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Identification of coal seams suitability for carbon dioxide sequestration with enhanced coalbed methane recovery: a case study in South Sumatera Basin, Indonesia

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Abstract Sequestering carbon dioxide $(CO₂)$ with enhanced coalbed methane recovery (ECBM) is a promising clean coal technology in Indonesia, which can reduce $CO₂$ emissions and potentially lower-cost alternative for fulfilling of future Indonesia's gas demand. Coal seams in South Sumatera Basin, Indonesia, are well placed to take advantage of $CO₂$ sequestration based on economical and regulatory criteria. From technical criteria assessment, there are very limited studies undertaken in this area, especially for identification of coal seams suitability for $CO₂$ -ECBM in South Sumatera Basin. This study has therefore aimed to propose the technical criteria of coal seams suitability for $CO₂$ -ECBM recovery as well as predicting $CO₂$ storage capacity by developing a novel numerical model based on the characteristics of coal seams in South Sumatera Basin. The comparison of primary and $CO₂$ -ECBM recovery was analysed by performing production forecasting for 30 year of simulation. A sensitivity study was then conducted in order to examine the performance of $CO₂$ -ECBM under the influences of permeability, a determining factor in the viability of a $CO₂$ storage in coal seams. A simplified method for estimating $CO₂$ storage capacity in coal seams has been proposed which was validated with the novel numerical model through parametric studies. From this study, one can screen the suitable coal seams for $CO₂$ storage with enhanced coalbed methane recovery and can quickly quantify the $CO₂$ storage capacity in the coal seams with general available data.

& Edo Pratama edo.pratama1@yahoo.com **Keywords** South Sumatera Basin \cdot CO₂-ECBM \cdot CO₂ storage capacity - Novel numerical model

Introduction

Indonesia has the highest carbon dioxide $(CO₂)$ emissions rate among the Southeast Asian region and the tenth largest $CO₂$ emitting country in the world with 611.4 MtCO₂ emissions in 2015 (BP [2016\)](#page-6-0). Carbon capture storage (CCS) provides an opportunity for the government of Indonesia's goal of improved energy supply and security, while also reducing $CO₂$ emissions. Studies regarding to CCS in Indonesia have been conducted since 2003, and the first CCS project was started in 2012 at the Gundih Gas Field in Central Java, Indonesia. According to LEMIGAS [\(2015](#page-6-0)), South Sumatera Basin is the third most suitable sedimentary basins for $CO₂$ storage due to wellcharacterized reservoirs, favourable and well-known geological structure, and there is potential to reuse existing infrastructure. The current studies regarding to $CO₂$ storage in South Sumatera are focusing in depleted oil and gas reservoirs. Coal seams also have good potential for $CO₂$ storage while enhancing coal seam gas recovery.

Coalbed methane (CBM) resource in Indonesia is identified of 453.3 TCF, and the biggest CBM resources are located in South Sumatera Basin which is about 183 TCF or 40.37% of total Indonesia's CBM resource (Stevens and Hadiyanto [2004](#page-6-0)). With regard to the increase of gas demand significantly in Indonesia, CBM will be potentially lower-cost alternative for fulfilling of future Indonesia's gas demand. South Sumatera has large presence of the industrial and power sector which resulted in high-purity $CO₂$ content and large $CO₂$ volume per year (LEMIGAS [2015\)](#page-6-0). The existing gas pipeline infrastructure

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can be used to accommodate the $CO₂$ captured from the $CO₂$ sources, as well as low cost $CO₂$ sources (World Bank [2015\)](#page-6-0). Gas supply shortages in Sumatra and West Java could provide a strong regional market opportunity for CBM (Wood Mackenzie [2017\)](#page-6-0). These conditions potentially make South Sumatera is well placed to take advantage of $CO₂$ sequestration opportunities. These facts encouraged the authors to conduct a comprehensive study on $CO₂$ sequestration with enhanced coalbed methane $(CO₂-ECBM)$ recovery, especially in South Sumatera Basin.

The issue related to the environment impact due to discharging $CO₂$ has been increasing recently. As a result, many are looking to storage $CO₂$ as an approach to reduce the carbon impact of stationary point sources of $CO₂$ (Hasaneen et al. 2014). Sequestration of $CO₂$ into coal seams is beneficial to mitigate greenhouse gas emissions and enhanced coalbed methane recovery. For the purpose of $CO₂$ emission reduction, $CO₂$ has to be stored in the coal permanently, the coal seams should be unmineable forever for storing $CO₂$, otherwise, coal mining, combustion, or gasification would release $CO₂$ stored in the coal (Li and Fang [2014\)](#page-6-0). Corum et al. ([2013](#page-6-0)) mentioned that unmineable coal seams have the potential to store large volume of $CO₂$. Coal that is considered unmineable because of geologic, technological, and economic factors (typically too deep, too thin, or lacking the internal continuity to be economically mined with today's technologies) may have potential for $CO₂$ storage (U.S. DOE [2012](#page-6-0)).

At present, $CO₂$ sequestration for the ECBM recovery has been studied to minimize the $CO₂$ release into the atmosphere, and these projects have been operating all over the world. Referring to the injection methodology, several methods have been introduced and applied in order to inject $CO₂$ into coal seams, such as the Fenn-Big Valley project in Canada, with two wells using a 'huff and puff' scheme (Gunter et al. [2004](#page-6-0)), Yubari project in Japan, with a vertical injection well and a producing well (Fujioka et al. 2008), APP CO₂-ECBM project in China, CO₂ was injected through multi-lateral horizontal well into coal seams (Pan [2012\)](#page-6-0). From technical or reservoir engineering aspect, permeability is a determining factor in the viability of a CO2 storage in coal seams (Bachu et al. [2007\)](#page-6-0). Permeability is a dynamic reservoir parameter which influences fluid flow in the porous medium. The gas rate (Q_g) is mainly affected by permeability following Darcy's law. As stated by Li and Fang (2014) (2014) , successful injection of $CO₂$ into coal seams requires sufficient permeability along pores and fractures, but it has not been defined yet. Type and criteria of permeability which have large impact on the $CO₂ - ECBM$ performance should be understood due to the coalbed methane reservoir has dual permeability system,

which are matrix and fracture permeability. The key criteria of reservoir characteristics are then extremely important for successful application of $CO₂$ -ECBM technique and it should be defined clearly.

Although the ECBM recovery process is one of the potential CBM production enhancement techniques, the effectiveness of the process is greatly dependent on the coal seam characteristics. The estimation of $CO₂$ storage capacity is highly important for further consideration in optimization of $CO₂$ sequestration. This study has therefore aimed to propose the identification of coal seams suitability for $CO₂-ECBM$ in terms of the technical criteria with a case study in South Sumatera Basin, Indonesia. To achieve the objectives, a novel three-dimensional (3D) numerical model was developed based on the characteristics of coal seams in South Sumatera Basin. Using numerical simulation, this paper presents the investigation of permeability effects on the performance of $CO₂$ -ECBM and proposes a simplified method for estimating $CO₂$ storage capacity in coal seams. From this study, one can screen the ideal candidates for $CO₂$ sequestration with enhanced coalbed methane recovery and can quickly quantify the $CO₂$ storage capacity in the coal seams without performing numerical simulation.

Methods

Numerical reservoir simulation is the preferred tool to be applied in this study due to the CBM flow problem that depends on many pressure-dependent parameters which can affect the fluid behaviour and the reservoir performance (Giamminonni et al. [2010\)](#page-6-0). Implementation of numerical simulation has successfully applied for $CO₂$ storage in saline aquifers in a field-scale study (Yang et al. [2012](#page-6-0)). A compositional numerical simulation was used to model the coalbed methane reservoir using Generalized Equation of State Model-Computer Modelling Group (GEM-CMG) compositional simulator. The simulator provides extended Langmuir isotherms to model the preferential adsorption of $CO₂$ and accurate early time water and methane production predictions. Modelling was developed by combining all of the supporting data in terms of geology and reservoir, and then the next step is to conduct the initialization process to validate the reservoir model. The Gas in Place (GIP) resulted from the model was compared with volumetric computational method, and initial reservoir pressure from the model was compared with actual pressure data. The reservoir pressure was derived from hydrostatic pressure calculation as a function of coal seam depth. The standard volumetric computation for estimating Original Gas in Place or OGIP (Stevens and Hadiyanto [2004](#page-6-0)) is shown below:

$$
OGIP = \begin{cases} \text{Coal thickness, } m \times (1 - \text{ash content, frac}) \times (1 - \text{moisture content, frac}) \times \\ \text{coal density, } kg/m^3 \times (1 - CO_2 \text{content, frac}) \times CH_4 \text{content, } m^3/kg \times \text{Propective area, } m^2 \end{cases}
$$
(1)

Having obtained the valid model, a vertical well was then designed and modelled to produce coalbed methane with the primary recovery. Afterwards, a vertical $CO₂$ injector well was designed and modelled to inject $CO₂$ for the ECBM recovery. A comparison of primary CBM production and ECBM methods was analysed by performing production forecasting for 30 year. A sensitivity study was then conducted in order to examine the performance of ECBM in terms of methane $(CH₄)$ production recovery and $CO₂$ storage under the influences of reservoir permeability (k) which are fracture and matrix permeability. Having performed the sensitivity analysis, the reservoir criteria for successful application of $CO₂$ -ECBM in a vertical well was then proposed and defined. With regard to $CO₂$ storage capacity in coal seams, it was predicted using the proposed equation and validated with the novel numerical model through sensitivity studies.

A cartesian grid with $21 \times 21 \times 3$ (1323 grid) model which covers 1.1025 km^2 of unmineable coal seams lying ± 760 m below the ground surface with total thickness of 25 m was considered for the model development. The model parameters used in this study were based on the coal seams characteristics in South Sumatera Basin, Indonesia (Stevens and Hadiyanto [2004\)](#page-6-0). Storage and compositional properties (Sosrowidjojo [2013\)](#page-6-0) and gas composition (Mazumder et al. [2010](#page-6-0)) from CBM wells in South Sumatera Basin were also considered during model construction. The novel model constructed has coal seams laterally continuous (Bowe and Moore [2015\)](#page-6-0), and the geological structure is simple (CBMA [2013\)](#page-6-0), and there is no fault neither fold in the model. The reservoir properties used for construction of base case model are given in Table 1. The reservoir has $100\% \text{ CH}_4$ saturation in the coal matrix while cleat or fracture porosity is saturated by 100% water. The reservoir was assumed homogenous where the permeability values are same in any direction (i, j, k) which of four (4) mD whether for matrix or fracture permeability. The reservoir was assumed as finite without driving mechanism from outside or only natural depletion drive was considered as the reservoir drive mechanism, and there was no skin found in the wellbore. Figure 1 shows the coal seams model constructed for the simulation study.

Having constructed a novel 3D numerical model, the model was then validated by initializing the results of Gas in Place with volumetric computation method and initial reservoir pressure from model with actual pressure data. The GIP resulted from model of about 224.15 MMm³ while GIP from volumetric computation was estimated of about 205.09 MMm³, it resulted in differences of about 9.22%. Initial reservoir pressure at reference depth of 760 m resulted from the model of about 7576.2 kPa, with the differences of about 1.65% from actual pressure data (7453.05 kPa at 760 m). According to these results, the differences of both parameters below 10% are considered

Table 1 Reservoir parameters used for construction of CBM reservoir model

Reservoir parameters	Dimension	Value
Surface area	m ²	1,102,500
Coal thickness	m	25
Rock density	kg/m ³	1459.27
Gas saturation	Fraction	0 (100% CH ₄)
Water saturation	Fraction	1
Rock compressibility	1/kPa	2×10^{-5}
Matrix porosity	Fraction	0.02
Fracture porosity	Fraction	0.005
Matrix permeability (i, j, k)	mD	4
Fracture permeability (i, j, k)	mD	4
Reservoir temperature	$^{\circ}C$	68
Datum depth	m	760
Initial pressure @datum	kPa	7453.05
Langmuir pressure	kPa	3500
Langmuir volume	m^3/t	7

Fig. 1 CBM model constructed for simulation study

good match and acceptable in reservoir engineering practice. It can be inferred that the developed CBM reservoir model is valid, and it is then applicable to perform reservoir simulation study.

Primary methane production recovery from the coal seams was examined using a vertical well which was perforated in all of coal layers during 30 year of simulation. In primary recovery, CBM was produced by natural flow or known as depletion method. The $CH₄$ production performance from primary production was then analysed and compared to the $CO₂$ -ECBM technique. For $CO₂$ -ECBM purposes, a vertical CO2 injector well was modelled with the well-spacing between CBM producer and $CO₂$ injector of about 200 m. The $CO₂ - ECBM$ technique was examined by injecting $CO₂$ into the coal seams at the maximum of 10,000 kPa injection pressure and injection rate of 10,000 m^3 /d. Source of CO₂ was considered comes from Merbau Gas Gathering Station (GGS) based on LEMIGAS study (2015) (2015) . The CO₂ sources from the Merbau GGS contain high-purity $CO₂$ content where $CO₂$ absorber unit discharges about 363 t/d CO₂.

Results and discussion

Comparison of primary CBM and ECBM recovery

According to the production simulation results from 2016 until 2046 (Fig. 2), total cumulative $CH₄$ production with primary CBM production is about $36,882.3$ t CH₄. With the simulation results of $CO₂$ -ECBM, the model forecast showed total cumulative CH_4 production with the vertical well injector of 41,373.4 t. From the results, application of $CO₂$ sequestration in a vertical well for ECBM can obtain additional recovery factor of about 1.12 times the primary recovery method (base case). With regard to the pressure depletion, the decrease of reservoir pressure with $CO₂$ -

Fig. 2 Comparison of production performance of depletion and $CO₂$ -ECBM recovery

ECBM (magenta line) is not significant as the decrease of reservoir pressure with primary recovery method (green line). It shows that injecting $CO₂$ into coal seam(s) help in maintaining CBM reservoir pressure. The $CO₂$ which is injected into coal seam(s) will be adsorbed in the coal matrix. The process of adsorption causes the $CO₂$ to bond to the coal causing the $CO₂$ to be physically and permanently trapped on the coal provided sufficient pressure is maintained. Subsequently, $CH₄$ is replaced by injected $CO₂$ and desorbed from coal matrix and it is then flow through the matrix into natural fracture network.

The $CO₂$ storage mechanism considered in this study is adsorption trapping. In the adsorption trapping mechanism, the accumulation of injected $CO₂$ is absorbed on the surface of coal matrix. The capacity of this mechanism is mostly depend on Langmuir isotherm (Jasinge and Ranjith [2011\)](#page-6-0). From the simulation results, the model resulted in the $CO₂$ storage capacity of about 384,579.07 t. With the base case $CO₂$ -ECBM, total of CO_2 injected is 204,814 t while CO_2 that can be stored of about 124,930.5 t. The $CO₂$ storage efficiency of coal seams was calculated by comparing the $CO₂$ stored from $CO₂$ -ECBM and the total of storage capacity. From the result obtained, the $CO₂$ storage efficiency of 32.5%. For the optimization purposes, this number can be increased by optimizing the $CO₂$ injection operation parameters, e.g. increasing $CO₂$ injection rate/amount introduced into the coalbed methane reservoir, and using horizontal well as the $CO₂$ injectivity enhancing technology (Ridha et al. [2017\)](#page-6-0). These are also beneficial to maintain reservoir pressure and increase methane production.

Sensitivity analysis

Having performed $CO₂$ -ECBM technique, a sensitivity analysis was carried out to examine the influences of reservoir permeability on the novel numerical model in

Fig. 3 Permeability versus additional $CH₄$ production: blue line indicates that CH_4 recovery due to CO_2 sequestration increases proportionally with increments in fracture permeability and vice versa, there is no effect of matrix permeability (*orange line*) on $CO₂$ -ECBM

order to assess the performance of $CO₂-ECBM$. The recovery factor obtained from the model was examined under the influences of fracture and matrix permeability. Figure [3](#page-3-0) shows the influences of reservoir permeability on additional CH₄ production from CO₂-ECBM. From the results, it can be seen that fracture permeability $(k_{fracture})$ has a significant impact on the performance of $CO₂$ -ECBM, and vice versa, there is no effect of matrix permeability (k_{matrix}) on CH₄ production recovery due to CO₂ sequestration. This is caused by gas flow or migration in the coal matrix due to diffusion or differences of the gas molecular concentration (Thimons and Kissell [1973\)](#page-6-0), CH4 will diffuse from matrix surface to cleats/micro-pores (desorbed from coal matrix), while injected $CO₂$ is replacing CH4 and adsorbed in coal matrix. With regard to the fluid flow concept in the porous medium, gas flow in the cleats and natural fractures to the wellbore by Darcy's flow, where the gas rate as a function of fracture permeability. Due to this concept, recovery factor obtained from $CO₂$ -ECBM increases proportionally with an increase in fracture permeability. In regard to $CO₂$ storage capacity, increase of fracture permeability from 2 to 20 mD leads to increase of $CO₂$ storage efficiency from 32.1 to 38.2% (Fig. 4). Even though fracture permeability at 1 mD resulted in storage efficiency of 38%, there is no effect of $CO₂$ sequestration in increasing $CH₄$ production at this point.

Based on the results of model development and sensitivity studies, the technical criteria of coal seam(s) suitable for $CO₂$ sequestration with enhanced coalbed methane recovery were then proposed. The key criteria are likely to be:

Homogeneous reservoir: The coal seam(s) reservoir should be laterally continuous in terms of the reservoir homogeneity. This ensures the lateral sweep efficiency of injectant through the reservoir and the volume of $CO₂$ stored in coal seams will be also optimum.

Simple structure: The geological structure of the reservoir should be simple in terms of minimally faulted and folded. The faults may divert injectant away from the

reservoir, reducing the efficiency of sequestration and enhanced recovery. Structurally complex areas frequently have damaged coal properties in particularly fracture permeability become lower.

Fracture permeability: The coal seam reservoir(s) should have fracture permeability more than 2 mD. The injection flow rate through the porous medium is proportional to the fracture permeability. The greater the fracture permeability, the deeper invading $CO₂$ reaches; it will result in high efficiency of $CO₂$ sequestration and enhanced coalbed methane recovery.

Suitability of coal seams in South Sumatera Basin for $CO₂$ sequestration with ECBM recovery

In the South Sumatera Basin, there are two main coal formations; these are the Oligocene Talang Akar and the Miocene Muara Enim formations. Based on a preliminary study by Kurnely et al. ([2003\)](#page-6-0), Muara Enim Formation (MEF) is the best coal to be developed in South Sumatera Basin due to the CBM field located in onshore, the infrastructure have been settled, and the markets are in there. Muara Enim coals have potential gas contents of around 7 m³/t, and CBM targets have low $CO₂$ which of less than 5% (Stevens and Hadiyanto [2004](#page-6-0)). Muara Enim coals have also good coal thickness and favourable depth for CBM production (Muksin et al. [2012\)](#page-6-0). With the coal seams are laterally continuous over tens of kilometres (Bowe and Moore [2015](#page-6-0)), few faults and flat dips (CBMA [2013](#page-6-0)), and permeability less than 10 mD (Sosrowidjojo [2013](#page-6-0)), these make coal seams in the South Sumatera Basin in generally, Muara Enim formation in particularly, suitable for the application of $CO₂$ sequestration with enhanced coalbed methane recovery. With the base case simulation scenario, coal seams in the South Sumatera Basin have good potential for $CO₂$ sequestration with storage efficiency up to 36.5% (Fig. 4). With regard to the ECBM recovery, the model resulted in additional $CH₄$ production recovery up to 1.226 times the primary recovery method (Fig. [3\)](#page-3-0). These number can be increased by performing an optimization on the injecting parameters of the $CO₂$ injection, e.g. $CO₂$ injection rate and well-spacing optimizations.

Prediction of CO₂ sequestration capacity

Carbon dioxide can be stored in coal by sorption and diffusion. In unmineable coal seams, adsorption trapping is the main sequestration method. Two assumptions have been made in order to simplify the calculation based on the volumetric Original Gas In Place (OGIP) method; there is no water saturation in the coal matrix and no gas saturation Fig. 4 Fracture permeability sensitivity on CO₂ storage in the coal fracture (S_w matrix = 0 and S_g fracture = 0),

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Table 2 Parameter used in sensitivity analysis	Reservoir parameters	Low case	Base case	High case
	Prospective area (A) , m ²	640,000	1,102,500	1,690,000
	Coal seams thickness (h) , m	12.5	25	37
	Coal density $(\rho_{\rm b})$, kg/m ³	1300	1459.27	1500
	Gas sorption capacity (GSC), m^3/t	2.5		-

Fig. 5 Tornado plot indicating the influences of different reservoir parameters on $CO₂$ storage capacity resulted from the simplified OGIP computation (proposed equation)

Fig. 6 Tornado plot indicating the influences of different reservoir parameters on $CO₂$ storage capacity resulted from numerical simulation

and adsorption trapping is the main sequestration method in coal seams, which was considered as the only storage mechanism in this study. By simplifying the OGIP volumetric calculation, the $CO₂$ storage capacity in the coal seams can be calculated as:

CO₂ storage capacity = $\rho_{CO_2} \times A \times h \times \rho_b \times G_{CS}$, (2)

where $\rho_{\text{CO2}} = 1.873 \text{ kg/m}^3$, $A = 1102,500 \text{ m}^2$, $h = 25 \text{ m}$, $\rho_{\rm b} = 1459.27 \text{ kg/m}^3$, $G_{\rm CS} = 7 \text{ m}^3$ /t, CO₂ storage capacity = 413.9 \times 10³ t. The CO₂ storage capacity resulted from the proposed equation was then compared with the novel numerical model through sensitivity analysis. It is important to perform a parametric study to address the uncertainty of the parameters input to the $CO₂$ storage capacity and improves the results of prediction. The 'High', 'Low' and 'Base' cases were designed for the value of each uncertain parameter, which were quantified through the sensitivity analysis. The values assigned in each case are summarized in Table 2.

The results of $CO₂$ storage capacity for each methods and sensitivity studies are presented in the tornado plot in

order to show the comparison of the sensitivities of each parameter. Figures 5 and 6 show $CO₂$ storage capacity resulted from the simplified OGIP computation and numerical simulation. The error obtained for each case was calculated. The average error obtained for 'High' case of 7.53%, 'Low' case of 7.68% and 'Base' case of 7.62%. In average, the total error resulted in about 7.61%. From these results, the error resulted from the simplified OGIP computation or proposed method is not too significant or less than 10%, which is considered good matches and it can be used and applicable to estimate the $CO₂$ storage capacity in the coal seams. From the results of tornado plot, gas sorption capacity, coal thickness and prospective area prove to be the parameter with large impact on $CO₂$ storage capacity. It is therefore required that parameter be precisely estimated to improve accuracy of the prediction.

Conclusion

Based on the results of model development and sensitivity studies, the technical criteria of coal seams suitable for $CO₂$ sequestration with enhanced coalbed methane recovery $(CO₂-ECBM)$ have been fully defined. The proposed key criteria are likely to be homogeneous reservoir, simple structure (minimally faulted and folded), and fracture permeability should be more than 2 mD. Based on these criteria, coal seams located in South Sumatera Basin, especially in Muara Enim formation (MEF), are suitable for the application of this clean coal technology, which can storage $CO₂$ in the coal seams and help in increasing the CH_4 production recovery. The method for estimating $CO₂$ storage capacity in coal seams has been successfully proposed by simplifying the Original Gas in Place (OGIP) volumetric computation. The proposed equation is applicable for 100% gas saturation in coal matrix and adsorption process as the main and the only storage mechanism in coal seams. From this study, one can screen the suitable coal seams for $CO₂$ storage with enhanced coalbed methane recovery purposes and can quickly quantify the $CO₂$ storage capacity in coal seams without performing numerical simulation.

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