ORIGINAL ARTICLE

Study on desulfurization performance of MnO₂-based activated **carbon from waste coconut shell for diesel emissions control**

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Abstract

Increasing concern about the air pollution caused by sulfur dioxide $(SO₂)$ from diesel exhaust has resulted in the improvement of low-temperature desulfurization materials for the combined $SO₂$ trap. In this study, coconut shell activated carbon (AC) is pretreated by nitric acid to prepare $MnO₂$ -based activated carbon materials for $SO₂$ removal. The prepared materials are characterized intensively by SEM, TEM, BET, XRD, FTIR, and XPS. The $SO₂$ capture capacity of these materials are measured at low temperature by thermogravimetry, and the SO_2 equilibrium adsorption characteristic is also investigated. The results show that the concentrations of nitric acid do not significantly change the textural properties of MnO₂-based AC materials. The content of surface-oxygenated groups (carbonyl carbon and transition) initially increases with the $HNO₃$ concentration rising and reaches the maximum value when the $HNO₃$ concentration is 10 mol/L, resulting in the enhancement of the SO_2 capture capacity. SO_2 capture capacity of MnO₂-based activated carbon decreases after regeneration and keeps stable after several cycles of thermal regeneration. The experimental data for SO_2 adsorption on MnO_2 -based AC composite can fit the Freundlich model well in comparison with Langmuir model.

Keywords $SO_2 \cdot \text{MnO}_2 \cdot$ Activated carbon \cdot Nitric acid \cdot Freundlich model

Introduction

Sulfur dioxide $(SO₂)$ from diesel engine exhaust is a serious threat to the environment and human health, because SO_2 has the major role in generating acid rain and deactivating the NO_x removal catalysts $[1-3]$ $[1-3]$ $[1-3]$. Many technologies have

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been proposed to remove $SO₂$ from diesel engine exhaust. Among these, the compact SO₂ trap device upstream of NO_x conversion device has been used successfully for the removal of SO_2 to improve the longevity of NO_x removal catalysts against SO_2 poisoning $[4-6]$ $[4-6]$.

As the temperature of diesel engine exhaust is in a wide region from 50 to 650 °C, a combined SO_2 trap is proposed to completely capture the $SO₂$ in this tempera-ture region [[7\]](#page-6-4). The combined $SO₂$ trap has three parts: high temperature materials, middle temperature materials and low-temperature materials. The desulfurization material is an important factor for designing the combined $SO₂$ trap device. The carbonates exhibits good reactivity with SO_2 at the reaction temperature range from 400 to 650 °C, and the desulfurization rate declines below 400 °C for the reason that the reaction activity is limited by decarbona-tion [\[8\]](#page-6-5). Metal oxides (such as MgO $[9]$, V₂O₅ [[10\]](#page-6-7) and hydrotalcite-like compounds [\[11](#page-6-8)]) with sulfate reaction path $(M_xO_y + ySO_2 + 0.5yO_2 \rightarrow M_x(SO_4)_y)$ have good SO₂ capture performance over the temperature range from 200 to 450 °C. Based on these fundamental studies, it has been found that most desulfurization materials are focused on the desulfurization performance from 200 to 650 $^{\circ}$ C for SO₂

traps, and limited studies on the desulfurization performance from 50 to 200 °C desulfurization materials for the combined $SO₂$ trap have been reported.

For developing the desulfurization performance of the combined $SO₂$ trap, the improvement of low-temperature desulfurization activity of materials for the combined $SO₂$ trap is needed. Rubio $[12]$ $[12]$ investigated the SO₂ capture performance of coal fly ash based on carbon materials at flue gas desulfurization conditions. Tseng [\[13\]](#page-7-1) studied the desulfurization activity of copper oxide (CuO) supported on activated carbon over the low-temperature range. In the previous studies $[14, 15]$ $[14, 15]$ $[14, 15]$, MnO₂ has been found to exhibit remarkable sulfur dioxide capture capacity. $MnO₂$ supported on AC have a promising prospect used as low-temperature desulfurization materials for the combined SO_2 trap [\[7](#page-6-4)]. Manganese supported on activated carbon treated by $HNO₃$ exhibited high SO_2 removal capacity [\[16](#page-7-4)]. However, the relationship between the amount of surface-oxygenated groups and $SO₂$ removal capacity of $MnO₂$ -based AC has not been reported yet.

In the present work, the high-specific-surface-area coconut shell AC is pretreated by nitric acid to modify the surface functional groups and used as a support to prepare $MnO₂$ -based AC composite by situ deposition method. Effects of the surface-oxygenated groups of $MnO₂$ -based AC composite by nitric acid treatment on the SO_2 capture capacity are studied. The $SO₂$ adsorption characteristics and regeneration performance of $MnO₂$ -based activated carbon composite at low-temperature range are also investigated.

Experimental section

Materials

The activated carbon (BET surface area of $1250 \text{ m}^2/\text{g}$) made from waste coconut shells was supplied by Xinsen Chemical Industry Co. Ltd. Potassium permanganate and manganese acetate tetrahydrate were purchased from Beijing Chemical Co., Ltd., People's Republic of China and were of analytical reagent grade.

The MnO_2 -based AC composites were prepared by situ deposition method, the formation procedures as shown in Fig. [1](#page-1-0). The activated carbon was pretreated with different concentrations of HNO₃ (from 0 to 15 mol/L) at 80 °C for 6 h, then washed with a lot of distilled water, and dried in a vacuum at 110 °C overnight. 2 g pretreated AC was added to 0.03 mol/L 100 mL $KMnO₄$ solution and stirred at room temperature condition for 2 h, then gradually added 0.045 mol/L 100 ml $Mn(CH_3COO)$, solution and stirred at room temperature condition for 5 h, then washed with a lot of distilled water, and eventually dried in air dry oven at 110 °C overnight. The product is denoted as $MnO₂–ACx$, where x represents the concentration of $HNO₃$.

Characterization

In this study, the textural properties of the samples were analyzed by N_2 adsorption–desorption isotherms using Micromeritics ASAP 2020 apparatus. The specific surface area of these samples was measured by the Brunauer–Emmett–Teller (BET) with the nitrogen adsorption uptake at the boiling point of nitrogen of 77 K using a capacitive measurement method. The pore volumes were measured by nitrogen physisorption under normal relative pressure of 0.1–1.0 using the Barrett–Joyner–Halenda (BJH) method. Surface observation of the samples was conducted by scanning electron microscopy (SEM, Hitachi S-4800). Before SEM experiment, the sample was pretreated by goldsputtering. Transmission electron microscopy (TEM) images were recorded on a JEOL JEM-2100F electron microscope. The powder sample was ultrasonically dispersed in acetone for 30 min at room temperature and dipped onto a carboncoated copper grid. The crystal structures were further determined by X-ray diffraction (XRD, X'Pert Pro MPD, Cu Kα radiation). Fourier transform infrared (FTIR) spectra were recorded using a Tensor 27 spectrometer with KBr pellet method. X-ray photoelectron spectroscopy (XPS) was conducted to determine the chemical composition and functional groups using an XSAM-800 spectrometer (Kratos, UK) with Al (1486.6 eV) under ultrahigh vacuum (UHV) at 12 kV and 15 mA. Energy calibration was performed by recording the core level spectra of Au $4f_{7/2}$ (84.0 eV) and Ag $3d_{5/2}$ (368.30 eV).

SEM and TEM analyses are employed to visualize the morphology and structure of AC and $MnO₂$ –AC10, as shown in Fig. [2.](#page-2-0) It can be seen that AC is a planar architecture with a well-defined pores (Fig. [2a](#page-2-0)). This planararchitecture structure of AC facilitates the adsorption of reagents and exposes more active sites for SO_2 removal. After deposition, a large number of nano-flake $MnO₂$ particles are only formed and highly dispersed on the surface

Fig. 1 Illustration of the formation procedures of $MnO₂$ -based AC composite

Fig. 3 XRD patterns of AC and $MnO₂$ –AC10 (filled circle) reflections of $MnO₂$ (filled diamond) reflections of carbon

of AC and no free nanoparticles are formed outside the AC nanosheets (Fig. [2b](#page-2-0), d). The $MnO₂$ nanoparticles are confirmed by XRD analysis (Fig. [3\)](#page-2-1). The diffraction peaks of as-prepared $MnO₂ - AC10$ are similar to those of hexagonal $MnO₂$ (JCPDS 30-0820) and the reflection peaks of layered AC become much lower, which also indicating that nano-flake $MnO₂$ particles are homogeneously formed on the AC surface.

Fig. 4 Schematic drawing of TG analysis

Desulfurization performance evaluation

Thermogravimetry (TG) was used in this study to measure the SO_2 capture performance of the prepared materials. Figure [4](#page-2-2) shows a schematic drawing of the TG analysis experiment. The amount 50 mg of a sample on a quartz crucible was slowly (5 K/min) heated to the target temperature in the atmosphere of nitrogen, and maintained this condition for about 2 h. Reactant gas flow (500 ppm SO_2 in base N_2) was controlled by mass flow controller. The total flow gas rate was 2 Ls/min. The reaction temperature of the TG experiment ranged from 50 to 200 °C for 40 min. The used $MnO₂$ –AC were regenerated in N₂ atmosphere at a flow rate of 500 mL/min and at 360 °C for 1 h. Then the regenerated

sample was cooled to reaction temperature under pure $N₂$ steam. After that, a 2 Ls/min gas mixture (500 ppm SO_2 in base N_2) was controlled by mass flow controller and added into the reactor for further desulfurization–regeneration testing.

The $SO₂$ capture performance of samples was measured. The SO_2 capture performance per unit mass *P* is expressed by the following equation:

$$
P = \frac{s_t - s_0}{s_0} \left[g_{\text{SO}_2} / g_{\text{Material}} \right]
$$
 (1)

where P is the SO_2 capture performance per unit mass $[g_{SO2}/g_{\text{Material}}]$, s_0 is the initial weight [mg], and s_t is the weight after *t* seconds [mg].

Results and discussion

SO₂ capture performance of the prepared materials

The SO_2 capture performance of the prepared MnO₂-based activated carbon composites $(MnO₂-AC0, MnO₂-AC5,$ $MnO₂$ –AC10 and $MnO₂$ –AC15) was measured at the following conditions: 100 °C and 500 ppm SO₂ in base N₂ for 40 min. Figure [5](#page-3-0) shows the SO_2 capture capacity of the prepared materials. The $SO₂$ capture performance of $MnO₂$ –AC0 was 26 mg/g. The SO₂ capture performance of $MnO₂$ -based activated carbon composite increased after

Fig. 5 SO_2 capture performance of the prepared samples (experimental conditions: 100 °C, 500 ppm SO_2 in base N_2)

nitric acid pretreatment. When the acid concentration is below 10 mol/L, the SO_2 capture capacity has improved with the increase of treatment concentration, and the $SO₂$ capture capacity has attained the highest as the treatment concentration is 10 mol/L. The $SO₂$ capture capacity of $MnO₂$ –AC10 is 44 mg/g, which is significantly higher than the low-temperature desulfurization material, such as coal fly ash (13 mg/g) [\[12\]](#page-7-0) and CuO/AC (below 10 mg/g) [\[13](#page-7-1)]. However, when the pretreatment concentration is above 10 mol/L, the SO_2 capture capacity has reduced with the increase of treatment concentration. The $SO₂$ capture capacity of $MnO₂$ –AC15 has decreased to 28 mg/g. It is reported that the content of the surface-oxygenated groups of activated carbon increases with the increase of the acid treatment concentration [\[17](#page-7-5)], and the surface functional groups are the important factors for the SO_2 removal [[16\]](#page-7-4).

Textural characteristic analysis of MnO₂-based AC **materials**

The textual properties of the prepared $MnO₂$ -based activated carbon are characterized by $N₂$ adsorption–desorption instruments apparatus and are shown in Table [1.](#page-3-1) The BET surface area and pore volume of the MnO_2 –AC0 are 1012 m²/g and $0.17 \text{ cm}^3/\text{g}$, respectively. After pretreated by HNO_3 , the pore volume and average pore diameter of $MnO₂$ -based activated carbon are in the range of $0.17-0.20$ cm³/g and 3.12–3.15 nm, respectively. It has been reported in many works that the liquid phase oxidation by $HNO₃$ may not significantly change the textural properties of AC [[18,](#page-7-6) [19](#page-7-7)]. The BET surface areas of the $MnO₂$ -based activated carbon are slightly reduced from 1012 to 918 m^2/g after nitric acid treatment. The slight decrease in the surface area of $MnO₂$ -based AC may be due to the abundant presence of oxygenated groups introduced on the surface of the AC by the pretreatment with $HNO₃$, which possibly block the entry of N_2 inside the small pores [[17,](#page-7-5) [20\]](#page-7-8).

Surface functional groups on MnO₂-based AC samples

The FTIR was carried out to determine the functional groups on the prepared $MnO₂$ -based activated carbon composites. The FTIR spectrum of the prepared materials $(MnO₂-AC0,$

Table 1 Textural prope $MnO₂$ -based AC mater $MnO₂–AC5$, $MnO₂–AC10$, and $MnO₂–AC15$) is illustrated in Fig. [6](#page-4-0). From the FTIR spectrum of the prepared materi-als shown in Fig. [6](#page-4-0), the peaks around 3430 cm⁻¹ should be attributed to the O–H stretching vibration [[21](#page-7-9)], and the bands around 1623 cm−1 are normally attributed to O–Hbending vibrations combined with Mn atoms [\[22](#page-7-10)]. The relatively sharp peaks around 1395 cm^{-1} should be ascribed to

Fig. 6 FTIR spectrum of MnO_2 -AC0 (**a**), MnO_2 -AC5 (**b**), MnO_2 - $AC10$ (**c**), and $MnO₂–AC15$ (**d**)

spectra: $MnO₂ - ACO (a)$,

C=O stretch from carboxylic groups $[23]$ $[23]$. The C=O stretch peaks of $MnO₂$ –AC10 are highest than the other prepared samples. The bands around 448 and 650 cm⁻¹ should be ascribed to the Mn–O and Mn–O–Mn vibrations in octahedral MnO₂ [22 , $24-26$], which further confirms the successful integration of $MnO₂$ on the surface of activated carbon.

Surface functional groups on the prepared samples were further investigated by XPS analyses. Figure [7](#page-4-1) shows the XPS spectrum of the prepared materials $(MnO₂-AC0,$ $MnO₂$ –AC5, MnO₂–AC10, and MnO₂–AC15). The C 1 s pattern of the prepared samples included four peaks with binding energy at around 284.5, 286, 288, and 290 eV. These peaks correspond to graphitizing carbon (C–C), phenolic (C–O), carbonyl carbon (C=O) and transition $(\pi-\pi^*)$, respectively [[27](#page-7-14), [28\]](#page-7-15). The corresponding binding energy and relative content of the samples are listed in Table [2.](#page-5-0) As shown in Table [2](#page-5-0), compared with that in $MnO₂–AC0$, the content of graphitizing carbon (C–C) in $MnO₂$ –AC5, $MnO₂$ –AC10 decreases, while the content of transition (*π*–*π**) slightly increases. After acid pretreatment of AC, the content of carbonyl carbon (C=O) initially increases with the $HNO₃$ concentration rising and reaches the maximum value when the $HNO₃$ concentration is 10 mol/L. The maximum content of carbonyl carbon (C=O) of the as-prepared $MnO₂$ –AC10 was 16.55%. However, when the HNO₃ concentration further increases, the content of carbonyl carbon

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Table 2 Binding energy (BE) and relative content (RC) of C 1 s for $MnO₂/AC$ samples

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(C=O) is decreased instead. This result showed a similar change trend with that of FTIR spectra for the prepared samples (shown in Fig. [5](#page-3-0)).

It is reported that the oxygenated groups of carbonyl carbon (C=O) and transition $(\pi-\pi^*)$ with the basic nature are more favorable for SO_2 capture [\[28–](#page-7-15)[31\]](#page-7-16). Therefore, the change of surface-oxygenated groups, carbonyl carbon (C=O), and transition $(\pi-\pi^*)$, was responsible for the better SO_2 capture capacity of acid-pretreatment MnO₂/AC composite. Thus, $MnO₂ - AC10$ with the maximum contents of carbonyl carbon (C=O) and transition $(\pi-\pi^*)$ exhibits the best $SO₂$ capture capacity among all the prepared materials.

SO2 capture performance of fresh and regenerated MnO₂-based AC composite

 $MnO₂$ –AC10 was chosen to investigate the SO₂ capture performance in low-temperature region due to its superior SO_2 capture performance. The SO_2 capture performance of $MnO₂–AC10$ is measured by a thermogravimetry (TG) device at various temperatures (50, 100, 150, and 200 °C) for 40 min with a 2 L/min flow gas containing 500 ppm $SO₂$ in nitrogen, and the results are shown in Fig. [8.](#page-5-1) From the results shown in Fig. 8 , the SO₂ capture performance of $MnO₂$ –AC10 increases with the experimental temperature rising. The prepared $MnO₂$ –AC10 has good SO₂ capture performance with absorbance about 78.3, 59.2, 44.0, and 30.8 mg/g at 200, 150, 100, and 50 °C, respectively.

To investigate the thermal regeneration of $MnO₂$ -based activated carbon composites, the $SO₂$ capture performance of MnO₂–AC10 sample is studied at 200 and 50 $^{\circ}$ C with consecutive desulfurization regeneration cycles, and the results are shown in Fig. 9 . The SO₂ capture performance of $MnO₂ - AC10$ decreases after thermal regeneration and the decrease trend is more evident at 200 $^{\circ}$ C. At 50 $^{\circ}$ C, $MnO₂$ –AC10 has relatively stable regeneration performance with the increase of regeneration cycles, and the $SO₂$ capture performance of $MnO₂-AC10$ is about 18 mg/g after two cycles of thermal regeneration. It is reported that $SO₂$ capture performance of the Mn-modified activated coke decreases after regeneration in N_2 steam, and the desulfurization capacity keeps stable after several cycles of thermal regeneration [\[28](#page-7-15)].

Fig. 8 Temperature dependence of SO_2 capture performance of $MnO₂$ -based activated carbon

Fig. 9 SO₂ capture performance of $MnO₂–AC10$ with different regeneration cycles at 50 and 200 °C

Adsorption mechanism

Langmuir and Freundlich models are the most conventional equilibrium adsorption isotherm models to represent the obtained equilibrium data for heterogeneous adsorption on the surface of materials with a chemisorption process.

In this study, the values of the constants for Langmuir and Freundlich models obtained from the experimental equilibrium data of $MnO₂$ -based activated carbon composite (MnO₂–AC10) at a reaction temperature of 100 $^{\circ}$ C are displayed in Table [3](#page-6-9). It is seen that Freundlich model fit the data reasonably well and the value of R-square is as high as 0.998. Freundlich constant (K_f) related to the adsorption capacity of 1.43 was calculated from the intercept of the linear form of the Freundlich model. Freundlich constant (*n*) related to the adsorption intensity of 2.03 was calculated from the slope of the linear form of Freundlich model. In comparison with the value of Freundlich constant *n* (1.059) of zeolitic tuff calculated by Al-Harahsheh [\[32\]](#page-7-17), it is evidenced that the $MnO₂$ -based activated carbon composite exhibits high activity for SO_2 adsorption.

Furthermore, the thermodynamic parameters, such as heat of adsorption (ΔH^0) , entropy (ΔS^0) changes, and free energy of the process (ΔG^0) are determined by the following equations (2) and (3) (3) :

$$
\Delta G^0 = -RT \ln K_f \tag{2}
$$

$$
\ln K_f = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT}
$$
\n(3)

where *R* is the gas constant $[8.314 \text{ J/(mol K)}]$ and *T* is the temperature (K), and K_f is the Freundlich constant (L/mg). ΔH^0 and ΔS^0 can be obtained from the slope and intercept of the linear plot of $\ln K_f$ versus 1/T, respectively.

The decrease in negative values of the free energy (ΔG^0) from −1.11 kJ/mol at 100 °C to −3.67 kJ/mol at 200 °C suggests that the SO_2 adsorption on MnO_2 -based activated carbon composite is a more favorable adsorption process at elevated temperature [\[32](#page-7-17)]. The calculated values of ΔH^0 and ΔS^0 are 13.36 kJ/mol and 48.45 J/(mol K), respectively. The positive ΔS^0 and ΔH^0 values indicate that the degrees of freedom increased at the solid–gas interface during the sulfur dioxide capture process [[33\]](#page-7-18).

Conclusions

In this study, a series of $MnO₂$ -based AC materials are successfully prepared by deposition method with various concentration of nitric acid treatment to study the influence

of surface-oxygenated groups on the $SO₂$ capture capacity. After preparation, nanoneedle $MnO₂$ particles are formed and homogeneously dispersed on the AC surface. The $SO₂$ capture performance of $MnO₂$ -based activated carbon composite initially increases with the $HNO₃$ concentration rising and reaches the maximum value when the $HNO₃$ concentration is 10 mol/L because the as-prepared $MnO₂$ –AC10 has the maximum content of surface-oxygenated groups (carbonyl carbon and transition) for capturing SO_2 more favorably. The maximum SO_2 -capture capacity of MnO_2 -AC10 is 44 mg/g. The SO_2 -capture performance of MnO₂–AC10 decreases after regeneration, and the decrease trend is more evident at higher temperature. Furthermore, compared with Langmuir model the experimental data for $SO₂$ adsorption on $MnO₂-AC10$ fits the Freundlich model better. The calculated values of ΔH^0 and ΔS^0 were 13.36 kJ/mol and 48.45 J/ (mol K), respectively, indicating that the SO_2 adsorption on $MnO₂$ -based activated carbon is a spontaneous process.

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References

- 1. Osaka Y, Kito T, Kobayashi N et al (2015) Removal of sulfur dioxide from diesel exhaust gases by using dry desulfurization MnO2 filter. Sep Purif Technol 150:80–85
- 2. Lee KT, Bhatia S, Mohamed AR (2005) Preparation and characterization of sorbents prepared from ash (waste material) for sulfur dioxide $(SO₂)$ removal. J Mater Cycles Waste $7(1):16-23$
- 3. Hunsinger H, Andersson S (2014) The potential of $SO₂$ for reducing corrosion in WtE plants. J Mater Cycles Waste 16(4):657–664
- 4. Limousy L, Mahzoul H, Brilhac JF et al (2003) A study of the regeneration of fresh and aged SO*x* adsorbers under reducing conditions. Appl Catal B: Environ 45(3):169–179
- Limousy L, Mahzoul H, Brilhac JF et al (2003) SO₂ sorption on fresh and aged SOx traps. Appl Catal B: Environ 42(3):237–249
- 6. Tikhomirov K, Krocher O, Elsener M et al (2006) Manganese based materials for diesel exhaust $SO₂$ traps. Appl Catal B: Environ 67(3–4):160–167
- Liu XC, Osaka Y, Huang HY et al., Development of low-temperature desulfurization performance of a $MnO₂/AC$ composite for a combined SO₂ trap for diesel exhaust. RSC Adv. 2016, 6, (98), 96367–96375
- 8. Osaka Y, Kurahara S, Kobayashi N, Hasatani M, Matsuyama A (2015) Study on SO_2 -absorption behavior of composite materials for DeSO(x) filter from diesel exhaust. Heat Transfer Eng 36(3):325–332
- 9. Sohn HY, Han DH (2002) Ca-Mg acetate as dry SO_2 sorbent: III. Sulfation of MgO plus CaO. Aiche J 48(12):2985–2991
- 10. Zhang D, Ji L, Liu Z et al (2015) Kinetics of thermal regeneration of SO_2 -captured V_2O_5/AC . Ind Eng Chem Res 54(38):9289–9295
- 11. Cantu M, Lopez-Salinas E, Valente JS (2005) SO*x* removal by calcined MgAIFe hydrotalcite-like materials: Effect of the chemical

composition and the cerium incorporation method. Environ Sci Technol 39(24):9715–9720

- 12. Rubio B, Izquierdo MT (2010) Coal fly ash based carbons for $SO₂$ removal from flue gases. Waste Manage 30(7):1341–1347
- 13. Tseng HH, Wey MY (2004) Study of $SO₂$ adsorption and thermal regeneration over activated carbon-supported copper oxide catalysts. Carbon 42(11):2269–2278

14. Liu X, Osaka Y, Huang H et al (2016) Development of highperformance SO_2 trap materials in the low-temperature region for diesel exhaust emission control. Sep Purif Technol 162:127–133

- 15. Liu X, Osaka Y, Huang H et al (2017) Development of compact $MnO₂$ filter for removal of SO₂ from diesel vehicle emission. RSC Adv 7:18500–18507
- 16. Liu Y, Qu Y, Guo J et al (2015) Thermal regeneration of manganese supported on activated carbons treated by $HNO₃$ for desulfurization. Energy Fuels 29(3):1931–1940
- 17. Zhang G, Li Z, Zheng H et al (2015) Influence of the surface oxygenated groups of activated carbon on preparation of a nano Cu/AC catalyst and heterogeneous catalysis in the oxidative carbonylation of methanol. Appl Catal B: Environ 179:95–105
- 18. Xu J, Zhao J, Xu J et al (2014) Influence of surface chemistry of activated carbon on the activity of gold/activated carbon catalyst in acetylene hydrochlorination. Ind Eng Chem Res 53(37):14272–14281
- 19. Alegre C, Gálvez ME, Baquedano E et al (2013) Oxygen-functionalized highly mesoporous carbon xerogel based catalysts for direct methanol fuel cell anodes. J Phys Chem C 117(25):13045–13058
- 20. Rodrigues EG, Pereira MFR, Chen X et al (2011) Influence of activated carbon surface chemistry on the activity of Au/AC catalysts in glycerol oxidation. J Catal 281(1):119–127
- 21. Aguilar C, García R, Soto-Garrido G et al (2003) Catalytic wet air oxidation of aqueous ammonia with activated carbon. Appl Catal B: Environ 46(2):229–237
- 22. Yuan A, Zhang Q (2006) A novel hybrid manganese dioxide/activated carbon supercapacitor using lithium hydroxide electrolyte. Electrochem Commun 8(7):1173–1178
- 23. Xia Y, Meng L, Jiang Y et al; Zhao M (2015) Facile preparation of $MnO₂$ functionalized baker's yeast composites and their adsorption mechanism for Cadmium. Chem Eng J 259:927–935
- 24. Lu L, Tian H, He J et al., Graphene-MnO₂ Hybrid nanostructure as a new catalyst for formaldehyde oxidation. J Phys Chem C 2016, *120*, (41), 23660–23668
- 25. Xie X, Gao L (2007) Characterization of a manganese dioxide/ carbon nanotube composite fabricated using an in situ coating method. Carbon 45(12):2365–2373
- 26. Chu HY, Lai QY, Wang L et al (2010) Preparation of MnO₂/ WMNT composite and $MnO₂/AB$ composite by redox deposition method and its comparative study as supercapacitive materials. Ionics 16(3):233–238
- 27. Guo JX, Fan L, Peng JF et al (2014) Desulfurization activity of metal oxides blended into walnut shell based activated carbons. J Chem Technol Biotechnol 89(10):1565–1575
- 28. Yang L, Jiang X, Yang ZS et al (2015) Effect of MnSO₄ on the removal of $SO₂$ by manganese-modified activated coke. Ind Eng Chem Res 54(5):1689–1696
- 29. Fan L, Chen J, Guo J et al (2013) Influence of manganese, iron and pyrolusite blending on the physiochemical properties and desulfurization activities of activated carbons from walnut shell. J Anal Appl Pyrol 104:353–360
- 30. Shangguan J, Li CH, Miao MQ et al (2008) Surface characterization and $SO₂$ removal activity of activated semi-coke with heat treatment. New Carbon Mater 23(1):37–43
- 31. Zuo Y, Yi H, Tang X, Zhao S, Zhang B, Wang Z, Gao F (2015) Study on active coke-based adsorbents for $SO₂$ removal in flue gas. J Chem Technol Biotechnol 90(10):1876–1885
- 32. Al-Harahsheh M, Shawabkeh R, Batiha M et al (2014) Sulfur dioxide removal using natural zeolitic tuff. Fuel Process Technol 126(0):249–258
- 33. Gupta VK, Ali I, Suhas et al (2003) Equilibrium uptake and sorption dynamics for the removal of a basic dye (basic red) using low-cost adsorbents. J Colloid Interface Sci 265(2):257–264