

Guided Waves in the Multilayered One-Dimensional Hexagonal Quasi-crystal Plates

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ABSTRACT Guided waves in the multilayered one-dimensional quasi-crystal plates are, respectively, investigated in the context of the Bak and elasto-hydrodynamic models. Dispersion curves and phonon and phason displacements are calculated using the Legendre polynomial method. Wave characteristics in the context of these two models are analyzed in detail. Results show that the phonon–phason coupling effects on the first two layers are the same at low frequencies; but, they are more significant on the first layer than those on the second layer at high frequencies. These obtained results lay the theoretical basis of guided-wave nondestructive test on multilayered quasi-crystal plates.

KEY WORDS Multilayered structures, Quasi-crystal plate, Guided wave, Phonon–phason coupling effect

1. Introduction

As a novel kind of solid matter, quasi-crystals (QCs) are of long-range orientational order and symmetries that are prohibitive in crystal matters [1], such as fivefold, tenfold and twelvefold rotational symmetries. Owing to their unique structures, quasi-crystals own a lot of advantageous performances, such as low adhesion, thermal conductivity and friction coefficient, and high abrasion resistance and resistivity [2]. Accordingly, quasi-crystals can be utilized as coatings or thin films in engineering [3, 4].

Multilayered structures are commonly used in engineering to take advantage of the superior performances of each layer. Numerous investigations on mechanical properties of multilayered crystal structures have been conducted [5-7]. Recently, mechanical investigations on multilayered quasi-crystal structures have also received increasing attention [8-10]. However, they were mainly focused on the statics of quasi-crystals because the dynamic deformation of quasi-crystals is extremely complicated owing to the coupled phonon and phason fields. There are two different dynamic models for the dynamic deformation. The Bak model [11] assumed that the phason field is similar to the phonon field denoted by wave propagation. The elasto-hydrodynamic model presented by Lubensky et al. [12] considered phason modes to be diffusive with a large diffusive time. These two models are, respectively, used to investigate dynamics of quasi-crystal structures, such as conservation laws [13], free vibration and harmonic response [14, 15], bending analyses [16], wave propagation [17] and other dynamic problems [18, 19]. From the above review, rare references of guided waves in the multilayered quasi-crystal structures are available.

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Due to the limit of manufacturing techniques and processes, the bonding of the multilayered quasicrystal plate would cause micro-cracks in joints. Therefore, to ensure the safety of structures, it is necessary to develop an efficient nondestructive testing method. The guided-wave nondestructive test technology has been successfully applied to a lot of crystal structures [20], which also has promising applications on quasi-crystal structures. However, the prerequisite for using it is to understand guided wave characteristics in detail. Therefore, guided waves in the multilayered one-dimensional (1D) hexagonal quasi-crystal plates in the context of Bak and elasto-hydrodynamic models are, respectively, investigated. The traction-free boundary condition is assumed.

2. Mathematics and Formulation

An infinite horizontally N-layered quasi-crystal plate with a total thickness of h_N is illustrated in Fig. 1. The horizontal (x, y)-plane is placed on the top surface, and it occupies the region $0 \le z \le h_N$ in the positive z-direction.

Combining the Bak's and elasto-hydrodynamic models, the dynamic governing equations without body forces are as follows [21]:

$$T_{ij,j} = \rho \ddot{u}_i, H_{ij,j} = \kappa \dot{w}_i + \rho_p \ddot{w}_i \tag{1}$$

where ρ is the density; u_i and w_i represent displacement components; T_{ij} and H_{ij} are phonon and phason stress tensors, respectively; $\kappa = 1/\Gamma_w$ is the friction coefficient; and ρ_p is the effective phason mass density. If $\rho_p = 0$, the elasto-hydrodynamic model is recovered. If $\kappa = 0$ and $\rho_p = \rho$, the Bak's model is recovered.

The generalized relationships of strain-displacement are as follows:

$$\varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right), \qquad w_{ij} = \frac{\partial w_i}{\partial x_j}$$
(2)

where ε_{ij} and w_{ij} are phonon and phason strain tensors, respectively.

For the multilayered quasi-crystal plate, its initial boundary conditions are required: (a) the normal stresses are 0 at the top and bottom surfaces $(T_{zz} = T_{xz} = T_{yz} = H_{zz} = 0)$; (b) the normal stresses and displacements are continuous at the interfaces. To deal with it, a window function is introduced.

$$I_{h_0,h_N}(z) = \text{Heaviside}[h_0] - \text{Heaviside}[h_N] = \begin{cases} 1, h_0 \le z \le h_N \\ 0, \text{ elsewhere} \end{cases}$$
(3)

where $h_0 = 0$.

Material parameters of the N-layered quasi-crystal plates are written as:

$$C_{ij}^{(N)} = \sum_{n=1}^{N} C_{ij}^{(n)} I_{h_{n-1},h_n}, \ K_i^{(N)} = \sum_{n=1}^{N} K_i^{(n)} I_{h_{n-1},h_n}, \ R_i^{(N)} = \sum_{n=1}^{N} R_i^{(n)} I_{h_{n-1},h_n}$$

$$\rho^{(N)} = \sum_{n=1}^{N} \rho^{(n)} I_{h_{n-1},h_n}, \ \kappa^{(N)} = \sum_{n=1}^{N} \kappa^{(n)} I_{h_{n-1},h_n}$$
(4)



Fig. 1. Schematic diagram of an infinite multilayered quasi-crystal plate

where $C_{ij}^{(n)}, K_i^{(n)}, R_i^{(n)}, \rho^{(n)}$ and $\kappa^{(n)}$ are, respectively, elastic parameters in the phonon and phason fields, phonon-phason coupling coefficients, density and friction coefficient of the *n*th layer.

For the 1D hexagonal quasi-crystal plate, only one direction is quasi-periodic. If the quasi-periodic axis is consistent with the x-axis, it is named as the x-direction plate. Similarly, there are also the y-direction and z-direction plates. Guided waves in these three cases are investigated in detail, respectively.

(1) The z-direction plate (1)

For the z-direction plate, only the phason displacement in the z-direction is not 0. Therefore, the displacements of guided wave propagating in the x-direction are as follows:

$$u_x = U(z)e^{ikx - iwt}, u_y = V(z)e^{ikx - iwt}, u_z = W(z)e^{ikx - iwt}, w_z = \gamma(z)e^{ikx - iwt}$$
(5)

where U(z), V(z), W(z) and $\gamma(z)$ represent phonon displacement amplitudes in the x-, y- and zdirection and the phason displacement amplitude, respectively.

The constitutive equations [22] are as follows:

$$\begin{aligned} T_{xx} &= C_{11}^{(N)} \varepsilon_{xx} + C_{12}^{(N)} \varepsilon_{yy} + C_{13}^{(N)} \varepsilon_{zz} + R_{1}^{(N)} w_{zz} \\ T_{yy} &= C_{12}^{(N)} \varepsilon_{xx} + C_{11}^{(N)} \varepsilon_{yy} + C_{13}^{(N)} \varepsilon_{zz} + R_{1}^{(N)} w_{zz} \\ T_{zz} &= C_{13}^{(N)} \varepsilon_{xx} + C_{13}^{(N)} \varepsilon_{yy} + C_{33}^{(N)} \varepsilon_{zz} + R_{2}^{(N)} w_{zz} \\ T_{yz} &= T_{zy} = 2C_{44}^{(N)} \varepsilon_{yz} + R_{3}^{(N)} w_{zy} \\ T_{xz} &= T_{zx} = 2C_{55}^{(N)} \varepsilon_{xz} + R_{3}^{(N)} w_{zx} \\ T_{xy} &= T_{yx} = 2C_{66}^{(N)} \varepsilon_{xy} \\ H_{zz} &= R_{1}^{(N)} \varepsilon_{xx} + R_{1}^{(N)} \varepsilon_{yy} + R_{2}^{(N)} \varepsilon_{zz} + K_{1}^{(N)} w_{zz} \\ H_{zx} &= 2R_{3}^{(N)} \varepsilon_{xz} + K_{2}^{(N)} w_{zx} \\ H_{zy} &= 2R_{3}^{(N)} \varepsilon_{yz} + K_{2}^{(N)} w_{zx} \end{aligned}$$
(6a)

Submitting Eqs. (2)-(6) into Eq. (1), the differential equations of wave motion are obtained:

$$-C_{11}^{(N)}k^{2}U + C_{55}^{(N)}U'' + (C_{13}^{(N)} + C_{55}^{(N)})ikW' + (R_{1}^{(N)} + R_{3}^{(N)})ik\gamma' + (C_{55}^{(N)})'U' + (C_{55}^{(N)})'ikW + (R_{3}^{(N)})'ik\gamma] = -\rho^{(N)}\omega^{2}U$$
(7a)

$$-C_{66}^{(N)}k^{2}V + C_{44}^{(N)}V'' + \left(C_{44}^{(N)}\right)'V' = -\rho^{(N)}\omega^{2}V$$
(7b)

$$(C_{13}^{(N)} + C_{55}^{(N)})ikU' - C_{55}^{(N)}k^2W + C_{33}^{(N)}W'' - R_3^{(N)}k^2\gamma + R_2^{(N)}\gamma'' + \left(C_{13}^{(N)}\right)'ikU + \left(C_{33}^{(N)}\right)'W' + \left(R_2^{(N)}\right)'\gamma' = -\rho^{(N)}\omega^2W$$

$$(7c)$$

$$(R_1^{(N)} + R_3^{(N)})ikU' - R_3^{(N)}k^2W + R_2^{(N)}W'' - K_2^{(N)}k^2\gamma + K_1^{(N)}\gamma'' + \left(R_1^{(N)}\right)'ikU + \left(R_2^{(N)}\right)'W' + \left(K_1^{(N)}\right)'\gamma' = -\rho_p^{(N)}\omega^2\gamma - \kappa^{(N)}i\omega\gamma$$
(7d)

where (') denotes the derivation with respect to z. SH waves are governed by Eq. (9b) that is independent of the phason field. So, SH waves are not investigated in this case.

Subsequently, the phonon and phason displacements of each layer are expanded into the Legendre orthogonal polynomial series.

For the first quasi-crystal layer:

$$u_a^1 = \sum_{m=0}^{\infty} p_m^{a,1} Q_m^1(z) \exp(ikx - i\omega t), \quad w_z^1 = \sum_{m=0}^{\infty} r_m^1 Q_m^1(z) \exp(ikx - i\omega t)$$
(8)

where

$$Q_m^1(z) = \sqrt{\frac{2m+1}{h_1 - h_0}} P_m\left(\frac{2z - (h_1 - h_0)}{h_1 - h_0}\right)$$

$$u_a^1(z=h_1) = u_a^{1,h_1} = \sum_{m=0}^{\infty} p_m^{a,1} Q_m^1(z=h_1) \exp(ikx - i\omega t)$$
$$w_z^1(z=h_1) = w_z^{1,h_1} = \sum_{m=0}^{\infty} r_m^1 Q_m^1(z=h_1) \exp(ikx - i\omega t)$$

where $p_m^{a,n}(n = 1, 2)$, r_m^1 denote expansion coefficients, P_m represents the *m*th Legendre polynomial, and u_a are u_x and u_z , respectively.

For the second quasi-crystal layer:

$$u_a^2 = u_a^{1,h_1} + (z - h_1) \sum_{m=0}^{\infty} p_m^{a,2} Q_m^2(z) \exp(ikx - i\omega t)$$
$$w_z^2 = w_z^{1,h_1} + (z - h_1) \sum_{m=0}^{\infty} r_m^2 Q_m^2(z) \exp(ikx - i\omega t)$$
(9)

where

$$Q_m^2(z) = \sqrt{\frac{2m+1}{h_2 - h_1}} P_m \left(\frac{2z - (h_2 - h_1)}{h_2 - h_1}\right)$$
$$u_a^2(z = h_2) = u_a^{2,h_2} = u_a^{1,h_1} + (z - h_1) \sum_{m=0}^{\infty} p_m^{a,2} Q_m^2(z = h_2) \exp(ikx - i\omega t)$$
$$w_z^2(z = h_2) = w_z^{2,h_2} = w_z^{1,h_1} + (z - h_1) \sum_{m=0}^{\infty} r_m^2 Q_m^2(z = h_2) \exp(ikx - i\omega t)$$

For the Nth quasi-crystal layer:

$$u_{a}^{N} = u_{a}^{N-1,h_{N}} + (z - h_{N}) \sum_{m=0}^{\infty} p_{m}^{a,N} Q_{m}^{N}(z) \exp(ikx - i\omega t)$$
$$w_{z}^{N} = w_{z}^{N-1,h_{N}} + (z - h_{N}) \sum_{m=0}^{\infty} r_{m}^{N} Q_{m}^{N}(z) \exp(ikx - i\omega t)$$
(10)

where

$$Q_m^N(z) = \sqrt{\frac{2m+1}{h_N - h_{N-1}}} P_m \left(\frac{2z - (h_N - h_{N-1})}{h_N - h_{N-1}}\right)$$
$$u_a^N(z = h_N) = u_a^{N,h_N} = u_a^{N-1,h_N} + (z - h_N) \sum_{m=0}^{\infty} p_m^{a,N} Q_m^N(z = h_N) \exp(ikx - i\omega t)$$
$$w_z^N(z = h_N) = w_z^{N,h_N} = w_z^{N-1,h_N} + (z - h_N) \sum_{m=0}^{\infty} r_m^N Q_m^N(z = h_N) \exp(ikx - i\omega t)$$

Submitting Eqs. (8)–(10) into Eq. (7), multiplying the obtained equations by $Q_j^1(z), Q_j^2(z) \cdots Q_j^N(z)$ with j running from 0 to M, and integrating over z from h_1 to h_N , the following equation is deduced:

$$\begin{bmatrix} {}^{n}A_{11}^{m,j} & nA_{12}^{m,j} & nA_{13}^{m,j} \\ {}^{n}A_{21}^{m,j} & nA_{22}^{m,j} & nA_{23}^{m,j} \\ {}^{n}A_{31}^{m,j} & nA_{32}^{m,j} & nA_{33}^{m,j} \end{bmatrix} \begin{cases} {}^{p}p_{m,j} \\ {}^{p}p_{m,j} \\ {}^{r}m,j \end{cases} = -\omega^{2} \begin{bmatrix} {}^{n}M_{m,j} & 0 & 0 \\ 0 & {}^{n}M_{m,j} & 0 \\ 0 & 0 & {}^{n}M_{m,j} \end{bmatrix} \begin{cases} {}^{p}p_{m,j} \\ {}^{p}p_{m,j} \\ {}^{p}m,j \end{cases}$$
(11)

where ${}^{n}A_{q,s}^{m,j}(q = 1, 2, 3 \text{ and } s = 1, 2, 3)$ and ${}^{n}M_{m,j}$ are matrix elements that can be obtained from Eq. (7). Therefore, it is transformed into an eigenvalue problem. Angular frequencies are square roots of eigenvalues. Phonon and phason displacement components can be calculated from eigenvectors. (2) The y-direction plate

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The phonon displacements are the same as those in Eq. (5), and only the phason displacement in the *y*-direction is not 0, which is as follows:

$$w_y = \beta(z) \mathrm{e}^{\mathrm{i}kx - \mathrm{i}\omega t} \tag{12}$$

where $\beta(z)$ represents the phason displacement amplitude.

The constitutive equations are as follows:

$$T_{zz} = C_{11}^{(N)} \varepsilon_{zz} + C_{12}^{(N)} \varepsilon_{xx} + C_{13}^{(N)} \varepsilon_{yy} + R_1^{(N)} w_{yy}$$

$$T_{xx} = C_{12}^{(N)} \varepsilon_{zz} + C_{22}^{(N)} \varepsilon_{xx} + C_{13}^{(N)} \varepsilon_{yy} + R_1^{(N)} w_{yy}$$

$$T_{yy} = C_{13}^{(N)} \varepsilon_{zz} + C_{13}^{(N)} \varepsilon_{xx} + C_{33}^{(N)} \varepsilon_{yy} + R_2^{(N)} w_{yy}$$

$$T_{xz} = T_{zx} = 2C_{66}^{(N)} \varepsilon_{xz}$$

$$T_{yx} = T_{xy} = 2C_{44}^{(N)} \varepsilon_{yx} + R_3^{(N)} w_{yx}$$

$$T_{yz} = T_{zy} = 2C_{44}^{(N)} \varepsilon_{yz} + R_3^{(N)} w_{yz}$$

$$H_{yy} = R_2^{(N)} \varepsilon_{yy} + R_1^{(N)} \varepsilon_{zz} + R_1^{(N)} \varepsilon_{xx} + K_1^{(N)} w_{yy}$$

$$H_{yx} = 2R_3^{(N)} \varepsilon_{yx} + K_2^{(N)} w_{yz}$$

$$(13b)$$

Submitting Eqs. (12)–(13) and Eq. (2) into Eq. (1), the differential equations of wave motion are obtained:

$$-C_{22}^{(N)}k^{2}U + C_{66}^{(N)}U'' + (C_{12}^{(N)} + C_{66}^{(N)})ikW' + (C_{66}^{(N)})'U' + (C_{66}^{(N)})'ikW = -\rho^{(N)}\omega^{2}U$$
(14a)

$$-C_{44}^{(N)}k^{2}V + C_{44}^{(N)}V'' - R_{3}^{(N)}k^{2}\beta + R_{3}^{(N)}\beta'' + \left(C_{44}^{(N)}\right)'V' + \left(R_{3}^{(N)}\right)'\beta' = -\rho^{(N)}\omega^{2}V$$
(14b)

$$\left(C_{12}^{(N)} + C_{66}^{(N)}\right)ikU' - C_{66}^{(N)}k^2W + C_{11}^{(N)}W'' + \left(C_{12}^{(N)}\right)'ikU + \left(C_{11}^{(N)}\right)'W' = -\rho^{(N)}\omega^2W$$
(14c)

$$-R_{3}^{(N)}k^{2}V + R_{3}^{(N)}V'' - K_{2}^{(N)}k^{2}\beta + K_{2}^{(N)}\beta'' + \left(R_{3}^{(N)}\right)'V' + \left(K_{2}^{(N)}\right)'\beta' = -\rho_{p}^{(N)}\omega^{2}\beta - \kappa^{(N)}i\omega\beta$$
(14d)

The Lamb waves are governed by Eqs. (16a) and (16b) that are independent of the phason field. Therefore, Lamb waves are not investigated in this case.

(3) The x-direction plate

The phonon displacements are also the same as those in Eq. (5), and the phason displacement in the x-direction is not 0, which is:

$$w_x = \alpha(z) \mathrm{e}^{\mathrm{i}kx - \mathrm{i}\omega t} \tag{15}$$

where $\alpha(z)$ represents the phason displacement amplitude.

The constitutive equations are as follows:

$$\begin{split} T_{yy} &= C_{11}^{(N)} \varepsilon_{yy} + C_{12}^{(N)} \varepsilon_{zz} + C_{13}^{(N)} \varepsilon_{xx} + R_{1}^{(N)} w_{xx} \\ T_{zz} &= C_{12}^{(N)} \varepsilon_{yy} + C_{22}^{(N)} \varepsilon_{zz} + C_{13}^{(N)} \varepsilon_{xx} + R_{1}^{(N)} w_{xx} \\ T_{xx} &= C_{13}^{(N)} \varepsilon_{yy} + C_{13}^{(N)} \varepsilon_{zz} + C_{33}^{(N)} \varepsilon_{xx} + R_{2}^{(N)} w_{xx} \\ T_{yz} &= T_{zy} = 2C_{66}^{(N)} \varepsilon_{yz} \\ T_{xz} &= T_{zx} = 2C_{44}^{(N)} \varepsilon_{xz} + R_{3}^{(N)} w_{xz} \\ T_{xy} &= T_{yx} = 2C_{44}^{(N)} \varepsilon_{xy} + R_{3}^{(N)} w_{xy} \\ H_{xx} &= R_{2}^{(N)} \varepsilon_{xx} + R_{1}^{(N)} \varepsilon_{yy} + R_{1}^{(N)} \varepsilon_{zz} + K_{1}^{(N)} w_{xx} \\ H_{xz} &= 2R_{3}^{(N)} \varepsilon_{xz} + K_{2}^{(N)} w_{xz} \\ H_{xy} &= 2R_{3}^{(N)} \varepsilon_{xy} + K_{2}^{(N)} w_{xy} \end{split}$$
(16b)

Submitting Eqs. (15)-(16) and Eq. (2) into Eq. (1), the differential equations of wave motion are obtained:

$$-C_{33}^{(N)}k^{2}U + C_{44}^{(N)}U'' + (C_{13}^{(N)} + C_{44}^{(N)})ikW' - R_{2}^{(N)}k^{2}\alpha + R_{3}^{(N)}\alpha'' + \left(C_{44}^{(N)}\right)'U' + \left(C_{44}^{(N)}\right)'ikW + \left(R_{3}^{(N)}\right)'\alpha' = -\rho^{(N)}\omega^{2}U$$
(17a)

$$-C_{66}^{(N)}k^{2}V + C_{44}^{(N)}V'' + \left(C_{44}^{(N)}\right)'V' = -\rho^{(N)}\omega^{2}V$$
(17b)

$$(C_{13}^{(N)} + C_{44}^{(N)})ikU' - C_{44}^{(N)}k^2W + C_{22}^{(N)}W'' + (R_3^{(N)} + R_1^{(N)})ik\alpha' + (C_{44}^{(N)})'ikU + (C_{44}^{(N)})'W' + (R_3^{(N)})'ik\alpha = -e^{N}\omega^2W$$

$$(17c)$$

$$(R_{1}^{(N)} + R_{3}^{(N)})ikW' - R_{2}^{(N)}k^{2}U + R_{3}^{(N)}U'' - K_{1}^{(N)}k^{2}\alpha + K_{2}^{(N)}\alpha'' + \left(R_{3}^{(N)}\right)'ikW + \left(R_{3}^{(N)}\right)'U' + \left(K_{2}^{(N)}\right)'\alpha' = -\rho^{(N)}\omega^{2}\alpha$$
(17d)

The SH waves are governed by Eq. (17b) that is independent of the phason field. Therefore, SH waves are not investigated in this case.

3. Numerical Results

In this section, dispersion curves and phonon and phason displacements are calculated using the software "Mathematica". For the multilayered 1D quasi-crystal plates, they are composed of two kinds of quasi-crystal materials (simplified as QC1 and QC2), whose material parameters are listed in Table 1. As a special case, the dissipative kinetic coefficients Γ_{ω} of QC1 and QC2 are assumed to be the same.

3.1. Validation of the Proposed Method

To our best knowledge, rare references about Lamb wave propagating in the multilayered quasicrystal plates are available for comparison. However, the accuracy of the proposed method to investigate guided waves in multilayered crystal plates has been detailed in [7]. Therefore, it is also appropriate for quasi-crystal structures. Subsequently, the convergence of the present method is confirmed. The frequencies with different M of a z-direction sandwich plate (a) with QC1/QC2/QC1-1mm/1mm/1mm are calculated and listed in Table 2. Here, there are two kinds of wave modes in the quasi-crystal plates. A kind of wave modes whose wave characteristics are similar to those of the elastic wave modes in crystal plates are defined as phonon modes. The others are phason modes attributed to the phason field. Comparing these data, we conclude that the present method is convergent. Furthermore, the convergence speed at smaller kh is much faster. For example, when M = 7, the first three modes are convergent at kh = 3, but only one mode is convergent at kh = 15. Hereafter, M = 30 is assumed in the following calculation.

3.2. Lamb Waves

3.2.1. Comparison Between Two Models

Firstly, the dispersion curves of plate (a) in the context of the Bak and elasto-hydrodynamic models are illustrated in Fig. 2. Meanwhile, the case of the corresponding crystal plate ($R_i = K_i = 0$) is investigated. The phonon modes for Lamb waves are divided into symmetric and anti-symmetric modes,

Property	C_{11}	C_{12}	C_{13}	C_{22}	C_{23}	C_{33}	C_{44}	C_{55}
QC1	23.433	5.741	6.663	23.433	6.663	23.222	7.019	7.019
QC2	20	10	10	20	10	15	5	5
	C_{66}	ρ	R_1	R_2	R_3	K_1	K_2	Γ_{ω}
QC1	8.846	4.186	0.8846	0.8846	0.8846	12.2	2.4	4.8
QC2	5	5.07	0.5	0.5	0.5	5	2	4.8
		2	- 0				2	

Table 1. Material parameters of the z-direction QC plate ([14, 23])

units: $C_{ij}(10^{10} \text{N/m}^2)$, $\rho(10^3 \text{kg/m}^3)$, $R_i(10^9 \text{N/m}^2)$, $K_i(10^{10} \text{N/m}^2)$, Γ_{ω} $(10^{-10} \text{cm}^3 \mu \text{s g}^{-1})$

Table 2. Frequencies $\omega(10^3)$ of the three fundamental modes with different M

	M = 6	M = 7	M = 8	M = 9	M = 10	M = 11
1st phason mode	2.24674	2.24674	2.24674	2.24674	2.24674	2.24674
1st phonon mode	2.86670	2.86645	2.86645	2.86645	2.86645	2.86645
2nd phonon mode	4.73497	4.73494	4.73494	4.73494	4.73494	4.73494
1st phason mode	11.0278	11.0278	11.0278	11.0278	11.0278	11.0278
1st phonon mode	17.0811	17.0687	17.0709	17.0704	17.0704	17.0704
2nd phonon mode	18.1748	18.1411	18.1535	18.1534	18.1539	18.1539
	1st phason mode 1st phonon mode 2nd phonon mode 1st phason mode 1st phonon mode 2nd phonon mode	M = 6 1st phason mode 2.24674 1st phonon mode 2.86670 2nd phonon mode 4.73497 1st phason mode 11.0278 1st phonon mode 17.0811 2nd phonon mode 18.1748	M = 6 $M = 7$ 1st phason mode 2.24674 2.24674 1st phonon mode 2.86670 2.86645 2nd phonon mode 4.73497 4.73494 1st phason mode 11.0278 11.0278 1st phonon mode 17.0811 17.0687 2nd phonon mode 18.1748 18.1411	M=6 $M=7$ $M=8$ 1st phason mode 2.24674 2.24674 2.24674 1st phonon mode 2.86670 2.86645 2.86645 2nd phonon mode 4.73497 4.73494 4.73494 1st phason mode 11.0278 11.0278 11.0278 1st phonon mode 17.0811 17.0687 17.0709 2nd phonon mode 18.1748 18.1411 18.1535	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$



Fig. 2. Dispersion curves for plate (a) in the context of two models

which are similar to the elastic wave modes in crystal plates. Similarly, they are also named as A0, S0, A1, S1..... And the phason modes are named as PL0, PL1..... Moreover, the phonon-phason coupling effect on dispersion curves in the context of Bak model is considerable. The first three modes have no cut-off frequencies, not as to the crystal plates, whose first two modes have no cut-off frequencies. Besides, the phonon-phason coupling effect on phonon modes is weak because R_i is far smaller than C_{ij} and K_{ij} . For example, the phase velocity of A0 mode in Fig. 2a slightly increases.

For the elasto-hydrodynamic model, it is observed from Fig. 2b(I) that there are only phonon modes, no phason modes. Actually, there are phason modes. However, their phase velocities are very low in Fig. 2b(II). And the roots of phason modes are complex, whose imaginary parts are very large. For example, as fh = 1 MHz*mm, its imaginary part of the PL0 mode is 522336i. Therefore, they are attenuated instantaneously and not propagative. The reason for this is that their friction coefficients are too large.



Fig. 3. Dispersion curves of two models with different R_i

Then, the phonon-phason coupling effect on dispersion curves is studied in detail. Figure 3 shows dispersion curves of these two models with different R_i . All R_i are simultaneously varied. It can be seen from Fig. 3a that the phonon-phason coupling effect on the phason modes is more significant than on the phonon modes. Furthermore, the phase velocities of phason modes decrease, and phase velocities of phonon modes increase at high frequencies as R_i increase. However, the phonon-phason coupling effect in Fig. 3b only affects the non-propagative phason modes, not the phonon modes. And the phase velocities of phason modes decrease as R_i increase. Therefore, only the Bak model is utilized to investigate the phonon-phason coupling effect in the following subsections.

Next, the phonon-phason coupling effects on the first and second layers are, respectively, analyzed. Firstly, the materials of three layers are assumed to be QC1. Then, R_i of the first and second layers are multiplied by 5 times, respectively. The dispersion curves are illustrated in Fig. 4. The phonon-phason coupling effects on the first two layers are the same at low frequencies. However, they are more significant on the first layer at high frequencies. The reason lies in the fact that energies at high frequencies mainly propagate in the first layer.

3.2.2. Influences of Volume Fractions and Stacking Sequences

Influences of volume fractions and stacking sequences on wave characteristics are illustrated in Fig. 5. Here, we consider other three kinds of z-direction sandwich quasi-crystal plates, which are plate (b): QC1/QC2/QC1-2mm/1mm/1mm; plate (c): QC1/QC2/QC1-1mm/2mm/1mm; and plate (d): QC2/QC1/QC1-1mm/1mm/1mm. Compared with plate (a), the volume fraction of QC1 in plate (b) increases, and that in plate (c) decreases. It is observed from Fig. 5a that phase velocities increase as the volume fraction of QC1 increases, since the wave velocities of QC1 for the phonon and phason modes are larger than those of QC2. Furthermore, it can be observed from Fig. 5b that the stacking sequences have a significant influence on dispersion curves, especially at high frequencies.



S0 mode

Fig. 4. Dispersion curves of the influence of the first and second layers



Fig. 5. Phase velocity dispersion curves with different volume fractions and stacking sequences





Fig. 6. Displacement distributions of the first three modes at kh = 60

3.2.3. Phonon and Phason Displacements

Displacements of the first three modes at kh = 60 are illustrated in Fig. 6. It can be seen that the symmetry of the phason displacement component γ is always consistent with that of the phonon displacement component W. Furthermore, amplitudes of the phonon displacement components U and W of the phonon modes are far greater than that of the phason displacement component γ . However, they are opposite to the phason modes. Moreover, the phonon and phason displacements at high frequencies are mainly distributed in the QC2 layer, i.e., energies are mainly distributed in the QC2 layer. This lies in the reason that elastic modulus and stiffness of the QC2 layer are smaller than those of the QC1 layers.

3.2.4. The Influence of Quasi-Periodic Direction on Wave Characteristics

Figure 7 illustrates the dispersion curves with different quasi-periodic directions. The x-direction sandwich plate with QC1/QC2/QC1-1mm/1mm/1mm is assumed. It is observed that the influence of quasi-periodic direction is weak on the phonon modes, but considerable on the phason modes. The phase velocities of phason modes in the x-direction plate are much higher than those in the z-direction plate.

3.3. SH Waves

Figure 8 shows the dispersion curves of SH waves in a sandwich *y*-direction plate with QC1/QC2/QC1-1mm/1mm/1mm. It can be seen that the phonon modes of SH waves are similar to the elastic wave modes in the crystal plates. Similarly, they are also named as SH0, SH1...... Phason modes are named as PSH0, PSH1...... Furthermore, the phonon–phason coupling effect on phonon modes is also very weak. Moreover, the trend of the phonon modes is similar to that of the phason modes.



Fig. 7. Dispersion curves of Lamb waves with different quasi-periodic directions



Fig. 8. Dispersion curves of SH waves in the sandwich y-direction QC plate



Fig. 9. Phase velocity dispersion curves of the sandwich quasi-crystal plate with different R_i

Subsequently, the phase velocity dispersion curves with different phonon-phason coupling coefficients R_i are illustrated in Fig. 9. It can be seen that the influence of phonon-phason coupling coefficients on the phason modes is more significant than on the phonon modes. Furthermore, the influences on the phonon and phason modes are opposite. As R_i increase, phase velocities of the phason modes decrease, and those of the phonon modes increase.

4. Conclusions

Guided waves in the multilayered 1-D hexagonal quasi-crystal plates in the context of Bak and elasto-hydrodynamic models are, respectively, investigated using the Legendre orthogonal polynomial

method. Dispersion curves and phonon and phason displacement distributions are calculated. Based on the numerical results, the following conclusions can be drawn:

- (1) The phonon-phason coupling effects in the context of Bak model on phonon and phason modes are significant. However, the phonon-phason coupling effects in the context of elasto-hydrodynamic model just affect the non-propagative phason modes, not the phonon modes.
- (2) The phonon-phason coupling effects on the first two layers are the same at low frequencies. However, they are more significant on the first layer than those on the second layer at high frequencies.
- (3) Energies of both phonon and phason modes at high frequencies mainly propagate in the layer with smaller elastic modulus and stiffness.

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References

- Shechtman DG, Blech IA, Gratias D, et al. Metalic phase with long-range orientational order and no translational symmetry. Phys Rev Lett. 1984;53(20):1951–3.
- [2] Fan T. Mathematical theory of elasticity of quasicrystals and its applications. 2nd ed. Heidelberg: Springer; 2016.
- [3] Sakly A, Kenzari S, Bonina D, et al. A novel quasicrystal-resin composite for stereolithography. Mater Des. 2014;56(4):280-5.
- Cao ZH, Ouyang LZ, Wang H, et al. Composition design of Ti-Cr-Mn-Fe alloys for hybrid high-pressure metal hydride tanks. J Alloy Compd. 2015;639:452-7.
- [5] Boscolo M, Banerjee JR. Layer-wise dynamic stiffness solution for free vibration analysis of laminated composite plates. J Sound Vib. 2014;333(1):200-27.
- [6] Ngo-Cong D, Mai-Duy N, Karunasena W, et al. Free vibration analysis of laminated composite plates based on FSDT using one-dimensional IRBFN method. Comput Struct. 2011;89(1-2):1-13.
- [7] Yu JG, Lefebvre JE, Elmaimouni L. Guided waves in multilayered plates: an improved orthogonal polynomial approach. Acta Mech Solida Sin. 2014;27(5):542–50.
- [8] Sun TY, Guo JH, Zhang XY. Static deformation of a multilayered one-dimensional hexagonal quasicrystal plate with piezoelectric effect. Appl Math Mech. 2018;39(3):335–52.
- [9] Li Y, Yang LZ, Gao Y. An exact solution for a functionally graded multilayered one-dimensional orthorhombic quasicrystal plate. Acta Mech. 2019;230(4):1257–73.
- [10] Yang LZ, Li Y, Gao Y, et al. Three-dimensional exact electric-elastic analysis of a multilayered twodimensional decagonal quasicrystal plate subjected to patch loading. Compos Struct. 2017;171:198–216.
- Bak P. Symmetry, stability, and elastic properties of icosahedral incommensurate crystals. Phys Rev B Condens Matter. 1985;32:9(13):5764–72.
- [12] Lubensky TC, Ramaswamy S, Toner J. Hydrodynamics of icosahedral quasi-crystals. Phys Rev B Condens Matter. 1985;32(15):7444–52.
- [13] Shi WC. Conservation laws of a decagonal quasicrystal in elastodynamics. Eur J Mech A Solids. 2005;24(2):217–26.
- [14] Waksmanski N, Pan E, Yang LZ, et al. Free vibration of a multilayered one-dimensional quasi-crystal plate. J Vib Acoust Trans ASME. 2014;136(4):041019.
- [15] Waksmanski N, Pan E, Yang LZ, et al. Harmonic response of multilayered one-dimensional quasicrystal plates subjected to patch loading. J Sound Vib. 2016;375:237–53.
- [16] Chiang YC, Young DL, Sladek J, et al. Local radial basis function collocation method for bending analyses of quasi-crystal plates. Appl Math Model. 2017;50:463–83.
- [17] Chellappan V, Gopalakrishnan S, Mani V. Wave propagation of phonon and phason displacement modes in quasi-crystals: determination of wave parameters. J Appl Phys. 2015;117(5):6778–86.
- [18] Akmaz HK, Umit A. On dynamic plane elasticity problems of 2D quasicrystals. Phys Lett A. 2009;373(22):1901–5.
- [19] Zhu AY, Fan TY. Dynamic crack propagation in decagonal Al–Ni–Co quasi-crystal. J Phys Condens Matter. 2008;20(20):295217.
- [20] Lowe MJ, Cawley P, Galvagni A. Monitoring of corrosion in pipelines using guided waves and permanently installed transducers. J Acoust Soc Am. 2012;132(3):1932.

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- [21] Li XF. Elastohydrodynamic problems in quasicrystal elasticity theory and wave propagation. Philos Mag. 2013;93(13):1500-19.
- [22] Chen WQ, Ma YL, Ding HJ. On three-dimensional elastic problems of one-dimensional hexagonal quasicrystal bodies. Mech Res Commun. 2004;31(6):633–41.
- [23] Wang YW, Wu TH, Li XY, et al. Fundamental elastic field in an infinite medium of two-dimensional hexagonal quasicrystal with a planar crack: 3D exact analysis. Int J Solids Struct. 2015;66:171–83.