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Experimental study on multiple propagation characteristics of stress wave and surface displacement behavior in coal based on SHPB and DIC

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Abstract

Understanding the damage evolution behavior of coal under stress wave can provide a theoretical basis for preventing rock burst. In this work, the impact experiments of coal samples were carried out by split Hopkinson pressure bar (SHPB); the stress wave propagation characteristics were recorded by dynamic strain acquisition instrument; the evolution behaviors of coal samples' surface displacement were analyzed by digital image correlation (DIC); the correlation between stress wave and displacement were discussed based on the multi-fractal theory. The results proved the stress wave propagates in the non-linear attenuation mode of multiple incidences, refection, and transmission. Among them, the attenuation velocity of the incident wave is the largest, followed by the refected wave, and the transmitted wave is the smallest. The incident and refected stress waves are mainly dominated by high amplitude signals, while the transmitted stress waves are mainly dominated by low amplitude signals. The horizontal displacement on the coal sample surface is changed in the form of variable velocity, acceleration, and direction during the process of the stress wave propagation. The impact velocity is favorably linked with the amplitudes and attenuation velocities of incident, refected, and transmitted waves as well as the surface displacement, displacement velocity, and acceleration of coal samples. The multi-fractal characteristic parameters of stress wave and displacement show that the proportional relationship and diference between the large- and small-scale displacement are infuenced by those between the high- and low-intensity signal of the stress wave, and the transmission wave can exert greater infuence.

Keywords SHPB · DIC · Stress wave · Displacement · Multi-fractal characteristics

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Introduction

Rock burst, as a destructive mine earthquake induced by mining activities, seriously threatens the safe production of mines with its sudden, sharp, and violent damage characteristics, and has caused huge economic losses and casualties to coal mines in China (Wang et al. [2019](#page-22-0); Vardar et al. [2022](#page-22-1); Yang et al [2022\)](#page-22-2). The occurrence of rock burst can not only cause roadway damage and casualties, but also induce coal and gas outburst, gas explosion, roof accident, and other major underground malignant accidents (Zhao et al. [2018](#page-22-3); Mondal and Roy [2019](#page-22-4); Zhang et al. [2021](#page-22-5); Liu et al. [2022b,](#page-21-0) [2023](#page-21-1); Li et al. [2023](#page-21-2); Yang et al. [2023](#page-22-6)). It seriously afects the safe and efficient mining of coal mines.

Numerous feld studies have proved that the occurrence of rock burst can be signifcantly afected by various disturbance factors in coal mining (Gu et al. [2023](#page-20-0); Tian et al. [2023](#page-22-7)), such as hard thick roof fracture (Wang et al. [2015\)](#page-22-8), coal fracture in stress concentration area (Zhou et al. [2011](#page-22-9)), thrust fault slip

(Wang et al. [2017;](#page-22-10) Yang et al. [2019](#page-22-11); Wang and Luan [2022](#page-22-12)), engineering blasting (Wu et al. [2019\)](#page-22-13), and mining disturbance (Zhou et al. [2022\)](#page-22-14). As a result, dynamic load would be generated and then propagate in the form of stress waves in coal and rock strata (Feng et al. [2016](#page-20-1)). When the stress wave propagates in the coal and rock stratum, it will refract, refect and scatter, leading to a strong stress concentration around the free surface. When the dynamic stress is greater than the strength of the coal, the coal will be damaged, which will induce the rock burst (Feng et al. [2020b](#page-20-2); Tan et al. [2021](#page-22-15)). So, it is necessary to study the propagation characteristics of stress waves and the damage evolution behavior of coal and rock under dynamic loading.

Hopkinson pressure bar is an important instrument for studying the dynamic behavior of coal and rock in the laboratory (Kai-Xin and Xu-Dong [2006](#page-21-3); Li et al. [2008](#page-21-4)). Many scholars have used this equipment to study the propagation characteristics of stress waves and the mechanical behavior of coal and rock under dynamic loads. These studies mainly focus on the propagation and attenuation laws of stress waves (Ju et al. [2007;](#page-21-5) Xia et al. [2008](#page-22-16); Han et al. [2022](#page-20-3)), the transfer model of stress waves (Li and Ma [2010](#page-21-6); Ma et al. [2011](#page-22-17)), the infuence of joint characteristics on transmission and reflection coefficients (Li et al. [2011a,](#page-21-7) [b](#page-21-8); Wu et al. [2014](#page-22-18); Chai et al. [2016](#page-20-4); Li et al. [2017b,](#page-21-9) [2019b\)](#page-21-10), the relationship between the transmissive and refective characteristics of stress waves and external load forms (Li et al. [2019a;](#page-21-11) Kong et al. [2021a,](#page-21-12) [2022](#page-21-13)), the strength of coal and rock (Huang et al. [2010;](#page-21-14) Li et al. [2016\)](#page-21-15), the deformation of coal and rock (Tan et al. [2018](#page-22-19)), the energy evolution laws (Hong et al. [2009;](#page-20-5) Liu et al. [2015](#page-21-16)), the propagation forms of surface cracks in coal and rock (Chen et al. [2009;](#page-20-6) Dai et al. [2010](#page-20-7)), the dynamic constitutive model and equation of coal and rock (Ma et al. [2017;](#page-22-20) Kong et al. [2021b](#page-21-17); Hou et al. [2023](#page-20-8)), and the fracture morphology (Zhang and Zhao. [2013](#page-22-21); Li et al. [2021c](#page-21-18)). The results show that the stress waves propagate in coal and rock in the form of incidence, refection, and transmission (Li et al. [2008](#page-21-4)). For a constant impact velocity, the amplitude of the refected wave increases as the porosity of the sample increases, while the amplitude of the transmitted wave decreases (Ju et al. [2007](#page-21-5)). However, with the surface roughness of the sample joint increases, the transmitted wave amplitude gradually decreases, while the refected wave amplitude gradually increases (Li et al. [2011a,](#page-21-7) [2017b,](#page-21-9) [2019b](#page-21-10)). The existence of static stress in rock has a signifcant impact on the stress waveform. When the static stress is constant, the stress waveform at diferent locations is approximately the same, while when the static stress changes, the stress waveform at the same location changes greatly (Cheng et al. [2019](#page-20-9)). In addition, the attenuation of incident, refected, and transmitted waves is closely related to impact velocity, axial pressure, and confning pressure (Kong et al. [2020](#page-21-19)). When the dynamic load is constant, with the increase of axial pressure and confning pressure, the strength of coal and rock frst increases and then decreases (Liu et al. [2019;](#page-21-20) Hao et al. [2020](#page-20-10)). Under the same axial pressure and surrounding rock conditions, with the increase of impact velocity, the strength of coal and rock materials increases within a certain range (Yao et al. [2019\)](#page-22-22). The dynamic tensile strength of coal and rock is smaller than its dynamic compressive strength (Zhao et al. [2016](#page-22-23); Ai et al. [2019](#page-20-11)). Diferent anisotropy of coal and rock leads to diferent dynamic tensile strength of coal and rock (Zhao et al. [2014;](#page-22-24) Wang et al. [2017](#page-22-10)). With the increase of bedding angle, the dynamic tensile strength of coal and rock frst decreases and then increases (Zhao et al. [2017](#page-22-25)). During the dynamic failure process of coal and rock, the incident energy is mainly consumed by refected energy and transmitted energy, while less incident energy is consumed in the form of absorbed energy (Yan et al. [2021\)](#page-22-26). The axial fracture of coal is directly caused by the incident compressive stress wave, while the lateral fracture is caused by the tensile stress wave refected from the interface between the coal sample and the transmission rod (Feng et al. [2020a](#page-20-12)). The initiation of surface cracks in the sample occurs in the direction of the incident wave, and the propagation rate of the cracks along the X–Y direction increases with the increase of impact velocity (Ai et al. [2019,](#page-20-11) [2020](#page-20-13)). The strain in the horizontal direction of the sample is significantly greater than the strain in the vertical direction (Ai et al.[2019,](#page-20-11) [2020](#page-20-13)). The failure mode of rock materials under dynamic load is mainly transgranular fracture, supplemented by intergranular fracture (Li et al. [2021b](#page-21-21)).

With the development of computer technology and image processing technology, the combination of high-speed camera and digital correlation technology has become an important auxiliary means to study the fracture characteristics of the samples under dynamic load. Digital image correlation (DIC) is a non-contact, optical, non-destructive, and full feld method, which can track the deformation and strain of the sample surface (Gao et al. [2015;](#page-20-14) Xing et al. [2020;](#page-22-27) Li et al. [2022b](#page-21-22)). Many scholars have studied the failure process of the material under the dynamic load by the DIC measurement technology, which drawn many valuable conclusions. Among them, Zhou et al. [\(2018\)](#page-22-28) used the modifed SHPB experimental system to carry out dynamic compression and shear load tests on granite, analyzed the evolution law of surface strain feld by using DIC measurement technology, and proved the feasibility and accuracy of using DIC measurement technology to characterize the damage evolution behavior of materials. Li et al. ([2020a\)](#page-21-23) carried out dynamic load experiments on granite with holes and obtained the evolution law of the maximum principal strain and local strain of the granite surface in the whole feld using the DIC measuring system. Yan et al. [\(2021](#page-22-26)) used an improved SHPB system combined with DIC testing technology to test multi-fracture rock samples under static and dynamic coupling compression, obtained the evolution law of the surface displacement feld of rock samples, and proposed a new crack classifcation direction based on the displacement trend line method. Yue et al. ([2022](#page-22-29)) studied the dynamic fracture behavior of rock samples with sharp V-shaped notches using the digital image correlation (DIC) method. The displacement feld of the sample surface was obtained, and the stress intensity factor, dynamic stress intensity factor at the crack tip, and crack growth rate were got from the displacement.

However, the above scholars' research on the mechanical behavior of samples subjected to stress waves remains within the frst wave propagation, ignoring the impact of multiple propagation of stress waves on the mechanical behavior of specimens. In fact, after the completion of the frst stress wave propagation, the stress wave does not immediately disappear, but attenuates in the form of multiple incidence, refection, and transmission, still causing sustained damage to the sample. Under a fxed impact load, the sample may be damaged by multiple actions of stress waves. If the sample is not be broken during the frst wave propagation process, it may be broken during the subsequent stress wave propagation process (Lu et al. [2017](#page-21-24)). Compared to the frst wave, the crack propagation degree of the sample under the subse-quent stress wave is greater (Hao et al. [2020\)](#page-20-10), and the splash degree of the fragments is also stronger (Lai et al. [2022](#page-21-25)). Therefore, it is of great signifcance to study the attenuation behavior of stress waves and their impact on the specimen after the propagation of the frst wave.

Due to the stress waves propagate and attenuate in the form of multiple incidence, refection, and transmission, their time series signal evolution behavior is relatively complex. The surface displacement of coal sample varies continuously with the multiple incidence, refection, and transmission of stress waves. The velocity and acceleration of displacement are non-linear and complex. If a mathematical method can be used to simply and comprehensively describe the changing laws of stress wave and displacement, as well as the relationship between them, the evolution behavior of stress wave propagation and displacement can be more intuitively understood. As a classical method of data statistics, multi-fractal theory can extract targeted research elements from complex and variable information and can concisely and comprehensively refect the essential characteristics of complex time series (Lyubushin et al. [2013,](#page-21-26) [2014\)](#page-21-27). Many scholars used the multi-fractal theory to obtain the response signals in the process of coal and rock failure: potential signals (Niu et al. [2022](#page-22-30)), acoustic emission signals (Liu et al. [2022a\)](#page-21-28), and electromagnetic radiation signals (Li et al. [2022a\)](#page-21-29). The multi-fractal characteristic parameters are used to characterize the damage degree and failure types of coal and rock. Therefore, if the stress wave signal and the surface displacement have the characteristics of multi-fractal, the corresponding multi-fractal parameters can be used to characterize the multiple propagation behaviors of the stress wave, the displacement evolution laws, and the correlation between them.

In this paper, the impact tests of coal samples were carried out by the split Hopkinson pressure bar (SHPB). The super dynamic strain acquisition instrument of the SHPB experimental system was used to collect the voltage signals throughout the stress wave attenuation and summarize the multiple propagation laws. A digital image correlation (DIC) measurement system was used to analyze the changes in horizontal displacement, displacement velocity, and displacement acceleration of coal surface points during the stress wave multiple propagations. The multi-fractal theory guided the analysis of distribution laws of high and low amplitude signals in the stress waves and the variation characteristics of large-scale and small-scale displacement of coal sample surface points. Finally, the correlation was analyzed using their multi-fractal characteristics. The study can provide theoretical support for monitoring, early warning, and preventing the rock burst.

Experiment and processes

Experimental samples

The coal samples used in this experiment were taken from the Jining coal mine in Shandong, China. According to the experimental requirements, the specimens were made into $70 \text{ mm} \times 70 \text{ mm}$ square samples after drilling, cutting, and polishing. The end face of the sample was perpendicular to the axis, with a maximum deviation of no more than 0.25°, and the parallelism of both ends was controlled to \pm 0.02 mm. The basic physical and mechanical characteristic parameters of coal samples used in this experiment are shown in the Table [1.](#page-3-0)

After processing the coal sample, it is necessary to make speckles on the surface of the coal sample. The sample surface is sprayed with white paint with a thickness of 1 mm as the background color. After the white paint on the surface of the coal sample is dry, the sample surface is randomly sprayed with black scattered spots of diferent sizes by black paint.

Experimental instruments

The equipment used in this experiment is the SHPB experimental system (Fig. [1](#page-3-1)), which is composed of an incident rod, a transmission rod, an energy absorber, an axial compression loading system, a bullet launching system, a laser velocimeter, a dynamic strain acquisition instrument, a high-speed image acquisition system, four strain gauges, two Wheatstone bridges, and the connectors. Among

Table 1 Basic parameters of coal samples

Number	Density (g) cm^3)	P wave velocity(m/s)	Elastic modulus (GPa)	Poisson's ratio
1	1.33	1452	1.90	0.28
2	1.33	1425	1.89	0.28
3	1.32	1410	1.89	0.30
4	1.34	1472	1.91	0.29
5	1.34	1486	1.90	0.30
6	1.32	1494	1.91	0.29
7	1.33	1506	1.90	0.30
8	1.34	1478	1.88	0.30
9	1.32	1448	1.91	0.29
10	1.34	1436	1.88	0.28
11	1.33	1446	1.89	0.28
12	1.33	1428	1.88	0.28

them, both the incident rod and the transmission rod are high-strength steel with a diameter of 100 mm, and their lengths are 5000 mm and 3000 mm, respectively. The elastic modulus was 210 GPa, and the longitudinal wave velocity was 5100 m/s. The overall view of the SHPB experimental system is shown in Fig. [1k](#page-3-1), and the detailed views of each subsystem are shown in Fig. [1](#page-3-1)a to i. The strain gauges were attached at the distance of 2000 mm from the incident rod/transmission rod (near the side of the coal sample), and they were connected to the connector through a Wheatstone bridge. The connector and the dynamic strain gauge were connected through wires. The high-speed camera system consists of a high-speed camera and two lighting fxtures. Among them, the high-speed camera is connected to the control system through wires. The axial pressure loading system consists of an axial pressure loading device and an oil pump.

The DIC test system consists of a high-speed system and Match ID-2D software, among which the high-speed camera used in this experiment is Phantom VEO710L. The minimum time interval between two exposures is 300 ns, and the sensitivity (ISO) is 32,000. The camera has a maximum shooting frequency of 1,000,000 fps/s and a maximum resolution of 1280×800 . The shooting frequency in this experiment is 200,000 fps/s. That is, take a picture every 5 microseconds. The resolution at this shooting frequency (200,000 fps/s) is 128×128 . The Match ID software can calculate the global and local displacement, displacement velocity, displacement acceleration, strain, and other parameters of the sample surface. The boundary compensation function in the software can ensure that the surface boundary of the sample is also effectively calculated. The performance analysis (PA) module in the software can realize the quantifable DIC calculation results according to the optimization of the parameter settings, and the signal can be de-noised by setting the parameters such as subset, step size, strain fltering window, shape function, and interpolation algorithm.

Experimental process

The impact compression experiments with impact speeds of 1 m/s, 1.5 m/s, 2 m/s, and 2.5 m/s were carried out by the SHPB testing system. The data acquisition system, dynamic strain gauge, and strain gauge were used to collect the voltage signal of the stress wave attenuation process of the coal

Fig. 1 Experimental system

sample under the dynamic load. During the experiment, the strain gauge attached to the incident rod recorded the incident wave and refected wave signals, while the strain gauge attached to the transmission rod recorded the transmission wave. The surface changes of coal samples were photographed by a high-speed camera, whose pictures were analyzed by Match ID-2D software in the DIC test system. First, start the axial loading device in the SHPB system, and the axial pressure of 1 MPa was used to fx the coal sample between the incident rod and the transmission rod; second, the air compressor in the SHPB experimental system was used to inject air pressure into the air chamber in the bullet triggering system in the SHPB; third, unlock the laser velocimeter, the dynamic strain acquisition instrument, and the data acquisition system; fourth, start the pre-trigger system in the SHPB system to check whether the laser velocimeter and high-speed camera worked normally; and fnally, start the synchronous trigger system in SHPB system for experiment. Each experiment was conducted three times to avoid experimental errors. The relevant data of the experiment were sorted out for further analysis and discussion.

Experimental results and discussions

The propagation characteristics of stress waves

The propagation process of the dynamic load stress wave is shown in the Fig. [2](#page-4-0).

According to the principle of SHPB experimental system, the incident wave is recorded by the strain gauge attached to the incident rod before it propagates to the A_1 end of the coal sample. When the incident wave propagates to the A_1 end of the coal sample, it will generate refection and transmission to form refection and transmission waves. The refected wave propagates in the opposite direction to the incident wave and is recorded by the strain gauge attached to the incident rod. Because the amplitude of the incident wave in this experimental system is negative, the amplitude of the refected wave is positive. The transmitted wave passes through the A_2 end of the coal sample and is recorded by the strain gauge attached to the transmission rod. At this experiment, the propagation direction of the transmitted wave is the same as the incident wave, but opposite to the refected wave. Therefore, the amplitude of the transmitted wave is negative. When it propagates to the end of the transmission rod, the propagation direction of the transmission wave is reversed and recorded again by the strain gauge attached to the transmission rod. This time, the transmission wave was frst recorded by the strain gauge attached to the transmission rod and then propagated to the A_2 end of the coal sample. So, the amplitude of the transmitted wave at this time is positive. Because positive transmission waves are generated by reversing the propagation direction of negative transmission waves, the positive transmission wave experiences a longer path and consumes more energy. Therefore, the absolute value of the amplitude of the positive transmission wave is smaller than that of the negative transmission wave. The stress waves propagate through coal in the form of multiple incidence, refection, and transmission until they are depleted.

The propagation characteristics of the incident and refected wave

Figure [3](#page-5-0) shows the attenuation characteristics of the incident wave and refected wave.

As shown in Fig. [3](#page-5-0), the attenuation process of the incident wave and refected wave is all non-linear. The amplitude of the end wave of the incident (refected) is about 18 to 21% of its frst wave. At diferent impact velocities, the attenuation modes of the incident and refected waves are almost the same, but there are signifcant diferences in amplitude. With the impact velocity increases, both the amplitude of the frst and the end of the incident and refected waves increase. When the impact velocity is 1 m/s, the amplitude of the first wave (end wave) of the incident wave and the refected wave is−0.112 V (−0.022 V) and 0.106 V (0.020 V), respectively. When the impact velocity increases to 2.5 m/s, the amplitude of the frst wave (the end wave) of the incident

Fig. 3 The attenuation process of incident and refected waves (**a**: 1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s)

wave and the reflected wave is -0.261 V (-0.052 V) and 0.242 V (0.043 V).

The propagation characteristics of the transmitted wave

The attenuation characteristics of the transmitted wave are shown in Fig. [4](#page-6-0).

As shown in Fig. [4](#page-6-0), the attenuation mode of transmitted wave is the same as that of incident and refected waves, but its amplitude is much smaller than that of incident and refected waves. In addition, transmitted waves have two forms, positive negative transmission and positive transmission. When the transmitted wave frst passes through the A_1 end of the coal sample and is recorded by the strain gauge attached to the transmission rod, the obtained transmission wave is the negative transmission wave (Fig. [2\)](#page-4-0). The propagation direction of the negative transmitted wave is the same as that of the incident wave, but opposite to that of the refected wave. When the negative transmission wave propagates to the end of the transmission rod, its propagation direction is reversed. At this time, the transmitted wave frst passes through the strain gauge attached to the transmission rod and then propagates to the A_1 end of the coal sample (Fig. [2](#page-4-0)). This type of transmitted wave is called the positive transmitted wave, and the propagation direction is the same as that of the refected wave, but opposite to that of the incident wave. Compared to negative transmitted waves, the positive transmitted has a longer propagation path and consumes more energy. Therefore, the absolute value of the positive transmitted wave amplitude is less than that of the negative transmitted waves. With increased impact velocity, the frst wave amplitudes of positive and negative transmitted waves continued to grow. When the impact velocity is 1 m/s, the maximum amplitudes of positive and negative transmitted waves are 0.0129 V and−0.0165 V, respectively. When the impact velocity increases to 2.5 m/s, the maximum

Fig. 4 The attenuation characteristics of the transmitted wave (**a**: 1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s)

amplitudes of positive and negative transmitted waves are 0.0182 V and−0.0285 V, respectively. Therefore, the absolute value of the amplitude of the transmitted wave is positively correlated with the impact velocity.

The propagation velocity of the stress wave

In order to quantitatively characterize the evolution process of the stress wave attenuation velocity under diferent impact velocities, frst, non-linear ftting is performed on the amplitude of the stress wave to obtain the attenuation trend line of the amplitude of the stress wave (Figs. [3](#page-5-0) and [4](#page-6-0)). According to the ftting results, the ftting degree of the stress wave amplitude attenuation trend line exceeds 0.9, indicating a good ftting degree (Figs. [3](#page-5-0) and [4\)](#page-6-0). Then, the stress wave attenuation velocity trend line is obtained by solving the slope of the stress wave attenuation trend line (Figs. [5](#page-7-0) and [6](#page-7-1)).

With the time increases, the attenuation velocities of the incident, refected, and transmitted waves are not fxed, but decrease non-linearly; that is, the amplitudes of the incident, refected, and transmitted waves are attenuated in the form of variable deceleration (Figs. [5](#page-7-0) and [6](#page-7-1)). At the same impact velocity, the attenuation velocity of the incident wave is the largest, followed by the attenuation velocity of the refected wave, and the attenuation velocity of the transmitted wave is the smallest. Taking the impact velocity of 1 m/s as an example, the attenuation velocities of the frst incident wave, the refected wave, the positive transmitted wave, and the negative transmitted wave are 2.81 V/s, 2.11 V/s, 0.25 V/s, and 0.47 V/s, respectively. It is worth noting that although the transmission wave has the smallest attenuation velocity, it takes the shortest time to reach a stable velocity. With the impact velocity increases, the attenuation velocities of the incident wave, refected wave, positive transmitted wave, and negative transmitted wave all increase. When the impact

Fig. 5 Attenuation velocity of incident and refected waves (**a**: Incident wave, **b**:Refect wave)

Fig. 6 Attenuation velocity of transmitted waves (**a**: Positive transmission wave, **b**: Negative transmission wave)

velocity is 2.5 m/s, the attenuation velocities of the frst incident wave, refected wave, forward transmitted, and negative transmitted wave are 7.31 V/s, 5.57 V/s, 2.16 V/s, and 0.93 V/s, respectively. Compared to the impact velocity of 1 m/s, it is increased by 2.60, 2.64, 8.64, and 1.98 times, respectively. So, not only the absolute values of the amplitude of incident, refected, and transmitted waves are positively correlated with the impact velocity, but also their attenuation velocity is positively correlated with the impact velocity.

Displacement characteristics

During the stress wave attenuation, the incident, refected, and transmitted waves continued to pass through the coal. The stress wave always afected the coal, and its horizontal surface displacement was in dynamic changed (Fakhimi et al. [2018;](#page-20-15) Cong et al. [2021\)](#page-20-16). So, the fve points a, b, c, d, and e were selected on the coal surface (Fig. [7\)](#page-7-2). The coordinates of points a, b, c, d and e are (10, 35), (22.5, 35), (35, 35), (47.5, 35), and (60, 35), respectively (Fig. [7](#page-7-2)). The changes of displacement at a, b, c, d, and e in the horizontal direction during the dynamic load stress wave were analyzed by the DIC measurement system.

The basic principle of the DIC method was to match the geometric points on the digital speckle image under diferent states of the object surface and track the movement of the points to obtain the deformation information of the object surface (Xing et al. [2020](#page-22-27)). The speckle on the coal surface was sprayed randomly, and the small area around each point on the speckle image was called sub-areas. The sub-areas centered on a certain point in the speckle feld were used as the carrier of the displacement of the point (Golewski. [2021\)](#page-20-17), which could be obtained by searching and analyzing the movement and change of the sub-area (Jobin et al. [2021;](#page-21-30) Yu et al. [2021](#page-22-31)). As shown in Fig. [5,](#page-7-0) the reference area S_1 centered on the feature point P_1 (x_1 , y_1) is a subarea with a size of 128×128 pixels. After the face moved, the sub-area S_1 moved to the position of the sub-area S_2 so that the deformed position P_2 (x_2 , y_2) of the feature point P_1 was obtained. Thus, the displacement of the P_1 point was obtained. The evolution characteristics of the displacement feld of the coal sample surface in the process of dynamic stress wave propagation were shown in Fig. [8](#page-8-0) and Fig. [9\)](#page-9-0).

As shown in the Fig. [8,](#page-8-0) the surface displacement of the coal sample increases with time during the frst wave propagation $(t=0-1.20 \text{ ms})$, and the displacement direction is negative at this period. The coal sample surface experiences its maximum horizontal displacement following the frst stress wave propagation, which is around seven times more than the maximum displacement experienced during the frst wave. The displacement direction of the coal sample

Fig. 7 DIC measurement principle (**a**: Calculation Principles, **b**: Coal sample testing)

Fig. 8 Evolution process of surface displacement of coal samples (2.5 m/s)

Fig. 9 Maximum surface displacement of coal samples (diferent impact velocity)

surface was changed between 51.05 seconds and 80.65 seconds. The maximum positive displacement was attained at 68.50 ms in time. The displacement tends to decrease in the positive direction after reaching its maximum positive value. Also, the coal sample's surface displacement shows a distribution pattern that is "small on the left and high on the right," which denotes that the displacement is larger close to the dynamic load source and smaller farther away from the dynamic load source. The greatest horizontal displacement of the coal sample surface rises along with the impact velocity. When the impact velocity is 1 m/s, the coal sample surface experiences the largest horizontal displacement of−0.49 mm, and when the impact velocity is 2.5 m/s, an increase of 2.98 times, the displacement increases to−1.40 mm. Although the maximum amount of horizontal displacement on the surface of coal samples varies depending on the impact velocity (Fig. [9](#page-9-0)), the pattern of horizontal displacement distribution on the surface of the coal sample is almost the same under diferent impact velocities. The side closer to the dynamic load source (right) has greater displacement, and the side farther away from the dynamic load source (left) has smaller displacement.

According to the principle of DIC testing, the displacement change on the surface of the coal sample is caused by the movement of many points on its surface. The displacement changes of coal samples' surface points under diferent impact velocities are shown in the Fig. [10](#page-10-0).

As shown in the Fig. [10](#page-10-0), the value and direction of point displacement on the coal surface change in the form of oscillation in dynamic load stress wave attenuation. The

Fig. 10 Displacement of coal sample surface points (**a**:1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s)

oscillation process included negative oscillation increasing period, negative oscillation decreasing period, positive oscillation increasing period, and positive oscillation decreasing period. The horizontal displacement of coal surface points has the same displacement degree in the negative oscillation increase period and the negative displacement decrease period. The displacement degree of the two was the largest in the four stages, but the negative oscillation increase period consumed a shorter time, showing that the displacement rate was the fastest during the increase period of negative displacement oscillation. When the displacement direction is negative, its moving direction is the same as the propagation direction of incident wave, but opposite to the propagation direction of refected wave. At this time, the surface displacement of coal sample is mainly controlled by the compression of stress wave. When the displacement direction is positive, its moving direction is the same as the propagation direction of refected wave, but opposite to the propagation direction of incident wave. At this time, the surface displacement of coal sample is mainly controlled by the tension of stress wave. The displacement direction of coal sample surface is dominated by the compression and tension of dynamic load stress wave.

It is worth noting that when the frst stress wave propagation ends, the displacement of the coal sample surface does not reach the maximum value, and the maximum horizontal displacement of the coal sample surface appears after the frst stress wave propagation. At the same time, the direction of the maximum displacement during the stress wave propagation is the same as that during the frst

Fig. 10 (continued)

wave propagation. Taking 2.5 m/s impact velocity as an example, the maximum displacement of coal sample surface points a, b, c, d and e during the frst wave propagation is−0.129 mm,−0.141 mm,−0.150 mm,−0.167 mm, and−0.188 mm, respectively. The maximum displacement during stress wave propagation is−1.313 mm,−1.335 mm ,−1.364 mm,−1.378 mm, and−1.393 mm, respectively. Although the energy carried by the frst stress waves is greater than that carried by subsequent stress waves, the multiple efects of stress waves enhance the activation of microcracks in coal samples, weaken their ability to resist stress waves, and increase their deformation ability. Therefore, the subsequent stress wave will lead to greater displacement of the coal sample surface; that is, the deformation of the coal sample in the subsequent stress wave propagation process is greater than the frst wave propagation process.

The horizontal displacement variation laws of coal surface points a, b, c, d, and e were roughly the same under the same impact velocity, but the displacement values difered. In the early stage of stress wave attenuation, the displacement of the point close to the dynamic load source was large, and the displacement of the point away from the dynamic load source was small. Thus, it could be concluded that the displacement of point e was the largest and that of point a was the smallest. At the later stage of stress wave attenuation, the horizontal displacement values at diferent positions were similar. The point closer to the dynamic load source was preferentially afected by the stress wave in the early stage of attenuation, while the displacement of the point away from the dynamic load source decreases due to the lag of the position. At the late stage of oscillation, the oscillation propagation of the stress wave gradually stabilized, and the carried energy declined. Therefore, the horizontal displacements at diferent positions were similar in the later period of oscillation. With the increase of impact velocity, the maximum horizontal displacement value of each point kept increasing, and the horizontal displacement of coal surface points was positively correlated with impact velocity.

Velocity and acceleration of displacement

The displacement of coal surface points does not always increase or decrease but varies in an oscillatory manner. In the complex change process of displacement, the velocity and acceleration of displacement could change dynamically. Analyzing the change of velocity and acceleration of surface point displacement of coal contributed to further explaining the evolution characteristics of displacement. In this paper, Match ID software in the DIC test system was used to analyze the displacement, velocity, and acceleration of coal surface points. The displacement velocity was the frst derivative of displacement, and the displacement acceleration was the second derivative (Wang et al. [2021](#page-22-32)). The changes of displacement velocity and acceleration in the horizontal direction of coal surface points a, b, c, d, and e are shown in Figs. [11](#page-13-0) and [12.](#page-15-0)

The values and directions of horizontal displacement velocity and displacement acceleration at points a, b, c, d, and e on the coal surface changed from time to time (Figs. [11](#page-13-0) and [12](#page-15-0)). Diferences occurred in the changes in displacement velocity and acceleration in diferent stages of displacement. The velocity and acceleration of negative displacement appeared before that of positive displacement with increasing negative displacement oscillation, and the maximum velocity of negative displacement was greater than that of positive displacement, which directly resulted in the negative increase of displacement. The negative displacement velocity gradually decreased when the negative displacement oscillation declined. The acceleration of positive displacement was much greater than that of negative displacement, which explained why the displacement tended to decrease in the negative direction in the form of variable deceleration. The positive displacement velocity and acceleration were larger than the negative ones during the increase of positive displacement oscillation, directly transforming the displacement direction from negative to positive. The velocity and acceleration of displacement were signifcantly lower than that of displacement in the decreasing period of positive displacement oscillation and later tended to be stabilized, which was also the direct reason for the displacement decrease. Notably, the surface point displacement of coal changed in the form of variable acceleration and velocity.

The variation trends of displacement velocity and displacement acceleration at diferent positions on the coal surface were similar under the same impact velocity but with diferent values. With the decrease of the distance from the dynamic load source, the negative and positive displacement velocity and displacement acceleration tended to increase. In other words, the displacement velocity and displacement acceleration of point a were the smallest, and those of point e were the largest, which was similar to the changing trend displacement. Under diferent impact velocities, the horizontal displacement velocity and acceleration of coal sample surface points difered as well. The negative and positive displacement velocity and displacement acceleration of coal surface point a, b, c, d, and e increase with impact velocity. When the impact velocity was 2.5 m/s, the negative and positive displacement velocity and acceleration reached the maximum. It could be concluded that the horizontal displacement velocity and displacement acceleration of coal surface points were positively correlated with the dynamic load velocity. Furthermore, the largest displacement velocity and acceleration of the coal sample surface occur after the frst wave propagation, which is consistent with the displacement evolution law. As a result, the highest deformation of the coal sample surface, as well as the deformation velocity and acceleration, occurs after the frst wave propagation.

Multi‑fractal characteristics and correlation

The stress wave and the displacement of coal surface points changed in the form of non-linearity and heterogeneity. The multi-fractal theory is efective in studying the non-linear and heterogeneous changes of complex time series characteristic parameters (Lyubushin et al. [2013](#page-21-26), [2014\)](#page-21-27). Multi-fractal is defned as an infnite set of fractal measures composed of multiple scaling indices on the fractal structure, which can comprehensively reflect the singularity of complex time series, the degree of heterogeneity, and volatility (Li et al. [2017a](#page-21-31), [2020b\)](#page-21-32). If the attenuation of stress wave and the change of horizontal displacement of coal sample surface points have multiple classifcation characteristics, the distribution law of high-intensity and low-intensity signals in stress wave and the change characteristics of large-scale and small-scale displacement can be analyzed using multifractal characteristic parameters. In addition, the correlation between the stress wave and coal surface point displacement can also be revealed based on the correlation between the two multi-fractal characteristic parameters.

Multi‑fractal characteristics

The calculation formula of the multi-fractal spectrum is as follows (Li et al. [2017a,](#page-21-31) [2020b\)](#page-21-32):

Fig. 11 Displacement velocity (**a**: 1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s)

$$
f(\alpha) = \alpha q - \tau(q) \tag{1}
$$

where α refers to singularity; $f(\alpha)$ is the frequency of the subset represented by α in the subset set and also the fractal dimension of subset α ; and $\tau(q)$ is the quality index (Li et al. [2021a\)](#page-21-33). The width of the multi-fractal spectrum is defned as follows (Li et al. [2021a](#page-21-33)):

$$
\Delta \alpha = \alpha_{max} - \alpha_{min} \tag{2}
$$

where α_{max} represents the small-scale signal subset and α_{min} represents the large-scale signal subset. The width Δα of the multi-fractal spectrum can refect the diference between signals. Larger $\Delta \alpha$ gives rise to a greater difference in signal distribution, representing a greater diference between large-scale and small-scale signals (Li et al. [2021a](#page-21-33)). The relationship between the frequency of small-scale and large-scale signals can be obtained through the following equation (Li et al. [2017a,](#page-21-31) [2020b](#page-21-32)):

$$
\Delta f = f(\alpha_{max}) - f(\alpha_{min}) \tag{3}
$$

Smaller Δ*f* corresponds to a larger proportion of largescale signals, and vice versa. If $\Delta f > 0$, the small-scale signal is dominant; if $\Delta f < 0$, the large-scale signal is dominant (Li et al. [2017a,](#page-21-31) [2020b\)](#page-21-32).

Before using multi-fractal theory to analyze stress waves and displacements, it is necessary to check whether stress waves and displacements have multi-fractal characteristics. The $\ln Xq$ (*k*)— $\ln (k)$ curve of stress wave and displacement can prove whether they have multi-fractal (Fig. [13\)](#page-17-0).

Fig. 11 (continued)

As shown in the Fig. [13,](#page-17-0) the $\ln Xq(k)$ —ln (*k*) curves have a linear relationship and converge at a point, which shows that the time series of stress wave and displacement meet the scaling invariance and have multi-fractal characteristics.

The multiform patterns of incident rod end stress wave P_{IR} and transmitted rod end stress wave P_t and the changes of their characteristic parameters under diferent impact velocities were shown in Fig. [14\)](#page-17-1).

As shown in Fig. [14](#page-17-1), the incident rod end stress wave and transmitted stress wave signals have multi-fractal characteristics. However, obvious diferences can be found in the shape and parameters of its multi-fractal spectrum. The multi-fractal spectrum of the stress wave at the incident rod end is "left hook", and $\Delta \alpha_{IR}$ is greater than 0, but Δf_{IR} is less than 0. The multi-fractal spectrum of transmission wave

is "right hook", and $\Delta \alpha_T$ and Δf_T are greater than 0. There are huge diferences between the high amplitude and low amplitude signals of incident rod end stress waves and transmitted waves. However, the incident rod-end stress waves are dominated by high amplitude signals and the transmitted waves by low amplitude signals. Both similarities and diferences can be found in the characteristic parameters of multi-fractal of incident rod end stress waves and transmitted waves under different impact velocities. $\Delta \alpha_{IR}$ of incident rod end stress wave and $\Delta\alpha_T$ of transmitted stress wave increase with impact velocity, which shows that the diference of stress wave time series signals increases with growing impact velocity. In other words, it means larger differences between high and low amplitude signals and more obvious multi-fractal characteristics of stress waves. With

Fig. 12 Displacement acceleration (**a**: 1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s)

the increase of impact velocity, the Δf_{IR} of incident rod end stress wave fuctuates between−0.47 and 0.41, while the Δf _{*T*} of the transmitted wave increases continuously, which shows that the proportion of low and high amplitude signals of incident rod end stress wave is less afected by impact velocity compared with that of the transmitted stress wave.

In the stress wave attenuation process, the multi-fractal characteristics of horizontal displacement of coal sample surface points (a, b, c, d, and e) are shown in Fig. [15.](#page-18-0)

As shown in Fig. [15,](#page-18-0) the horizontal displacement of coal sample surface points (a, b, c, d, and e) are multi-fractal, and a "left hook" shaped multi-fractal spectrum, where $\Delta \alpha_{D} > 0$ and Δf_D < 0. The fluctuation of horizontal displacement on the surface of the coal sample is strong. Meanwhile, the difference between large-scale and small-scale displacement is large, with a larger proportion of large-scale displacement. Under the same impact velocity, the multi-fractal characteristic parameters of points a, b, c, d, and e are diferent. With a shorter distance from the dynamic load source, $\Delta \alpha_D$ decreases continuously. The horizontal displacement fuctuation of the points far away from the dynamic load source and the diferences between large-scale and small-scale displacement are relatively large with relatively obvious multi-typing features. The fuctuation of horizontal displacement near the dynamic load source and the diference between large-scale and small-scale displacement are relatively small with weak multi-taxing features. With increased impact velocity, large-scale and small-scale displacement diferences become larger, with more obvious multi-fractal displacement characteristics. The diference between the

Fig. 12 (continued)

large-scale and small-scale displacement of coal surface particles is positively correlated with impact velocity. As impact velocity increases, the diference experienced an inverted v-shape change (increase frst and then decrease). Besides, the proportion of large-scale and small-scale displacement on the coal sample surface shows the same changing trend with increased impact velocity.

Correlation between stress wave and displacement

Figure [16](#page-19-0) shows the variation of multi-fractal characteristic parameters of horizontal displacement of points on the coal sample surface with multi-fractal parameters of the stress wave.

With the increase of multi-fractal parameters $\Delta \alpha_{IR}$ and $\Delta \alpha_{\rm T}$, the $\Delta \alpha_{\rm D}$ of coal sample surface displacement increases continuously. The fuctuation of horizontal displacement of the coal sample surface is positively correlated with the fuctuation of the dynamic load stress wave. In other words, the diference between large-scale and small-scale displacement is positively correlated with the diference between the high and low amplitude signals of the dynamic load stress wave. When $\Delta\alpha$ ^{*D*} takes a certain value, which is when the difference between large-scale and small-scale displacement on the coal sample surface is constant, $\Delta \alpha_T$ is much less than $\Delta \alpha_{IR}$. When there is little difference between high and low amplitude signals of the transmitted wave, the diference between large-scale and small-scale displacement will greatly change. However, larger diferences are required for

(a) Stress wave

Fig. 13 The relationship between $\ln X_a(k)$ and $\ln(k)$

Fig. 14 Multi-fractal characteristics of stress wave (**a**: Incident rod end stress wave, **b**: Transmitted rod stress wave, **c**: the $\Delta \alpha_{IR}$ and Δf_{IR} at different impact velocity, \mathbf{d} : the $\Delta\alpha_{\rm T}$ and $\Delta\mathbf{f}_{\rm T}$ at different impact velocity)

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Fig. 15 Multi-fractal parameters of surface point displacement of coal samples (**a**: 1m/s, **b**: 1.5m/s, **c**: 2m/s, **d**: 2.5m/s, **e**: the $\Delta \alpha_{\text{D}}$ at different impact velocity, **f**: the Δf_D at different impact velocity)

the stress wave signal at the incident rod end to bring about the same change of displacement. In the case of the point a, for example, when $\Delta \alpha_{\text{D}}$ is 0.66, $\Delta \alpha_{\text{IR}}$ is 0.55, but $\Delta \alpha_{\text{T}}$ is only 0.12. When $\Delta \alpha_D$ increases to 1.14, $\Delta \alpha_{IR}$ is 0.96 and $\Delta \alpha_T$ is only 0.19. The transmission wave has a greater impact on the diference between the large-scale and small-scale displacement of the coal sample surface. With the increase of Δf_{IR} and Δf_T , Δf_D increases first and then decreases. In

Fig. 16 Correlation characteristics (**a**: the correlation between $\Delta \alpha_{\text{R}}$, **a**nd $\Delta \alpha_{\text{R}}$, **b**: the correlation between $\Delta \alpha_{\text{D}}$ and $\Delta \alpha_{\text{T}}$, **c**: the correlation between Δf_D and Δf_R **d**: the correlation between Δf_D and Δf_T)

a certain range, the high amplitude signal of the stress wave is positively correlated with the large-scale displacement of the coal sample surface. However, when it exceeds the critical value, the high amplitude signal of the stress wave will be negatively correlated with the large-scale displacement of the coal sample surface, which is more obvious in the transmitted wave.

Conclusions

In this paper, the impact experiments of coal were carried out using SHPB and DIC. The author systematically studied the multiple propagation characteristics of the stress wave, evolution patterns of horizontal displacement, displacement velocity, and displacement acceleration of coal under dynamic load. The correlation between dynamic load stress wave and the horizontal displacement of coal surface points

was analyzed based on multi-fractal theory. The detailed conclusions are as follows:

1. The stress wave propagates in the non-linear attenuation mode of multiple incidences, refections, and transmissions. And the attenuation velocity of the stress wave amplitude also decreases in a non-linear form. Among them, the attenuation velocity of the incident wave is the largest, followed by the attenuation velocity of the refected wave, and the attenuation velocity of the transmitted wave is the smallest. The incident and refected stress waves, which are dominated by high amplitude signals and those of transmitted stress waves, are dominated by low amplitude signals. Not only the absolute values of the amplitude of incident, refected, and transmitted waves are positively correlated with the impact velocity, but also their attenuation velocity is positively correlated with the impact velocity.

- 2. The horizontal displacement of the coal surface points change in the form of variable velocity and acceleration during the attenuation of the stress wave. And the displacement direction of coal sample surface is dominated by the compression and tension of the stress wave. The change process can be divided into four stages, i.e., two stages of increase and decrease in negative displacement oscillations and two similar stages in positive ones. Among them, the displacement and its rate in the increasing period of negative oscillation are the largest.
- 3. The stress wave and the surface point displacement of coal have multi-fractal characteristics. Herein, the stress wave at the incident rod end has a "left hook" shaped multi-fractal spectrum with $\Delta \alpha_{IR}$ greater than 0 and Δf_{IR} less than 0. The multi-fractal spectrum shape of transmission wave is "right hook", with $\Delta \alpha_T$ and Δf_T larger than 0. The multi-fractal spectrum shape of horizontal displacement of the coal sample surface is "left hook type" with $\Delta \alpha_D$ 0 but Δf_D <0. According to the characteristic parameters of multi-fractal, the high amplitude signal accounts for a larger proportion in the incident rod end stress wave, while the low amplitude one accounts for a larger proportion in the transmitted wave. The large-scale displacement determines point displacement on the surface of coal samples. The proportional relationship and diference between large-scale and smallscale displacement are afected by those between high and low amplitude signals of the stress wave, and the infuence of the transmission wave is greater.

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Author contribution Xiaoliang Li: Methodology, Formal analysis, Visualization, Writing-Original draft preparation.

Enlai Zhao: Conceptualization, Resources, Funding acquisition. **Zhentang Liu:** Funding acquisition, Project administration, Supervision.

Yubing Liu: Software, Validation.

Xiaojun Feng: Validation, Data Curation.

Zhoujie Gu: Investigation, Writing-Reviewing and Editing.

Declarations

Conflict of interest The authors declare no competing interests.

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