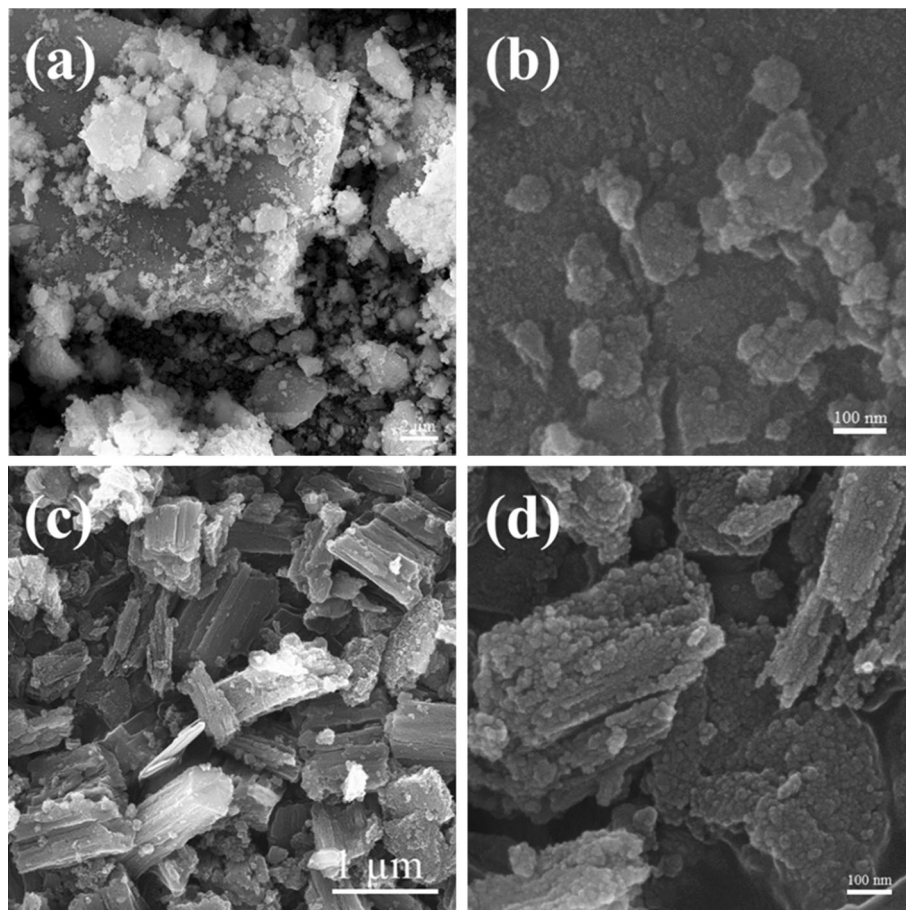
TEM and HRTEM images of CP-1.38K and HY-1.32K catalysts are shown in Fig. 6. It can be seen that the as-prepared CP-1.38K catalyst shows irregular agglomeration of

4 nm nanoparticles (Fig. 6a), while the HY-1.32K catalyst is composed of uniform particles, which are about 11 nm in diameter (Fig. 6c). The HRTEM images further illustrate that the exposed crystal planes of CP-1.38K catalyst are dominated by (104) plane of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> (Fig. 6b), while HY-1.32K catalyst mainly exposes (110) plane (Fig. 6d). This is in agreement with the phenomenon in XRD. As suggested by Li et al. [35], precipitated Fe–Mo Fischer–Tropsch catalysts were dominated by (104) plane of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>. Cornell et al. [36] reported that the (110), (100), (012) and (113) planes were fringed with singly coordinated hydroxyls in pairs, whereas (104) and (001) planes were covered with bi-coordinated hydroxyl, which was a stronger ligand. In fact, this feature is utilized to preferably adsorb H<sub>2</sub>PO<sub>4</sub><sup>−</sup>, thus makes the (104) plane growth halt, and to control the morphology of Fe<sub>2</sub>O<sub>3</sub> powder [37]. The CP-1.38K catalyst is rich in (104) plane and bi-coordinated hydroxyl group, so the particle tends to merge via hydroxyl bridge.

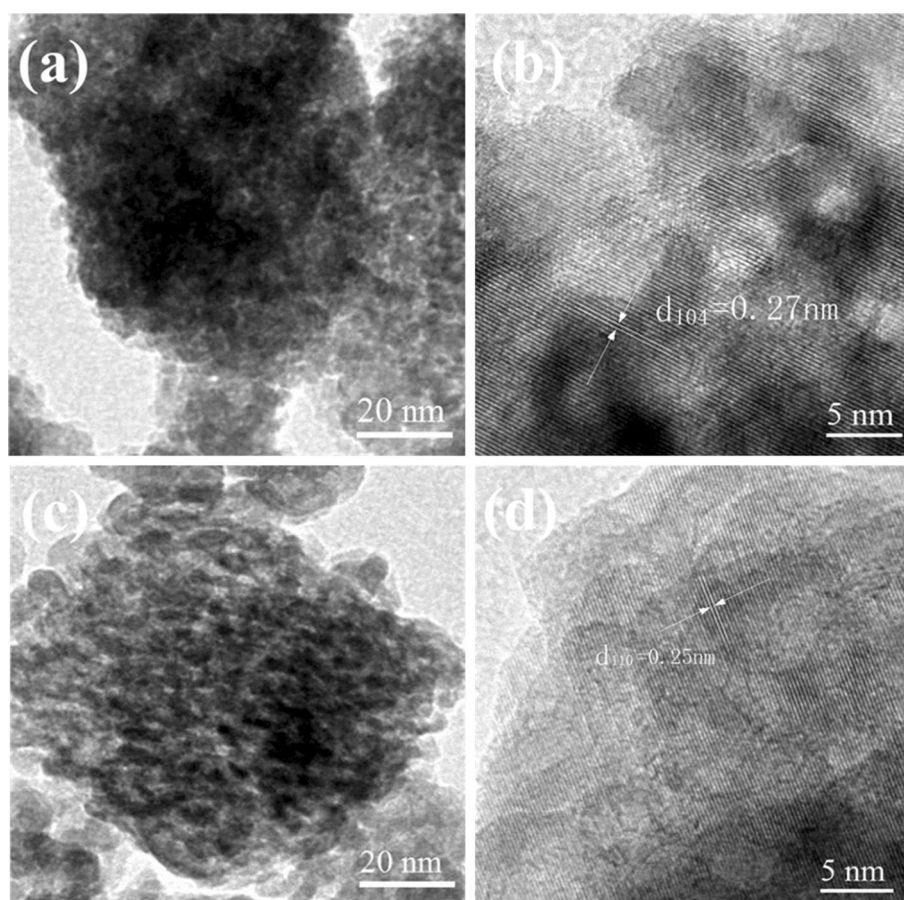
### 3.4 Reduction Behaviors of Catalysts

The reduction behaviors of catalysts were studied by H<sub>2</sub>-TPR. The reduction profiles and H<sub>2</sub> consumption for the

**Fig. 5** SEM images of catalysts as-prepared: (a, b) CP-1.38K; (c, d) HY-1.32K

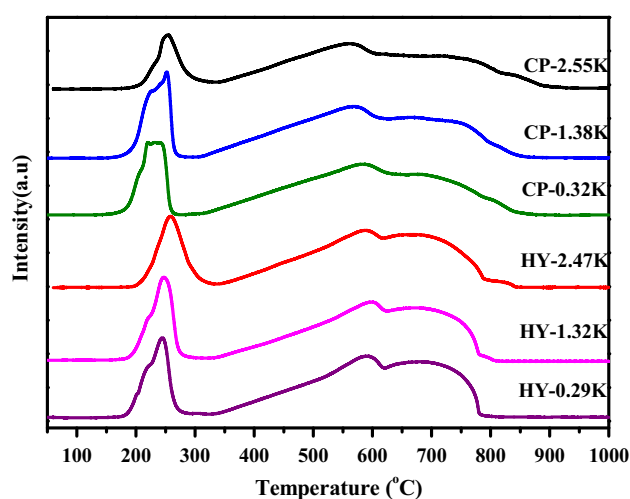


**Fig. 6** TEM and HRTEM images of catalysts as-prepared: (a, b) CP-1.38K; (c, d) HY-1.32K



catalysts are presented in Fig. 7 and Table 3, respectively. It is reasonable to assume that only the  $\text{Fe}_2\text{O}_3$  phase was primarily present after calcination based on the similar TPR profiles for all the catalysts. Figure 7 reveals that all catalysts show multiple reduction peaks, which can be assigned to two different reduction stages of iron oxides. The first stage (lower-temperature reduction peak) is assigned to the transformations of  $\text{CuO} \rightarrow \text{Cu}$  and  $\text{Fe}_2\text{O}_3 \rightarrow \text{Fe}_3\text{O}_4$ , whereas the second stage (two higher-temperature reduction peaks) represents the transformation of  $\text{Fe}_3\text{O}_4 \rightarrow \text{Fe}$  [38]. The sum of  $\text{H}_2$  consumption for first stage (0.15–0.19 mol  $\text{H}_2$ /mol M), consistent with the theoretical value of  $\text{CuO} \rightarrow \text{Cu}$  and  $\text{Fe}_2\text{O}_3 \rightarrow \text{Fe}_3\text{O}_4$  (0.208 mol  $\text{H}_2$ /mol M), verifies the above statement.

For the CP-xK catalysts, the reduction peaks for the first stage are sawtooth shaped and not smooth. However, for the HY-xK catalysts, the reduction peaks for the first stage are smooth, meaning that the iron is mixed well with copper in the latter and the promotion of Cu is more efficient. There appears to be better synergistic interaction between the copper promoter and the iron in HY-xK catalysts so that copper is more effective to the reduction of catalysts. It suggests that HY-xK catalysts form a uniform Fe–Cu matrix after hydrothermal treatment, while CP-xK catalysts form inhomogeneous Fe–Cu



**Fig. 7**  $\text{H}_2$ -TPR profiles of catalysts

matrix. Comparison of the  $\text{H}_2$ -TPR profiles of the CP-xK and HY-xK catalysts with similar K content clearly shows that the reduction of CP-xK catalysts starts at slightly lower temperature, but the reduction of HY-xK catalysts finishes at lower temperature. When K content is low, both CP-xK and HY-xK catalysts display comparable reduction temperature (Fig. 7).

**Table 3** Quantitative results of H<sub>2</sub> consumption for catalysts in H<sub>2</sub>-TPR

Catalyst	Peak (°C)	H <sub>2</sub> consumption <sup>a</sup>	
		Mol H <sub>2</sub> /mol M <sup>b</sup>	Mol H <sub>2</sub> /mol Fe
CP-2.55K	254	0.15	
	551		0.73
	758		0.27
CP-1.38K	236	0.19	
	557		0.72
	738		0.17
CP-0.32K	228	0.18	
	574		0.75
	737		0.11
HY-2.47K	259	0.16	
	584		0.72
	714		0.15
HY-1.32K	243	0.17	
	586		0.70
	716		0.15
HY-0.29K	236	0.17	
	583		0.74
	716		0.16

<sup>a</sup> The H<sub>2</sub> consumption was measured from the area under the corresponding peak

<sup>b</sup> M = Fe + Cu

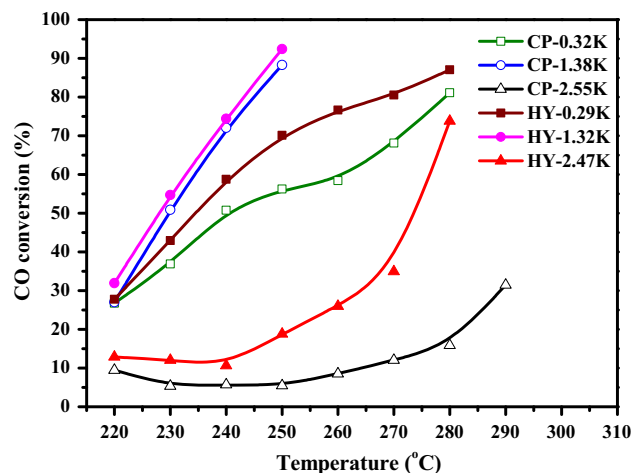
When K content is high, the peak of first stage is shifted to higher temperature [39]. Rankin and Bartholomew [40] have reported that the interaction of iron oxide and potassium oxide could cause a delay in the reduction of iron oxide due to the suppressed adsorption of H<sub>2</sub>.

### 3.5 TGA

TGA profile of catalysts after calcination is not shown. In the TGA curve of HY-1.32K, there is a small weight loss of about 4.3 % due to desorption of physisorbed water molecules from 100 to 300 °C. No further weight loss and no thermal effect are observed after 300 °C. But in the TGA curve of CP-1.38K, there is weight loss of about 8 % due to desorption of physisorbed water molecules from 100 to 300 °C. In addition, a significant weight loss of about 9.8 % is observed in the temperature range of 300–520 °C, due to the condensation dehydration of surface hydroxyl groups [41]. It indicates that HY-1.32K catalyst displays less hydroxyl amounts, in accordance with HRTEM characterization.

### 3.6 FTS Performance

The activities of the two series of catalysts in the temperature range of 220–290 °C are shown in Fig. 8. As expected,

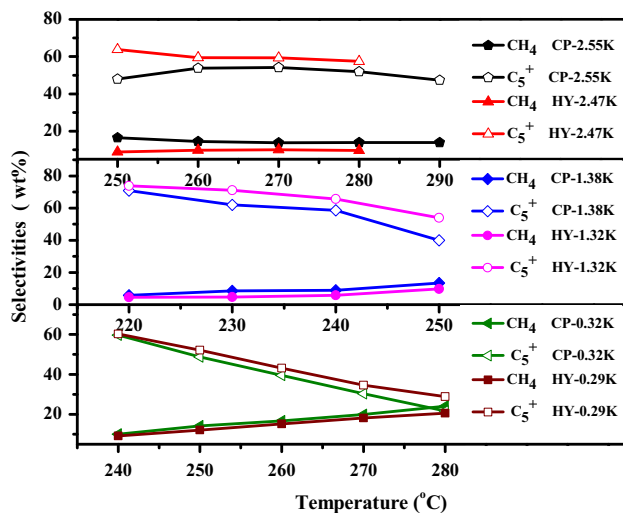


**Fig. 8** Effects of potassium content and temperature on carbon monoxide conversion of catalysts

all catalysts show increased CO conversion with increasing temperatures from 220 to 290 °C. The activity of HY-xK catalysts is higher than that of CP-xK catalysts if the K content is comparable. Also, turnover frequencies (TOFs) of HY-xK catalysts are higher than that of CP-xK catalysts at the same temperature. Ignoring consideration of the BET area, the close activity of two series catalysts is astonishing. Possibly, the texture is transformed into a final state no matter what the initial structure is. Mahajan et al. [42] reported that the final state of nanometer iron was similar to that of micronmeter iron in FTS. The CO conversion increases significantly with increasing K content and passes through a maximum at 1.32 wt% for HY-xK catalysts and 1.38 wt% for CP-xK catalysts. Further increase in K content leads to a decrease in CO conversion for both catalysts [14]. The FTS activity depends on both the K content and the preparation method. The effect of K content on the FTS performance of the catalysts observed here is in agreement with the studies on other iron-based catalysts [14]. Miller and Moskovits [10] found that there was a competition between dissociative CO chemisorption and H<sub>2</sub> adsorption on the active sites of catalysts, which led to a maximum in conversion as a function of alkali-metal content. When the K content is even higher, CO dissociation proceeded faster than carbon hydrogenation, leading to an excessive carbon deposition that eventually deactivates the catalyst [43], which explains the lower activity of the catalysts with higher K content. The catalysts after hydrothermal treatment are more sensitive to K content, probably due to the uniform dispersion of Cu or the regular crystallite.

The methane and high-molecular-weight hydrocarbon (C<sub>5</sub><sup>+</sup>) selectivities of catalysts under different temperatures are shown in Fig. 9. Hydrocarbon product distributions of catalysts are summarized in Table 4. The methane selectivity of HY-xK catalysts is slightly lower than the

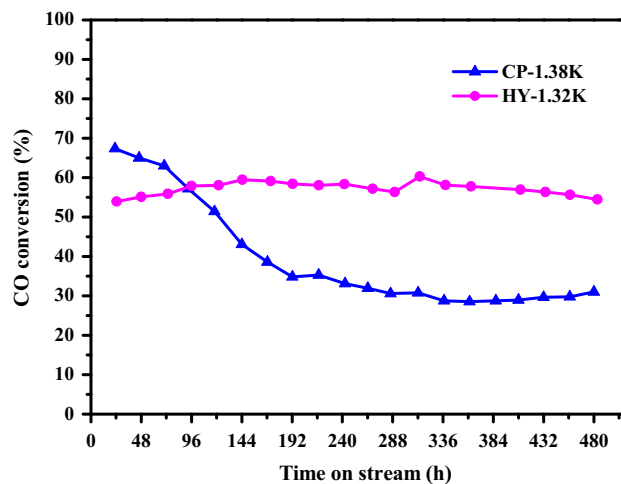




**Fig. 9** Effects of potassium content and temperature on  $\text{CH}_4$  and  $\text{C}_5^+$  selectivity of catalysts

corresponding CP-xK catalysts. The  $\text{C}_5^+$  selectivity of HY-xK catalysts is slightly higher than the corresponding CP-xK catalysts. It indicates that hydrothermal treatment can decrease methane selectivity and increase  $\text{C}_5^+$  selectivity of the iron-based catalyst in FTS reaction.

The influence of preparation method on catalyst stability is presented in Fig. 10. The CO conversion of CP-1.38K



**Fig. 10** CO conversion as a function of time on stream of catalysts (CP-1.38K: reaction temperature 235 °C; HY-1.32K: reaction temperature 230 °C)

catalyst quickly decreases from 67 % at the beginning of the reaction to about 30 % at 480 h. However, the steady CO conversion of HY-1.32K catalyst is quickly stabilized at a relatively high level (58 %). It is known that the interconversion between iron oxides and iron carbide is dynamic and reversible depending upon the environment in FTS. When the  $\text{H}_2\text{O}$  partial pressure is high, iron carbide

**Table 4** Activity and selectivity of catalysts

Catalyst	CP-0.32K		CP-1.38K		CP-2.55K		HY-0.29K		HY-1.32K		HY-2.47K	
Temperature (°C)	240	280	240	250	240	290	240	280	240	250	240	270
CO <sup>a,b</sup> conversion (%)	50.78	81.11	72.07	88.32	5.67	31.50	58.77	87.08	74.40	92.44	10.65	34.96
TOF <sup>c</sup> × 10 <sup>-3</sup> (s <sup>-1</sup> )	0.97	1.42	1.45	1.78	0.10	0.56	1.50	2.22	1.78	2.05	0.28	0.94
(CO + H <sub>2</sub> ) conversion (%)	37.48	54.88	41.60	60.88	3.48	22.71	38.43	57.13	45.30	54.44	7.29	25.80
H <sub>2</sub> conversion (%)	31.52	44.21	28.03	48.65	2.48	18.71	29.03	43.28	33.17	39.78	5.84	21.82
H <sub>2</sub> /CO (in tail gas)	3.11	7.26	5.79	9.87	2.27	2.61	3.72	9.50	6.26	20.65	2.43	2.77
H <sub>2</sub> /CO usage	1.39	1.34	0.87	1.24	0.96	1.31	1.07	1.08	1.07	1.12	1.26	1.44
CO <sub>2</sub> percent (mol %)	24.74	28.73	31.73	30.88	8.81	25.65	34.52	36.31	30.88	26.34	20.75	26.34
HC <sup>b</sup> selectivity (wt%)												
C <sub>1</sub>	10.07	24.09	8.94	13.40	16.49	13.92	9.16	20.61	5.79	9.81	8.43	10.01
C <sub>2</sub> -C <sub>4</sub>	30.30	54.27	32.51	46.58	38.35	38.71	30.67	50.55	28.56	36.17	25.61	30.61
C <sub>5</sub> <sup>+</sup>	59.63	21.64	58.55	40.03	45.16	47.37	60.18	28.84	65.64	54.02	65.96	59.39
C <sub>2-4</sub> O/P	1.48	0.64	2.02	1.70	0.90	1.74	1.60	1.07	2.87	1.84	1.51	1.49
Alcohols <sup>d</sup> (wt%)	2.21	0.69	6.64	3.13	1.31	1.58	2.37	1.49	7.20	3.88	2.76	6.07

<sup>a</sup> Reaction condition: 1.5 MPa,  $\text{H}_2/\text{CO} = 2.0$ , and  $\text{GHSV} = 2,000 \text{ h}^{-1}$

<sup>b</sup> Max error = ±5 %

<sup>c</sup> Apparent turnover frequency: numbers of CO molecules converted per adsorption site per second

<sup>d</sup> Alcohols in total hydrocarbon and oxygenates

will be oxidized to  $\text{Fe}_3\text{O}_4$ , which leads to the deactivation of iron-based FTS catalysts [34]. In FTS, a large amount of  $\text{H}_2\text{O}$  will be produced, which in turn oxidizes the iron carbide. The structure of HY-1.32K catalyst can quickly remove  $\text{H}_2\text{O}$  by the broad pore size distribution and uniform particles; thus, oxidization of iron carbide is suppressed, which stabilizes the iron carbide. This result discloses the unique merits of the hydrothermal treatment in promoting the iron-based FTS catalysts.

#### 4 Conclusions

In this study, two series of Fe/Cu/K catalysts were prepared by co-precipitation and by co-precipitation accompanied with hydrothermal treatment, respectively. The catalysts after hydrothermal treatment, have relative low BET surface area, uniform morphology and Fe–Cu matrix. In addition, hydrothermal treatment remarkably influences the growth orientation of hematite nanocrystals, resulting in the preferential exposure of the (110) plane.

In FTS reaction, the catalysts after hydrothermal treatment exhibit higher activity than the catalysts prepared by co-precipitation, which is attributed to the more iron carbide during the FTS process. In addition, the stability of catalysts after hydrothermal treatment is very stable, while the stability of catalyst prepared by co-precipitation is very poor during a period of 480 h. It is probably due to the broad pore size distribution and uniform particles of the catalysts after hydrothermal treatment.

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