**RAPID COMMUNICATION** 

# Interlayer shear strength of single crystalline graphite

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Abstract Reported values (0.2 MPa–7.0 GPa) of the interlayer shear strength (ISS) of graphite are very dispersed. The main challenge to obtain a reliable value of the ISS using conventional measuring methods was the unavailability of sufficiently large single crystalline graphite. Here we present a novel experimental method to measure the ISS, and obtain the value as ~0.14 GPa. Our result can serve as an important basis for understanding mechanical behavior of graphite or graphene-based materials.

Keywords Shear strength · Single crystalline graphite

# **1** Introduction

Graphitic systems are used for a wide variety of applications, ranging from lubricant materials [1] to graphite intercalation compounds [2], graphene-based composite materials [3] and graphene oxide papers [4, 5]. Graphite is also widely used as a raw material to obtain graphenes [6, 7]. Despite the technological and scientific importance of graphitic systems, the knowledge of their mechanical properties, especially the interlayer shear strength (ISS), say  $\tau_s$ , is unexpectedly poor [8, 9].

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The first measurement of  $\tau_s$  was done more than forty years ago by Soule and Nezbeda [10]. Their static test on highly anisotropic-annealed natural graphite gave the values of  $\tau_s$  in the range of 0.25–0.75 MPa, with the average value of 0.48 MPa that has been widely adopted in Refs. [4, 11-15]. In their experiment, the basal plane shear stiffness constant  $C_{44}$  was measured as 0.13–1.4 GPa, which is much lower than other previously reported values. This difference was attributed to the basal plane dislocations [16]. The follow-up measurement by Blakslee et al. [17] on compression-annealed pyrolytic graphite yielded the value  $\tau_s$  of 0.9–2.5 MPa. Surprisingly, except for the above-mentioned two works, there seems to be no other directly measured ISS, as pointed out by Popov et al. [18]. The main challenge to use the conventional static mechanical test to measure the interlayer shear strength is the unavailability of sufficiently large single crystalline graphite [9]. Indeed, the typical sizes of single crystalline grains in graphite are in the micrometer range and thicknesses in the nanometer range [12, 19].

Very recently, Ding et al. [20] used a thermal excitation method in a scanning tunneling microscope (STM) for a highly oriented pyrolytic graphite (HOPG) under compressive stress. They reported a shear strength value as high as 7 GPa with caution "The atomistic process for tip-sample interaction in STM might be more complicated than described here. To confirm the mechanism and to calculate the error for the experimental result of shear strength, further studies are of great help." [20]. In fact, the same method used by Snyder et al. [21] to measure the ISS of HOPG lead to a value of 5 MPa, which is three orders in magnitude lower.

Theoretically, graphite presents a major challenge for quantum physics computations due to the two completely different types of inter-atomic bonds: an exceptionally strong sp<sup>2</sup> covalent intra-layer bonding and an extremely weak van der Waals (vdw) interlayer interaction. Tight-binding atomistic simulations yielded the values of  $\tau_s$  as 0.434 GPa by Bonelli et al. [22] and 0.9 GPa by Guo et al. [23]. For density functional theory (DFT), it remains notoriously dif-

ficult to describe the weak van der Waals interlayer interaction [24, 25]. The standard approximations used in DFT, such as the local-density approximation (LDA) and generalized gradient approximation (GGA), can not accurately describe long-distance interactions such as that of the van der Waals force. An alternative to standard DFT is the van der Waals density functional method, which was developed to account for the long-range interaction component by using an explicit nonlocal functional of the density. However, different vdw DFT methods have lead to very scattered results on the van der Waals interactions in graphite [26].

The above brief review calls for a non-conventional method to experimentally measure a reliable ISS for single crystalline graphite. In this paper, we introduce a novel method, which is inspired by our recent observations of the self-retracting motion of micrometer graphite flakes on graphite mesas [11] and of the microscale superlubricity phenomenon [12]. We obtain the value of  $\tau_s$  about 0.14 GPa.

# 2 Experiments

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The samples that we used to study the interlayer shear strength were microscale graphite/SiO<sub>2</sub> square mesas that are lithographically constructed, as illustrated in Fig. 1a, with a typical edge size (*L*) ranging from 0.5 to 20  $\mu$ m and heights (*H*) from 100 to 500 nm. The fabricating processes of the mesas were described in details in Ref. [11], following the method proposed in Ref. [27]. Using a microtip equipped to a micromanipulator MM3A (Kleindiek) to apply

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**Fig. 1** a Sketch of a mesa with an edge length *L* and a height *H*; **b** Sketch of shearing out a top graphite flake and a subsequent rotation into a lock-in state; **c** Shearing the top flake again resulting in a new sliding interface; **d-f** SEM images: **d** A graphite/SiO<sub>2</sub> flake was sheared out from its platform by a microtip; **e** it can self-retract to its platform after disengaging the tip **e**; **f** Multiple graphite flakes obtained by repeating the processes of **b** and **c** 

a shear force on the SiO<sub>2</sub> top surface of a mesa, as schematically illustrated in Figs. 1b–1c with a straight arrow indicating the shear force, we can shear off a graphite/SiO<sub>2</sub> flake. For mesas with side lengths (*L*) smaller than 10  $\mu$ m, we found that many of the sheared flakes after being released can spontaneously move back to their before-sheared positions (Figs. 1d–1e) [12]. We also noted that if the sheared flake was rotated at certain angles, as illustrated in Figs. 1b– 1c with a circular arrow indicating the torque, the two surfaces locked together [12]. These "lock-ins" occurs at 60° intervals, which is consistent with the hexagonal symmetry of the graphite lattices [12].

Graphite is a layered material composed of single carbon layers–graphenes, in which carbon atoms are located in a hexagonally lattice. In single crystalline graphite, two adjacent graphenes are AB-stacked as shown in Fig. 2a. The main mechanisms of the self-retraction and lock-in phenomena were revealed in Ref. [12] and summarized in following:

(1) Provided a contact between two self-retractable graphenes incommensurate: not only non-AB-stacked, but also have different lattice orientations as illustrated in Fig. 2b, a negligible friction (a superlubricity state) and thus a self-retraction are observed [12].

(2) Provided an AB-stacking (as in single crystal graphite), a "lock-in" state appears because of the drastically large shear resistance force per unit contact area in such a commensurate contact.

Thus, the external force required to unlock a "lock-in" state corresponds to the interlayer shear strength of single crystalline graphite,  $\tau_s$ .



**Fig. 2** a Sketch of two graphene layers in an AB-stacking state; b Sketch of two graphene layers in a non-AB-stacking state generated by a relative rotation, resulting in a clear Moire pattern (different colors represent different layers)

Electron back scattered diffraction (EBSD) images (Figs. 3a and 3b) show that the HOPG sample is composed of single crystalline graphite grains with a typical size of several micrometers. Recent experiments combining focused-ion-beam/SEM and HRTEM [19] and our experiments on the self-retraction of graphite flakes [11, 12, 26] reveal the thickness of graphite single crystal grains about 5–60 nm. Based on these experimental facts, we proposed a brick-wall model for HOPG polycrystalline structure: single crystal grains (i.e., the bricks) with c-axis well aligned within a few degrees but rotationally mis-oriented in the basal plane [12].

Thus adjacent graphene layers within a graphite grain are in AB-stack (commensurate) while those between different grains are most likely incommensurate. For a mesa with a few micrometers in size and about one hundred nanometers in height, there is a certain probability of existing a grain boundary or equivalently an incommensurate contact that crosses all over the mesa. We found that all fully selfretractable contacts are atomically smooth and incommensurate [12] (Figs. 3c and 3d). The resistant shear strength against the sliding motion determined in our experimented is very small, with an upper bound of 0.06 MPa. When continuously rotating a self-retractable flake, it will eventually be locked in. Then, when we try to shear the flake again, it is often observed that a new flake is sheared out at another incommensurate contact. Repeating the above shearing (to open an incommensurate contact) and rotating (to lock-in) processes (Figs. 1b and 1c), we can ensure that all the contacts in the graphite mesa are AB-stacking, as illustrated in Fig. 1f, which is crucial for measuring the ISS of graphite.



Fig. 3 a Color map of graphite grain orientation from EBSD experiments with different colors corresponding to different grains. The histogram of grain size, where the diameter of each grain is defined as the mean square root of its area, is shown in the inset. The average grain size is  $\sim 10 \ \mu\text{m}$ ; b Crystal-direction map (IPF mapping image) from EBSD with the crystal orientation represented by the inverse pole figure in the inset. c-d STM scan of a typical contact interfaces where graphite flake exhibits fully self-retraction, which clearly indicates atomically smooth surface in the self-retraction islands (the surface roughness is below 0.5 nm over a length of 1  $\mu$ m)

By chance, we obtained a few mesas containing only one incommensurate contact interface. After shearing out the upper flake of such a mesa and rotating it to a lock-in orientation, the obtained sample is an ideal form to determine the ISS for single crystalline graphite. The created lockedin contact area (AB-stacking) is smaller than others in the single crystal grains of the mesa sample (also AB-stacking), which will ensure the unlocking of AB-stacking occurring at the newly created contact interface.

The microtip is then used to shear the top flake of the graphite mesa. From the deformations of the microtip in

quasi-static loading and unloading, we can estimate the interlayer shear strength for single crystal graphite. The position of the tip and the loading velocity can be precisely controlled with an accuracy of the micromanipulator (Kleindiek) up to 5 nm. Figures 4a and 4b show such a mesa that is selfretractable. Comparing the shapes of the probe in loading (Fig. 4a) and unloading (Fig. 4b), no detectable deformation is observed with the optical microscope resolution. Shearing a flake from a square graphite mesa of edge length *L* to a distance *x* creates new surfaces of total area 2Lx (Fig. 1d) and thus an excess surface free energy of  $U = 2\gamma Lx$ , where  $\gamma$  is the graphite basal plane surface energy which is estimated to be about 0.1–0.15 J/m<sup>2</sup> [26, 28]. The corresponding selfretraction force is thus  $F_{\text{retract}} = |-dU/dx| = 2\gamma L$ . The friction resistance force is  $F_{\text{f}} = \tau_{\text{s}}L(L-x)$ . Since the flake self-retracts, we can conclude that this force overcomes the friction at the interface. So we obtain an upper bound estimate of the areal friction stress as  $\tau_{\text{s}}^{\text{upper}} = 2\gamma/(L - x_{\text{max}})$ , where  $x_{\text{max}}$  is the maximum sheared distance in our experiments, typically ~ 5 µm for a 10 µm mesa. This analysis yields the upper bound estimate  $\tau_{\text{s}}^{\text{upper}} \approx 0.04$ –0.06 MPa between incommensurate graphene layers.



**Fig. 4 a, b** Two image frames taken from in-situ Movie. Shearing a self-retractable graphite flake using the microtip of a micromanipulator (Kleindiek) within an optical microscope (OM, HiRox KH-3000). No obvious deformation of the microtip was observed within the resolution of the optical microscope. **c, d** two selected image frames from an in-situ Movies. Shearing a top flake in a lock-in state. Image **c** records the moment just before the top flake begins to move. After unloading, a plastic deformation of the microtip can be seen

For a lock-in state, Fig. 4c is the frame just before the top flake begins to move (selected from an in-situ movie). After unloading, the microtip remains bent (Fig. 4d), indicating a plastic deformation has occurred while attempting to shear the top flake. The critical shearing resistance force in the lock-in state is equal to the force exerted on the microtip from the top flake. The latter force can be estimated from the deformation of the microtip in Fig. 4c by finite element method (FEM) modeling.

#### 3 Finite element analysis and results

In our FEM model (Fig. 5a), the top flake is considered as a rigid body, since the deformation of the top flake can be neglected in comparison to the deformation of the microtip as observed in experiments. A classic elastic-linear plastic model with isotropic hardening was used for the mechanical analysis of the tungsten microtip The elastic modulus of the microtip is 201 GPa measured from the uni-axial tensile stress-strain curve (Fig. 5b) of a tungsten thread (raw material to fabricate the microtip in our experiments) with a diameter of 0.30 mm (WDW3020, Changchun Branch, a strain rate of about  $2 \times 10^{-4}$  s<sup>-1</sup>). The Poisson ratio is selected as 0.284 [29]. Displacement controlled loading is implemented to the microtip in the far end. Different displacement values result in different shapes of neutral surface of the microtip (theoretical shapes) as shown in Fig. 5c. The red-dotted line is the neutral surface measured from experiments (Fig. 4c). Through a comparison, the best fitting yields the critic resultant force exerted on the microtip as  $F_c \sim 0.65$  mN. The resultant force is perpendicular to the loading edge of the top flake because the contact between the microtip and the top flake is considered as frictionless in our FEM model.



Fig. 5 a FEM model simulating the loading process in experiments (see text for details); b Stress–strain curve of a tungsten thread with diameter 0.30 mm subject to a uni-axial quasi-static tension (WDW3020, Changchun Branch, strain rate  $\sim 2 \times 10^{-4} \text{ s}^{-1}$ ); c Comparison between the shapes of neutral surface of the microtip at different displacements in FEM models and the experimental results (measured from Fig. 4c and denoted as red-dot line). The optimal fitting yields the critic resultant force exerted to the microtip

With the determined critical force and the contact area between the graphite/SiO<sub>2</sub> flake and the graphite platform measured in our experiment  $S = 4.5 \ \mu m^2$ , we can estimate the ISS of the AB-stacked graphite layers as  $\tau_{s,lock-in} =$ 0.14 GPa. This value is about two orders of magnitude higher than those measured in macroscale shear experiments (0.25–2.5 MPa). We believe that the much smaller ISS measured in the previous experiments can be attributed to the existence of many incommensurate contacts in their samples, which could significantly reduce the shear strength because of the superlubricity.

## 4 Summary

In summary, a novel experimental method is presented to directly measure and estimate the interlayer shear strength for single crystal graphite as  $\tau_s \sim 0.14$  GPa This value is about two orders of magnitude higher than the measured values in previous macroscale shear experiments (0.25– 2.5 MPa) We attributed the drastic difference to the presence of stacking faults (incommensurate contact) in the samples used in the macro-scale experiments. Our results can serve as a benchmark for the shear strength of single crystal graphite.

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