



# Mitigation of hazardous ammonia and hydrogen sulphide emissions using carbon based nanometal oxides adsorbents

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## Abstract

Carbon based nano TiO<sub>2</sub>-ZnO composite adsorbents were developed and evaluated for simultaneous adsorption of ammonia (NH<sub>3</sub>) and hydrogen sulphide (H<sub>2</sub>S). Screening of composites with different ZnO and TiO<sub>2</sub> loadings in terms of adsorption capacities identified a composite with 10% ZnO and 5% TiO<sub>2</sub> (10ZnO-5TiO<sub>2</sub>-AC) as the most suitable. Breakthrough experiments with pre-mixed gases containing 50 to 550 mg L<sup>-1</sup> of each NH<sub>3</sub> and H<sub>2</sub>S at 22 to 280 °C showed that increase in NH<sub>3</sub> and H<sub>2</sub>S concentrations led to higher equilibrium adsorption capacities for both gases. Increase of temperature decreased NH<sub>3</sub> equilibrium adsorption capacity but for H<sub>2</sub>S higher values were observed at higher temperatures. The highest equilibrium adsorption capacity of 5.71 mg NH<sub>3</sub> g<sup>-1</sup> was obtained with a mixture of 500 ppmv NH<sub>3</sub> and 550 ppmv H<sub>2</sub>S at 22 °C, while for H<sub>2</sub>S the highest value of 29.64 mg H<sub>2</sub>S g<sup>-1</sup> was seen with a mixture of 300 ppmv NH<sub>3</sub> and 300 ppmv H<sub>2</sub>S at 280 °C. Multicomponent Langmuir isotherm described the simultaneous adsorption of NH<sub>3</sub> and H<sub>2</sub>S with the high level of accuracy. The negative value of enthalpy of adsorption for NH<sub>3</sub> confirmed the exothermic and potentially physical nature of ammonia adsorption, while a positive value for H<sub>2</sub>S adsorption pointed out to the endothermic and chemisorption nature of this process. Examination of fresh and exposed composite adsorbents by XRD and FTIR confirmed the chemical nature of H<sub>2</sub>S adsorption.

**Keywords** NH<sub>3</sub> and H<sub>2</sub>S emissions · Nano metal oxides · Carbon-based nanoadsorbent · Multicomponent isotherm

## 1 Introduction

Ammonia (NH<sub>3</sub>) and hydrogen sulphide (H<sub>2</sub>S) are two toxic and environmentally hazardous gases that co-exist in emissions from livestock operations, landfills, wastewater treatment plants and sewage sludge [5, 9, 13, 26]. Simultaneous presence of ammonia and hydrogen sulphide in biogas, fuel gases generated from biomass gasification and coke oven gas is also well documented [5, 13]. Concentrations of NH<sub>3</sub> and H<sub>2</sub>S in these emissions depend on the source and could vary in the range 2–14,000 and 4–2174 ppm, respectively [9, 13]. Apart from detrimental effects on the human and animal

health and severe corrosivity that could damage transportation and storage equipment, NH<sub>3</sub> and H<sub>2</sub>S emissions contribute to the formation of primary air pollutants such as SO<sub>x</sub> and NO<sub>x</sub>, and other air pollutants classified as photochemical oxidants. Processes for the treatment of gases contaminated with both NH<sub>3</sub> and H<sub>2</sub>S can be classified as biological and physicochemical processes. Application of biological processes have been reported for treating a mixture of NH<sub>3</sub>, H<sub>2</sub>S, butyric acid, and ethyl mercaptan [9], removal of NH<sub>3</sub> and H<sub>2</sub>S from wastewater treatment plant emissions [2], tannery emissions [8], odorous gases from a domestic waste landfill site [29], raw biogas [5], and for the deodorization of compost [10]. The focal point of physicochemical treatments has been mainly on adsorption of NH<sub>3</sub> and H<sub>2</sub>S by carbon-based adsorbents [3, 6] and catalytic oxidation by metal oxides [14, 15, 20]. A close look at previous studies on simultaneous removal of NH<sub>3</sub> and H<sub>2</sub>S by carbon-based adsorbents and metal oxide catalyst-sorbent, as outlined in a recent review article [13] reveals that these works have been conducted at high gas concentrations (5000 ppmv NH<sub>3</sub> and 10,000 ppmv H<sub>2</sub>S) and high temperatures (650 to 800 °C).

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Considering that in many practical cases such as emissions from livestock operations, raw biogas, and emissions from landfills much lower concentrations of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  are encountered and the emitted gases are at lower temperatures, it is important to investigate the simultaneous removal of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  for the lower ranges of concentration and temperature and verify the effects of gas concentration and temperature on the effectiveness of the treatment process.

As part of an earlier work, we have investigated the effectiveness of pure (commercial)  $\text{TiO}_2$  and  $\text{ZnO}$  nanoparticles mixture for simultaneous removal of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  from gases simulating the emissions from livestock operations for a range of gas mixture concentrations and temperatures [26]. Given the challenges associated with the use and handling of pure nanoparticles in large-scale treatment systems and their high cost, in the present work carbon-based nano metal oxide adsorbents, hereinafter referred to as  $\text{ZnO-TiO}_2\text{-AC}$ , were synthesized and used for simultaneous capture of  $\text{NH}_3$  and  $\text{H}_2\text{S}$ . Effects of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  concentrations (50–500  $\text{mg L}^{-1}$  of each gas in mixture) and temperature (22–280 °C) on the adsorption process were investigated. Examination of fresh and exposed adsorbents with XRD and FTIR allowed us to develop an insight on the nature of adsorption processes. Finally, the Langmuir multicomponent adsorption isotherm was used to describe the simultaneous adsorption of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  and the important adsorption and thermodynamic parameters were determined.

## 2 Materials and methods

### 2.1 Chemicals and gases

Zinc nitrate hexahydrate (98%,  $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ ; CAS# 10196-18-6) and titanium isopropoxide (97%,  $\text{Ti}[\text{OCH}(\text{CH}_3)_2]_4$ ; CAS# 546-68-9) were obtained from Sigma-Aldrich and used as precursors of zinc oxide ( $\text{ZnO}$ ) and titanium oxide ( $\text{TiO}_2$ ), respectively. Activated charcoal (Darco G-60; CAS# 7440-44-0) with 100 mesh size (particle size < 0.149 mm) was from Fisher Scientific and used together with zinc nitrate hexahydrate and titanium isopropoxide to synthesize the  $\text{ZnO-TiO}_2\text{-AC}$  composite adsorbents. Ammonia (1000 ppmv) and hydrogen sulfide (1000 ppmv) gases, each balanced with He, and industrial grade He (99.99%) were obtained from Air Liquide, and PraxAir, Canada, respectively and used to perform the adsorption experiments.

### 2.2 Synthesis of nano $\text{ZnO-TiO}_2\text{-AC}$ composite adsorbents

Sol-gel method was used for the synthesis of nano  $\text{ZnO-TiO}_2\text{-AC}$  adsorbents with different compositions of 10%  $\text{ZnO}$  and 5%  $\text{TiO}_2$ , 15%  $\text{ZnO}$  and 5%  $\text{TiO}_2$  and 15%  $\text{ZnO}$  and 10%  $\text{TiO}_2$ . The synthesis was carried out using two solutions containing the  $\text{TiO}_2$  and  $\text{ZnO}$  precursors at the stoichiometric level required for the designated metal oxide loading on 10 g activated carbon [16]. Solution A was prepared by dissolving the stoichiometric quantity of titanium isopropoxide (as  $\text{TiO}_2$  precursor) in 30 mL pure ethanol. Solution B was made by dissolving the stoichiometric amount of zinc nitrate hexahydrate (as  $\text{ZnO}$  precursor) in a mixture of 67.5 mL pure ethanol, 2 mL of acetic acid, and 7.2 mL of deionized water. The dissolution in either case was done by vigorous mixing at room temperature for one hour. This was followed by drop-wise addition of solution A to solution B and mixing over a period 30 min until a homogeneous solution was obtained. Activated carbon (10 g) was then added to this solution. The mixture was stirred for 2 h and left at room temperature for 24 h for gelation to occur. The resulting gel was separated from the liquid by vacuum filtration and washed with ethanol and water. The gel was dried at 120 °C for 12 h and calcined at 450 °C for 2 h under Argon atmosphere. Finally, the calcined solid ( $\text{ZnO-TiO}_2\text{-AC}$  composite) was crushed and sieved to obtain a powder with 100 mesh particle size [22]. The prepared composites were analyzed for  $\text{ZnO}$  and  $\text{TiO}_2$  contents by an external laboratory (SRC Geoanalytical Laboratories, SK, Canada).

### 2.3 Experimental set-up for adsorption study

The adsorption experimental set-up used in this work has been described elsewhere [26]. In summary, as shown in Fig. 1, the main part of the experimental set-up was a pyrex glass adsorption column (diameter: 1.27 cm and height: 29.5 cm) that was equipped with heating tape (HTS-Ampetek Co., USA) and a temperature controller (Omega K type, Stamford, USA), a differential pressure transducer and pressure gauges (Honeywell, USA). Three gas cylinders containing  $\text{NH}_3$  (1000 ppmv, balanced with He),  $\text{H}_2\text{S}$  (1000 ppmv, balanced with He), and He (99.99% purity) with stainless steel connection tubes and associated mass flow controllers (Model GFC17, Aalborg Instruments and Controls, USA) were used to supply the feed gas mixtures with the designated composition into the adsorption column [26]. The treated gas (outlet) was connected to a gas chromatograph for real time measurement of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  concentrations. A bypass line and two valves were devised to determine the concentrations of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  in the feed (inlet) gas. To

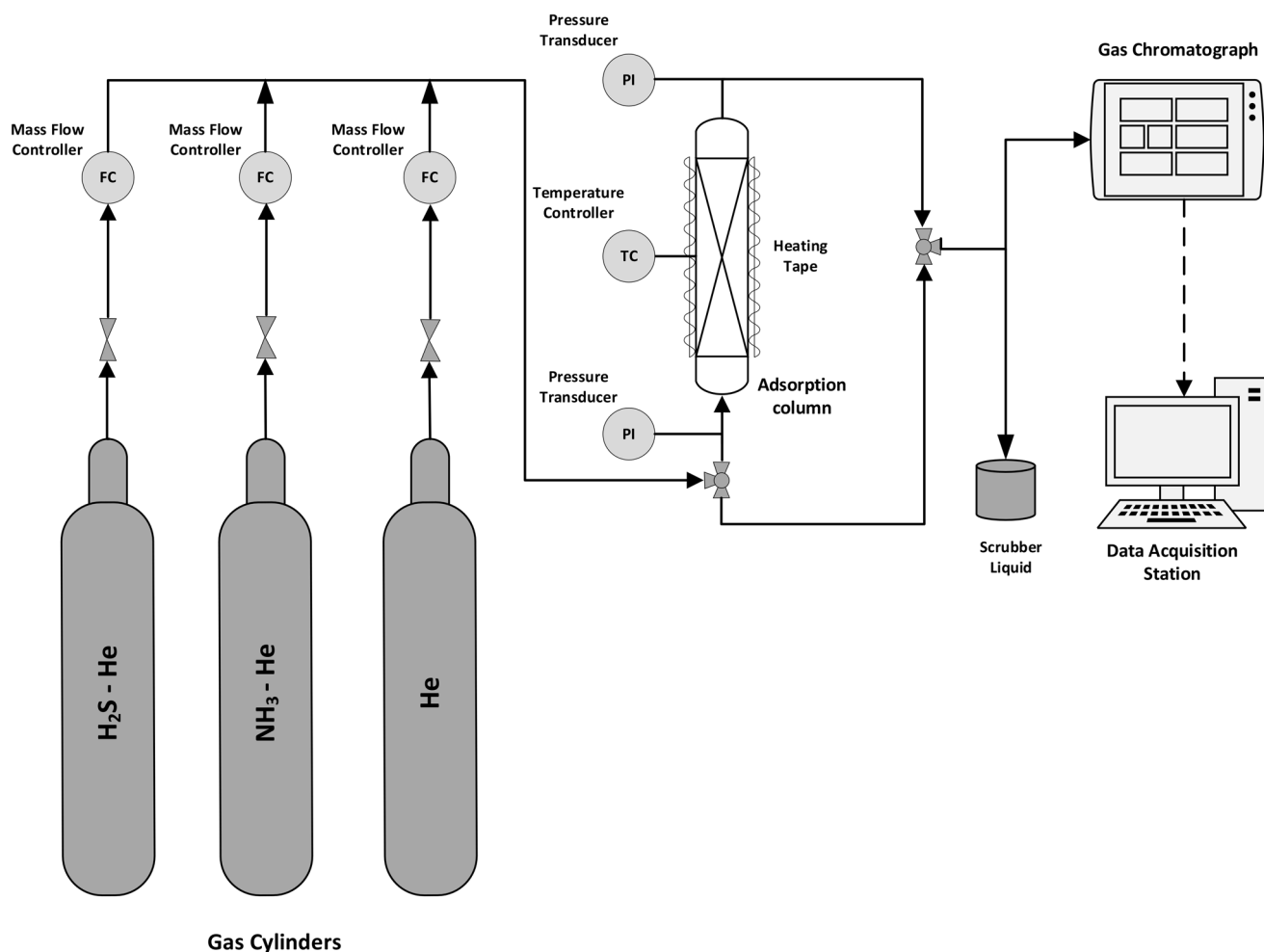


Fig. 1 Schematic flow diagram of the experimental set-up

prevent unintentional release of the hazardous gases into the environment and ensure safety, the experimental set-up and gas cylinders were placed inside a walk-in fume hood.

## 2.4 Experimental procedures

Adsorption experiments were carried out in two parts. First, the synthesized  $ZnO-TiO_2-AC$  composites of different composition were evaluated for their ability in simultaneous removal of  $NH_3$  and  $H_2S$ . This was done by conducting adsorption experiments at room temperature (22 °C), using a feed gas mixture with 500 ppmv  $NH_3$  and 550 ppmv  $H_2S$ , balanced with He. A set of control experiments was also conducted with activated carbon (no  $ZnO$  or  $TiO_2$ ) that had undergone calcination, crushing and sieving in a similar fashion to that of composite adsorbents. The composite with the best performance in terms of  $NH_3$  and  $H_2S$  adsorption capacities and preferably lower  $ZnO$  and  $TiO_2$  contents was then identified and used for evaluating the effects of  $NH_3$  and  $H_2S$  concentrations (50–50, 100–100, 200–200,

300–300, 400–400, 500–550 ppmv  $NH_3$  and  $H_2S$ ) and temperature (22, 70, 140 and 280 °C) on simultaneous removal of  $NH_3$  and  $H_2S$ . The evaluated  $NH_3$  and  $H_2S$  concentrations (50–500 ppmv) and temperatures (22–280 °C) covered the typical values observed in the emissions from livestock operations and industrial settings such as wastewater treatment plants and anaerobic digesters for production of biogas. Additionally, they were consistent with those applied in our previous work on simultaneous removal of  $NH_3$  and  $H_2S$  with commercial (pure)  $ZnO$  and  $TiO_2$  nanoparticles [26], thus allowing the comparison of the results. It should be emphasized that at each temperature all five gas combinations were tested.

The experimental procedure was the same in all cases and included the loading of adsorption column with a mixture of 0.2 g composite adsorbent and 0.8 g silicon carbide (125 micron). The rationale for addition of silicon carbide and the chosen ratio is given elsewhere [23, 26]. To support the adsorbent and to prevent its carry over by the flowing gas, the adsorbent was sandwiched between two layers

of glass wool followed by glass beads that filled the empty space below and above the adsorbent layer [23, 26]. The adsorption column was heated at 70 °C under helium flow for one hour to remove any adsorbed water. This was followed by adjusting the temperature to desired value and introducing the gas mixture with the designated composition into the column at a total flow rate of  $100 \pm 0.2$  mL  $\text{min}^{-1}$  [23]. The concentrations of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  in the outlet gas was monitored in real time, using the gas chromatograph. Experimental run was stopped once breakthrough for both gases occurred (i.e., less than 1% change in  $\text{NH}_3$  and  $\text{H}_2\text{S}$  concentrations). Concentrations of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  in the inlet gas (feed) were also measured at the beginning, during and at the end of each experimental run to ensure there was no deviation from the designated values. Another set of control experiments was conducted with calcined AC with a gas mixture containing 500 ppmv  $\text{NH}_3$ -550 ppmv  $\text{H}_2\text{S}$  at 22, 70, 140, and 280 °C.

The experimental data generated in each run were used to calculate the equilibrium adsorption capacities for  $\text{NH}_3$  and  $\text{H}_2\text{S}$ . This was done by numerical integration of breakthrough curves, using MATLAB R2006a software. Calculation procedure including the relevant mathematical expression have been described elsewhere [23]. The fresh (unused) and spent adsorbents after exposure to 500 ppmv  $\text{NH}_3$  and 550 ppmv  $\text{H}_2\text{S}$  at 22 and 280 °C (lowest and highest temperatures) were examined for their BET surface area and pore volume, X-ray diffraction (XRD), and FT-IR spectra. The fresh (unused) adsorbent was also examined by transmission electron microscopy (TEM) to determine the particle size distribution of metal oxides on activated carbon.

## 2.5 Analysis and characterization methods

A Varian Gas Chromatograph (Varian 3800, USA) with a thermal conductivity detector (TCD) connected to a CP-Pora PLOT Amines column (Agilent Technologies, CP7591) was used to measure the concentrations of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  in real time. The GC oven and TCD filament temperatures were set at 120 °C and 220 °C, respectively. The carrier gas flowrate (helium) was maintained at  $10$  mL  $\text{min}^{-1}$  and a split ratio of 1 was used. Automatic gas sampling was carried out in 6.5 min intervals which allowed sufficient time for elution of  $\text{NH}_3$  and  $\text{H}_2\text{S}$ , before the next sampling event [26].

BET surface area and pore volume of fresh and selected exposed composite adsorbents were determined by a Micromeritics ASAP 2000 instrument. BET surface was determined using adsorption data for nitrogen at partial pressures of 0.05 and 0.3 ( $P/P_{\text{atm}}$ ). Total pore volume was calculated using the amount of nitrogen adsorbed at a partial pressure of 0.95. Fresh and selected exposed composites were also

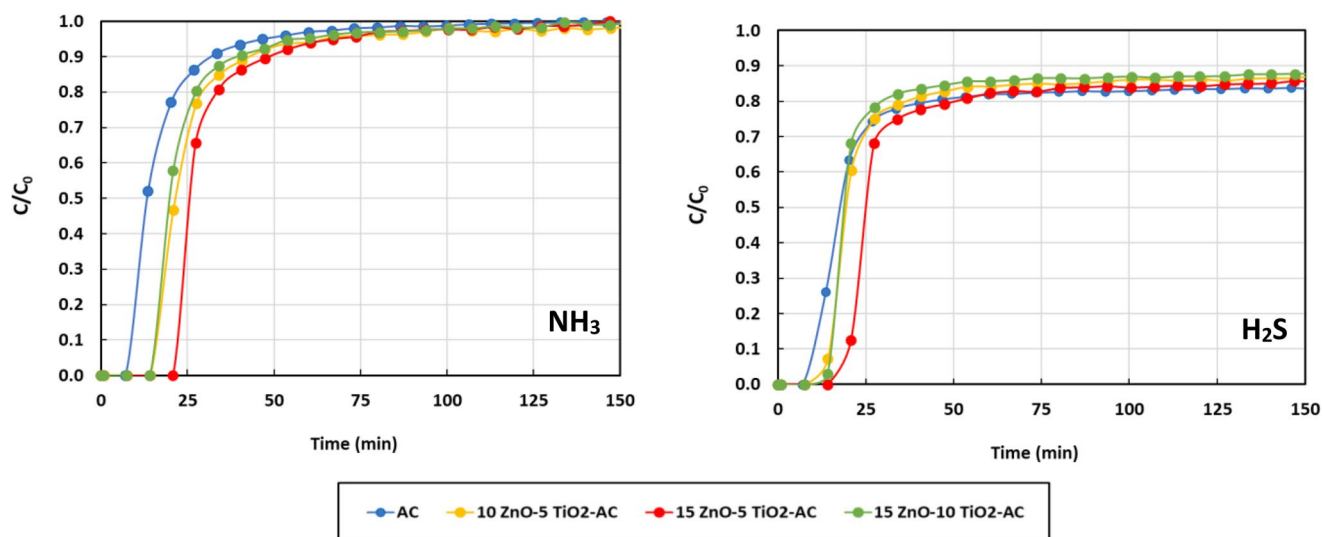
examined by a D8-Advance Bruker Diffractometer XRD with a Cu  $K\alpha$  detector (Bruker, USA), and a Fourier-Transform Infrared (FTIR) spectrometer (Bruker Vertex 70, USA). The  $2\theta$  range for the XRD was 10–80° with a step size of 0.02°, and the FTIR was employed in the range of 400–4000  $\text{cm}^{-1}$  at 4  $\text{cm}^{-1}$  resolution. Finally, the unused composite adsorbent was examined by transmission electron microscopy (TEM), using a microscope (JEOL, 200 kV, USA), equipped with EDAX energy dispersive X-ray system (Genesis, USA) for EDS analysis. TEM micrographs were analyzed by Microstructure Measurement software to generate the particle size distribution of metal oxides.

## 3 Results and discussion

### 3.1 Performance of synthesized composite adsorbents

Figure 2 presents the  $\text{NH}_3$  and  $\text{H}_2\text{S}$  breakthrough curves obtained with synthesized composites and calcinated activated carbon. Information on the metal oxides loading of each synthesized adsorbent and important adsorption characteristics including breakthrough times and equilibrium adsorption capacities for each adsorbent are provided in Table 1. Measurement of ZnO and  $\text{TiO}_2$  contents of the synthesized adsorbents showed that the actual metal oxide loadings deviated slightly from the nominal loadings, despite the careful preparation and post treatment. Examination of the breakthrough curves and the associated data that are included in Table 1 showed that with all synthesized adsorbents,  $\text{H}_2\text{S}$  breakthrough time was shorter than that for  $\text{NH}_3$ . In case of calcined AC, the breakthrough of  $\text{NH}_3$  and  $\text{H}_2\text{S}$  occurred closely but the breakthrough times were substantially shorter than those observed with the composites, indicating better performance of the composite adsorbents.

As far as the equilibrium adsorption capacities were concerned, all adsorbents including calcined AC displayed substantially higher capacities for  $\text{H}_2\text{S}$  when compared with  $\text{NH}_3$ . To be more specific, the  $\text{H}_2\text{S}$  adsorption capacities with all composite adsorbents were 4–5 folds higher than that for  $\text{NH}_3$  and more than 7 folds higher with AC. Among the three synthesized composites, the 10ZnO-5 $\text{TiO}_2$ -AC composite showed the highest  $\text{NH}_3$  and  $\text{H}_2\text{S}$  equilibrium adsorption capacities, despite the lowest metal oxides content. The adsorption capacities obtained for 15ZnO-5 $\text{TiO}_2$ -AC and 15ZnO-10 $\text{TiO}_2$ -AC were close. The observed  $\text{NH}_3$  adsorption capacity of 10ZnO-5  $\text{TiO}_2$ -AC composite was 61% higher than that of calcined activated carbon (5.30 vs. 3.29 mg  $\text{NH}_3$   $\text{g}^{-1}$ ) but was around 5% lower in the case of  $\text{H}_2\text{S}$  (22.24 vs. 23.67 mg  $\text{H}_2\text{S}$   $\text{g}^{-1}$ ). It is also important to re-emphasize that the breakthrough times with this composite



**Fig. 2** Ammonia (left panel) and hydrogen sulphide (right panel) breakthrough curves for synthesized ZnO-TiO<sub>2</sub>-AC composites and calcined activated carbon (AC). Inlet gas composition: 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S- balanced He, temperature: 22 °C

**Table 1** Comparison of breakthrough times and adsorption capacities of ZnO-TiO<sub>2</sub>-AC composites with different ZnO and TiO<sub>2</sub> loadings. Adsorption experiments were conducted with a feed gas mixture of 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S at 22 °C. Data for calcined AC included in this table have been obtained under similar conditions

Adsorbent	Nominal loading of ZnO and TiO <sub>2</sub> (%)	Actual loading of ZnO and TiO <sub>2</sub> (%)	NH <sub>3</sub> breakthrough time (min)	Equilibrium adsorption capacity(mg NH <sub>3</sub> g <sup>-1</sup> )	H <sub>2</sub> S breakthrough time(min)	Equilibrium adsorption capacity(mg H <sub>2</sub> S g <sup>-1</sup> )
10ZnO-5TiO <sub>2</sub> -AC	10 and 5%	8.4 and 6.0%	14.1	5.30	11.5	22.24
15ZnO-5TiO <sub>2</sub> -AC	15 and 5%	15.8 and 5.6%	20.8	4.50	14.1	21.57
15ZnO-10TiO <sub>2</sub> -AC	15 and 10%	14.9 and 8.5%	14.1	4.22	13.5	21.33
Calcined AC*	-	-	7.4	3.29	7.0	23.67

\*AC: Activated carbon

were substantially higher than those for calcined AC (14.1 vs. 7.4 min for NH<sub>3</sub> and 11.5 vs. 7.0 min for H<sub>2</sub>S). Given the better performance of 10ZnO-5TiO<sub>2</sub>-AC and its lowest metal oxides contents, this composite adsorbent was selected to assess the effects of NH<sub>3</sub> and H<sub>2</sub>S concentrations and temperature on simultaneous removal of these gases and for developing the adsorption isotherms.

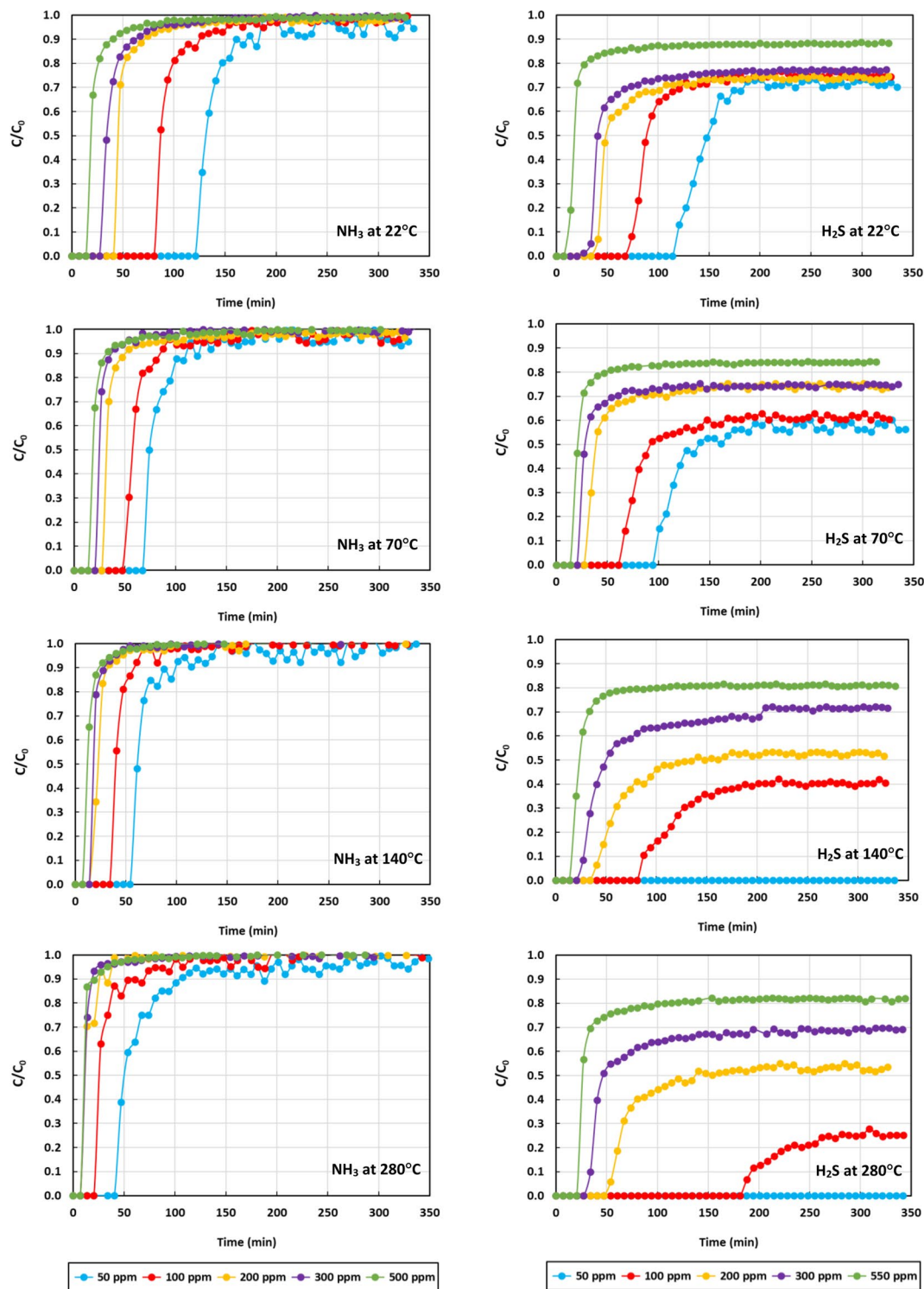
### 3.2 Adsorption isotherms for 10ZnO-5TiO<sub>2</sub>-AC composite

Figure 3 presents the NH<sub>3</sub> and H<sub>2</sub>S breakthrough curves obtained with 10ZnO-5TiO<sub>2</sub>-AC composite at different gas compositions and temperatures. The breakthrough times and equilibrium adsorption capacities for each set of conditions are summarized in Table 2. Ammonia breakthrough curves (Fig. 3, left panels) and data compiled in Table 2 show that increases in NH<sub>3</sub> concentration and temperature shifted the curves to the left, a clear indication of decrease in breakthrough time. The effect of NH<sub>3</sub> concentration on the breakthrough time was more pronounced at lower

temperatures. For instance, at 22 °C the breakthrough time decreased from 120.7 to 13.8 min when NH<sub>3</sub> concentration increased from 50 to 500 ppmV but the corresponding values at 280 °C were 40.4 and 7.1 min, respectively. Based on the data compiled in Table 2, the equilibrium adsorption capacity of 10ZnO-5TiO<sub>2</sub>-AC composite for NH<sub>3</sub> showed an increasing trend with increase of NH<sub>3</sub> concentration, but temperature had an opposing effect and lower adsorption capacities were seen with the increase in temperature. Specifically, the highest adsorption capacity of 4.60–5.71 mg NH<sub>3</sub> g<sup>-1</sup> was achieved with 500 ppmv NH<sub>3</sub> at 22 °C.

As seen in Fig. 3 (right panels), the impact of H<sub>2</sub>S concentration on breakthrough time was similar to that of NH<sub>3</sub> and shorter breakthrough times were observed as H<sub>2</sub>S concentration was increased but there were several distinctions between NH<sub>3</sub> and H<sub>2</sub>S. First, with 50 ppmv H<sub>2</sub>S, breakthrough did not occur at 140 and 280 °C, even after a prolonged period of experiment. Second, the H<sub>2</sub>S breakthrough curves were not as steep as those for NH<sub>3</sub> and although plateau region was observed, adsorbent never reached the saturation state (C/C<sub>0</sub> = 1) under any conditions. The ultimate





**Fig. 3** Ammonia (left panels) and hydrogen sulphide (right panels) breakthrough curves obtained with 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent at different gas concentrations and temperatures

value of  $C/C_0$  was dependent on concentration of H<sub>2</sub>S, with the higher  $C/C_0$  values observed at higher H<sub>2</sub>S concentrations. These trends that are consistent with those obtained in our earlier work on with a mixture of pure ZnO and TiO<sub>2</sub>

nanoparticles [26], is likely due to the chemical reaction between H<sub>2</sub>S and ZnO (chemisorption) and the endothermic nature of this reaction, where higher temperatures lead to faster reaction rates. In fact, examination of the exposed

**Table 2** Comparison of breakthrough times and adsorption capacities of composite 10ZnO-5TiO<sub>2</sub>-AC, commercial (pure) ZnO and TiO<sub>2</sub> nanoparticles mixture [26], and calcined AC. Equilibrium adsorption capacities are not reported when breakthrough did not occur

NH <sub>3</sub> -H <sub>2</sub> S concentrations(ppmv)	Temperature (°C)	NH <sub>3</sub> breakthrough time(min)				Equilibrium adsorption capacity(mg NH <sub>3</sub> g <sup>-1</sup> )				H <sub>2</sub> S breakthrough time(min)				Equilibrium adsorption capacity(mg H <sub>2</sub> S g <sup>-1</sup> )				
		10 ZnO-5 TiO <sub>2</sub> -AC	AC	ZnO & TiO <sub>2</sub> mixture	10 ZnO-5 TiO <sub>2</sub> -AC	10 ZnO-5 TiO <sub>2</sub> -AC	AC	ZnO & TiO <sub>2</sub> mixture <sup>a</sup>	10 ZnO-5 TiO <sub>2</sub> -AC	10 ZnO-5 TiO <sub>2</sub> -AC	AC	ZnO & TiO <sub>2</sub> mixture <sup>a</sup>	10 ZnO-5 TiO <sub>2</sub> -AC	AC	ZnO & TiO <sub>2</sub> mixture <sup>a</sup>	10 ZnO-5 TiO <sub>2</sub> -AC	AC	ZnO & TiO <sub>2</sub> mixture <sup>a</sup>
50-50	22	120.7		358.9		2.54	6.92	114	199.7	6.74	14.55							
	70	67.3		233		1.55	6.04	94.2	272.9	7.26	20.56							
	140	54.0		246.8		1.31	5.22	-	446.3	-	-							
100-100	280	40.4		-		1.26	-	-	-	-	-							
	22	80.5		192.6		3.39	8.06	67.1	126.5	10.35	18.88							
	70	47.2		153.4		2.28	6.9	60.6	153.4	12.1	28.49							
200-200	140	33.9		132.4		1.53	6.18	80.8	278.22	16.71	38.29							
	280	20.3		40.7		1.24	1.35	181.4	604	21.45	-							
	22	40.7		100.9		3.72	9.67	34.0	40.8	17.15	19.23							
300-300	70	27.2		87.5		2.85	8.31	27.2	87.5	15.95	30.59							
	140	13.7		60.4		1.56	7.41	33.8	139.9	18.34	49.36							
	280	7.1		27.4		0.94	1.67	47.1	207.3	26.50	-							
500-550	22	27.0		73.9		4.38	11.27	20.3	27.3	22.49	20.62							
	70	20.4		67.3		2.95	10.14	20.4	34.1	22.25	30.21							
	140	13.7		40.7		1.92	5.69	20.5	80.5	27.32	45.56							
500-550	280	7.1		27.5		1.41	3.7	27.3	193.6	29.64	-							
	22	13.8		7.0		4.60-5.71 <sup>b</sup>	3.29	7.3	7.1	20.52-22.24 <sup>b</sup>	23.67							
	70	13.6		7.0		4.13	2.44	13.6	6.9	23.93	21.81							
500-550	140	7.0		6.9		2.43	1.87	13.6	7.1	26.70	52.31							
	280	7.1		6.9		2.22	1.83	20.4	13.5	28.40	23.44							

<sup>a</sup> The adsorption capacities reported by Valdes Labrada et al. [26] are calculated by assuming that NH<sub>3</sub> was exclusively adsorbed by TiO<sub>2</sub> nanoparticles and H<sub>2</sub>S was adsorbed only by ZnO nanoparticles. <sup>b</sup> Experiments for this set were done twice

adsorbents by XRD and FTIR, as presented in the latter parts of this article, confirmed the validity of this speculation. The increase in H<sub>2</sub>S concentration and temperature both enhanced the H<sub>2</sub>S adsorption capacity of 10 ZnO-5 TiO<sub>2</sub>-AC. This indicated that while the impact of concentration was similar to the trend observed for NH<sub>3</sub>, the temperature effect was opposite of that for NH<sub>3</sub>.

Included in Table 2 are also the NH<sub>3</sub> and H<sub>2</sub>S breakthrough times and equilibrium adsorption capacities obtained for the calcined activated carbon when exposed to a gas mixture containing 500 ppmv NH<sub>3</sub>-550 ppmv H<sub>2</sub>S at 22 to 280 °C (control experiments). Comparing these data with the corresponding values for 10ZnO-5TiO<sub>2</sub>-AC composite reveals that the breakthrough times in the case of composite adsorbent in general are 1.5-2 times longer than those for calcined AC. Moreover, the loading of activated carbon with small quantities of ZnO (8.4%) and TiO<sub>2</sub> (6%) enhanced its capacity for simultaneous removal of NH<sub>3</sub> and H<sub>2</sub>S, with the impact being more pronounced on adsorption capacity of NH<sub>3</sub>. To be specific, the enhancement in NH<sub>3</sub> adsorption capacity was in the range 21–73%, with the most impact observed at 22 and 70 °C, while the enhancement in the case of H<sub>2</sub>S was 10–21% with the effect being more pronounced at 140 and 280 °C. The only exception was the H<sub>2</sub>S adsorption capacity at 22 °C that showed 6% decrease with the composite adsorbent.

Table 2 also provides the NH<sub>3</sub> and H<sub>2</sub>S breakthrough times and equilibrium adsorption capacities obtained as part of an earlier work with the mixture of commercial (pure) ZnO and TiO<sub>2</sub> nanoparticles. As seen, the dependency of NH<sub>3</sub> and H<sub>2</sub>S breakthrough times and adsorption capacities on gas concentration and temperature were consistent with the trends observed with 10ZnO-5TiO<sub>2</sub>-AC composite. However, the breakthrough times with the mixture of commercial (pure) ZnO and TiO<sub>2</sub> nanoparticles were longer and the equilibrium adsorption capacities were also higher than those obtained with the composite. Given the small quantities of ZnO and TiO<sub>2</sub> in the composite adsorbent (8.4 and 6%, respectively), the higher adsorption capacities with mixture of pure ZnO and TiO<sub>2</sub> nanoparticles is not surprising.

To describe the equilibrium data obtained for simultaneous adsorption of NH<sub>3</sub> and H<sub>2</sub>S on the composite adsorbent, multicomponent Langmuir isotherm, represented by Eqs. 1 and 2, was used:

$$q_i = \frac{q_{si}K_iP_i}{1 + K_iP_i + K_jP_j} \quad (1)$$

$$q_j = \frac{q_{sj}K_jP_j}{1 + K_iP_i + K_jP_j} \quad (2)$$

where  $q_i$  and  $q_j$  are the equilibrium adsorption capacities of NH<sub>3</sub> and H<sub>2</sub>S (mg gas g<sup>-1</sup>),  $P_i$  and  $P_j$  are the partial pressures of NH<sub>3</sub> and H<sub>2</sub>S in the mixture (kPa),  $q_{si}$  and  $q_{sj}$  are the maximum adsorption capacities of NH<sub>3</sub> and H<sub>2</sub>S, and  $K_i$  and  $K_j$  are the equilibrium constants for NH<sub>3</sub> and H<sub>2</sub>S, respectively. The dependency of equilibrium constants on temperature was described by van't Hoff expression (Eqs. 3 and 4):

$$K_i = K_{0i} \exp\left(\frac{-\Delta H_i}{RT}\right) \quad (3)$$

$$K_j = K_{0j} \exp\left(\frac{-\Delta H_j}{RT}\right) \quad (4)$$

Substituting the  $K_i$  and  $K_j$  as defined by Eqs. 3 and 4 in the multicomponent Langmuir isotherm expressions (Eqs. 1 and 2) results in the extended form of these expressions:

$$q_i = \frac{q_{si}K_{0i} \exp\left(\frac{-\Delta H_i}{RT}\right) P_i}{1 + K_{0i} \exp\left(\frac{-\Delta H_i}{RT}\right) P_i + K_{0j} \exp\left(\frac{-\Delta H_j}{RT}\right) P_j} \quad (5)$$

$$q_j = \frac{q_{sj}K_{0j} \exp\left(\frac{-\Delta H_j}{RT}\right) P_j}{1 + K_{0i} \exp\left(\frac{-\Delta H_i}{RT}\right) P_i + K_{0j} \exp\left(\frac{-\Delta H_j}{RT}\right) P_j} \quad (6)$$

where  $K_{0i}$  and  $K_{0j}$  are the pre-exponential factors (kPa<sup>-1</sup>),  $\Delta H_i$  and  $\Delta H_j$  are the enthalpies of NH<sub>3</sub> and H<sub>2</sub>S adsorptions (kJ mol<sup>-1</sup>), respectively,  $T$  is temperature (K), and  $R$  is the universal gas constant (kJ mol<sup>-1</sup> K<sup>-1</sup>). The equilibrium data obtained for adsorption of NH<sub>3</sub> and H<sub>2</sub>S at different temperatures were then fit non-isothermally into Eqs. 5 and 6 and the value of various coefficients were determined. This was done using the built-in Solver in Excel and by minimizing an objective function (Eq. 7), defined as the sum of squares of differences of experimentally determined adsorption capacities and those calculated by the isotherm expressions:

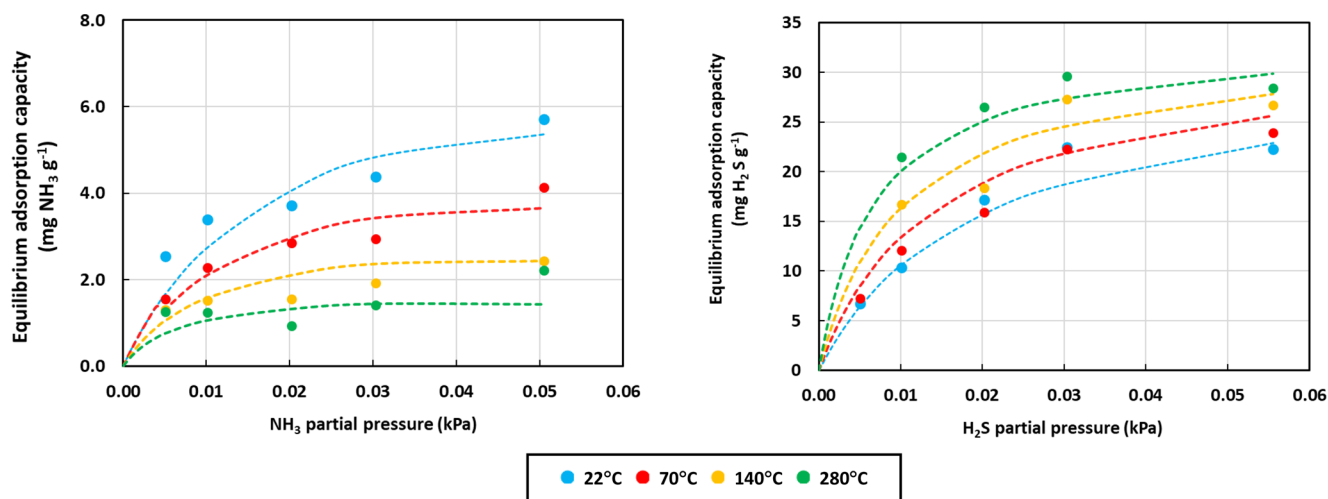
$$f = \sum_i \sum_j (q_{Exp.,ij} - q_{Calc.,ij})^2 \quad (7)$$

The coefficient of determination ( $R^2$ ) was determined from Eq. 8:

$$R^2 = 1 - \frac{\sum_i \sum_j (q_{Exp.,ij} - q_{Calc.,ij})^2}{\sum_i \sum_j (q_{Exp.,ij} - q_{mean})^2} \quad (8)$$

The values of  $q_s$ ,  $K_0$ , and  $\Delta H$  for NH<sub>3</sub> and H<sub>2</sub>S were 68.93 mg NH<sub>3</sub> g<sup>-1</sup> and 34.31 mg H<sub>2</sub>S g<sup>-1</sup>, 2.26 and 518 kPa<sup>-1</sup>, and





**Fig. 4** Ammonia (left panels) and hydrogen sulphide (right panels) adsorption isotherms for 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent. Symbol are experimentally determined adsorption capacities and dashed lines are Langmuir multicomponent model predictions (goodness of fit)

**Table 3** BET surface area, pore volume and average pore size of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent and the saturated composite adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550 ppmv H<sub>2</sub>S at 22 °C and 280 °C

Adsorbent	BET surface area (m <sup>2</sup> g <sup>-1</sup> )	Pore volume (cm <sup>3</sup> g <sup>-1</sup> )	Pore size (nm)
Fresh	914.55	0.73	3.17
Exposed (22 °C)	903.15	0.73	3.27
Exposed (280 °C)	854.74	0.67	3.15

– 2.40 and 5.83 kJ mol<sup>-1</sup>, respectively. The experimentally determined NH<sub>3</sub> and H<sub>2</sub>S equilibrium adsorption capacities and the corresponding predictions by the multicomponent Langmuir isotherm are contrasted in Fig. 4. The goodness of fit shown in this figure for both NH<sub>3</sub> and H<sub>2</sub>S and an R<sup>2</sup>=98.1% indicated that the multicomponent Langmuir model predicted the experimental data with high level of accuracy. The negative value of enthalpy of the adsorption for NH<sub>3</sub> (–2.4 kJ mol<sup>-1</sup>), confirmed the exothermic and potentially physical nature of ammonia adsorption on 10ZnO-5TiO<sub>2</sub>-AC, as reported in other works [22, 23], while in the case of H<sub>2</sub>S a positive value for adsorption enthalpy showed the endothermic and chemisorption nature of H<sub>2</sub>S adsorption.

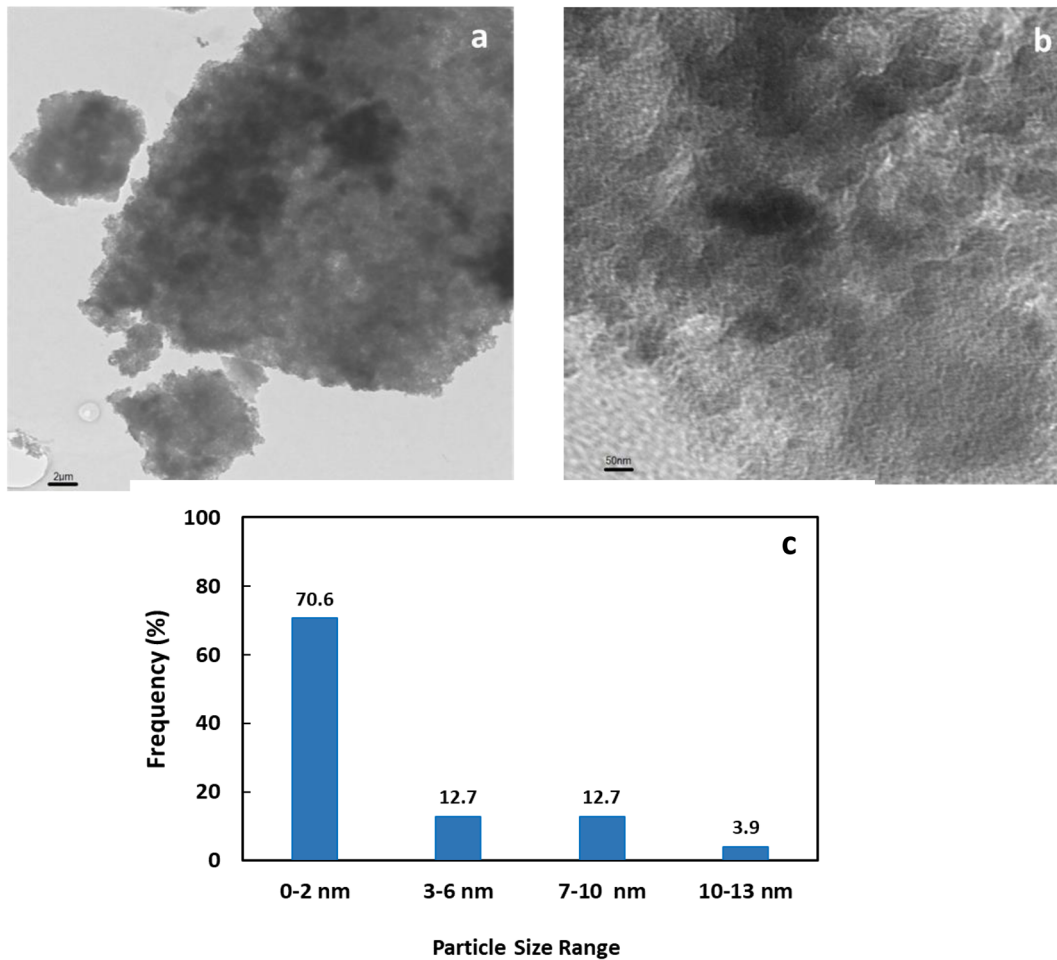
### 3.3 Characterization of fresh and exposed 10ZnO-5TiO<sub>2</sub>-AC adsorbents

Table 3 presents the BET surface area, pore volume and average pore size of the fresh 10ZnO-5TiO<sub>2</sub>-AC composite and saturated adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550 ppmv H<sub>2</sub>S at 22 °C and 280 °C. The fresh adsorbent had the highest BET surface area and pore volume (914.55 m<sup>2</sup> g<sup>-1</sup> and 0.73 cm<sup>3</sup> g<sup>-1</sup>) which were both lower

than the corresponding values for activated carbon (1122 m<sup>2</sup> g<sup>-1</sup> and 0.91 cm<sup>3</sup> g<sup>-1</sup>), as reported earlier [22, 23]. This is expected and caused by the dispersion of ZnO and TiO<sub>2</sub> on the surface and pores of activated carbon [22, 23]. The exposure of the composite to NH<sub>3</sub> and H<sub>2</sub>S decreased its surface area and pore volume, and the effect was pronounced at the higher temperature of 280 °C. As discussed in more details in the latter part of this section, the chemical nature of H<sub>2</sub>S adsorption led to formation of ZnS, with the reaction being temperature dependent. Thus, the lower surface area and pore volumes observed for the exposed adsorbents, especially at 280 °C, is not caused only by the addition of ZnO and TiO<sub>2</sub>, and the formation and deposition of ZnS on the activated carbon surface and pores is the other contributing factor.

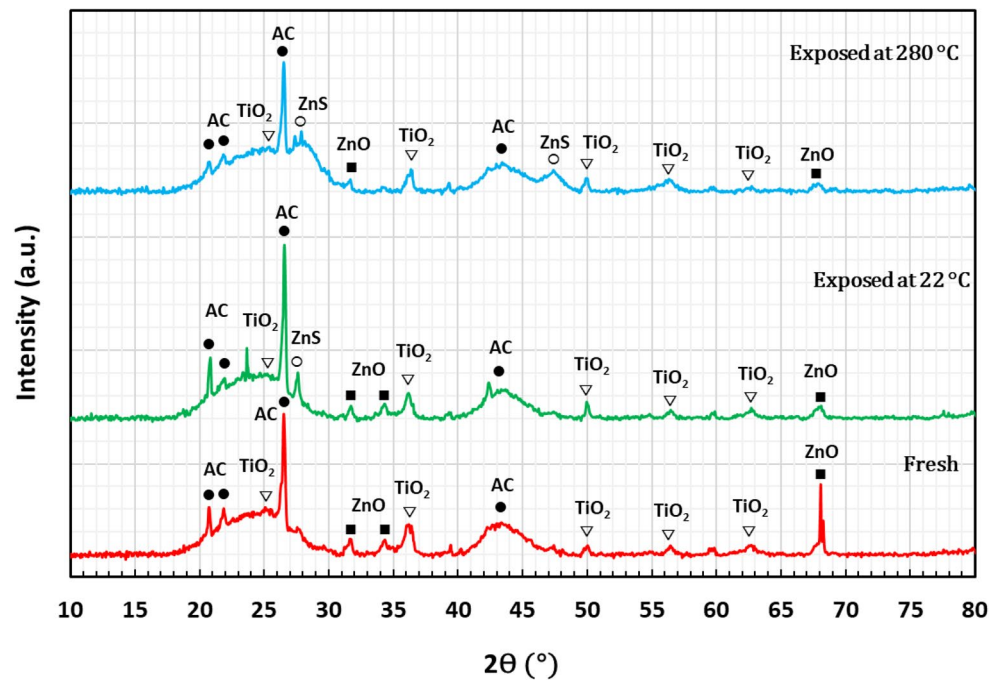
TEM images of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent (Fig. 5, panels a, b) clearly show the presence and distribution of metal oxides on the activated carbon. The particles size distribution for metal oxide, obtained by analysis of TEM images, revealed that most of the metal oxide particles (70.6%) were in a size range of 0–2 nm and a smaller percentage (21.6%) were 3–9 nm particles. The largest particles detected on the composite were in the size range of 10–13 nm and accounted for 7.8% of all particles (Fig. 5, panel c).

Figure 6 presents the XRD spectra of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent and saturated composite adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S at 22 °C and 280 °C. In all three cases, peaks corresponding to activated carbon were observed at 20.8°, 21.95°, 26.6°, and 43.4° [22]. Presence of TiO<sub>2</sub> was also evident through peaks at 25.4°, 36.4°, 50.1°, 56.6° and 62.8° that were seen in fresh and exposed adsorbent spectra and matched those of anatase TiO<sub>2</sub> peaks as reported by

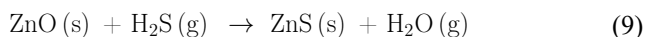


**Fig. 5** TEM images of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent at two different magnifications (panels a and b) and particle size distribution of nanoparticles (panel c)

**Fig. 6** XRD spectra of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent (red) and saturated adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550 ppmv H<sub>2</sub>S at 22 °C (green) and 280 °C (blue)



others [11, 19, 22, 27, 28]. Peaks at 31.7°, 34.4°, and 68.1° in the fresh adsorbent and those exposed to NH<sub>3</sub> and H<sub>2</sub>S confirmed the presence of ZnO in the composite adsorbents [24]. Spectra of exposed adsorbents included a peak at 28.1° that corresponded to zinc sulfide (ZnS) and confirmed the chemisorption of H<sub>2</sub>S on ZnO in accordance with Eq. 9 [21, 24–26].



The chemisorption nature of H<sub>2</sub>S adsorption was also supported by substantial decrease in intensity of ZnO peak at 68° in the exposed adsorbents, indicating the conversion of ZnO to ZnS. It is important to point out that in the case of adsorbent exposed to 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S at 280 °C, an additional peak that corresponds to ZnS polycrystalline structure is seen at 47.5° [12]. These evidence all point to endothermic chemisorption of H<sub>2</sub>S adsorption, as confirmed by a positive value for enthalpy of H<sub>2</sub>S adsorption described in Sect. 3.2.

The FTIR spectra of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent and saturated composite adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S mixture at 22 °C and 280 °C are shown in Fig. 7. The FTIR spectra in all three cases displayed the adsorption bands that are associated with oxygen-containing functional groups. The patterns in the region of 3900 and 3600 cm<sup>-1</sup> is associated with O-H stretching of water [18] and/or -OH groups of alcohol or phenols on the activated carbon surface [7]. The broad band between 1600 and 1400 cm<sup>-1</sup> is attributed to skeleton vibration of aromatic C=C groups and stretching of C=O in COOH groups on the surface of activated carbon [7, 18]. The strong band at 607 cm<sup>-1</sup> observed in all three

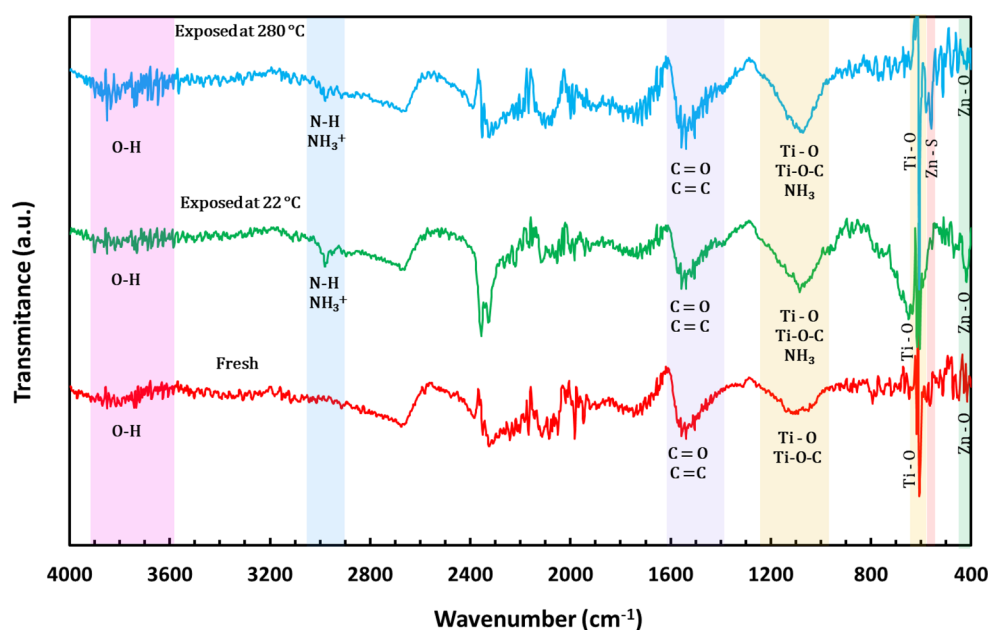
adsorbents corresponds to bulk titania skeletal [7]. The peak observed at 1060–1070 cm<sup>-1</sup> is related to the Ti-O stretching and the surface conjugation between the activated carbon and the Ti-O bonds as Ti-O-C [4].

The peaks associated with the vibrational band of liquid ammonia, the hydrogen bonded ammonia to the surface Bronsted acid sites, and the symmetric bending mode ( $\delta_{\text{sym}}$ ) of ammonia molecules that are reported to occur at 1054 cm<sup>-1</sup>, 1100 and 1105 cm<sup>-1</sup>, and 1150 and 1236 cm<sup>-1</sup>, respectively [23], all coincide with the broad band observed between 1600 and 1400 cm<sup>-1</sup> in Fig. 7 that could indicate overlapping of carbon and ammonia related peaks in the exposed adsorbents. The peak at 2979 cm<sup>-1</sup> that is only observed in the exposed sample coincides with the stretch of NH<sub>3</sub><sup>+</sup> species and the overtone of N-H vibration [17].

A peak that has been attributed to vibration Zn-O bonds (420–410 cm<sup>-1</sup>) is clearly seen in the spectra of fresh adsorbent and adsorbent exposed to the mixture of NH<sub>3</sub> and H<sub>2</sub>S at 22 °C but for the exposed adsorbent at 280 °C this peak is not visible. The reason for absence of this peak is the reaction of H<sub>2</sub>S with ZnO and formation of ZnS according to Eq. 9, as demonstrated earlier by examining the XRD spectra of fresh and exposed adsorbents. The chemisorption of H<sub>2</sub>S by ZnO is further supported by the existence of a peak at 559 cm<sup>-1</sup> in the spectra of adsorbent exposed to NH<sub>3</sub> and H<sub>2</sub>S at 280 °C that has been attributed to vibrations of ZnS bonds [1]. The small magnitude or absence of this peak in the case of adsorbent exposed to NH<sub>3</sub> and H<sub>2</sub>S at 22 °C once again point to endothermic nature of this chemisorption process and the positive impact of higher temperatures on the reaction.

As indicated in the introduction, several recent works have been dedicated to simultaneous removal of NH<sub>3</sub> and

**Fig. 7** FTIR spectra of fresh 10ZnO-5TiO<sub>2</sub>-AC composite adsorbent (red) and saturated adsorbents after exposure to 500 ppmv NH<sub>3</sub>-550ppmv H<sub>2</sub>S at 22 °C (green) and 280 °C (blue)



H<sub>2</sub>S from gaseous streams, using metal oxide catalyst-adsorbents. Jung et al. [14] used Zn–Al-based sorbents, promoted with cobalt, nickel and iron oxides for the removal of NH<sub>3</sub> and H<sub>2</sub>S from coal-based synthesis gas that contained 5,000 ppmv NH<sub>3</sub> and 10,000 ppmv H<sub>2</sub>S. The adsorption of H<sub>2</sub>S (sulfidation) and decomposition of NH<sub>3</sub> before and after sulfidation process were evaluated in a micro-reactor at 1 atm and 650 °C with a gas flow rate of 50 mL h<sup>-1</sup>. Cobalt, nickel and iron oxides were active components in decomposition of NH<sub>3</sub> and absorption of H<sub>2</sub>S, while ZnO and Al<sub>2</sub>O<sub>3</sub>, major constituents of each adsorbent, did not show any activity in NH<sub>3</sub> decomposition. Among cobalt, nickel and iron oxides, cobalt oxide was most effective in decomposition of NH<sub>3</sub>. In a follow-up study with hot coal gases under similar operating conditions, cobalt oxide, molybdenum oxide, and nickel oxide were all shown to be effective in decomposition of NH<sub>3</sub> alone but the presence of hydrogen sulfide and sulfidation reaction substantially decreased their effectiveness in removal of NH<sub>3</sub> [20]. To improve the removal of NH<sub>3</sub> and H<sub>2</sub>S, Zn-based adsorbents with either cobalt, molybdenum, or nickel oxide were also evaluated. The Zn-based adsorbent CZ-30 that contained 30% cobalt oxide and 70% ZnO outperformed the other two adsorbents, with the breakthrough capacities at 1 atm and 650 °C with 5000 ppmv NH<sub>3</sub> and 10,000 ppmv H<sub>2</sub>S were reported as 88 mg NH<sub>3</sub> g<sup>-1</sup> and 370–425 mg H<sub>2</sub>S g<sup>-1</sup>. Lim et al. [15] extended this work by impregnating Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, and ZrO<sub>2</sub> supports with Mo and Co oxides and evaluated the resulting catalyst-adsorbents for simultaneous removal of 5,000 ppmv NH<sub>3</sub> and 10,000 ppmv H<sub>2</sub>S at 650 °C. All catalyst-adsorbents had similar removal capacities for NH<sub>3</sub> alone but in the presence of H<sub>2</sub>S only Co–Mo–Al<sub>2</sub>O<sub>3</sub> showed effectiveness in decomposition of NH<sub>3</sub>. These authors reported an H<sub>2</sub>S adsorption capacity of 176 mg g<sup>-1</sup> and an NH<sub>3</sub> removal percentage of 95% but no information on adsorption capacity of NH<sub>3</sub> was provided. Studying the simultaneous removal of toluene, NH<sub>3</sub> and H<sub>2</sub>S from biomass-generated producer gas that contained 300 ppmv NH<sub>3</sub> and 150 ppmv H<sub>2</sub>S, Bhandari et al. [3] employed a Mo and Al mixed metal oxide catalyst-adsorbent and achieved NH<sub>3</sub> and H<sub>2</sub>S adsorption capacities of 8 and 30 mg g<sup>-1</sup>, respectively at 800 °C. Comparing these results with those obtained with biochar and activated carbon, Bhandari et al. [3] concluded that NH<sub>3</sub> adsorption capacities of activated carbon and mixed metal oxide catalyst were much higher than that of biochar, whereas H<sub>2</sub>S adsorption capacity of mixed metal oxide was higher than activated carbon and biochar.

The overview of the recent literature, provided here, clearly shows the lack of information on simultaneous removal of NH<sub>3</sub> and H<sub>2</sub>S at low concentration and temperature range that are encountered in many practical situations such as emissions from livestock operations, wastewater

treatment plants and landfills, and in raw biogas. Moreover, one can notice that in none of the earlier works impacts of NH<sub>3</sub> and H<sub>2</sub>S concentrations and temperature on simultaneous adsorption NH<sub>3</sub> and H<sub>2</sub>S have been investigated. The results of the present study indicate that the developed carbon-based adsorbent with relatively low metal oxides loading is a suitable candidate for the adsorptive removal of NH<sub>3</sub> and H<sub>2</sub>S in applications where low gas concentrations and temperatures are encountered.

## 4 Conclusion

The findings of the present study on simultaneous adsorption of NH<sub>3</sub> and H<sub>2</sub>S by activated carbon-based composite adsorbents, revealed that among the three synthesized adsorbents with ZnO and TiO<sub>2</sub> loadings of ~10 and 5%, 15 and 5%, and 15 and 10%, the composite with 10% ZnO and 5%TiO<sub>2</sub> (10ZnO-5TiO<sub>2</sub>-AC) had the highest equilibrium adsorption capacities for NH<sub>3</sub> and H<sub>2</sub>S, while the corresponding values for the other composites were close. Detailed evaluation of selected adsorbent (10ZnO-5TiO<sub>2</sub>-AC) for simultaneous adsorption of NH<sub>3</sub> and H<sub>2</sub>S under various gas concentrations and low temperature range revealed that equilibrium adsorption capacity for NH<sub>3</sub> increased with the increase of NH<sub>3</sub> concentration, but temperature had an opposing effect and lower adsorption capacities were obtained with the increase of temperature. In the case of H<sub>2</sub>S, increase of concentration and temperature both enhanced the equilibrium adsorption capacity. These trends were consistent with those reported for a mixture of pure (commercial) TiO<sub>2</sub> and ZnO nanoparticles when applied for simultaneous removal of NH<sub>3</sub> and H<sub>2</sub>S. The multicomponent Langmuir isotherm described the equilibrium data for adsorption of NH<sub>3</sub> and H<sub>2</sub>S with high level of accuracy. The negative value of adsorption enthalpy for NH<sub>3</sub> confirmed the exothermic and potentially physical nature of ammonia adsorption, while in the case of H<sub>2</sub>S a positive value of adsorption enthalpy revealed the endothermic and chemisorption nature of the adsorption process. The chemical nature of H<sub>2</sub>S adsorption was also confirmed through examination of fresh and exposed adsorbents by XRD and FTIR that clearly showed representative peak for ZnS, a product of H<sub>2</sub>S and ZnO reaction. Although mixture of pure (commercial) TiO<sub>2</sub> and ZnO nanoparticles provides higher adsorption capacities when compared to the composite adsorbent, the challenges associated with the use and handling of pure nanoparticles and their cost, makes the carbon-based composite adsorbent developed in this work a more feasible and practical choice for the large-scale capture of NH<sub>3</sub> and H<sub>2</sub>S from gaseous emissions.

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## Declarations

**Ethical approval** Not applicable.

**Competing interests** The authors declare no competing interests.

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