TECHNICAL ARTICLE

Removal of Zinc Ions from Acid Aqueous Solutions and Acid Mine Drainage Using Zeolite-Bearing Tuff

Afrodita Zendelska1 [·](http://orcid.org/0000-0001-5109-1465) Mirjana Golomeova¹ · Blagoj Golomeov1 · Boris Krstev1

Received: 11 May 2017 / Accepted: 10 September 2018 / Published online: 18 September 2018 © Springer-Verlag GmbH Germany, part of Springer Nature 2018

Abstract

Zeolite-bearing tuff (stilbite) was shown to be an effective and efficient adsorbent for treating acid mine drainage (AMD). We tested the adsorption of zinc ions from a synthetic acid aqueous solution and AMD from the Sasa mine. The concentration of zinc ions in the AMD decreased from 2.219 to 0.564 mg/dm³ (74% removal). The solution pH, prior to treatment with the zeolite-bearing tuff, was 3.90, and following treatment, it was 5.36. The physical and chemical properties of the tuff were characterized by X-ray diffraction, scanning electron microscopy, and energy dispersive spectroscopy. The concentrations of dissolved metal ions before and after treatment was determined by AES—ICP. The tuff's maximum capacity was determined in equilibrium studies. Experimental data were fitted to adsorption models; the best fit was obtained with the Freundlich adsorption isotherm.

Keywords Raw material · Adsorption · Metals · Equilibrium studies · Sasa mine

Introduction

Mining exposes mineral deposits containing pyrite, sphalerite, galena, or other sulphide minerals to weathering, often producing acid mine drainage (AMD). To meet environmental quality standards, zinc must be removed from polluted surface water and groundwater resources. Conventional methods typically involve such processes as coagulation, precipitation, ion-exchange, electrochemical methods, membrane processes, extraction, and adsorption. Some widely used adsorbents for metals include activated carbon (Kobya et al. [2005](#page-9-0)), clay minerals (Ammann [2003\)](#page-8-0), biomaterials (Reddad et al. [2002;](#page-9-1) Sag and Aktay [2000](#page-9-2)), industrial solid wastes, and zeolites (Babel and Kurniawan [2003](#page-8-1); Blanchard et al. [1984;](#page-8-2) Cabrera et al. [2005;](#page-8-3) Erdem et al. [2004;](#page-8-4) Motsi [2010;](#page-9-3) Pradeep et al. [2015;](#page-9-4) Taffarel and Rubio [2009](#page-9-5); Zendelska et al. [2015](#page-9-6)).

Electronic supplementary material The online version of this article [\(https://doi.org/10.1007/s10230-018-0560-y\)](https://doi.org/10.1007/s10230-018-0560-y) contains supplementary material, which is available to authorized users.

 \boxtimes Afrodita Zendelska afrodita.zendelska@ugd.edu.mk

Zeolites are crystalline micro-porous minerals that are broadly distributed in nature and are often used as absorbents. Natural zeolite is an attractive alternative for wastewater treatment because of its low cost (Cui et al. [2006\)](#page-8-5) and high surface area, which in turn is due to its porous and rigid structure (Alvarez-Ayuso et al. [2003\)](#page-8-6). Zeolites also act as molecular sieves and this property can easily be modified to increase its performance (Sprynskyy et al. [2006](#page-9-7)). Zeolites have a favourable cation exchange capacity (Yuan et al. [1999\)](#page-9-8), high selectivity for cations (Malliou et al. [1994](#page-9-9)), good structural stability in acidic conditions, and can be easily regenerated. They can also have a buffering effect, in that they assist in neutralising acidic solutions via cation exchange (Leinonen and Letho [2001](#page-9-10)).

The objective of this research was to examine the potential treatment of AMD using a zeolite-bearing tuff from the Vetunica deposit in Macedonia. The zeolite-bearing tuff was characterised using classical chemical analysis, X-ray diffraction (XRD), and scanning electron microscopy with energy dispersive spectroscopy (SEM/EDS). The research was conducted using a synthetic acid aqueous solution and AMD from the Sasa lead and zinc mine (Makedonska Kamenica) in Macedonia. The Sasa mine is one of the largest production facilities on the Balkan Peninsula for lead and zinc ore extraction, flotation separation, and recovery of Pb

¹ Faculty of Natural and Technical Sciences, Goce Delcev University, Stip, Macedonia

and Zn concentrate. One of the Sasa mine's negative effects on the environment is its AMD discharge.

Materials and Methods

Analytical Methods

The mineralogical structure of the zeolite-bearing tuff sample was studied using an X-ray diffractometer (Shimadzu 6100). The X-ray diffractometer was equipped with a Cu anode with a radiation wavelength of $CuKa = 1.54178$ Å. The operating voltage was $U=40.0 \text{ kV}$ and current intensity *I*=30.0 mA. Samples were examined within 10.0–80.0 with 2.0 s on each step in a controlled rotational mode at 60.0 rpm. The data were compared to the International Centre for Diffraction Data database, to identify the material in the solid samples.

The surface morphology of the sample was studied using a VEGA3 LMU SEM, which was fitted with an Inca 250 EDS system. An Agilent inductively coupled plasma atomic emission spectroscope (ICP-AES) was used to analyse the concentration of metal ions in solution before and after treatment. Based on material balance, the adsorption capacity was calculated by using the following expression:

$$
q_e = \frac{V(C_o - C_e)}{m}, (mg/g)
$$
 (1)

where q_e is the mass of adsorbed metal ions per unit mass of adsorbent (mg/g), C_o and C_e are the initial and final metal ion concentrations $(mg/dm³)$, respectively, V is the volume of the aqueous phase $(dm³)$, and m is the mass of adsorbent used (g). The degree of adsorption, in percentage, is calculated as:

$$
AD\% = \left(1 - \frac{C_e}{C_o}\right) \cdot 100. \tag{2}
$$

Experimental Procedure and Conditions

The rate of adsorption is a complex function of several factors including: the initial solution pH and concentration, mass of adsorbent, adsorbent particle size, temperature, flow rate in columns, and in the case of batch experiments, agitation speed. Overall reaction rate may be influenced by the separate or combined effect of these factors. In this study, some of these factors were investigated with regards to their effect on the efficiency of zeolite-bearing tuff in removing zinc from solution.

Contact time is one of the most important parameters that influence the adsorption process. For this reason, all experiments were performed within certain time intervals.

Adsorption of zinc ions on zeolite-bearing tuff was performed with different initial concentration (5, 25, 50, 200, and 400 mg/dm^3) of synthetic single ion solutions of zinc ions, and AMD from the Sasa mine with an initial zinc concentration of 2.219 mg/dm^3 . Synthetic single component solutions of this metal were prepared by dissolving a weighed mass of the analytical grade salt $ZnSO_4$ ·7H₂O in 1 dm³ distilled water. The multi-component solution of the metals were prepared by dissolving a weighed mass of the analytical grade salts, $CuSO₄·5H₂O$, $ZnSO₄·7H₂O$, $MnSO₄·H₂O$, and $Pb(NO₃)₂$ in 1 dm^3 distilled water.

The initial pH of the prepared solutions was adjusted by adding 2% sulphuric acid and controlled by a 210 Microprocessor pH meter. The initial pH of the tested solutions was 2.5, 3.5, and 4.5. The experiments were performed in a batch mode in a series of beakers equipped with magnetic stirrers using 2, 5, and 10 g of the tuff in 0.4 dm^3 of zinc ions solution. A magnetic stirrer was used for agitation at 400 rpm, up to 360 min, at temperatures of 20 °C and 60 °C. The final pH was also measured. After a predetermined time, the suspension was filtered and the filtrate's concentration of metal ions in solution was analysed by ICP-AES.

Equilibrium Studies

Equilibrium studies generally involve the determination of the adsorption capacity of a given material. This determination is important in accessing the potential of the material as an economic and commercially viable adsorber. The adsorption of zeolite-bearing tuff was predicted by fitting the experimental data to conventional adsorption mathematical models, namely the Freundlich and Langmuir models.

Langmuir Model

The Langmuir isotherm model (Langmuir [1918\)](#page-9-11), based on monolayer coverage of adsorbent surfaces by the adsorbate at specific homogeneous sites within the adsorbent, is represented as:

$$
q_e = \frac{q_m K_l C_e}{1 + K_l C_e} \tag{3}
$$

where q_e , mg/g, is the amount of solute adsorbed per unit mass of adsorbent at equilibrium; C_e , mg/dm³, is the residual adsorbate concentration in solution at equilibrium; q_m , mg/g, is the amount of solute adsorbed per unit mass of adsorbent corresponding to complete coverage of available sites, K_l , dm³ /mg, is the Langmuir adsorption coefficient, this constant is related to the affinity between the adsorbent and solute, which is evaluated by linearization of Eq. [4](#page-1-0):

$$
\frac{1}{q_e} = \frac{1}{k_l q_m C_e} + \frac{1}{q_m} \tag{4}
$$

The essential characteristics of the Langmuir isotherm can be described by a dimensionless constant called the equilibrium parameter, R_{L} , which is usually defined by:

$$
R_L = \frac{1}{(1 + K_l C_0)}\tag{5}
$$

where K_l is the Langmuir constant that indicates the nature of adsorption and C_0 is the highest initial metal concentration (mg/dm³). The value of R_L indicates if the adsorption isotherm is irreversible ($R_L = 0$), favourable ($0 < R_L < 1$), linear ($R_L = 1$), or unfavourable ($R_L > 1$).

Freundlich Model

The Freundlich isotherm model (Freundlich [1906](#page-8-7)), based on monolayer adsorption on heterogeneous surfaces with a nonuniform distribution of adsorption heat, is represented as:

$$
q_e = k_f C_e^{1/n} \tag{6}
$$

where q_e is the amount of solute adsorbed per unit mass of adsorbent at equilibrium (mg/g) , C_e is the residual adsorbate concentration in solution at equilibrium $(mg/dm³)$, and k_f and *n* are empirical Freundlich constants. k_f (mg/g) is an indicator of adsorption capacity, while n (g/dm^3) is related to the adsorption intensity or binding strength. Their val ues were determined from the linear form of the Freundlich equation:

$$
\log q_e = \log k_f + \frac{1}{n} \log C_e \tag{7}
$$

where $1/n$ is the heterogeneity factor. Values of $1/n < 1$ indicate heterogeneous adsorbents, while values closer to or equal to 1 indicate a material with relatively homogeneous binding sites (Papageorgiou et al. [2006\)](#page-9-12). The zeolite should be a heterogeneous adsorbent due to its porous nature. [Alvare](#page-9-13)z-Ayuso et al. ([2003](#page-8-6)), Avila ([2005\)](#page-8-8) and Gunay et al. [\(2007](#page-9-13)) successfully used the Freundlich adsorption isotherm to model their results from equilibrium experiments.

Results and Discussion

Characteristics of the Adsorbent

The zeolite-bearing tuff was from the Vetunica deposit, which is localised in the northern marginal parts of the well-known Kratovo-Zletovo volcanic area in the Republic of Macedonia. The particle sizes ranged from 0.8 to 2.5 mm. The general characteristics of the zeolite-bearing tuff, such as chemical composition and physical characteristics, are presented in Table [1](#page-2-0) .

The sample was analyzed to determine the content and type of exchangeable cations. The dominant ion, in the exchangeable position, was K^+ (66.5 meq/100 g), followed by Ca²⁺ (21.5 meq/100 g), Mg^{2+} (8.5 meq/100 g), and Na⁺ (3.5 meq/100 g). The total cation exchange capacity was 0.94–1.07 meq/g. The XRD results (Fig. S-1) show that the minerals present in the sample were: stilbite, albite, anorthite, kaolinite, and quartz.

The surface morphology of the sample was studied using the SEM (Fig. [1\)](#page-3-0). The micrographs clearly show a number of micro-pores and well defined crystals of stilbite in the zeolite structure.

Effect of Initial Metal Concentration in Solution

The effect of the initial metal concentration was investigated by contacting 5 g of the zeolite-bearing tuff, at pH 3.5, with different concentrations of the single-component solutions $(5, 25, 50, 200, \text{ and } 400 \text{ mg/dm}^3)$. An increase in concentration generally results in an increase in the amount of zinc adsorbed. This may be due to more collisions between the reactants, leading to an observed increase in reaction rate and capacity (Connors [1990](#page-8-9)). Increasing the initial metal concentration in solution until the system reaches a saturation point will increase the amount adsorbed (q_e) . After reaching saturation, increasing the zinc concentration will

Fig. 1 Micrographs of sample obtained from SEM analysis

not result in any significant change in the amount adsorbed. Results of this investigation are presented (Table [2;](#page-4-0) Fig. [2](#page-4-1)).

These results indicate that the amount of zinc adsorbed by the zeolite-bearing tuff at equilibrium is dependent on the initial dissolved metal concentration. This was expected because it is a consequence of an increase in the concentration-driving force. The concentration-driving force is important because it is responsible for overcoming the mass transfer resistance associated with the adsorption of metals from solution by the adsorbent (Barrer [1978](#page-8-10)). An increase in initial metal concentration in solution not only results in an increase in the amount adsorbed (q_e) but also decreases the efficiency of adsorbents used for the removal of zinc (Table [2](#page-4-0)). Golomeova and Zendelska ([2016\)](#page-8-11), Motsi ([2010](#page-9-3)), and Sprynskyy et al. ([2006\)](#page-9-7) also found a similar trend, that is, less efficient on metal adsorption from solution by zeolite.

Effect of the Mass of the Adsorbent

The effect of the mass of the adsorbent was investigated by contacting 2, 5, and 10 g of zeolite-bearing tuff, at pH

Table 2 Effect of initial ions concentration on the adsorption capacity of zeolite bearing tuff

Initial concentration C_0 (mg/dm ³)	Amount adsorbed q_e (mg/g)	Percentage adsorbed $(\%)$		
5	0.3896	97.4		
25	1.937	96.84		
50	3.632	90.8		
200	13.152	82.2		
400	25.408	79.4		

Fig. 2 Adsorption of zinc ions over time for differing initial ion concentrations

3.5, with the 25 mg/dm^3 Zn solution. An increase in the adsorbent mass should increase the adsorption of zinc ions, because more adsorption sites are available per unit mass of adsorbent. The results confirmed that an increase in the adsorbent mass slightly increased the adsorption of zinc ions (Fig. [3](#page-5-0)); the adsorption of zinc ions was 92% with 2 g of adsorbent and 98% using 10 g of adsorbent.

Effect of the Initial pH of the Solution

The effect of the initial pH of the solution was investigated by contacting 5 g of zeolite-bearing tuff at three pH values $(2.5, 3.5, \text{ and } 4.5)$, with the 25 mg/dm³ Zn solution. As expected, as the pH was decreased, zinc removal efficiency also decreased. This is because $H⁺$ ions compete with zinc cations for the same exchange sites (Alvarez-Ayuso et al. [2003](#page-8-6)), and the electrostatic repulsion between the zinc cations in solution and the protonated zeolite surface increases as more H^+ ions are adsorbed (Cabrera et al. [2005](#page-8-3)). With an increasing pH, the adsorbent surface becomes more negatively charged, thus facilitating greater metal uptake (Turan and Mesci [2011](#page-9-14)).

Figure [4](#page-5-1) shows how the adsorption capacity of zeolitebearing tuff was affected by the solution's pH. Similar results have been obtained by others (Alvarez-Ayuso et al. [2003](#page-8-6); Moreno et al. [2001;](#page-9-15) Motsi [2010](#page-9-3)).

Effect of Temperature

The effect of the temperature of the solution was investigated by contacting 5 g of the zeolite-bearing tuff with the 25 mg/ $dm³$ Zn solution at a pH of 3.5 and temperatures of 20 and 60 °C. Adsorption was quicker at the higher temperature,

Fig. 4 Adsorption capacity over time for solutions of differing initial pH

though the adsorption of zinc ions reached the same level at equilibrium. The duration of the adsorption process can be reduced to 240 min with the same degree of adsorption (Fig. [5\)](#page-5-2).

Effect of Competing Cations

The effect of competing cations was also investigated using a mixture of four metal ions: Cu^{2+} , Mn^{2+} , Zn^{2+} , and Pb^{2+} . The experiments were completed by contacting 5 g of the zeolite-bearing tuff, at pH 3.5 and 20 °C with multi-component solutions of 25 mg/dm 3 Cu, 25 mg/dm 3 Zn, 25 mg/dm 3 Mn, and 25 mg/dm^3 Pb.

Fig. 5 Adsorption of zinc ions over time as a function of temperature

Figure [6](#page-6-0) compares the adsorption of zinc ion from the single- and multi-component solutions. The results show that the amount of Zn^{2+} adsorbed from the multi-component solution was more than 50% less than from the single component solution. This was expected because of the increased amount of competing cations.

The difference in the zeolite-bearing tuff's adsorption capacity for the metal ions can be affected by factors such as the hydration radii, hydration enthalpies, and cation solubility. The hydration radii of the cations are: $r_H Zn^{2+} =$ 4.30 Å, $r_H Cu^{2+} = 4.19$ Å, $r_H Pb^{2+} = 4.01$ Å, and $r_H Mn^{2+}$ $= 4.38$ Å (Nightingale [1959](#page-9-16)). The smallest cations should ideally be adsorbed faster and in larger quantities than the larger cations, since the smaller cations can pass through the micro-pores and channels of the zeolite structure with ease (Calvo et al. [2009\)](#page-8-12). Furthermore, adsorption should be described using hydration enthalpy, which is the energy that permits the detachment of water molecules from cations and thus reflects the ease with which the cation interacts with the adsorbent. Therefore, the more a cation is hydrated, the stronger its hydration enthalpy, and the less it can interact with the adsorbent (Motsi [2010\)](#page-9-3). Because of its high Si:Al ratio, zeolite has a low structural charge density. Therefore, divalent cations with low hydration energies are sorbed preferably compared to cations with high hydration energies (Colella [1991\)](#page-8-13). The hydration energies of the cations are: -2010 , -1955 , -1760 , and -1481 kJmol⁻¹ for Cu²⁺, Zn^{2+} , Mn²⁺, and Pb²⁺ respectively (Mobasherpour et al. [2012](#page-9-17); Nightingale [1959](#page-9-16)). According to the hydration radii,

the order of adsorption should be $Pb^{2+} > Cu^{2+} > Zn^{2+} >$ Mn^{2+} , and according to the hydration enthalpies, the order should be $Pb^{2+} > Mn^{2+} > Zn^{2+} > Cu^{2+}$.

Of the studied cations, the lead cations have the smallest hydration energy and hydration radius and the zeolitebearing tuff will prefer Pb over Cu, Zn, and Mn in multicomponent solutions. Therefore, it is to be expected that Pb concentrations will limit the uptake of Zn, Cu, and Mn.

Equilibrium Experiments

Equilibrium experiments were carried out to determine the maximum Zn adsorption capacity of the zeolite-bearing tuff by contacting 5 g of adsorbent at pH 3.5 and temperature of 20 ± 1 °C with different concentrations of single component solutions 5, 25, 50, 200, and 400 mg/dm³ of Zn^{2+} . The experimental data from these experiments were fitted to the Langmuir and Freundlich adsorption isotherms (Table [3](#page-6-1)).

According to the Freundlich model, the values for the heterogeneity factor, 1/n, indicate that the zeolite-bearing tuff is a heterogeneous adsorbent, because the value of heterogeneity factor is $<< 1$. Based on the correlation coefficients $(R²)$, the adsorption isotherms can be better described by the Freundlich model. The R_L values (Table [3\)](#page-6-1) confirmed that the behaviour of Zn^{2+} adsorption onto used adsorbent was favorable $(0 < R_L < 1)$.

Figures [7](#page-7-0) and [8](#page-7-1) compares the adsorption isotherms based on the Langmuir and Freundlich models with the experimental data. The Freundlich adsorption isotherm is a better

■ Zn in multi component solution ■ Zn in single component solution

Table 3 Calculated equilibrium adsorption isotherm constants for the uptake of zinc from solution by zeolite bearing tuff

Experimental		Langmuir			Freundlich				
q_e (mg/g)	C_e (mg/dm ³)	q_m (mg/g)	k_1 (dm ³ /mg)	\mathbb{R}^2	R_{I}	k_f (dm ³ /mg)	1/n	$n(g/dm^3)$	R^2
25.408	82.4	29.0698	0.0464	0.845	0.0511	.6118	0.6128	1.6319	0.9849

Fig. 7 Equilibrium isotherms: **a** Langmuir model; **b** Freundlich model

Fig. 8 Equilibrium isotherms for Zn adsorption onto zeolite-bearing tuff (stilbite)

fit to the experimental results (Fig. $\frac{8}{15}$). Figure $\frac{8}{15}$ also shows that as the initial concentration of zinc cations increases, the amount of metal adsorbed per gram of adsorbent (q_e) increases too. This is mainly due to the fact that at high metal concentrations, there is a higher solute concentration gradient, which provides the necessary driving force for metal ions to displace exchangeable cations on the surface and from the zeolite's internal micro-pores (Cagin [2006](#page-8-14); Motsi [2010](#page-9-3)). However, this increasing trend is valid up to the point at which the maximum capacity of the adsorbent samples for the respective metal cation is achieved, that is, its saturation point.

The pH was measured before and after treatment for each equilibrium study. Figure [9](#page-7-2) presents the variation in the equilibrium pH values with respect to the initial zinc concentration. The pH values at equilibrium were greater than the initial pH values. As initial zinc concentration increases, the pH increases to 6, then eases and settles at \approx 5.8, regardless of concentration. The adsorption of H^+ ions from solution will cause a pH increase. As the initial zinc concentration increases, the concentration-driving force begins to favor the adsorption of zinc ions over H^+ . According to the results (Fig. [9\)](#page-7-2), it can be confirmed that the zeolite-bearing tuff has a buffering effect.

Acid Mine Drainage Treatment

According to the results obtained with the synthetic acid solutions, it can be concluded that zinc ions were adsorbed efficiently onto zeolite-bearing tuff at the studied conditions. Based on that, the investigation continued with AMD from the Sasa mine. The experiment was performed by contacting 5 g of zeolite-bearing tuff in 0.4 dm^3 of AMD. The magnetic stirrer was agitated at 400 rpm for up to 360 min, at 20 °C. The initial zinc concentration and pH of the AMD are presented in Table [4.](#page-8-15)

The initial concentrations and pH values confirmed that the drainage from the Sasa mine is acidic, with a high concentration of zinc ions. Table [4](#page-8-15) also shows the remaining zinc concentration and the pH of the AMD after treatment. Figures [10](#page-8-16) and [11](#page-8-17) presents the results of the reaction of the AMD with the zeolite-bearing tuff and its effect on рН with respect to contact time.

It can be seen that the zinc ions in the AMD were efficiently adsorbed by the zeolite-bearing tuff; more than 74%

Fig. 9 Variation in pH values with respect to initial zinc concentrations at equilibrium

Table 4 Initial and remain concentration and pH of acid mine drainage from Sasa mine

Fig. 10 Adsorption of zinc ions from acid mine drainage onto zeolitebearing tuff

Fig. 11 Variation in рН values vs. contact time

of the zinc ions were removed. However, the zinc adsorption was lower than in the synthetic acid solution experiment, since other metal ions were present to compete with the zinc ions. The presence of lead ions limited the uptake of others ions because of its small hydrated energy and hydrated radius. Again, the pH zeolite-bearing tuff had a buffering effect, even with AMD.

Conclusion

The adsorption of zinc ions onto a zeolite-bearing tuff was shown to occur efficiently. It was most effective at lower concentrations of zinc ions, a higher adsorbent mass, and higher pH and was faster at a higher temperature. The maximum capacity of the tuff for removal of zinc ions from solution was determined and, in general, the Freundlich adsorption isotherm was a better fit with the experimental results. While investigating the effect of the competing cations, it was concluded that the presence of cations with smaller hydration energies and hydration radii, such as lead cations, limits the uptake of zinc cations. The investigation then tested the adsorption of zinc ions onto the zeolite-bearing tuff from the Sasa mine AMD and more than 74% of the zinc ions were removed.

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