#### **RESEARCH PAPER**

# Supercritical CO<sub>2</sub> applications in microfluidic systems

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#### **Abstract**



Supercritical fuid technology has been used for a variety of applications for decades and received special attention in the felds of analytics, extraction and purifcation of valuable compounds and preparation of drug carriers. Among supercritical fluids, supercritical  $CO<sub>2</sub>$  is the most attractive one as being nontoxic, nonflammable and chemically inert. In addition, the critical temperature and pressure of  $CO<sub>2</sub>$  is quite moderate which makes supercritical  $CO<sub>2</sub>$  a popular solvent for a wide range of applications from laboratory to industrial scale. In recent years, a promising research feld called as supercritical microfuidics was developed to merge the advantages of supercritical fuids and microfuidics, the science and technology of manipulating liquids in extremely small volume. This review discusses the recent progress in supercritical microfuidics with a focus on supercritical  $CO<sub>2</sub>$ , the most commonly used solvent in supercritical fluid processes, and some applications of supercritical  $CO<sub>2</sub>$  in microscale such as extraction of valuable compounds, determination of dissolution characteristic in various solvents, performing chemical reactions and particle synthesis are presented.

**Keywords** Microfuidics · Supercritical fuids · Carbon dioxide · Microreactor · Fabrication

## **1 Introduction**

Microfuidic systems are three dimensional structures consisting of micron-size (10–1000 μm) channel networks at different geometries and enable to handle liquids in extremely small volumes (Coyle and Oelgemöller [2008](#page-12-0); Theberge et al. [2010\)](#page-14-0). High surface area to volume ratio and short difusion distances in microfuidic systems allow to reach enhanced mass and heat transfer and faster reaction rates which are not approachable in traditional batch systems (Teh et al.  $2008$ ). As a result of laminar flow in microchannels, microfuidic systems are operated with diferent fow scenarios like parallel, plug flow or slug flow and reaction conditions are highly controlled (Krühne et al. [2014;](#page-13-0) Qian et al. [2019\)](#page-14-2). By taking these advantages, several potential applications of microfuidic systems such as conducting reactions with explosive and hazardous reagents and products (Janicke et al. [2000;](#page-13-1) Palde and Jamison [2011](#page-14-3)), reducing the consumption of expensive reagents (Liu et al. [2003](#page-13-2)) and

 $\boxtimes$  Aslihan Kazan kazanaslihan@gmail.com performing exothermic reactions with fast energy transfer demand (Antes et al. [2003](#page-12-1); Wang et al. [2011](#page-14-4)) are reported.

A supercritical fuid is defned as a substance with pressure and temperature above the critical values and has both liquid and gas-like properties (Blanchard and Brennecke [2001](#page-12-2)). Supercritical fuids have liquid-like density, gas-like viscosity and difusivity and their density can be easily tuned by small pressure changes in the critical region (Nalawade et al. [2006](#page-13-3)).

 $CO<sub>2</sub>$  is the most commonly used solvent in supercritical fuid applications as it is cheap, nontoxic, nonfammable, chemically inert, classifed as generally recognized as safe and has convenient critical values such as critical pressure of 7.383 MPa and critical temperature of 31 °C (Fig. [1](#page-1-0)) (Williams et al. [2002;](#page-14-5) Tyśkiewicz et al. [2018](#page-14-6); Yahya et al. [2018](#page-14-7); Zhu et al. [2018\)](#page-15-0). Having a critical temperature quite lower than most commonly used solvents such as ethanol ( $T_c$ =240.9 °C), methanol ( $T_c$ =239.6 °C), acetone  $(T_c=235.1 \text{ °C})$  and water  $(T_c=374.1 \text{ °C})$  makes CO<sub>2</sub> more advantageous particularly in terms of energy requirement of the process and thermal destruction of valuable compounds (Sahena et al. [2009\)](#page-14-8). Besides these properties, easier downstream processing like removing from the system by simple depressurization, higher stability and more environment friendly nature makes supercritical  $CO<sub>2</sub>$  more advantageous

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#### <span id="page-1-0"></span>**Fig. 1** Phase diagram of  $CO<sub>2</sub>$



than organic solvents (Leitner  $2002$ ). Supercritical  $CO<sub>2</sub>$  has been widely used in various applications such as extraction of bioactive compounds from various natural sources (Mendes et al. [2003](#page-13-5); Uwineza and Waśkiewicz [2020\)](#page-14-9), supercritical fuid chromatography as an analytic tool (Taylor [2009](#page-14-10)), an environmentally benign reaction medium for catalysis (Leitner [2002](#page-13-4)), production of biofuels (Boock et al. [2019](#page-12-3)), polymer synthesis and modifcation (Nalawade et al. [2006](#page-13-3)), production of nanomaterials like nanoparticles and nanocellular foams for pharmaceutical and medical purposes (Reverchon and Adami [2006\)](#page-14-11), using as a medium for dyeing of textiles without the need of drying (Knittel et al. [1993](#page-13-6)), degreasing, fber separating and tanning in leather processing with reduced ecological burden (Hu and Deng [2016](#page-13-7)), gelation of biopolymers (Gurikov et al. [2015\)](#page-12-4), drying of hydrogels to obtain aerogels (Tang and Wang [2005;](#page-14-12) Brown et al. [2010\)](#page-12-5), preparation of scafolds for tissue engineering applications (Kumari and Dutta [2010](#page-13-8); Pisanti et al. [2012\)](#page-14-13).

Supercritical microfuidics is a recently developed feld combining the advantages of supercritical fuids and micro-fluidics (Ciceri et al. [2014\)](#page-12-6). One of the advantages of microfluidic systems is the efficient mixing characteristic. Ionic liquid and  $CO<sub>2</sub>$  mixture is a new green solvent system for the separation and purifcation of chemicals and natural products. Since the density diference between the ionic liquids and  $CO<sub>2</sub>$  and also the higher viscosity of ionic liquids, it is difficult to mix two phases using traditional equipments. Qin et al. [\(2018a,](#page-14-14) [b](#page-14-15)) developed a micromixer based on passive mixing technology to mix supercritical  $CO<sub>2</sub>$  and a representative ionic liquid, 1-ethyl-3-methylimidazolium tetrafuoroborate ([Emim][BF4]). The system consisted of a T-junction and a tube both made by stainless steel and the inner diameters were 0.75 mm. The system was operated under diferent temperature (308–343 K) and pressure values (0.1–15 MPa) and the effects of  $CO<sub>2</sub>$  and ionic liquid flow rates and flow rate ratio on the bubble formation were examined. It was shown that bigger bubbles were obtained at higher  $CO_2$ /ionic liquid flow rate ratio and supercritical  $CO<sub>2</sub>$  bubbles with average diameter between  $0.3-1.2$  mm with lower polydispersity indexes than 35% were prepared successfully.

## **2 Characteristics of supercritical fuids in microscale**

Supercritical microfuidics combines the advantages of supercritical fluids and liquid microfluids (Fig. [2](#page-2-0)). In microchannels, fluid flow is characterized as laminar flow with low Reynolds number. The Reynolds number, the ratio of inertial forces to viscous forces, gives an information on the characteristics of fuid (density and viscosity) and the environment (fuid velocity and characteristic dimension) where the fuid fows (Elvira et al. [2013\)](#page-12-7). As the physicochemical properties of supercritical fuids such as density and viscosity can be easily manipulated by the variation of temperature and pressure, the fow regime of a supercritical fuid in a microchannel can be tuned from laminar to turbulent. The friction factor and heat transfer coefficient values significantly differ in two flow regimes and directly afect the performance of the system. Not only the Reynolds number but also the angle between the channels in merging points, the roughness and geometry of channels afect the transition from laminar to turbulent



<span id="page-2-0"></span>**Fig. 2** Main advantages of microfuidic systems over conventional reactors

flow in microscale (Morini et al. [2009](#page-13-9)). Although the transition from laminar to turbulent flow occurs for the Reynolds number around 2000 in conventional systems, the critical Reynolds number is lower in microfuidic systems. Diferent critical values for laminar to turbulent transition between 200–900 were reported and it was showed that the hydraulic diameter of a microchannel signifcantly afects the critical Reynolds number diferently from conventional systems (Peng and Peterson [1996](#page-14-16); Pohar and Plazl [2008](#page-14-17)).

Mixing in microchannels is dependent on the difusion between the fluids since the fluid flow is generally in laminar regime. To enhance the mixing of fuids, various passive or active micromixers were developed (Karimi et al. [2021](#page-13-10)). However, systems become more complex by the addition of these mixers and their characterization is also challenging. Segmented liquid–liquid or gas–liquid flows also provide enhanced mixing and the main advantage is that the mixing can be achieved in non-pattern, regular microchannels and an additional fabrication step for the micromixers is not required (Günther and Jensen [2006\)](#page-12-8). The mixing time in a microchannel is a function of flow width and diffusion coefficient. In general, the diffusion coefficients of molecules in supercritical fluids are higher than in liquids (at least two orders of magnitude) which results in better mixing and lower mixing time for supercritical microfuidics compared to liquid microfuidics (Marre and Jensen [2010\)](#page-13-11). In addition, the low viscosities of supercritical fuids also reduce the mixing time and enable the narrower residence time distribution which increases the yield of chemical reactions or enhances the product quality of particle synthesis conducted in microchannels (Song et al. [2006](#page-14-18); Marre et al. [2008;](#page-13-12) Mou et al. [2022\)](#page-13-13).

# **3 Physical dissolution of CO<sub>2</sub> in different solvents in microscale**

The knowledge of dissolution behavior of  $CO<sub>2</sub>$  in different solvents, the equilibrium between two phases and mass transfer in multi-phase systems are important to design a high-pressure system and to understand and optimize the  $CO<sub>2</sub>$  reactions. In conventional systems, samples are physically taken from the system for the analysis which disturbs the phase equilibrium. The requirement for the depressurization, cleaning, reflling and pressurization after each sampling makes the system material and time consuming. Combining microfuidic systems with optical measurement methods such as ultraviolet (UV), near-infrared, fuorescence or Raman spectroscopy enables the continuous monitoring and data acquisition (Table [1\)](#page-3-0) (Stratmann and Schweiger [2002](#page-14-19); Adami et al. [2013](#page-12-9)).

A method was developed for the economic and fast determination of binary and ternary vapor–liquid equilibrium in a microcapillary using a Raman spectroscopy (Fig. [3](#page-4-0)a). The system was operated under high pressure ranging from 6 to 10 MPa for one binary and two ternary systems consisted of acetone– $CO_2$ , acetone– $CO_2$ –water and acetone– $CO_2$ – $N_2$ , respectively. It was shown that the obtained results for binary and ternary mixtures were in agreement with literature data and the combination of microfuidic technology and Raman spectroscopy can provide reliable data without taking samples and also reduce the equipment and chemical costs (Luther et al. [2015](#page-13-14)). Blanch-Ojea et al. ([2012\)](#page-12-10) used a nonadiabatic microfuidic T-junction with a semicircular cross section to investigate the effect of temperature and pressure on the behavior of  $CO_2$ –ethanol and  $CO_2$ –methanol systems and an inverted microscope with a CCD-high speed camera

Microreactor	Mixtures	Conditions	Measurement method	Reference	
Borofloat glass microfluidic chip	$CO2$ -Ethanol $CO2$ -Methanol	7–18 MPa 294-474 K	Inverted microscope with CCD high-speed camera	Blanch-Ojea et al. (2012)	
Silica capillaries	CO <sub>2</sub> –Water	8-16.5 MPa $20 - 50$ °C	Binocular microscope with high-speed camera	Guillaument et al. (2013)	
Y-channel glass microfluidic system	CO <sub>2</sub> –Water	10 MPa $50^{\circ}$ C	High-speed camera	Ogden et al. (2014)	
Polyimide coated glass capil- laries and stainless steel T-crossing	AcceptCO <sub>2</sub> Acetone– $CO2$ –Water Acetone– $CO_2$ –Nitrogen	$6-10$ MPa 303-333 K	Phase selective Raman spec- troscopy	Luther et al. $(2015)$	
Double Y-channel glass micro- chip	CO <sub>2</sub> –Water	11.4 MPa $40^{\circ}$ C	High-speed camera	Knaust et al. $(2016)$	
Borosilicate glass microfluidic chip	$CO2-Brine$	7.45 MPa $35^{\circ}$ C	Digital camera	Zheng et al. $(2017)$	
Combination of OSTEMER and glass	$CO2$ -Ethanol	4.5-9 MPa $40^{\circ}$ C	High-speed camera	Martin et al. $(2018)$	
Glass microfluidic chip	$CO2$ , Nitrogen or Water in decane	10 MPa 50 °C	Fluorescence microscope with digital camera	Nguyen et al. $(2018)$	
T-junction silicon-glass micro- chip	CO <sub>2</sub> –Water	8.5-9.5 MPa $35^{\circ}$ C	Inverted microscope with high- speed camera	Ho et al. $(2021a)$	
PDMS channel in a metal platform	CO <sub>2</sub> –Water	6.5 MPa 23.5 $\degree$ C	Inverted microscope with high- speed camera	Ho et al. $(2021b)$	
Silica capillaries embedded in epoxy	CO <sub>2</sub> –Water	10 MPa 303 K	High-speed camera	Deleau et al. $(2022)$	

<span id="page-3-0"></span>**Table 1** CO<sub>2</sub> dissolution in different solvents in microscale

was used for the image recording. Based on the applied temperature and pressure,  $CO<sub>2</sub>$  was in liquid, gas or supercritical state and vapor–liquid equilibrium with separated phases or a single phase was obtained. For vapor–liquid equilibrium Taylor, annual and wavy flow regimes were observed and temperature was shown to be more determinant than pressure on the system. In another study, a numerical approach was developed for the modeling of  $CO<sub>2</sub>$  and water flow in a microchannel under high pressure conditions. The surface wettability was changed from hydrophilic to hydrophobic by the variation of contact angle and a continuous water phase with  $CO<sub>2</sub>$  droplets was obtained for hydrophilic state while water droplets were observed in a continuous  $CO<sub>2</sub>$ flow for hydrophobic surface that indicated the strong effect of contact angle on the fnal hydrodynamic structures shape (Guillaument et al.  $2013$ ). The influence of surface modifications on microflows of supercritical  $CO<sub>2</sub>$  and water was investigated by Knaust et al. ([2016\)](#page-13-15). A double Y-channel glass microchip was used as uncoated or coated (with hydrocarbon or fuorocarbon) forms with diferent wettings. The results showed that an increased control can be achieved for either segmentation or parallel flow with surface modifcations. The efect of fow rate and relative fow rate on the flow regime of supercritical  $CO<sub>2</sub>$ –liquid water system was evaluated in a borosilicate glass microfuidic system with a Y-channel. The segmented flow was observed even at high fow rates as a result of low viscosity of supercritical  $CO<sub>2</sub>$  and at the bifurcating exit of the microfluidic system, the splitting of supercritical  $CO<sub>2</sub>$  droplets was shown to be affected by wetting characteristics, total flow rate and droplet length while water plugs showed no such dependence (Fig. [3b](#page-4-0), c) (Ogden et al. [2014\)](#page-13-16). Martin et al. ([2018\)](#page-13-17) studied the hydrodynamics of  $CO_2$ –ethanol flow in a microchannel under high pressure conditions and investigated the efect of pressure and  $CO<sub>2</sub>$ –ethanol composition on the developed fow regime. The results showed that diferent fow regimes namely two-phase Taylor flow, dissolving Taylor flow, single-phase jetting-dissolving flow and single-phase supercritical jetting-fow depending on the pressure and mixture composition. The Taylor bubble size was also afected by pressure and mixture composition as a result of changes the density and  $CO<sub>2</sub>$  mass flow rate, respectively. The bubble size increased with increasing  $CO<sub>2</sub>$  velocity at ambient conditions but decreased in the channel before reaching the equilibrium as  $CO<sub>2</sub>$  dissolves in ethanol. Most common flow patterns in microchannels were illustrated in Fig. [3d](#page-4-0)–g.

The knowledge of the  $CO<sub>2</sub>$  dissolution in different solvents is also applicable for the studies on deep geological formations since the ocean and sedimentary rocks are the main  $CO<sub>2</sub>$  reservoirs. The field studies of  $CO<sub>2</sub>$  dissolution and solubility are expensive and time consuming. However, it is possible to mimic the diferent environmental conditions using microfuidic systems (Abolhasani et al. [2014\)](#page-12-12). Qin et al. [\(2018a](#page-14-14), [b\)](#page-14-15) used a micro T-junction to investigate the



<span id="page-4-0"></span>**Fig. 3 a** Scheme of a micro capillary combined with Raman spectroscopy to determine vapor–liquid equilibrium, reproduced with permission (Luther et al. [2015](#page-13-14)) from ACS. Splitting behaviour at bifurcating

exit of a microsystem for **b** 20 μL/min and **c** 160 μL/min, reproduced with permission (Ogden et al. [2014](#page-13-16)) from Springer. Common flow patterns in microchannels: **d** Taylor, **e** wavy, **f** annual, **g** jetting-fow

shrinkage behavior of flowing supercritical  $CO<sub>2</sub>$  microdroplets in a water-carrier fow inside a straight microchannel for the applications on deep underground or oceanic  $CO<sub>2</sub>$ storage. Nguyen et al. ([2018\)](#page-13-18) investigated the effectiveness of nitrogen and supercritical  $CO<sub>2</sub>$  in the huff-and-puff method for enhanced oil recovery since the current oil recovery methods have a low recovery efficiency of about 10%. For this purpose, they used a microfuidic system to reveal

the mechanisms and to quantify the recovery rates of oil from fracture networks. The results showed that injection of supercritical  $CO_2$  resulted in the highest recovery rate  $90\%$ and 60% while the recovery rates for  $N_2$  were 40% and 25% in the connected and dead-end fracture networks respectively since  $N_2$  has lower solubility in oil. In another study, a brine saturated microfuidic chip was used to investigate the effect of fluid viscosity, interfacial tension, injection rate

and the phase of  $CO<sub>2</sub>$  on the geological  $CO<sub>2</sub>$  sequestration (Zheng et al. [2017\)](#page-15-1).

# **4 Supercritical microreactors: materials and fabrication methods**

The main challenge for the combining of supercritical fuids and microfuidics is the design and fabrication of a system that can be operated successfully under process conditions especially elevated pressures. Several materials such as glass, metals, ceramics, polymers are available for the manufacturing of microfuidic systems. The material choice is highly dependent on the desired application conditions such as temperature, pressure, corrosivity of fuids, electrical and thermal properties and it has an impact on the selection of fabrication technique (Brandner [2013](#page-12-16)).

Rapid prototyping methods based on polymer molding are very popular as easy, fast and inexpensive fabrication techniques. Polydimethylsiloxane (PDMS) is the most commonly preferred polymer and used for the fabrication of transparent microchips which are suitable for the optical visualization and measurement techniques. However, PDMS cannot be suitable for the production of microreactors for high pressure applications since it has poor temperature and pressure resistance (Martin et al. [2016;](#page-13-19) Ostmann and Kähler [2022](#page-14-20)). To reduce the channel deformation, a PDMS channel was sandwiched between two glass slides and the channel deformation was reported to be three times lower than the standard PDMS chips. Scientists also worked on the alternative polymers that are more pressure resistant than PDMS such as thermoset polyester (TPE), polyurethane methacrylate (PUMA) or Norland Adhesive 81 (NOA81). However, their pressure resistances were still low for the supercritical applications (Sollier et al. [2011\)](#page-14-21). Martin et al. ([2016\)](#page-13-19) presented an inexpensive rapid prototyping method for the fabrication of microchannels made of UV-curable OSTEMER and glass to utilize with supercritical  $CO<sub>2</sub>$ . The fabricated microchips were shown to resist high pressures up to 20 MPa for several hours and their transparency ofered the possibility to observe and measure fow characteristics inside the microchannels (Fig. [4a](#page-5-0)).

Metals are most commonly used materials for conventional devices since they have chemical compatibility and thermal resistance. The main fabrication techniques for the metal microdevices are etching, micromachining and



<span id="page-5-0"></span>**Fig. 4** Microreactors for high pressure applications. **a** OSTOMER microreactor, reproduced with permission (Martin et al. [2016\)](#page-13-19) from Springer. **b**, **c** Si/glass microreactors, reproduced with permission

from (Trachsel et al. [2008](#page-14-22), [2009\)](#page-14-23) Elsevier. High pressure microsystem assembly. **d** scheme and **e** image, reproduced with permission (Marre et al. [2010\)](#page-13-20) from ACS

selective laser melting. A stainless-steel microreactor was used for the gasifcation of glucose to hydrogen by supercritical water and it was shown that microreactors are promising tools to intensify the thermochemical conversion of biomass constituents to chemicals and fuels (Goodwin and Rorrer [2008\)](#page-12-17). Yao et al. ([2017\)](#page-14-24) fabricated microchannels on stainless plates by chemical etching and using this microreactor, they studied the hydrodynamics and mass transfer of CO<sub>2</sub> absorption into water under elevated pressures. Ceramic microreactors are typically used for extremely high temperatures that are reachable neither with metals nor polymers. The steam reforming of propane was studied at temperatures between 800 and 1000 °C in ceramic microreactors and its potential for efficient on-site hydrogen production from hydrocarbons was reported (Christian and Kenis [2006\)](#page-12-18). Despite its feasibility to high temperature applications, the interconnection between conventional equipments and ceramic devices is critical and special needs for sealing, assembling and joining have to be considered (Brandner [2013](#page-12-16)).

Glass is another popular material for the fabrication of microfuidic systems. It is chemically resistant against almost all chemicals and its optical transparency makes it a suitable material for applications which require optical visualization or measurements. Despite glass has high chemical resistance and structural stability, its tendency to fracture under tension makes it difficult to be structured. Silicon is another material which is also commonly used for the manufacturing of microsystems. Since the glass and silicon have similar mechanical properties, same fabrication techniques are used for both materials (Frank [2008;](#page-12-19) Han et al. [2021](#page-12-20)). Glass and silicon microreactors are manufactured by photolithographic techniques. In this technique, photolithographic glass plates coated with a thin metal and upper photoresist layers and desired channel network pattern is transferred from optical mask to the photoresist layer. At the next step, photoresist is exposed to light, developed and removed which is followed by etching and bonding processes (Watts and Haswell [2005](#page-14-25)). Trachsel et al. [\(2008](#page-14-22)) fabricated a Si/glass microreactor by a standard photolithography and dry etching technique and stainless steel capillaries were connected to microreactor by soldering (Fig. [4](#page-5-0)b). The system was mechanically tested by tensile and pressure tests and successfully applied for solid catalyzed exothermic hydrogenation at 5.1 MPa and 71 °C conditions. In the further study, they improved their design by adding a meandering mixing section (Fig. [4c](#page-5-0)) and used this microreactor for hydrogenation of cyclohexane by supercritical  $CO_2$  (Trachsel et al. [2009\)](#page-14-23). Tiggelaar et al. [\(2007\)](#page-14-26) used a glass microreactor to study the formation of the carbamic acid by the reaction of N-benzylmethylamine and  $CO<sub>2</sub>$ under high pressure conditions and reported that the glass microreactor could be used for pressures up to 40 MPa without failure. In another study, a microfuidic device fabricated by embedding the silicon capillaries in epoxy resin was suggested as transparent and inexpensive system for high pressure applications. They conducted experiments in an ionic liquid and supercritical  $CO<sub>2</sub>$  flow under isothermal conditions. The two-phase fow system was observed with a highspeed camera and operating pressures up to 30 MPa could be achieved in this system (Macedo Portela da Silva et al. [2014\)](#page-13-21). Although the low thermal conductivity of glass limits its applications requiring good heat transfer, the high pressures can be reached using glass microreactors and they can be successfully used with supercritical  $CO<sub>2</sub>$  which has a low critical temperature value.

The connection of microfuidic systems to the macroscopic fuid handling systems is more challenging when working under supercritical conditions. Since the fuidic connections can be fabricated to ft the commercially available fttings, metal microreactors can be easily packed. For other microreactors, permanent integrated connections can be used to connect tubings. Marre et al. ([2010\)](#page-13-20) used a modular design consisting of two stainless steel parts with O-rings to compress the silicon/Pyrex microreactor (Fig. [4](#page-5-0)d, e).

# **5 Supercritical microfuidic applications of CO<sub>2</sub>**

#### **5.1 Extraction**

Supercritical  $CO<sub>2</sub>$  is a green alternative to organic solvents in biorefnery applications such as biomass pretreatment, extraction and chemical conversion and has been proven commercially for coffee decaffeination and hops extraction. It is a common knowledge that solvent properties of supercritical  $CO<sub>2</sub>$  such as polarity, density and viscosity can be easily tuned by small variations in temperature and pressure. While high density of  $CO<sub>2</sub>$  under supercritical conditions contributes to solubilisation of compounds, low viscosity enhances penetration into extraction matrix, thus challenging extraction processes can be easily conducted by supercritical  $CO<sub>2</sub>$ . The low surface tension and absence of product contamination with solvent residues are other distinct advantages of supercritical  $CO<sub>2</sub>$  for extraction processes. In addition, properties such as electronic structure and charge separation affect the solvent properties of  $CO<sub>2</sub>$ . For instance,  $CO<sub>2</sub>$  can act as a Lewis base or acid and participate in hydrogen bond interactions that lead the specifc solute–solvent interaction and selective extraction of diferent compounds. Apart from solubility properties, external control and internal limitations for mass transfer signifcantly affect the rate of supercritical  $CO<sub>2</sub>$  extraction. Supercritical extraction processes mainly focus on extract yield which is not only dependent on temperature and pressure conditions but also physical characteristics of extraction matrix such porosity, density and geometry of bed, particle size and particle size distribution (Weibel and Ober [2003;](#page-14-27) Sahena et al. [2009](#page-14-8); Huang et al. [2012;](#page-13-22) Kazan et al. [2014](#page-13-23); Zhu et al. [2018](#page-15-0); Kwan et al. [2018\)](#page-13-24). Integration of supercritical extraction in microfuidic systems has drawn attention with the advantages of precise control and accelerated extraction properties. However, the main disadvantage of these systems is the separation since surface forces dominates over body forces in micro scale and separation by gravity cannot be applied.

Continuous extraction of vanillin, an important favoring agent, was carried out by segmented fow of supercritical  $CO<sub>2</sub>$  in a silicon/glass microextractor which was integrated with a capillary separation device (Fig. [5a](#page-7-0), b). The system operated under 8–11 MPa and equilibrium was reached after pretty short time (1.6–2.8 s) with highly reproducible equilibrium concentrations (Assmann et al. [2012\)](#page-12-21). Cheng et al. [\(2018\)](#page-12-22) performed supercritical  $CO<sub>2</sub>$  extraction of astaxanthin from *Haematococcus pluvialis* in a microfuidic reactor. A hydrothermal cell disruption step was added before the extraction since the direct extraction of wet microalgae biomass using supercritical  $CO<sub>2</sub>$  is generally not feasible as a result of the rigid cell wall. First, the cells were loaded into the microfluidic reactor and hydrothermal disruption of the cells was carried out at 200 °C and 8 MPa for 10 min that provided uniform and thorough disruption to all cells. Then, supercritical  $CO<sub>2</sub>$  extraction was carried out on disrupted cells with pure or co-solvent added  $CO<sub>2</sub>$  and a dark-feld microscope was used to observe the cells and the color change. The timescales of extraction process at 55 °C were reduced 1800-fold from 15 h to 30 s by the addition of ethanol as a co-solvent while the extraction was completed in 180 s for the using of olive oil as a co-solvent instead of ethanol. Assmann et al.  $(2013)$  $(2013)$  $(2013)$  used a continuous flow microfuidic device for direct extraction of lignin oxidation products such as vanillin, methyl vanillate and 5-carbomethoxy-vanillin from aqueous reaction mixture using supercritical  $CO<sub>2</sub>$  as a solvent. Higher quantities of monomers were extracted with increasing pressure and decreasing temperature with high selectivity. The results showed that diferent selectivity of supercritical  $CO<sub>2</sub>$  towards lignin oxidation products makes it a suitable solvent for separation and enables the use of this method to remove methyl 5-carbomethoxy-vanillate and concentrate vanillin and methyl vanillate in the raffinate phase.

Supercritical fuids are also used for the extraction of metal complexes from solid and aqueous media as an alternative to traditional solvent extraction methods. Ohashi et al. ([2011\)](#page-13-25) developed a microfuidic system to measure the distribution of tris(acetylacetonato)-cobalt(III)  $(Co (acac)<sub>3</sub>)$ between supercritical  $CO<sub>2</sub>$  and water. A glass microchip with and without modifcation by dichlorodimethylsilane was used and modifcation was shown to induce phase separation of  $CO_2$  and water inside microchannel and the  $(Co (acac)<sub>3</sub>)$ concentration in aqueous phase increased by the increasing the contact time of two phases.

#### **5.2 Reactions in microreactor with supercritical CO<sub>2</sub>**

Compared to the batch systems, continuously operated microfuidic systems allow the fast screening of reaction



<span id="page-7-0"></span>**Fig. 5 a** Silicon/glass microdevice and **b** scheme of the high pressure plant for vanillin extraction, reproduced with permission from (Assmann et al. [2012\)](#page-12-21) Elsevier. **c** Photograph of a microreactor for

phthalic anhydride esterifcation, reproduced with permission from (Benito-Lopez et al. [2007](#page-12-24)) RSC

conditions, consume small amount of reagents and due to the small volumes, minimize the risk that may arise from elevated pressure and temperature under supercritical conditions (Assmann et al. [2013](#page-12-23); Kazan et al. [2017](#page-13-26)). Enhanced heat and mass transfer properties lead to efective control of reaction conditions and make the microfuidic systems more advantageous to carry out highly exothermic reactions.

The variations in temperature and pressure afect some properties of supercritical  $CO<sub>2</sub>$  such as viscosity, density and dielectric constant and result in changes in reaction yields, kinetics and selectivity. Benito-Lopez et al. [\(2007\)](#page-12-24) described a glass microrector and studied the effects of pressure and supercritical  $CO<sub>2</sub>$  on the reaction rate of phthalic anhydride esterifcation (Fig. [5](#page-7-0)c). It was shown that the use of a microreactor for the esterifcation reaction enhanced the reaction rate constant even at low pressures  $(1.6 \times 10^{-3}$ and  $3.1 \times 10^{-3}$  M<sup>-1</sup> s<sup>-1</sup> at 9 and 11 MPa, respectively) and the ratio of microreactor and batch reaction rate constants increased with increasing temperature. Compared to conventional reaction systems, microreactors operated in continuous fow mode with pressure showed to signifcantly enhance the reaction rate. In another study, supercritical  $CO<sub>2</sub>$  was used as a solvent for the esterification of oleic acid with methanol in a microfuidic device. Results showed that esterifcation reaction occurred in less than 1 min even without any catalyst and addition of small amount of catalyst increased the yield fourfold and rate constant of uncatalyzed and catalyzed reactions were calculated as 0.0036 and  $0.0634$  s<sup>-1</sup>, respectively (Quitain et al. [2018\)](#page-14-28).

Hydrogenation reactions are a class of reactions which are important for pharmaceutical and chemical industries. The low interaction efficiency and mass transfer between different phases result in slow reaction rates. Since the transfer rate of hydrogen from gas phase to liquid phase is critical for the reaction rate, it is important to overcome both heat and mass transfer limitations between two phases. Although the addition of equipment for a higher interfacial area, variation of stirring speed or particle size are commonly used to enhance the mass transfer, these approaches have still limitations. In addition, transport limitations were shown to afect the product distribution for the hydrogenation of fatty oils over Ni catalyst. Therefore, development of new systems with higher interfacial area becomes important to enhance the mass and heat transfer between two phases (Singh and Vannice [2001;](#page-14-29) Kobayashi et al. [2004\)](#page-13-27). With large interfacial area and efective heat and mass transfer properties, microfuidics can be used as an alternative system for the hydrogenation reactions. Although the mechanism is not clear, solvent type also affects the reaction rate and product distribution probably by the solvent polarity or dielectric constant. While supercritical  $CO<sub>2</sub>$  has liquid-like properties that allow the dissolution of several organic compounds, its gas-like properties make it highly miscible in other gases such as hydrogen. The combination of supercritical  $CO<sub>2</sub>$  and microfuidics create a suitable system for high performance hydrogenation reactions. A Pd-immobilized microchannel reactor was prepared for the hydrogenation reaction in supercritical  $CO<sub>2</sub>$  and a variety of substrates were used and converted to desired products successfully. The reaction time was less than a second and using of supercritical  $CO<sub>2</sub>$  as a solvent both increased the solubility of hydrogen and productivity  $(0.1 \text{ mmol h}^{-1}$  per channel) compared to the experiments using tetrahydrofuran as a solvent  $(0.01 \text{ mmol h}^{-1})$  per channel) (Kobayashi et al. [2005](#page-13-28)). In another study, a packed bed Si/glass microreactor fabricated by photolithography was used for the hydrogenation of cyclohexene and supercritical  $CO<sub>2</sub>$  was used as reaction solvent. The microfluidic systems contained three inlets: cyclohexene and  $H_2$  were pumped through separate inlets to generate a segmented gas–liquid flow and supercritical  $CO<sub>2</sub>$  was pumped through the third inlet to dissolve the cyclohexene– $H_2$  mixture. To obtain a single phase reaction mixture, a meandering mixing channel was added to microreactor design which was followed by a packed bed channel containing catalyst particles. Molar ratio of  $CO_2$ :cyclohexene:H<sub>2</sub> kept constant at 90:5:5, temperature and pressure were varied to determine the efect of operating conditions on reaction performance. An increase about fvefold in reaction rate with increasing temperature from 40 to 70 °C was observed while pressure showed no significant effect on reaction rate. Performances of different reactor systems were compared in terms of space time yield  $(kg_{product}/hm^3_{\text{catalyst}})$  and the space time yield was one order of magnitude greater than larger scale systems. The results indicated that high pressure microreactor system was suitable for exothermic reactions as a result of efective heat removal characteristic (Trachsel et al. [2009\)](#page-14-23). Urakawa et al. ([2008\)](#page-14-30) combined this system with Raman spectroscopy to fast and simultaneous analysis of product concentration profile of cyclohexene hydrogenation in supercritical  $CO<sub>2</sub>$ . After mixing in meandering channel, the Raman spectrum showed only the characteristic bands of cyclohexene, while the product, cyclohexane, band gradually increased as the mixture fowed through the packed catalyst bed and the fnal conversion could be monitored at the outlet channel. Table [2](#page-9-0) summarizes high pressure reactions in microfuidic systems.

## **5.3 Synthesis of micro and nano sized materials in microfuidics**

In microfuidic systems, fuids can fow in single-phase or multi-phase state for miscible and immiscible fuids, respectively. For immiscible fuids, fuids can be either coflow or discontinuous flow of one fluid as droplets in the continuous fow of other fuid which is called as droplet microfuidics. Droplet microfuidics can also be applied to

Microreactor	Reaction	Conditions	Catalyst	Reaction time Main result		Reference
Glass microreactor	Esterification of phtalic anhydride with methanol	20–100 °C 9 and 11 MPa			Reaction rate enhancement	Benito-Lopez et al. (2007)
Stainless steel micro- reactor	Esterification of oleic $60-100$ °C 10 MPa acid with methanol		$H_2SO_4$	$<$ 1 min	fourfold increase in reaction yield	Ouitain et al. (2018)
Pd-immobilized glass microreactor	Hydrogenation of dif- ferent substrates	60 °C 9 MPa	Pd	1 s	High reaction pro- ductivity	Kobayashi et al. (2005)
Packed bed Si/glass microreactor	Hydrogenation of cyclohexene	40–70 °C 8 -15 MPa	$Pd/Al_2O_2$ –		Larger space time yield	Trachsel et al. $(2009)$
Packed bed Si/glass microreactor	Hydrogenation of cyclohexene	305-318 K 10 MPa	$Pd/Al_2O_3$ –		Potential of on-chip Raman analysis	Urakawa et al., 2008

<span id="page-9-0"></span>**Table 2** High pressure reactions in microfuidic systems

gas–liquid systems where the droplets were replaced with gas bubbles (Abolhasani et al. [2014](#page-12-12)).

Microbubbles, which consist of a shell and gas core, are theranostic agents that provide contrast for imaging (diagnostic) and drug delivery for targeted therapy simultaneously. The diameter of a microbubble is less than 10 μm which is equal to the size of a red blood cell. Since the bubbles at this size are unstable in aqueous media, surfactants, lipids, proteins and polymers are used separately or in combination to stabilize the shell structure. Microbubbles resonate by the sound wave of the ultrasound equipment and create a high contrast as a result of the diferent acoustic response of resonating microbubbles and surrounding tissue. The size of each microbubble is important and should be in a narrow range to obtain information with high efficiency. Although their properties have to be tailored to strict specifcations in medical applications, conventional microbubble preparation methods like sonication or layer-by-layer biopolymer deposition are insufficient to produce bubbles with controlled size. On the other hand, microfuidic systems provide an environment with a precise control for the microbubble formation (Ahmad et al. [2008](#page-12-25); Yang et al. [2009](#page-14-31); Sirsi and Borden [2009;](#page-14-32) Enayati et al. [2011](#page-12-26)). Tumarkin et al. ([2011\)](#page-14-33) used a microfuidic device to produce highly monodisperse particle-coated microbubbles and the response of  $CO<sub>2</sub>$  bubbles to the temperature variation was examined. They showed that the size of  $CO<sub>2</sub>$  bubbles decreased by lowering temperature as a result of enhanced  $CO<sub>2</sub>$  dissolution in water at reduced temperatures. In another study, an aqueous NaOH solution containing poly(styrene-*co*acrylic acid) nanoparticles and gaseous  $CO<sub>2</sub>$  were fed to a microfuidic device with a T-junction to produce plugs of  $CO<sub>2</sub>$ . Stable armored bubbles were obtained with a narrow size distribution (polydispersity of 2–5%) and method productivity was increased from 700 bubbles/s to 3000 bubbles/s by a microfuidic fow-focusing bubble generator (Park et al. [2009\)](#page-14-34).

Supercritical fuids are used for the preparation of microand nanoparticles for many years and supercritical  $CO<sub>2</sub>$  is one of the most attractive solvent due to its mild processing conditions. Mixing is the one of the most important parameter during particle synthesis and has a signifcant impact on particle size and size distribution. Since microsystems provide a strict control on synthesis conditions and enhanced mixing performance, supercritical microfuidics are more advantageous over conventional particle preparation approaches to produce particles with uniform size distribution in a narrow range. A high pressure silicon-Pyrex microreactor was designed for the preparation of poly-(3-hexylthiophene) (P3HT) nanoparticles by supercritical antisolvent (SAS) process (Fig. [6a](#page-10-0)). The system was operated under 40–50 °C temperature and 8–10 MPa pressure ranges.  $CO<sub>2</sub>$ was fed to system and after it reached the desired temperature and pressure values, P3HT solution was fed through the mixing point creating a full 3D coaxial injection. A jet was formed between the  $CO<sub>2</sub>$  and P3HT solution at the mixing point and quickly disappeared upon fast mixing leading to nanoparticle nucleation with an average size of 36 nm (Couto et al. [2015](#page-12-27)). Jaouhari et al. ([2020\)](#page-13-29) combined supercritical antisolvent (SAS) process and microfuidic systems to improve the control, performance and the reproducibility of the operation. Tetrahydrofuran (THF) was used as the solvent while supercritical  $CO<sub>2</sub>$  was antisolvent and tetraphenylethylene (TPE) nanoparticles were synthesized in a homemade silicon-Pyrex microchip under 40 °C and 10 MPa. Obtained nanoparticles were analyzed with transmission electron microscope and specifed by having particle sizes below 15 nm. Results also showed that the variation of experimental parameters such as initial TPE concentration and flow rates strongly affect the hydrodynamics of mixing process and mean particle size.

Jaouhari et al. [\(2022](#page-13-30)) fabricated a Pyrex/silicon microfuidic device by photolithography/wet etching/anodic bonding protocol. The device was used as a micromixer and operated under 40 °C and 10 MPa to analyze mixing, nucleation and



<span id="page-10-0"></span>**Fig. 6 a** Microsystem for P3HT nanoparticle synthesis, reproduced with permission from (Couto et al. [2015](#page-12-27)) RSC. **b** Micro-capillary system for emulsion extraction, reproduced with permission from

(Luther and Braeuer [2012](#page-13-31)) Elsevier. **c** Microreactor for quantum dot synthesis, reproduced with permission from (Yen et al. [2005\)](#page-15-2) Wiley

growth characteristics in THF/scCO<sub>2</sub> system. A fluorescent organic dye molecule was used for in situ visualization and particles with a mean size of 16 nm were successfully prepared.

Extraction of emulsions is another application of supercritical  $CO<sub>2</sub>$  for the production of nanoparticles. For instance, cholesterol acetate, griseofulvin and megestrol acetate nanoparticles were produced by extraction of oil-inwater emulsions using supercritical carbon dioxide (Shekunov et al. [2006\)](#page-14-35). Ajiboye et al. ([2018\)](#page-12-28) produced polycaprolactone (PCL) nanoparticles via supercritical fuid extraction of emulsions using supercritical  $CO<sub>2</sub>$  and spherical nanoparticles with mean particle sizes between 190 and 350 nm were obtained depending on the polymer concentration. Recently, microfuidic devices have been used for the emulsion extraction under high pressure conditions. In this approach, supercritical  $CO<sub>2</sub>$  was used to rapidly extract the solvent or oil phase of an emulsion that leads the precipitation of solute and results in an aqueous suspension containing nanoparticles. Luther and Braeuer ([2012\)](#page-13-31) used a microfuidic device consisting of thin fused silica capillaries to investigate the ethyl acetate–water–supercritical  $CO<sub>2</sub>$  solvent system for the particle formation by supercritical fuid extraction of emulsions method (Fig. [6b](#page-10-0)). They reported that properties of microfuidic systems provided homogenous conditions, fast process control and detection and production of monodisperse emulsion. In another work, supercritical  $CO<sub>2</sub>$  was applied to a microfuidic system with a T-junction for the

extraction of polyvinyl alcohol nanoparticles from ethyl acetate-water emulsion and slug-fow patterns were captured by a camera. No residual ethyl acetate was observed in the suspension that indicated the successful extraction of the ethyl acetate in emulsion by supercritical  $CO<sub>2</sub>$  and authors pointed their expectation for the reduction of cost and operation time for the production of nanoparticle suspensions in a microfluidic slug-flow system using supercritical  $CO<sub>2</sub>$ (Murakami and Shimoyama [2016\)](#page-13-32). Ibuprofen nanosuspension was fabricated by supercritical fuid extraction of emulsion in a microfuidic system and prepared nanoparticles were functionalized by chitosan. Authors showed that the size of particles in the suspension could be controlled by the amount of ibuprofen loaded in ethyl acetate droplets in ethyl acetate/water emulsion (Murakami and Shimoyama [2017](#page-13-33)). The effect of supercritical carbon dioxide on the formation and stability of water-in-oil emulsions was investigated under high pressure conditions. For this purpose, a Y-junction made of PMMA was designed and operated at pressures from 0.1 to 15 MPa with by monitoring with a high-speed camera. It was reported that larger droplets and thicker jets were produced with increasing pressure as a result of low capillary numbers and high Weber numbers (Jaouhari et al. [2020](#page-13-29)).

Nanometer-sized colloidal crystals, nanocrystals, have various applications in optoelectronics, catalyst and nanomedicine. For a successful application, properties of nanocrystals such as well-defned size, shape, composition

and crystallinity are important in all application felds. The main problem of the conventional production methods is the diference in product quality between batches. For improved product control, the better uniformity in thermal and chemical environment can be obtained using microfuidic systems (Phillips et al. [2014](#page-14-36)). The frst microfabricated gas–liquid segmented flow for high temperature nanocrystal synthesis was reported by Yen et al. ([2005\)](#page-15-2) (Fig. [6](#page-10-0)c). They prepared CdSe quantum dots from cadmium 2,4-pentanedionate and selenium at 260 °C. They showed that good size control could be achieved by tuning the injection rates of the cadmium an selenium precursor solutions and signifcantly narrower emission spectra than an equivalent single-phase synthesis was reported. The advantage of using a supercritical fuid for the nanocrystal synthesis was demonstrated in a study in which a high pressure high temperature microreactor and supercritical hexane was used for CdSe quantum dot synthesis (Marre et al. [2008\)](#page-13-12). Size distribution of quantum dots synthesized in supercritical hexane and in liquid phase was 4–6% and 9–12%, respectively that showed the advantage of microfuidic system with narrower residence time distribution and more homogenous reaction conditions. In another study, exciton luminescent ZnO nanocrystals were synthesized using continuous supercritical microfuidics and

<span id="page-11-0"></span>**Table 3** Micro and nano sized material synthesis in microfuidics

obtained ZnO nanocrystals with a better control in size and shape (Roig et al. [2011\)](#page-14-37). Palladium nanocrystals were synthesized in a co-fow capillary microsystem by the hydrogen reduction of palladium (II) precursors in the presence of organic stabilizers. Since the hydrogen is poorly soluble in toluene, a commonly used solvent, supercritical  $CO<sub>2</sub>$  was added to toluene to enhance the hydrogen solubility. Catalytic activity of nanocrystals is highly dependent on surface properties and co-axial fow was shown to allow precise construction of the catalyst architectures, as intended for a targeted reaction (Gendrineau et al. [2012](#page-12-29)). Table [3](#page-11-0) summarizes micro and nano-sized material synthesis in microfuidic systems.

## **6 Conclusions**

This paper presents a short overview of the supercritical  $CO<sub>2</sub>$ applications in microfuidic systems. Although the critical point of a substance was discovered in early nineteenth century, frst applications of supercritical fuids were started in mid 1900s and gained a huge attention over the last decades. As a newly developed feld, supercritical microfuidics has a great advantage by combining the properties of supercritical



fuids and microfuidics and already proved its potential with highly efficient and selective extraction processes, improved reaction conditions and strict control of particle formation. It is expected that the interest in supercritical microfuidics will continue to increase and advances in high pressure technologies and microfabrication techniques will open up new pathways for novel applications.

#### **Declarations**

**Conflict of interest** The author has no relevant fnancial or non-fnancial interests to disclose.

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