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Surface wettability effects on flow in rough wall nanochannels

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Abstract The effect of rough-wall/fluid interaction on flow in nanochannels is investigated by NEMD. Hydrophobic and hydrophilic surfaces are studied for walls with nearly atomic-size rectangular protrusions and cavities. Our NEMD simulations reveal that the number of liquid atoms temporarily trapped in the cavities is affected by the strength of the potential energy inside the cavities. Regions of low potential energy are possible trapping locations. Fluid atom localization is also affected by the hydrophilicity/hydrophobicity of the surface. Potential energy is greater between two successive hydrophilic protrusions, compared to hydrophobic ones. Moreover, groove size and wall wettability are factors that control effective slip length. Surface roughness and wall wettability have to be taken into account in the design of nanofluidic devices.

Keywords NEMD simulation - Rough-wall nanochannels · Surface wettability · Fluid atom trapping · Potential energy - Effective slip length

List of symbols

- F_{ext} Magnitude of external driving force
- h Gap between channel walls
- K Spring constant
- $k_{\rm B}$ Boltzman constant
- L_x Length of the computational domain in the x-direction
- L_v Length of the computational domain in the y-direction
- L_z Length of the computational domain in the z-direction
- L_s Slip length
- $L_{\text{s.eff}}$ Effective slip length
- m Atom mass
- N Number of atoms
- p Periodic roughness factor
- r_{eq} Position of a wall atom on fcc lattice site
- r_i Position vector of atom i
- \mathbf{r}_{ij} Distance vector between *ith* and *jth* atom
- T Temperature
- $u(r_{ii})$ LJ potential of atom *i* with atom *j*
- V Volume of the computational domain $(L_x \times L_y \times L_z)$

Greek symbols

- ϵ Energy parameter in the LJ potential
- σ Length parameter in the LJ potential
- v_w Fluid velocity at the channel wall
- $\langle v_w \rangle$ Average fluid velocity at the channel wall

1 Introduction

Flows at the nanoscale have been an intriguing subject studied both theoretically and experimentally during the past decade. At the boundary between wall and fluid, most fluid properties are affected by the wall/fluid interactions, and the precise description of phenomena taking place at these interfaces become very important in nanochannels. Fluid atom localization near the walls, fluid velocity, slip length, and temperature distribution vary depending on the degree of wall wettability (Galea and Attard [2004](#page-6-0);

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Heinbuch and Fischer [1989](#page-6-0); Nagayama and Cheng [2004](#page-6-0); Priezjev et al. [2005](#page-6-0)). A surface with increased wettability, i.e., one that attracts fluid atoms, is usually characterized as hydrophilic, while a surface is characterized as hydrophobic when fluid atoms forced away at very close distance from the surface repulsive force.

Walls cannot be classified as smooth in most nanochannels since atomic or thermal roughness exists due to wall atom position and movement, respectively, (Priezjev [2007;](#page-6-0) Sofos et al. [2009a\)](#page-6-0). Moreover, roughness elements can be added intentionally at the atomic wall level and various geometrical patterns can thus be created (Cao et al. [2006;](#page-6-0) Ziarani and Mohamad [2008](#page-6-0); Jabbarzadeh et al. [2000](#page-6-0); Kim and Darve [2006\)](#page-6-0). It is also shown (Sbragaglia et al. [2006;](#page-6-0) Cottin-Bizonne et al. [2003;](#page-6-0) Cottin-Bizonne et al. [2004\)](#page-6-0) that, under specific pressure conditions, a free space is created between a rough wall and liquid atoms and this leads to drag reduction. When hydrophobicity is coupled with appropriate roughness, the surfaces are characterized as ultra- or super-hydrophobic. Drag reduction in ultrahydrophobic surfaces (in microchannels) was experimentally proved, e.g., Ou et al. [\(2004](#page-6-0)). The slip length on various hydrophobic/hydrophilic rough surfaces was investigated in Tsai et al. ([2009](#page-6-0)).

In this study, the combined effects of rough wall geometry and wall wettability on fluid properties and the resulting flow are investigated. In order to investigate possible fluid atom localization, the potential energy map is extracted for every channel studied, and number density profiles are given. Moreover, the trapping time of a fluid atom inside the cavities is calculated. It has been discussed in Sofos et al. ([2009a](#page-6-0)) how the trapping time is affected by the length of wall cavities and this discussion is further amplified by the incorporation of wall wettability properties on the calculation of trapping time. The effective slip length calculation is of great interest near hydrophobic/ hydrophilic rough surfaces, since the variation of surface properties could be a means of controlling fluid slippage (Cao et al. [2009](#page-6-0)) and is presented in detail.

This article is set up as follows. In Sect. 2 simulation details are presented. Results are presented and discussed in Sect. [3](#page-2-0), and Sect. [4](#page-5-0) contains concluding remarks.

2 Simulation details

2.1 Molecular system model

Non-equilibrium molecular dynamics simulations were performed to simulate flow of a monoatomic liquid (such as argon) in various channels with rectangular protrusions and cavities. The lower wall of the channel is atomically rough while the rough upper wall is constructed by "adding'' extra wall atoms to form periodically spaced rectangular protrusions (see Fig. 1). We considered four different cases for the periodic roughness of the upper wall ($p = 1$, 2, 3, and 6, as shown schematically in Fig. 1), where p represents the number of rectangular grooves in the computational domain (Sofos et al. [2009a](#page-6-0)). The roughness depth, h_p , is about 2σ , which is relatively small (only twice the atomic diameter) and we remark that the roughness models presented are closer to atomic roughness models.

Particle interactions are described by Lennard-Jones (LJ) 12-6 potential

$$
u^{LJ}(r_{ij}) = 4\varepsilon((\sigma/r_{ij})^{12} - (\sigma/r_{ij})^6)
$$
 (1)

where the parameters of the LJ potential are $\sigma = 0.3405$ nm and $\varepsilon_{\text{fluid}}/k_{\text{B}} = 119.8 \text{ K (argon parameters)},$ the atomic mass for argon is $m_{\text{Ar}} = 39.95$ a.u. (from now on will be referred as *m*) and the cut-off radius is $r_c = 2.5\sigma$. We examine various wall/fluid interactions in order to report on the effect of wall interaction of fluid parameters, from the hydrophilic case $(\varepsilon_{wall}/\varepsilon_{fluid} = 1.5)$ to the less hydrophilic case $(\varepsilon_{wall}/\varepsilon_{fluid} = 1.0)$, the more hydrophobic case $(\varepsilon_{wall}/\varepsilon_{fluid} =$ 0.75) and the more hydrophobic with a weaker liquid–solid interaction case $(\varepsilon_{wall}/\varepsilon_{fluid} = 0.5)$.

Periodic boundary conditions are considered in x - and y directions. All channels consist of 504 wall atoms and

Fig. 1 Rough-wall channels studied. The system is assumed periodic in x- and y-directions. Each module shown corresponds to a computational cell. We denote the roughness depth by h_p , while cavity and protrusion lengths by l_c and l_p , respectively

1,368 fluid atoms. Wall atoms are bound on fcc sites and remain fixed to their original positions due to the effect of an elastic spring force $\mathbf{F} = -K(\mathbf{r}(t) - \mathbf{r}_{eq})$, where $\mathbf{r}(t)$ is the vector position of a wall atom at time t , \mathbf{r}_{eq} is its initial lattice position vector and K is the wall spring constant. As explained in Liem et al. ([1992\)](#page-6-0) and Sofos et al. [\(2009b](#page-6-0)), if we compute the second derivative of this potential and the second derivative of the LJ potential (Eq. [1](#page-1-0)), evaluate both derivatives at $r = r_0 = 2^{1/6}\hat{\sigma}$, and equate the results, we get $K = 57.15 \varepsilon/\sigma^2$. We remind the reader that $r_0 = 2^{1/6}\sigma$ is the distance where the LJ potential reaches its minimum. The value of $K = 57.15 \ \epsilon/\sigma^2$ was used in all our simulations.

Temperature is kept constant at $T^* = 1$ (ε/k_B , k_B is the Boltzman's constant) with the application of Nosé-Hoover thermostats. An external driving force $F_{ext} = 0.01344$ (ε/σ) is applied along the x-direction to drive the flow.

The simulation step for the system is $\Delta t = 0.005\tau$ (τ is in units of $\sqrt{m\sigma^2/\epsilon}$). In the beginning, fluid atoms are given appropriate initial velocities in order to reach the desired temperature $(T^* = 1)$. The system reaches equilibrium state after a run of 2×10^6 time steps. Then, a number of NEMD simulations are performed, each with duration of 5×10^5 time steps.

2.2 Computational details

Potential energy and number density profiles are evaluated as local values at various xz -positions of the channels. To achieve this, the channel is divided into $m \times n$ bins in the xz-plane, each one of volume $V_{\text{bin}} = (L_x/m) \times L_y \times (h/n)$, where $m = 48$, $n = 48$.

Potential energy as a local quantity, u_{bin} , is calculated in a bin as

$$
u_{\text{bin}}(r_{ij}^{\text{bin}}) = 4\varepsilon((\sigma/r_{ij}^{\text{bin}})^{12} - (\sigma/r_{ij}^{\text{bin}})^6)
$$
 (2)

 r_{ij}^{bin} being the distance between atoms i and j, where i corresponds to a particle inside the bin and j corresponds to interactions with all its neighbor particles either located inside the bin or outside the bin.

This permits to present potential energy contour plots. The interest for such plots comes from the fact that the more negative the potential energy is the higher the probability that at given temperature an atom will be located there for longer time. As the energy becomes less negative (and hereafter we refer to such energy as higher energy) then the probability that an atom located at such a region is displaced increases.

Number density is calculated by dividing the average number of particles located in the corresponding bin by the volume of the bin. The calculation takes only place to regions which are accessible to fluid atoms (core channel region and cavities). The bin size in the z-direction is less

than half σ , insuring adequate accuracy and smoothness of the results.

The slip length at the solid boundary, L_s , is generally calculated from the linear Navier boundary condition (Goldstein [1965\)](#page-6-0) as $L_s = v_w / \frac{dv}{dt}$ dz where the subscript w denotes quantities evaluated at the wall. Owing to the effect of the rough wall, we have extracted first the mean velocity profile across the channel and calculated the effective slip length as $L_{s,eff} = \langle v_w \rangle / \frac{d(v)}{dz}$ dz \int_{w} . The theoretical position of the upper rough wall in these calculations is considered in the midplane between the cavity and the protrusion width, as shown in Fig. [1](#page-1-0).

3 Results and discussion

3.1 Potential energy distributions

Contour plots of the potential energy obtained as values averaged in time inside the $p = 1$ nanochannel, for various hydrophobic/hydrophilic surface properties, are presented in Fig. [2a](#page-3-0)–d. Emphasis is given on the potential energy distribution adjacent to the rough wall, since there are no significant changes near the lower flat wall.

When $p = 1$, in a hydrophobic nanochannel $(\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 0.5)$, in Fig. [2](#page-3-0)a, potential energy contours follow the wall atoms morphology. We do not observe any low potential energy regions inside the wall cavities and this is an indication that there are no regions inside the wall grooves that fluid atoms could be trapped. Similar results are also observed for the less hydrophobic nanochannel $(\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 0.75)$, in Fig. [2b](#page-3-0).

On the other hand, for $\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 1.0$ (Fig. [2c](#page-3-0)), i.e., in a more hydrophilic scenario than the previous ones, we observe that inside each cavity there exist regions of low potential energy (the darker regions) flanked by high potential energy regions (the lighter regions). As fluid atoms tend to be localized in low potential energy regions, it is possible that fluid atoms could be trapped there, inside the cavities. In the most hydrophilic channel studied $(\varepsilon_{wall}/\varepsilon_{fluid} = 1.5)$, Fig. [2](#page-3-0)d), the low potential regions inside the cavity are more pronounced and it seems reasonable to expect that fluid atoms can be trapped there for significant time. More specifically, the regions close to the cavity corners are the more probable trapping positions.

Similar behavior for channels of $p = 2$, 3, and 6 are observed in every hydrophobic/hydrophilic case studied. For example, for $p = 2$, the potential energy map of the most hydrophobic wall studied is shown in Fig. [3](#page-3-0)a, while in Fig. [3](#page-3-0)b, the potential energy map of the most Fig. 2 Potential energy contours for $p = 1$. **a** $\varepsilon_{wall}/\varepsilon_{fluid} = 0.5$. **b** $\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 0.75$. c $\varepsilon_{wall}/\varepsilon_{fluid} = 1.0$, and **d** $\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 1.5$

hydrophilic wall studied is presented. As in the $p = 1$ case, the lower potential energy regions (represented by dark regions) are more pronounced inside the hydrophilic cavities, denoting that fluid atoms are subject to be trapped inside the cavities, while such regions are not observed in the case of the hydrophobic channel.

The potential energy map for all channels studied reveals that the existence of hydrophobic or hydrophilic rectangular anomalies at a channel wall results in the formation of different values of potential energy regions inside the rectangular grooves. As in Sofos et al. [\(2009a,](#page-6-0) [b](#page-6-0)), we expect that the localization and trapping of fluid atoms near a rough wall be affected.

3.2 Number density

The number density distribution for $p = 1$ is shown in the contour plots of Fig. [4a](#page-4-0)–d. The region near the rough wall is the most interesting, since density profiles near smooth hydrophobic/hydrophilic walls has been reported, e.g., (Cao et al. [2009;](#page-6-0) Galea and Attard [2004](#page-6-0)).

In the most hydrophobic case $(= 0.5)$, in Fig. [4a](#page-4-0), we observe that there exists weak fluid atom localization near the rough wall. Number density values inside the cavities are the same as in the center of the channel, where wall atom effects are minimized. Similar behavior is also observed in the case of the less hydrophobic nanochannel

contours for $p = 2$. **a** $\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 0.5$ and **b** $\epsilon_{wall}/\epsilon_{fluid} = 1.5$

 $\epsilon_{wall}/\epsilon_{fluid} = 1.5$

 $(= 0.75)$, in Fig. 4b. As the wall hydrophobicity decreases, as for $=1.0$, in Fig. 4c, it is seen that there is a kind of increased fluid atom localization. In the most hydrophilic channel studied $(= 1.5, Fig. 4d)$, fluid atoms near the walls (both at the upper rough and the lower atomically rough wall) seem to "stick" in the neighboring channel layers. This effect is more obvious inside the upper wall cavities.

Number density distributions, as shown in the twodimensional contour plots in Fig. 4a–d, are consistent with the potential maps shown in the respective diagrams of Fig. [2](#page-3-0)a–d. This is an indication that fluid atoms not only tend to be trapped inside the cavities, but this effect becomes more pronounced as the wall hydrophobicity decreases.

3.3 Calculation of trapping time

Average trapping time is defined as the total residence time of all particles detected inside the considered region divided by the mean number of particles detected inside this region. As control volume for the calculations we take the whole cavity volume in each case. As seen in Sofos et al. [\(2009a\)](#page-6-0), fluid atoms are partially trapped inside nanochannel grooves and the trapping time increases as the number of wall protrusions p increases, too. If we also take into account the rough wall hydrophobicity strength, we estimate the trapping time and present it in Fig. [5](#page-5-0). The simulation time refers to a time window $(t_0, t_0 + 45 \text{ ns})$. First of all, we observe that fluid atoms previously located inside a cavity tend to remain trapped there for a longer time when the walls are hydrophilic $(\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 1.5)$. This time increases as the number of protrusions increase and is always greater that the other channels. For the hydrophilic $(\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 1.0)$ case, trapping time is not affected for $p = 1$ and 2, but increases significantly as the number of protrusions increase ($p = 3$ and 6). For the two hydrophobic channels ($\varepsilon_{\text{wall}}/\varepsilon_{\text{fluid}} = 0.75$ and 0.5), average trapping times remain constant to a small value and are not affected by the existence of protrusions and cavities. The typical average trapping time close to the lower flat wall was found very small (of the order of few timesteps), approaching nearly zero values compared to the average trapping times in the cavities. This behavior seems to be compatible with what is observed from the potential energy, where close to the lower wall no significant low energy (highly negative) regions are found that could act as trap locations for atoms.

To sum up, the timing analysis of fluid atom trapping reveals that both hydrophilicity and small protrusion lengths at the channel walls are factors that enhance trapping. When the strength of hydrophilicity decreases significantly, the effect of roughness is minimized.

Fig. 5 Average trapping time of fluid atoms inside cavities for various hydrophobic/hydrophilic rough wall nanochannels

3.4 Calculation of effective slip length

In Fig. 6, the effects of wall wettability and roughness on the effective slip length are summarized. Taking into account that local velocity calculation near the rough wall is somewhat imprecise since velocity profiles are difficult to fit by a polynomial curve, the effective slip length calculation may only reveal trends and not exact values.

We observe that the effective slip length increases as the wall roughness factor p increases, i.e., the protrusion and cavity length decreases. This conclusion was also reached by Yang [\(2006](#page-6-0)). Moreover, as wall hydrophilicity increases, it appears that the effective slip length decreases. The effect of wall wettability on slip length is relatively small (Fig. 6) and this is due to the small range of wall wettability values investigated in our simulations. It is noted that

Fig. 6 Effective slip length in various hydrophobic/hydrophilic rough wall nanochannels

our results are in qualitative agreement with similar results reported by Nagayama and Cheng ([2004\)](#page-6-0) and Ziarani and Mohamad [\(2008](#page-6-0)).

Finally, we observe that the trapping time seems to be related to the slip length value. In Fig. 7, we present trapping time values versus slip length, for every p value. It is shown that as the trapping time increases, the slip length decreases.

4 Conclusions

We have presented non-equilibrium molecular dynamics simulations of liquid argon flow between atomically roughened walls formed by rectangular protrusions and cavities. The effect of wall roughness in conjunction with surface wettability on potential energy distribution, fluid atom localization/trapping, and effective slip length are investigated.

It has been presented in another work (Sofos et al. [2009a\)](#page-6-0), that the potential energy map for rough channels shows that there exist low and high potential energy regions inside the rectangular cavities, which are affected by the cavities length. In this study, it is shown how the potential map near the rough wall depends on surface hydrophobicity (or hydrophilicity). The potential map strength increases inside a cavity, as wall hydrophobicity decreases. This fact affects fluid atom localization near a rough wall.

Number density profiles in channel regions adjacent to the rough walls show that fluid atoms tend to be localized inside hydrophilic cavities and near hydrophilic protrusions. Hydrophobic walls do not attract fluid atoms as hydrophilic ones and this is verified by the respective number density profiles near the rough walls where it

Fig. 7 Slip length versus inverse trapping time for $p = 1, 2, 3$, and 6

seems that they are approaching their average value (as in the center of the channel).

This fluid atom localization affects fluid atom trapping time inside the wall grooves. It is of interest to notice that protrusion length does not significantly affects trapping time in an hydrophobic wall. When the strength of hydrophobicity is minimized (hydrophilic wall), fluid atom trapping time increases cavity length decreases. In particular, in the most hydrophilic wall studied, we show that fluid atoms are practically immobilised when wall roughness approaches the atomic scale roughness (case $p = 6$).

The effective slip length near a rough, hydrophobic wall is greater compared to a respective hydrophilic wall. The effective slip length also depends significantly on wall protrusion length, since it is greater when protrusions are of small length (e.g., $p = 6$).

Wall roughness is a primary feature that affects nanoflow systems, but, one has to bear in mind that wall wettability has also to be taken into account, in accordance with the assumption presented in Cao et al. (2009). Fluid atom trapping inside wall grooves varies depending on the wall properties and this could be a means of designing and controlling interface behavior for a wide range of applications.

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