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Thermostat choice significantly influences water flow rates in molecular dynamics studies of carbon nanotubes

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Abstract Extremely rapid water flow through carbon nanotubes has been observed in both experiment and simulation which has led to the suggestion that this material be used in a number of filtration applications. However, there is significant disparity in the magnitude of water permeability and the degree of flow enhancement compared with conventional porous materials in the literature. Here, we show that one of the causes of the disparity in simulation data is the variety of methods used to control temperature in molecular simulations. Not only can the choice of thermostat alter the flow rate and permeability by as much as five times, but it can determine whether the transport is observed to be frictionless or not. In addition to helping explain the disparate simulation results on transport in nanomaterials, this work provides some guidelines to help designing and interpreting molecular simulations of mass transport.

1 Introduction

Carbon nanotubes have been suggested for use in a vast number of applications including the desalination of sea

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water; the removal of dangerous contaminants from water supplies; the separations of gases, ions and biomolecules; the sequencing of DNA in electrical devices and biosensors; and in nanofluidic devices. All of the listed uses involve flowing liquids or gases through the interior of the nanotubes to make use of the highly regular structure of the pores and their unusual transport properties. Water has been shown to flow through nanotubes with very high fluxes, in both experimental (Majumder et al. [2005;](#page-6-0) Holt et al. [2006](#page-5-0)) and simulation studies, (Hummer et al. [2001](#page-5-0); Kalra et al. [2003;](#page-6-0) Corry [2008](#page-5-0); Joseph and Aluru [2008](#page-6-0); Thomas and McGaughey [2008;](#page-6-0) Song and Corry [2009](#page-6-0); Thomas et al. [2010;](#page-6-0) Corry [2011;](#page-5-0) Ritos et al. [2014](#page-6-0)) with the interior of the nanotube suggested to provide a nearfrictionless surface to water permeation. However, the predicted flow rates in the tubes differ by more than an order of magnitude amongst the many simulation studies, which is significant given that the magnitude of the water flux is essential to many of the suggested applications. Furthermore, while some studies claim no influence of nanotube length on the flow rate of water and infer frictionless flow (Kalra et al. [2003;](#page-6-0) Corry [2008;](#page-5-0) Nicholls et al. [2012a\)](#page-6-0), other studies suggest decreasing flow rates with pore length (Su and Guo [2012\)](#page-6-0). If molecular dynamics simulations are to be used to guide and understand the development of nanotube based technologies, then it is important that these disparate simulation results be reconciled.

One factor that may partly explain the different results from these studies is the distinct ways in which temperatures are controlled in these simulations. Usually simulations are compared to experimental conditions in which the average temperature of the system is constant. However, unmodified simulations yield a microcanonical ensemble in which the temperature is not controlled, but rather the

number of atoms N, volume V and energy of the system E is maintained. Thus, simulations will typically modify the dynamics of the system with a thermostating algorithm to control the simulation temperature; but different algorithms can yield differing dynamics (Hunenberger [2005](#page-5-0); Stoyanov and Groot [2005;](#page-6-0) Rosta et al. [2009\)](#page-6-0). While some of the published simulations examining flow rates in carbon and other nanotubes employ a Berendsen thermostat (Hummer et al. [2001](#page-5-0); Kalra et al. [2003;](#page-6-0) Peter and Hummer [2005;](#page-6-0) Won et al. [2006;](#page-6-0) Thomas and McGaughey [2008;](#page-6-0) Thomas et al. [2010;](#page-6-0) Nicholls et al. [2012a,](#page-6-0) [b\)](#page-6-0), other use a Nose–Hoover (Won and Aluru [2007;](#page-6-0) Joseph and Aluru [2008](#page-6-0); Won and Aluru [2008;](#page-6-0) Khademi and Sahimi [2011](#page-6-0); Cohen-Tanugi and Grossman [2012](#page-5-0); Su and Guo [2012;](#page-6-0) Kannam et al. [2013](#page-6-0)), Langevin (Corry [2008;](#page-5-0) Hilder et al. [2009](#page-5-0); Song and Corry [2009;](#page-6-0) Hilder et al. [2010](#page-5-0); Corry [2011;](#page-5-0) Majumder and Corry [2011\)](#page-6-0) or Gaussian (Liu et al. [2006](#page-6-0)) thermostat. A number of other studies do not specify how the temperature is controlled (Zhu and Schulten [2003;](#page-6-0) Li et al. [2007](#page-6-0); Gong et al. [2008;](#page-5-0) Suk et al. [2008](#page-6-0); Gong et al. [2010](#page-5-0)).

The precise influence of thermostating methods on the outcomes of molecular simulations is still not well understood, but previous studies have shown that temperature control algorithms can alter the dynamics of the system with respect to the microcanonical ensemble by, for example, damping the diffusion and rotational motion of molecules in the simulation. Furthermore, it has also been shown that different algorithms that adjust particle velocities in different ways can give significantly different dynamic properties (Basconi and Shirts [2013;](#page-5-0) Krishnan et al. [2013\)](#page-6-0). In particular, it has been shown that the selfdiffusivity, rotational correlation time and shear viscosity of water can all be altered by the thermostat choice (Basconi and Shirts [2013](#page-5-0)). While these studies examine the dynamics of liquids and solutes under equilibrium conditions, to our knowledge no systematic study has been made to examine the influence of temperature control algorithm in simulations of mass transport, in which there is directional flow of particles. Given the enormous interest in understanding mass transport in biological and synthetic nanoscale pores, we believe it is essential to see how different thermostating algorithms alter the simulated transport properties.

Here, we show that the water permeability and fluxes through carbon nanotube membranes found in molecular dynamics simulations are highly dependent on the thermostat that is used and that thermostat choice can have profound implications on whether friction is found within the flow. Not only does this help to explain some of the discrepancies amongst the published simulation data, it also provides a benchmark to aid in choosing the most appropriate thermostat in future simulations of mass transport.

2 Theoretical background

A large number of methods have been developed to control the temperature in molecular dynamics simulations. Rather than give a complete introduction to these here, we provide a summary of some of the differences critical to understanding this work and refer the reader to some excellent previous publications for further details. (Hunenberger [2005](#page-5-0); Stoyanov and Groot [2005](#page-6-0); Basconi and Shirts [2013](#page-5-0)).

As noted above, without applying a mechanism to control temperature, the simulations proceed in the microcanonical ensemble (NVE) according to Newton's equation of motion:

$$
m_i \frac{d^2 \mathbf{r}_i}{dt^2} = \mathbf{F}_i(\mathbf{r}_i)
$$

in which m , r and \overline{F} are the mass, position and force acting on each atom i. The instantaneous temperature of the system (T) is directly related to the particle velocities via,

$$
T = \frac{\sum_{i=1}^{N} m_i v_i^2}{3Nk}
$$

where k is the Boltzmann constant, N is the number of atoms each of which has mass m and velocity v . Thus, to control the temperature either the velocities of the particles or the equation of motion itself is modified. All of these approaches have the effect of coupling the system to a fictitious heat bath, and the degree of coupling determines how quickly deviations in from the target temperature are reined in. For understanding the influence of the thermostat algorithm on dynamic properties, it is useful to divide them into two categories following the lead of Basconi and Shirts [\(2013](#page-5-0)).

In the first group of algorithms, the velocities of particles are rescaled at regular intervals to bring the average temperature back towards the target value. This can be done by directly scaling the velocity of every particle individually, or more commonly be rescaling them together by a common factor such that the target temperature is automatically achieved. This second approach is the 'direct rescaling' method examined below. Alternatively, the rescaling can be done in a more subtle way so that the temperature decays more slowly towards the target value as in the Berendsen thermostat (Berendsen et al. [1984\)](#page-5-0) In this the particle velocities are scaled by a common factor such that the deviation of the instantaneous temperature from the target value (T_0) decays with a time constant τ :

$$
\frac{dT}{dt} = \frac{T_0 - T}{\tau}
$$

The Nose–Hoover method also scales the temperature so that it relaxes in an oscillatory manner towards the target value, but this is done using an extended system that incorporates terms relating to the heat bath (η) in the equation of motion (Nose [1984](#page-6-0); Hoover [1985\)](#page-5-0). Here, the velocities are scaled by a variable $p_{\eta} = Q^{d\eta}/dt$ equivalent to the momentum of the heat bath η of mass Q which is coupled to each particle and the instantaneous temperature of the system via the following coupled equations of motion

$$
\frac{d^2r_i}{dt^2} = \frac{F_i(r_i)}{m_i} - \frac{p_\eta}{Q}\frac{dr_i}{dt}
$$

$$
\frac{d^2\eta}{dt^2} = \frac{T - T_0}{Q}
$$

In the second group of algorithms, particle velocities are randomised rather than being scaled. In the Andersen thermostat, this is done by randomly choosing new velocities for some of the particles at regular intervals from a Boltzmann distribution at the desired temperature (Andersen [1980](#page-5-0)). The Lowe–Andersen thermostat used in our study is a modification of this, in which the relative velocity of pairs of particles is randomized instead of the velocities of individual particles themselves (Koopman and Lowe [2006\)](#page-6-0). This has the advantage of conserving linear and angular momentum. In Langevin dynamics, the equation of motion is modified to include additional frictional (γ) and random forces (R) on the individual particles

$$
m_i \frac{d^2 \mathbf{r}_i}{dt^2} = \mathbf{F}_i(\mathbf{r}_i) + m_i \gamma_i \frac{d \mathbf{r}_i}{dt} + \mathbf{R}_i(t)
$$

The choice of the friction constant (which is usually the same for all atoms in the system) and the strength of the random forces will dictate the final system temperature.

3 Results

To assess the magnitude of water flux, whether the water flow through single-walled carbon nanotubes is frictionless, and how this is influenced by the choice of thermostat, we determine the pressure-driven flow in (10,10) armchairtype carbon nanotubes (diameter 1.4 nm) of three different lengths (1.4, 5 and 10 nm) using four different thermostats: a direct velocity rescaling method, Lowe–Andersen, Langevin and a modified Langevin thermostat. Published data from pressure-driven simulations of (8,8) carbon nanotubes under a Nose–Hoover thermostat (Su and Guo [2012\)](#page-6-0) and a (7,7) nanotube with a Berendsen thermostat (Nicholls et al. [2012a](#page-6-0)) is also shown for comparison. While these studies employ slightly different water–CNT interactions and the later uses a TIP4P water model rather than TIP3P, we can still gain qualitative information about how the flow rate changes with nanotube length. Our simulation system comprises twelve nanotubes placed in a 3×4

Fig. 1 An example of the main simulation system used in this study. $A 4 \times 3$ array is made from (10,10) carbon nanotubes which separate two water-filled reservoirs. A periodic system in each dimension is used, and force is applied to water oxygen atoms in the pressure application region to generate a hydrostatic pressure difference across the nanotube array. Studies are made of nanotubes of 3 different lengths: 1.4, 5 and 10 nm

hexagonal array to form a membrane which is bounded on either side by a water box. A hydrostatic pressure difference is generated across the membrane using a method developed by Zhu and Schulten ([2003\)](#page-6-0) and implemented in many studies. In this, a force in the direction of the nanotube axis is applied to the oxygen atoms of water molecules in the half of each solvation box most distant from the membrane, as illustrated in Fig. 1. The water flux through the nanotubes was determined for a range of pressures (\sim 50–400 MPa), allowing us to calculate the permeability of the membrane from the slope of the flux versus pressure graph. Additional simulation details are given in the supplementary material.

In Fig. [2a](#page-3-0), we show how the water flux through the 1.4 nm-long nanotube changes with the hydrostatic pressure difference using four different thermostating methods. In all cases, the flux scales linearly with pressure as has been observed previously (Corry [2008](#page-5-0)), but the magnitude of the flux differs significantly with thermostat choice. Notably, the flux is almost thrice larger for the direct rescaling and Lowe–Andersen thermostats than it is using the Langevin thermostat with the default-coupling parameters in NAMD. Clearly, the choice of thermostat can influence the calculated water flux or flow enhancement found in simulations.

Fig. 2 Simulated water permeabilities with different thermostats. **a** The water flux at various pressures for a 4×3 array of 1.4–nmlong (10,10) carbon nanotubes for four different thermostats. A line of best fit is shown for each thermostat. **b** The permeability of 4×3 array of (10,10) carbon nanotubes of various length using different thermostat methods. c The percentage permeability relative to the shortest nanotube system found with different thermostats. Nanotubes

Ideally, we would like to compare the flow rates predicted by the simulations reported here with equivalent experimental measurements in order to know which protocol produces the best results. However, such a comparison is far from straightforward for two major reasons. Firstly, there are significant differences in the magnitude of flow rates seen in the various experimental studies (Ritos et al. [2014\)](#page-6-0). The major reason for this is that the experiments are conducted on different membranes containing different types of nanotubes, constructed in different ways. Secondly, the experiments are all made on systems containing a large number of nanotubes whose precise physical characteristics (such as length, width, chirality and defects) are not well defined. In contrast, simulations such as this are typically made on a small number of well-defined pristine nanotubes. While these simulations do see very rough order of magnitude agreement in terms of flow

are either constructed as 4×3 arrays, or as a single nanotube between a graphene bilayer. Values for the Nose–Hoover and Berendsen thermostats are taken from (Su and Guo [2012\)](#page-6-0) and (Nicholls et al. [2012a](#page-6-0)), respectively. **d** The water flux through a 4×3 array of 1.4-nm-long, (10,10) carbon nanotubes at 410 MPa for various values of the partial Langevin dynamics-coupling coefficient

enhancement over macroscopic theory as in experiment, (Ritos et al. [2014](#page-6-0)) a precise comparison of experimental and simulated flow rates cannot be made until the gulf between the systems being studied is overcome. This study aims to start bridging this gulf by determining inconsistencies in the simulation protocol.

Many simulation studies have suggested that the water flow through carbon nanotubes is near-frictionless, which implies that the permeability of the nanotubes is independent of their length. To assess whether the thermostat algorithm can influence the observed friction in the tubes, in Fig. 2b we plot the water permeability as a function of the nanotube length, while in Fig. 2c we show the permeability as a percentage of that found in the shortest tube. The permeability remains approximately the same across the different tube lengths using direct rescaling and Lowe– Andersen thermostats, implying that there is relatively little

friction between water molecules and the interior wall of the nanotube. This conclusion was also reached for the Berensden thermostat (Nicholls et al. [2012a\)](#page-6-0), where it was shown that the flow rate was constant for different lengths of nanotube. The Langevin thermostat, however, shows a significant decrease in permeability for longer tubes. A similar decrease in permeability with tube length is seen in previously published results employing a Nose–Hoover thermostat (Su and Guo [2012\)](#page-6-0). Remarkably, the choice of thermostating algorithm alters the conclusion as to whether the flow of water in nanotubes is frictionless or not.

The Langevin thermostat adds frictional and random forces to the atoms within Newton's equations of motion, and we expect that both of these could have a significant influence on the simulated water flux in our simulations. It has previously been shown that the randomization of particle velocities inherent in this algorithm can dampen the dynamics of the system, and this is likely to be the cause of the lower flow rate seen with this algorithm compared with the others. To confirm this, we devised an alternative version of the Langevin thermostat which we call the 'Partial Langevin' thermostat. In this, frictional and random forces are applied only to water molecules in the upper half of the upper water reservoir and the lower half of the lower reservoir, so that molecules diffusing through the pores are not directly influenced by frictional terms but still maintain temperature via coupling to the reservoirs. As seen in Fig. [2,](#page-3-0) the permeability is greater using this approach than using the traditional Langevin thermostat, but it is still lower than that found with direct rescaling or the Lowe–Andersen method. In addition, a decrease in permeability with length still occurs in this case, although it is not as marked as for the unmodified Langevin thermostat. While it may be possible to accurately capture transport in the nanotube by coupling to a large enough reservoir, this is not likely to be computationally feasible. Our results clearly show that applying the Langevin thermostat to water molecules inside the nanotubes does influence the simulated flow rate and length dependence of this flow.

As the random force in the Langevin thermostat applies separately to each atom in the system, it can act to reduce any coupled motion of atoms. This is likely to be important in these simulations where water molecules are seen to move in a 'plug-like' collective manner through the nanotube (Hummer et al. [2001;](#page-5-0) Corry [2008](#page-5-0); Majumder and Corry [2011;](#page-6-0) Ritos et al. [2014](#page-6-0)). As the nanotubes get longer, we expect more atoms to be moving in this collective manner, and so any term which reduces such coupled motion will become more apparent. The Nose–Hoover thermostat similarly adds random forces to atoms which would act to dampen dynamics and remove collective motion which may explain the length dependence of water

fluxes seen in that case. In contrast, thermostating algorithms that act globally to adjust the velocities of all atoms (such as velocity rescaling) or that only adjust the relative motion of atom pairs (e.g. Lowe–Andersen) will not act to reduce collective motion in this way, which may explain why no length dependence of flow is seen.

The frictional term in the Langevin equation could also influence the length dependence of flow rates. The size of the frictional term is controlled by the so-called damping coefficient which is typically (although not necessarily) the same for all atoms in the system. The use of small damping coefficients yields poor temperature control, while adding a larger coefficient dissipates kinetic energy more quickly and reduces variations in temperature. However, large frictional or random forces can perturb the dynamics of the system (Hunenberger [2005;](#page-5-0) Basconi and Shirts [2013\)](#page-5-0). To see how the choice of damping coefficient alters the flux of water through the nanotubes in our simulation system, we calculate the water flux using a variety of damping coefficient values with the partial Langevin algorithm. As can be seen in Fig. [2d](#page-3-0), the use of larger frictional terms reduces the net flux through the nanotubes, and the absolute value varies by almost tenfold across the range studied. An even greater influence of damping coefficient on water flux should be expected with the unmodified Langevin algorithm. Damping coefficients in the range of $2-15 \text{ ps}^{-1}$ are typically used in MD simulations (with a default value of 5 ps^{-1} found in NAMD), and these results show that careful consideration needs to be given when choosing a value if mass transport is being measured. As suspected from previous investigations, (Basconi and Shirts [2013\)](#page-5-0) results with the Langevin thermostat should approach those found in a microcanonical NVE ensemble (no temperature control) in the limit of weak damping.

4 Discussion

That the Langevin algorithm alters the dynamics of our pressure-driven system is not unexpected. Indeed, as has been noted in previous studies, the Langevin thermostat is not intended to be used to determine mass transport properties; instead it focuses on replicating energetics and maintaining dynamic stability (Hunenberger [2005\)](#page-5-0). However, given that this thermostat and the specific choice of coupling parameters can alter the simulated permeability of the nanotubes by several orders of magnitude and that they can influence the dependence of permeability on tube length provides a note of caution in both quantitative and qualitative studies.

As has been discussed elsewhere, the choice of an appropriate thermostat for specific MD applications is a subjective matter, with each approach having advantages

and disadvantages (Hunenberger 2005; Stoyanov and Groot [2005](#page-6-0); Basconi and Shirts 2013). The Langevin thermostat is dynamically stable and reproduces a canonical ensemble over long timescales, but the frictional and random forces can perturb the mass transport properties. While this can be minimised by only controlling the temperature in the distant reservoirs as in our partial Langevin method, extreme care must be taken in the choice of atomic damping coefficients. A decrease in nanotube permeability with nanotube length is also observed with the Nose– Hoover thermostat, (Su and Guo [2012\)](#page-6-0) producing similar results to those found with the Langevin thermostat. In contrast, results with direct rescaling, Berendsen and Lowe–Andersen thermostats both show no reduction in flow rate with nanotube length, although it is known that the Berendsen thermostat will not always reproduce the correct energy distribution. These results support previous findings that algorithms that randomise particle velocities (e.g. Langevin, Andersen) dampen the dynamics of the system, while those that effectively scale particle velocities (e.g. Berendsen, direct rescaling) do not (Basconi and Shirts 2013). The Nose–Hoover thermostat does give a good depiction of dynamics in equilibrium simulations, but performs less well here, presumably due to a damping of coupled motion. The Nose–Hoover thermostat is also not Galilean invariant, meaning that centre of mass motion such as seen in these simulations of mass transport has to be corrected for, otherwise it is seen as an increase in system temperature (Koopman and Lowe [2006](#page-6-0)).

Dissipative particle dynamics (DPD) is another approach for controlling molecular simulation (Groot and Warren 1997) that could avoid some of the problems experienced by the Langevin thermostat as it conserves momentum. While it also includes frictional and random terms, these forces are applied to particle pairs rather than individual particles, avoiding the damping of coupled motion. Alternatively, altering velocity only perpendicular to the flow would prevent the damping of the transport rate, although doing this using a velocity randomisation scheme may still dampen local motion.

Although not considered here, other simulation parameters such as the choice of water model could also influence simulated flow rates. For example, the self-diffusion coefficients found with different water models differ by up to threefold from each other and from experimental values (Mark and Nilsson [2001\)](#page-6-0) which may also alter the rate of pressure-driven flow rates.

5 Conclusions

By conducting simulations of water transport in carbon nanotubes under a hydrostatic pressure difference with a

variety of thermostats, we are able to show that the means of controlling simulation temperature can have profound implications on the observed transport properties. This knowledge helps to reconcile disparate simulation results which have predicted quantitative water permeabilities that differ by over an order of magnitude, as well as qualitative differences in the effect of changing the nanotube length. Furthermore, it provides a warning that the selection of which thermostat to employ and to which atoms it is applied should be carefully considered when conducting simulations of mass transport. These results suggest that existing studies using the Langevin or Nose–Hoover thermostats may be underestimating the likely nanotube permeability and may overestimate the reduction in flow with increasing nanotube length. These results support the claims of extremely and near-frictionless water flow in carbon nanotubes.

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