REVIEW

Potential of biodegradable microneedles as a transdermal delivery vehicle for lidocaine

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Abstract There has been an increasing interest in applying biotechnology in formulating and characterising new and innovative drug delivery methods, e.g., drug-loaded biodegradable microneedles within the area of transdermal delivery technology. Recently, microneedles have been proposed for use in pain management, e.g., post-operative pain management through delivery of a local anaesthetic, namely, lidocaine. Lidocaine is a fairly common, marketed prescription-based, local anaesthetic pharmaceutical, applied for relieving localised pain and lidocaineloaded microneedles have been explored. The purpose of this review is to evaluate the properties of biodegradable polymers that may allow the preparation of microneedle systems, methods of preparing them and pharmacokinetic conditions in considering the potential use of lidocaine for delivery through the skin.

Keywords Biodegradable · Drug delivery · Lidocaine · Microneedles · Substrate · Tensile strength

Introduction

There has been an increasing interest in applying biotechnology in formulating new and innovative drug

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delivery methods, including biodegradable microneedles within the area of transdermal drug delivery technology (Orive et al. 2003; Olatunji and Das 2010, 2011). Conventional hypodermic needle delivery causes pain and anxiety, and requires medical personnel for administration. In contrast, the biodegradable microneedle, a drug-loaded vehicle moulded into an all-in-one drug formulated micro-structure constructed from either biopolymer or sugar excipients, can be used to deliver drug almost painlessly to humans (e.g., Donnelly et al. 2010; Lhernould and Delchambre 2011; Olatunji and Das 2011; Gittard et al. 2012). These microneedles are economical due to using fairly cheap materials, give reproducible results and are generally safe even if microneedle fragments break off after piercing the skin surface as compared to other microneedles made with glass or metal.

Large molecular weight proteins such as bovine serum albumin (BSA), growth hormones and vaccines have been successfully loaded into biodegradable microneedles (Lee et al. 2008, 2011a; Raphael et al. 2010). Recently, the microneedles have also been explored for use in post-operative pain management through delivery of a local anaesthetic, lidocaine. Lidocaine provides short duration, superficial anaesthesia, to the pain-affected area (Kissin 2012). Lidocaine (Fig. 1a) comprises of a polar tertiary amine and a hydrophobic aromatic group on the opposite ends of the acetamide bond (Costa et al. 2008). It is hydrophobic as the basic drug but it is soluble in water as the ionised form of lidocaine hydrochloride (Fig. 1b) in



a
$$O$$
 HN
 H_3C
 CH_3
 CH_3
 C_2H_5
 CH_3
 C_2H_5

Fig. 1 a The chemical structure of hydrophobic form of local anaesthetic lidocaine (Costa et al. 2008). **b** The hydrophilic form of lidocaine known as lidocaine hydrochloride (Shaikh et al. 2011)

which the tertiary amine is protonated (Ullah et al. 2012; Rajabi et al. 2011; Shaikh et al. 2011). Therefore, lidocaine can be encapsulated or dispersed in a drug delivery vehicle which could be either hydrophobic or hydrophilic.

In the present context, a vehicle for drug delivery is taken as a support material for formulating drugs usually in liquid-based or a semi-solid form to remain on the skin surface and facilitate the conditions necessary for transdermal drug delivery (Allen et al. 2005; Djabri et al. 2012; Subedi et al. 2010). An ideal drug carrier system or vehicle is sought for identifying optimal conditions in controlled release and transdermal permeation kinetics of the drug lidocaine. The main objective of using a vehicle is either to allow for fast initial release or permeation in skin with consideration to the suitability of suturing a superficial cut or a slow initial release and longer steady state conditions lasting several hours with an alternative consideration to suturing and treating multiple lacerations at the localised area.

A formulation of lidocaine has been developed by Fiala et al. (2011) for EMLA (eutectic mixture of local anaesthetics) containing lidocaine and prilocaine in hydrofluoroalkane as a propellant enhancer spray. Kaewprapan et al. (2012) studied lidocaine-loaded nanoparticles of dextran decanoate esters with varying degrees of substitution for suspension in aqueous medium. Petrisor et al. (2012) mixed lidocaine with

silicone elastomer and analysed the controlled release effects of modifiers such as poly(vinylpyrrolidone), PVP, and poly(vinyl alcohol), PVA. Compared with injectable and skin-surface drug applicants, microneedles are highly beneficial in terms of constant needle lengths being below the length causing epidermal pain stimulation during insertion (Banga 2009), while being described as minimally invasive in forming micro-spaces (Daugimont et al. 2010) in conjunction to enhancing the movement of the active compounds through the skin (Ameri et al. 2010; Chu et al. 2010).

Besides the laboratory-based studies mentioned above, there are a number of proprietary transdermal delivery systems for lidocaine. These include proprietary medicines in solution, semi-solid and patch delivery system. For example, lidocaine in solution is combined with a bacterially-derived hyaluronic acid gel formula to minimise the discomfort of injection as a tissue filler in the cosmetics industry (Monhiet et al. 2009). The proprietary name of the formulation is Prevelle Silk (Mentor Pharmaceuticals, www.mentor corp.com). Lidocaine solution is marketed under the proprietary name of Xylocaine and is also available in an injectable format (www.astrazeneca.co.uk). Clinical research has shown that a 1 % (w/v) lidocaine subcutaneously injected once into the location of a lacerated, injured or tumour-affected hand allows for successful local anaesthesia followed by surgical treatment (Tzeng and Chen, 2012). A lidocaine patch for the application to skin is also marketed with the proprietary name Lidoderm (www.Lidoderm.com). A Lidoderm (5 % w/v) patch has been applied for the treatment of postherpetic neuralgia (Katz et al. 2002) and in the reduction of pain during treatment of Dercum's disease (Desai et al. 2008).

Conceptually, microneedle technology provides an attractive method for delivering lidocaine. For example, it may be possible to apply the drug over a large surface area on the body with no or little pain in contrast to traditional hypodermic injections. With microneedles it may be possible to control the drug delivery rate as well besides reducing wastage of the drug. As far as we know, there is no commercially-based lidocaine microneedle product available from pharmacies. However, there seems to be some developmental research for lidocaine microneedles. Recently, the 3 M Group developed a lidocaine solution mixed with dextran to uniformly coat



medical-grade, liquid crystalline polymer (class VI) for pre-clinical in vivo studies using biopsy porcine skin of live pigs. This resulted in successful delivery of lidocaine in a faster time compared to eutectic mixture of local anaesthetics (EMLA) composed of lidocaine and prilocaine as a combined eutectic formulation (Zhang et al. 2012; Schreiber et al. 2013). A highly significant development was made by Theraject Inc. (Kwon 2004) with regards to determining the permeation flux of lidocaine through the skin by testing a Theraject MAT dissolvable microneedle system. This vehicle comprised sodium carboxymethyl cellulose mixed with lidocaine and was cast, compressed and moulded to dryness with a subsequent diffusion characterisation that confirmed the permeation flux had increased up to 12-fold compared to 10 % (w/v) lidocaine as control (Kwon 2004). The degree of substitition, in terms of exchanged hydroxyl groups to carboxymethyl groups in sodium carboxymethyl cellulose, effected solubility, viscosity, gel strength and electro-analytical behaviour as an anionic polymer in solution requires further work in order to aim for a plastic material property (Kundu et al. 2011).

While the above studies show the potential for applying the principles of biotechnology for preparing lidocaine-loaded microneedles, there is a clear need to make further progress on the methods of preparation and characterisation of the microneedles for drug delivery. It may also be necessary to learn from what have been done elsewhere while loading and delivering other molecules (e.g., insulin) using biodegradable microneedles. To address these issues, this review paper aims to evaluate critically the current developments in biodegradable microneedle systems for possible applicability in transdermal lidocaine delivery. In particular, this paper reviews the methods of preparation and the properties of biodegradable polymers that may allow for the development of a desirable microneedle system for lidocaine delivery. It is expected this would be helpful in preparing biodegradable microneedle for lidocaine delivery.

Preparation of biodegradable microneedles

The first published paper on microneedles was in 1947 in which soft glass material (30 μ m tip diameter and 2.5 cm long) was an example of early microneedles in assisting the isolation of yeast ascospores (Thaysen

and Morris 1947). Gerstel and Place (1976) were the first to obtain a patent for the architecture of microneedle arrays, outlining a drug solution reservoir to a flow-through hollow microneedle. In 1998, a paper on the fabrication of microneedles used silicon-layered chromium for 'coat and poke' delivery of drugs (Henry et al. 1998). The first published fabrication of biodegradable microneedles used micromachining technology to mould polycaprolactone polymer into microneedles (Armani and Chang 2000; Park et al. 2003). At the moment, there is clearly an increasing interest in preparing biodegradable microneedles for a variety of applications.

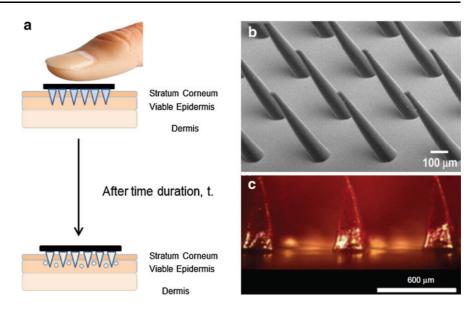
Preparation and treatment of normal skin surface before the application of a microneedle has not been recommended. Most papers suggest that pathogenic infections are not caused by using microneedles (Arora et al. 2008; Donnelly et al. 2009; Han et al. 2012). The removal of microneedles leaves indents on the skin and the main factors, such as microneedle length, number in an array and microneedle cross-sectional area, effect the time for natural skin resealing (Gupta et al. 2011). For example, Kalluri and Banga (2011) have characterised the micro-conduit channels caused by microneedles and pore re-sealing. They show that skin pores close partially in approx. 12 h and completely in approx. 15 h.

A direct thumb application for biodegradable microneedles allow the drugs encapsulated inside the microneedles to diffuse into the viable epidermis of the skin as outlined schematically in Fig. 2a (Shakeel et al. 2011; Kim et al. 2012a). However in the case of lidocaine, if the drug is concentrated in the middle to lower portion of the microneedle than the tip, the permeation is expected to be in the stratum corneum (SC) layer of the skin to anaesthetise a superficial cut.

As such, one needs to consider where the drug is loaded in the microneedle. Compared with glass and metal microneedles, biodegradable microneedles have no or little safety concern if they break and become embedded in the skin as a foreign body (Park et al. 2007a). Also, the manufacturing process and reproducibility of biodegradable microneedles are economical compared with conventional micro-machining manufacture (Donnelly et al. 2010). Figure 2b is an image of sodium carboxymethyl cellulose-biodegradable microneedles encapsulated with the drug sulforhodamine B and Fig. 2c is an SEM plan view of PLGA microneedles (Jeong et al. 2008; Park et al. 2007a).



Fig. 2 a Schematic outline of a diffusing biodegradable microneedle after skin insertion. b Pyramidal sodium carboxymethyl cellulose microneedles containing sulforhodamine B (Jeong et al. 2008). c Scanning electron microscope image of conical PLGA microneedles (Park et al. 2007)



Fabrication of biodegradable microneedles from substrate masters

Biodegradable microneedles have been fabricated by a variety of means. For example, silicon master substrate is adapted in MEMS applications and less time consuming, mass producing techniques were researched via operations from the microelectronics industry, known as microelectronic mechanical systems (MEMS) for the fabrication of a master microneedle array prior to micromoulding (Fujita 1997; Walraven 2003; Trautmann et al. 2005). SU-8, 1-methoxy-2-propyl acetate, (Microchem Corp, MSDS) is a negative photoresist material mixed with a sulfonium salt photoinitiator for inducing the mechanism of cationic polymerisation in epoxy groups of SU-8 monomers under UV (Zhang et al. 2001; Qvortrup et al. 2011). It is photosensitive to UV light and a special mask diffraction grating is required to direct a particular wavelength onto the SU-8 (Ami et al. 2011). SU-8 does not always provide accurate structures and cases of bending brought by high residual stress were observed when photoresist and substrate posses incompatible thermal expansion coefficients. As such, the UV exposure time and wavelength range need close monitoring to prevent the distorting structure (Safavieh et al. 2010; Del Camp and Greiner 2007). Marasso et al. (2011) implemented double spin coating with two different viscosities of SU-8 and observed good adhesion properties between copper substrate and SU-8 inconjunction to an aspect ratio of 7:1 without additional steps such as wafer removal and seed layer introduction, extending production period over 24 h. Also, the viscosity and set thickness of the SU-8 photoresist are dependent on the amount of γ -butyrolactone solvent dissolved in producing the solution (Lorenz et al. 1997).

A recent starting material for production of master templates was reported by Viero et al. (2012). They used reactive-ion etching (RIE) on a silicon-based master for the construction of microneedles. Chen et al. (2008) also outlined a fabrication process which used silicon oxide layers on silicon followed by a positive photoresist treatment for pattern transfer onto the silicon oxide layer via RIE and finally producing microneedle tips using an isotropic RIE process. Lhernould and Delchambre (2011) arrived at a design fabrication process of implementing laser ablation to create microchannels in polycarbonate material. Matteucci et al. (2009) adapted the micro-fabrication process known in German as Lithographie, Galvanoformung, Abformung (lithography, electroplating and molding) by Hruby (2001) which produced microneedles by double-exposure, deep X-ray lithography (Kim et al. 2004) using microcrystalline silicon wafers surfaced with Cr/Au bilayer as a template. Even though complicated multi-step processes and specialist resources are required in the production of a large quantity of master microneedles, the production of a single master is economical and time saving when considering the transferability in creating an inverse micromould for biodegradable microneedles (Kim et al. 2009, 2012b).



Fabrication of biodegradable microneedles from moulds

Biodegradable microneedles have been manufactured from micromoulds that are non-interconnecting micro-well structures (Ryu et al. 2007). There is a lack of publications that outline the micro-moulding fabrication processes methodically. However, the manufacturing processes of casting and hot embossing are common for biodegradable microneedles and are now discussed briefly. In the casting process, a master template is fabricated to develop a mould template for a molten drug formula to fill the mould contours, solidify under favourable temperature and pressure conditions and finally removal of the mould from the solidified drug formula (Bariya et al. 2011). Polydimethyl-siloxane (PDMS) is an ideal material for replica moulding of microneedles because of its nontoxicity, elastic properties and low cost (Saliterman 2006; Lee and Lee 2008) and, as such, it has been used in many studies. Laser ablation by focusing a CO₂ laser was used to create conical shaped voids in PDMS material moulds for vacuum setting sodium carboxymethylcellulose and polyacrylamide solution into solid microneedles (Kim et al. 2009). In another study, a pre-fabricated PDMS mould was used to vacuum set PLGA microneedles containing hydrogels (Kim et al. 2012b). PLGA is composed of DLpolylactic acid (PLA) and polyglycolic acid (PGA) monomers (Gabor et al. 1999; Danhier et al. 2012). As a biocompatible polymer, PLGA is used in biotechnology for the goal of preparing biodegradable microneedles and scaffolds in tissue engineering (Lee et al. 2004). It has been argued that PLGA with low molecular weights of less than 50 kDa and a DL-lactide/GA ratio of 50:50 are the most suitable for controlled drug release with respect to faster degradation rates (Fredenberg et al. 2011; Mundargi et al. 2008). PLGA in the context of merchandise is commercially and readily available from many suppliers.

Stages in a typical casting process (Fig. 3a, Chu et al. 2010) start with a PDMS mould (step 1), prefabricated from a PDMS male master coated with gold, and the mould is filled with sulforhodamine B (step 2). The residual drug solution is pipette extracted half-way to be reused later (step 3) and the remaining drug solution in the mould crevice is dried by centrifugation. The PVA/PVP blend devoid of drug

is casted into the mould by vacuum pressure (step 4), the combined polymer is air dried or is centrifuged at a low speed in drying (step 5) and an adhesive backing is used to prise the formed polymer microneedles from the PDMS mould (step 6). Another biodegradable polymer system, poly-lactide-co-glycolide (PLGA), fabricated by Park et al. (2003) (Fig. 3b) commenced with SU-8 substrate (step 1) by using the same PLGA polymer as a sacrificial filler on SU-8 (step 2) followed by copper-coating deposition and acid etching to cover the SU-8 epoxy cylinders as a pattern (step 3) with subsequent reactive ion etching (RIE) to asymmetrically etch the tips of epoxy cylinders (step 4) and an inverse PDMS mould was created (step 5) with the prior master structure from RIE method before casting new PLGA microneedles as the final product (step 6) (Park et al. 2003).

A more economical method using a natural clay, Chinese purple ceramic mould was formed by hydraulic pressing a bed of steel sticks into the soft pliable clay before furnace heating, slow cooling followed by pouring a mixture of PVA, dextran and carboxymethylcellulose polymers into the mould then vacuum setting, freeze thawing and finally drying into microneedles (Yang et al. 2012).

A less common fabrication technique, known as hot embossing, requires the application of heat above the glass transition temperature of the polymer product in contact with the mould followed by force to emboss the mould pattern to the polymer product and then cooling below the glass transition temperature before separation of mould and polymer product (Bodhale et al. 2009). Poly-L-lactic acid (PLLA) is commercially and readily available from many chemical suppliers. It is similar to PLGA. PLLA microneedles were fabricated by a hot embossing technique through a multi-step process via a PDMS replication and then heating and pressuring the PDMS mould and PLLA grains followed by unmoulding at room temperature to obtain the microneedles (Han et al. 2009). A more efficient process was studied by Youn et al. (2008) by fabricating silicon moulds using focused ion beam and then pressing the silicon mould in poly-methylmethacrylate (PMMA) polymer under applied temperatures above the glass transition temperature of PMMA and pressure followed by slow cooling resulted in good reproducibility of replicated structures (Youn et al. 2008). Hot embossing appears only suitable for high temperature stable drugs in a



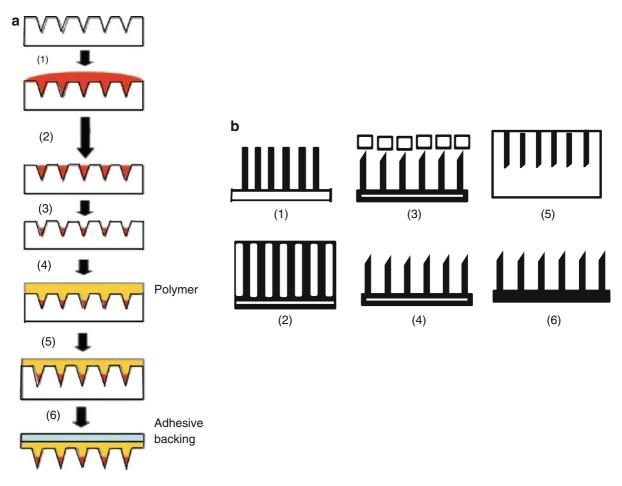


Fig. 3 a Stages in micromoulding of biodegradable PVP/PVA microneedles (Chu et al. 2010). b Stages in micromoulding of biodegradable PLGA microneedles (Park et al. 2003)

biodegradable polymer vehicle as temperatures of over 100 °C are required.

As a substantial number of biodegradable microneedles are classed polymers, a supposedly third fabrication technique called investment moulding has been used suitably for hollow non-biodegradable polymers in which a drug solution flows through the hollow part of the microneedles into the skin (Lippmann 2007; Lippmann and Pisano 2006). Melt injection processes in investment moulding are suitable for thermoplastics because in adaptation of micromoulding, very high shear is required to allow for lower viscous melt and low resistant flow but heat generation can cause degradation of the drug formulation (Zhao et al. 2003).

As mentioned earlier, currently there seems to be no lidocaine-loaded biodegradable microneedle polymer

systems published at present. Table 1 outlines the dissolvable or biodegradable materials as a vehicle for the drug and the method and conditions in manufacturing in-conjunction to significant dissolution or permeation results.

Possible biomaterials for controlled lidocaine release from microneedles

Lidocaine requires controlled release microneedles that allow for initial fast release into skin but reaches the desired plateau levels in which finite dosage is achieved. Therefore, the microneedles have to dissolve or disintegrate in the tissue fluids of physiological conditions at that site near the laceration before medics can treat the area by cleaning and suturing.



Table 1 Fabricated microneedles according	Table 1 Fabricated microneedles according to manufacture, dissolution and permeation of drug	eation of drug	
Microneedle materials	Methods of manufacture	Conditions of manufacture	Results of drug permeation or dissolution of vehicle
PLA, PLGA (50/50) and PEG unmixed initially (Park et al. 2007b)	Casting with PDMS (Park et al. 2007b; Xiangdong et al. 2009) SU-8* photoresist master (Natarajan et al. 2008), gold coating of 500 Å	Ultrasound pulses to weld polymer microparticles within mould to create porous structure (Park et al. 2007b). Vacuum pressure and oven heating for microneedle static shaping (Park et al. 2007b)	No publication found
Silk fibroin from B. mori c ocoons ^b (You et al. 2011)	Epoxy microneedle master from X-ray lithography to produce female PDMS ^c mould (You et al. 2011). Molten fibroin drug set into PDMS and mould removed (You et al. 2011)	Oven drying and vacuum pressure for shaping and solidifying microneedles (You et al. 2011)	No publication found.
Poly (methyl vinyl ether co-maleic acid) (Garland et al. 2012)	Blulase laser cutting for fabricated silicone elastomer moulds using Aluminium template (Garland et al. 2012)	40 °C heat for curing mould and centrifugation at 3,500 g for 15 min and microneedles dried for 24 h under ambient temperature (Garland et al. 2012)	In vitro studies with Neonatal procine skin reported 59 %, 39 % and 23 % cumulative release of caffeine, lidocaine and metronidazole respectively for combined concoction microneedles were tested (Garland et al. 2012)
20 % (w/w) aqueous blends of copolymer Gantrez [®] AN-139 (Donnelly et al. 2011)	Galvanometer controlled Excimer laser for variable height and interspacing of microneedle mould setup (Donnelly et al. 2011) Blulase laser cutting for fabricated silicone elastomer moulds using Aluminium template (Donnelly et al. 2011)	40 °C heat for curing mould and centrifugation at 3,500 g for 15 min and microneedles dried for 24 h under ambient temperature (Donnelly et al. 2011)	83 % of the drug, theophylline, contained in microneedles, permeated past the skin compared to 5.5 % with patch delivery over a 24 h period (Donnelly et al. 2011) The percentage is out of total drug loaded
Trehalose/mannitol (50:50 w/w), trehalose dihydrate/sucrose (75:25 w/w), trehalose/sucrose (75:25 w/w) and trehalose/sucrose (50:50 w/w) (Martin et al. 2012)	PDMS° mould created from wet etched silicon male master (Martin et al. 2012)	1 h vacuum pressure of (100 mbar) at room temperature conditions followed by 48 h dehydration without vacuum (Martin et al. 2012)	Sugar glass microneedles containing 2 % (w/w) methylene blue powder showed complete dissolution between 10 to 20 min after insertion into full thickness human skin (Martin et al. 2012)
Maltose monohydrate (1 g/ml) in deionised water (Lee et al. 2011b)	Stainless steel pillars and syringe pump to directly draw molten maltose into conical microneedles (Lee et al. 2011b)	Axial drawing at 400 µm/s for 1 s at 100 °C then 400 µm/s for 3 s at 96 °C, cooling to 60 °C and separation from attached support pillars at 700 µm/s (Lee et al. 2011b)	Optical micrography showed complete dissolution of maltose microneedle containing sulforhodamine B in guinea pig skin after 20 min (Lee et al. 2011b)
Maltose (analytical grade) in water (Kolli and Banga 2008)	Pre-fabricated inverse moulds formed by etching process (Texmac Inc)	Direct pouring of molten maltose at 95 °C into mould within one min and gradual cooling to 55 °C to prise out the mould from shaped microneedles (Kolli and Banga 2008; Miyano et al. 2005)	Nicardipine- hydrochloride loaded maltose microneedles recorded a mean flux of 7.05 µg/ml/h compared with control value of 1.72 µg/ml/h (Kolli and Banga 2008)

SU-8 is a high viscosity, negative based photo resist structure for moulding applications

 $^{^{}b}$ B. mori cacoons are natural silk cocoon fibrons spun by the silkworm, Bombyx mori

^c PDMS is a silicone based inert polymer material, polydimethylsiloxane

Drug molecules directly suspended in a well-mixed polymer microneedle matrix contribute to faster recorded time release than those encapsulated in microparticles followed by suspension in a second matrix vehicle as it is a two stage release mechanism with outer matrix dissolving first. For example, the time of drug release was 4 h when calcein was released from PLGA (85/15) obtained commercially in solid state via pre-processed moulded microneedles compared with the same drug encapsulated in NaCMC followed by PLGA which took 4 days (Garland et al. 2011; Park et al. 2006). The polymer and co-polymer monomeric ratios are influential in degradation for drug release. For example, single carbohydrate polymer poly-L-lactic acid (PLLA) with intrinsic viscosity

value 2.38 was acquired commercially as a solid and processed into films and showed significantly slower degradation by hydrolysis in the release of lidocaine compared with PLGA (80:20) films which controlled the release of over 60 % of lidocaine in 40 days (Loo et al. 2010). PLGA 50:50 microparticles loaded with lidocaine resulted in much faster controlled release of over 50 % in 10 days (Klose et al. 2010).

Lidocaine-loaded PLGA would be highly suitable for relieving long duration symptoms of skin irritation and discomfort caused by illnesses such as post-herpetic neuralgia, previously mentioned for commercially available lidoderm. PLLA's starting monomer, L-lactic acid (LLA), is derived using lactic acid bacteria (Garlotta 2001; Roy et al. 1982). The distinct

Table 2 Polymer biodegradation and morphology according to physiological plasma fluid conditions

Polymer	Morphological properties	Degradation studies in physiological ^a conditions
Poly–ε-caprolactone (PCL)	Injection moulded matrix, films and shre settings (Wahit et al. 2012)	General long term degradation from weeks to months (Dash and Konkimalla 2012). In vivo degradation cannot occur readily due to unavailability of desired enzymes and surface erosion caused by hydrolysis is the primary mechanism and the main reason for slow degradation of PCL (Ginde and Gupta 1987; Woodruff and Hutmaker 2010)
PLLA	200 micron and 20 micron films (Mattioli et al. 2012)	5 % weight loss by hydrolytic degradation after 49 days (Mattioli et al. 2012)
Mixed mPEG5000–PSA ^b and mPEG2000–PLLA ^c (Lai et al. 2012)	Spherical micelles with hydrophobic matrix and hydrophilic exterior layer (Lai et al. 2012)	Degradation measured from calculation percentage release of curcumin in PBS ^d . Burst release of curcumin near to 40 %. Maximum 75 % approximate release of curcumin on day 15 (Lai et al. 2012)
$P(LLA-co-\varepsilon CL)^{e}$ and $P(LLA-b-\varepsilon CL)^{f}$ (Choi et al.	240 micron thick films (Choi et al. 2002) Smooth surface Microspheres (Kalpan	No degradation studies carried out at physiological conditions so far
2002). P(LLA- <i>co</i> -ε CL) (90/10)	et al. 2007) Comb graft polymer films of 110 -120 microns (Dai et al. 2009)	60 % decrease by hydrolytic degradation in molecular weight after 112 days (Kalpan et al. 2007)
(Kalpan et al. 2007)		55 % weight loss after 70 days (Dai et al. 2009)
PHCL-g-PLLA ^g (Dai et al. 2009)		
PLGA	5,600 micron diameter Sirolimus ^h loaded films (Ro et al. 2012)	25 % weight loss after 13 days for Sirolimus loaded PLGA 50:50 (Ro et al. 2012)
		22 % mass loss after 55 days for Sirolimus loaded PLGA 75/25 (Ro et al. 2012)

^a Conditions refer to a plasma fluid of pH 7 and temperature of 37 °C

^h Sirolimus is an immunosuppressant drug



^b Methoxy poly(ethylene glycol) (mPEG), 5,000 Daltons, Poly(sebacic anhydride) (PSA)

^c Methoxy poly(ethylene glycol) (mPEG), 2,000 Daltons. Poly-L-lactide (PLLA)

^d Phosphate buffer solution, pH 7.4

^e P(LLA-b-_CL) is a diblock co-polymer with MW 15,200

^f P(LLA-co-_CL) is a random polymer with MW 51,000

^g PHCL-g-PLLA poly(4-hydroxyl-e-caprolactone-*co*-e-caprolactone)-g-poly(L-lactide)

synthetic step in the production of PLLA is the condensation polymerisation of LLA in which ester linkages between LLA monomers are formed and water is the by product (Mehta et al. 2005; Garlotta 2001). PLGA is synthesized by the mechanism of structural ring opening polymerisation of DL-lactide and glycolide by catalysis from stannous 2-ethyl hexanoate in conjunction with a molecular weight-regulating additive, triphenylsilanol with the overall objective of consistent chain length and reduction of side branch chains (Ouyang et al. 2011; Mazarro et al. 2009).

Biodegradation in the context for polymers is the breakdown of a high molecular weight molecule into smaller components of low molecular weight molecules caused by enzymes from microorganisms and/or environmental catalysts (Luckachan and Pillai 2011; Wang et al. 2003). Table 2 provides a summary of biodegradable polymer systems with respect of morphological properties and biodegradation measurements while physiological conditions according to plasma fluid are kept constant. The overall trend from

Table 2 shows that the degradation is faster for PLLA blends than PLLA itself. Also, it seems that PLGA 50:50 is much faster degrading than PLGA 75:25.

Tensile properties of biodegradable microneedles

Dissolvable/biodegradable microneedles require quality testing to determine the maximum direct force required on the base unit before fracturing or crumbling occurs from the tip to the body of the microneedles. Such a test can be done using an axial load testing station which relies on gradually moving the microneedles into a block of metals (e.g. aluminium) until needle breakages are evident (Bariya et al. 2011). A measured section of the metal block contains a predetermined thickness of skin attached by dual sticky tape and the other section of the block is connected to a compression cell containing microneedles and motorised actuator. The actuator provides a method for constant speed of microneedles insertion into the skin with the output measurement as force (Khanna et al.

Table 3 Mechanical force properties of microneedle materials and force test results of the microneedle systems

Microneedle system	Component with external force tolerance	Results of force tests
Polylactic acid (PLA) (Wang and Jeng. 2009)	Injection grade PLA (Wang and Jeng 2009)	73.11 % impact on structural due to melt temperature variable (Wang and Jeng 2009)
NIPAAm ^a based hydrogel loaded into Poly lactic- <i>co</i> -glycolic acid (PLGA) (Kim et al. 2012)	Mainly PLGA (Kim et al. 2012)	PLGA microneedles with 18 % v/v hydrogel deformed less than the 31 % v/v hydrogel ones (Kim et al. 2012)
Sugar glass disaccharide mixture of two sugar components except xylitol (Martin et al. 2012)	Similar molecular weight of two specific disaccharides that formed solid sugar (Martin et al. 2012)	Qualitative skin penetration tests showed most microneedles penetrated skin and complete dissolution in skin after 10 min (Martin et al. 2012)
Polyvinylpyrrolidone (PVP), PLGA, PVA (Ke et al. 2012)	PVP (10,000 MW) (Ke et al. 2012)	Microneedles fabricated with 600 mg/ml and 1,000 mg/ml PVP were robust as confirmed from SEM images after insertion. The latter PVP concentration showed no geometric change (Ke et al. 2012)
PVP, PVP-MAA ^b poly(vinyl pyrrolidone- <i>co</i> -methacrylic acid (Sullivan et al. 2008)	PVP (8,970 MW), MAA (Sullivan et al. 2008)	Displacement force tests proved that 1 % MAA in PVP-MAA contributed to nearly double the strength of PVP alone (Sullivan et al. 2008)
PVA/PVP blends (Chu et al. 2010)	PVA (2,000 MW) (Chu et al. 2010)	Qualitative skin penetration tests showed 80 % of microneedle tips of length 450 μ m dissolved in porcine skin after 2 min with bright field microscopy (Chu et al. 2010)

^a N-isopropylacrylamide (NIPAAm)



^b Poly (vinyl pyrrolidone-co-methacrylic) acid

2010). A number of components have been used to control tensile strength of dissolving microneedles as shown in Table 3.

Conclusions

Although a number of lidocaine-based transdermal products can be found in the market there is a large gap for lidocaine microneedle products, especially biodegradable microneedles. This implies that considerable amount of new research is required at the developmental and pre-clinical setting in order to achieve the desired controlled release of lidocaine into skin and maintain a steady drug concentration for a short duration of time for the purpose of superficial suturing of a cut. A biodegradable lidocaine microneedle system formulated from carboxymethylcellulose demonstrated the increase in pharmacokinetic permeation flux, thus highlighting further interest in research of other biodegradable materials as drug vehicles for lidocaine with the aim of achieving faster permeation kinetics in skin with the general idea of a minimal delayed therapeutic action. Also, the development of lidocaine microneedles may provide a scope for a cheaper product as compared with current EMLA formulations containing lidocaine in which a second local anaesthetic, prilocaine add to the material costs.

Manufacturing of biodegradable microneedles via a casting process with usage of SU-8 or PDMS moulds is economical mainly because these moulds can be reused numerous times in mass production of biodegradable microneedles. The mechanical penetration strengths are a highly important physical challenge seen in biodegradable microneedles. Not only is a sharp tip of microneedle necessary for cutting through skin but the casted, dissolvable material requires adequate resistant to compression forces that mimic finger or thumb pressures. Dissolvable materials with soft solid or brittle physical properties require mucoadhesive co-polymer agents, such as PVA or PVP, in the mixture to provide for mechanical strength.

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