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Artificial neural networks approach for estimating the groutability of granular soils with cement-based grouts

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Abstract A reliable estimation of the groutability of the target geomaterial is an essential part of any grouting project. An artificial neural network (ANN) model has been developed for the estimation of groutability of granular soils by cement-based grouts, using a database of 87 laboratory results. The proposed model used the water:cement ratio of the grout, relative density of the soil, grouting pressure, and diameter of the sieves through which 15% of the soil particles and 85% of the grout pass. A very good correlation was obtained between the ANN predictions and the laboratory experiments. Comparison of these results with those obtained using traditional methods for groutability prediction confirmed the viability of using ANN to estimate groutability.

Keywords Groutability · Artificial neural networks · Granular soil · Microfine cement

Résumé Une estimation fiable de l'injectabilité de géomatériaux constitue une question essentielle de tout projet d'injection. Dans ce contexte, un modèle de réseau de neurones artificiel (ANN) a été développé pour l'estimation de l'injectabilité de sols granulaires par des coulis à base de ciment, en utilisant une base de données établie à partir de 87 résultats d'essais en laboratoire. Le modèle proposé considère comme paramètres d'entrée: le rapport eau-ciment du coulis, la densité relative du sol, la pression d'injection, la taille de particule du sol correspondant au passant à 15% et la taille de particule du coulis

E. Tekin · S. O. Akbas (⊠) Department of Civil Engineering, Gazi University, Ankara, Turkey e-mail: SOA1@cornell.edu; soakbas@gmail.com; soakbas@gazi.edu.tr correspondant au passant à 85%. Un très bon accord a été obtenu à partir de la comparaison des résultats de l'analyse ANN avec ceux obtenus à partir des expérimentations. La comparaison de ces résultats avec ceux obtenus avec les méthodes traditionnelles pour les prévisions d'injectabilité confirment la possibilité d'utiliser le modèle ANN pour les estimations d'injectabilité.

Mots clés Injectabilité · Réseau de neurones artificiel · Sol granulaire · Ciment ultrafin

Introduction

Permeation grouting is a widely used ground improvement technique that involves the injection of suitable particulate grouts and chemical solutions into soil and rock with the aim of reducing the permeability and/or improving the mechanical properties (Jessberger 1983; Krizek 1985; Welsh 1986; Welsh and Burke 1991; Gouvenot 1998; Dupla et al. 2004. The properties and behaviour of cement grouts have been a major research focus in recent years (e.g. Zebovitz et al. 1989; Akbulut 1999; Kim et al. 2009) as, despite its advantages, there can be some adverse effects with the use of chemical solutions.

One of the main challenges in the utilization of cementbased grouts is the reliable estimation of the groutability (N) of the target geomaterial. The grouting process is based on the complex time-dependent transport process of cement grains through the soil matrix. This involves the grain size distribution of the soil and grout, the concentration and viscosity of the grout suspension, the pore size and hydraulic conductivity of the soil, the injection pressure etc. As a result, there is no agreement on a universal set of criteria or a methodology.

Because of their heuristic problem-solving capabilities. artificial neural networks (ANNs) have been applied successfully to many geotechnical engineering problems (Shahin et al. 2008). Within foundation design, ANNs have been used in predicting the settlement and bearing capacity of shallow foundations (e.g. Chen et al. 2006; Shahin et al. 2005; Padmini et al. 2008) and the axial and lateral load capacity of pile foundations, drilled shafts, and ground anchors (e.g. Abu-Kiefa 1998; Goh et al. 2005; Rahman et al. 2001). ANNs have also been employed in applications concerning earth retaining structures (e.g. Kung et al. 2007), site characterization (e.g. Najjar and Basheer 1996), mining (Rankine and Sivakugan 2005), dams (Kim and Kim 2008), tunnels (Yoo and Kim 2007), slope stability (e.g. Goh and Kulhawy 2003), blasting (Lu 2005) and geoenvironmental engineering (Shang et al. 2004). A comprehensive overview of ANN applications in geotechnical engineering is given by Shahin et al. (2008).

ANNs are particularly useful for constitutive modeling of soils, in which the complexity of the soil formation and excessive number of required empirical factors (Adeli 2001) prohibit the use of traditional theories to properly simulate the soil behavior. They are also valuable in soil property estimation, which is usually controlled by many interacting parameters that are difficult to handle by statistics alone. ANNs have been used in the estimation of pre-consolidation pressure and stress history (Celik and Tan 2005), swell pressure (Erzin 2007), liquefaction potential (e.g. Hanna et al. 2007), density (Goh 1995), shear strength (e.g. Lee et al. 2003), compaction and permeability (e.g. Sinha and Wang 2008). Interestingly, no studies have been performed on estimating the groutability of soils using ANNs.

Within this context, in this paper an ANN model was developed to estimate the groutability of granular soils with cement grouts. To achieve this, results from a database consisting of 87 laboratory grouting tests were used. The performance of the ANN model is compared with the most commonly used existing groutability estimation methods.

Existing methods for the estimation of groutability

Early studies on the estimation of groutability of granular soils involved only a comparison of the grain size of the host soils with that of the cement grout. Burwell (1958) and Mitchell (1981) defined groutability with the following simple and practical equation:

$$N = (D_{15})_{\text{basesoil}} / (d_{85})_{\text{cementgrout}} \tag{1}$$

in which D_{15} = the diameter of a sieve through which 15% of the soil passes and d_{85} = the diameter of a sieve through

which 85% of the cement grout passes. According to this equation, if N is larger than 25, then the grout can be successfully injected into the soil while if N is smaller than 11, sufficient grout will not be injected into the soil formation. For values of N between 25 and 11, in situ tests should be performed to determine if the grouting is possible.

According to Burwell (1958), even if N obtained from Eq. 1 is greater than 25, the following additional equation should be used to determine if grouting is possible:

$$N = (D_{10})_{\text{basesoil}} / (d_{95})_{\text{cementgrout}}$$
(2)

in which D_{10} = the diameter of a sieve through which 10% of the soil passes and d_{95} = the diameter of a sieve through which 95% of the cement grout passes. If the *N* value calculated using Eq. 2 is greater than 11, then grouting is possible. For values of *N* smaller than 5, the soil is not groutable with the particular cement type considered. Again, in situ tests are recommended for *N* values in between 5 and 11.

Another similar equation that considers the grain size of host soils and that of cement was developed by Incecik and Ceren (1995):

$$N = (D_{10})_{\text{basesoil}} / (d_{90})_{\text{cementgrout}}$$
(3)

in which d_{90} = the diameter of a sieve through which 90% of the cement grout passes. According to this approach, if the *N* value obtained by Eq. 3 is greater than 10, grouting is possible.

The permeability of soil has also been used to estimate groutability. Starting from the Hazen Formula, DeBeer (1970) developed the following equation to predict groutability:

$$k = 116(0.7 + 0.034t)(D_{10})^2 \tag{4}$$

in which k = hydraulic conductivity in cm/s, and t = temperature in °C. Note that the unit of D_{10} is cm. According to Landry et al. (2000), if the k value obtained using Eq. 4 is greater than 1×10^{-1} cm/s, the host soil is groutable by cement. For 1×10^{-1} cm/s > $k > 5 \times 10^{-3}$ cm/s, fine grained cement is required for grouting. If 5×10^{-3} cm/s > $k > 1 \times 10^{-4}$ cm/s, special chemical solutions are needed to ensure groutability.

Recent studies (e.g. Akbulut and Saglamer 2002; Tekin 2004; Kim et al. 2009) indicated the need for the consideration of additional parameters for a more reliable estimation of groutability. Based on a series of laboratory experiments on grouted sand samples prepared at various relative densities and grain size distributions, Akbulut and Saglamer (2002) developed the following empirical formula for the estimation of groutability of granular soils:

$$N = \frac{(D_{10})_{\text{base soil}}}{(d_{90})_{\text{cement grout}}} + k_1 \frac{w/c}{FC} + k_2 \frac{P}{D_r}$$
(5)

in which w/c = water/cement ratio of the grout, FC = content of soil passing through a 0.6 mm sieve, P = grouting pressure in kPa, and D_r = relative density of the host soil. $k_1 = 0.5$ (unitless) and $k_2 = 0.01$ in 1/kPa are the constants based on experimental observations to normalize the N values.

If the *N* value obtained from Eq. 5 is greater than 28, the granular soil can be grouted effectively by cement-based grouts. For *N* values smaller than 28, injection by cement-based grouts is not possible, and groutability using chemical grouts should be investigated. Note that Eq. 5 is most applicable for conditions where FC is smaller than 6%, water:cement ratio is between 0.8 and 2, and grouting pressure is between 50 and 200 kPa.

Modeling with artificial neural networks

An ANN is a collection of interconnected processing elements called neurons with performance characteristics similar to the biological neurons (Fausett 1994). These processing elements are organized in layers: an input layer, an output layer, and one or multiple intermediate layers, which are also called hidden layers. A typical ANN structure with five neurons in the input layer, three neurons in the hidden layer, and a single neuron in the output layer is shown in Fig. 1. Each neuron in a specific layer is connected to many other neurons with weighted connections; a zero weight implying no connection and a negative weight indicating a prohibitive relationship.

The simulation problem with an ANN consists of finding a satisfactory relationship between a set of neurons representing the input data and the associated outputs (Erzin 2007). The learning phase of ANN consists of using the input and output data for a specific problem and changing the weighting of among the neurons until the error is minimized. There are several learning algorithms; the most popular one is the feed-forward back-propagation algorithm, which is also used in the current study. The trained network is then tested in the validation phase based



Fig. 1 A typical ANN structure

on the predictions it makes using a completely new set of data. Details of artificial neural networks have been widely reported elsewhere; see for example Flood and Kartam (1994) and Zurada (1992).

ANN model for estimation of groutability

Identification and collection of data

As discussed previously, in the literature the simplified techniques for the prediction of groutability are based on a comparison between the grain size of the host soils and that of the cement grout, or the permeability of host soil. However, as shown in more recent studies (e.g. Akbulut and Saglamer 2002; Tekin 2004) various other parameters affect the groutability. It is believed that better predictions of groutability can be achieved by including as many influential soil and grout input parameters as possible in one model. In this way, the high parameter recognition capacity of ANN can be utilized to improve the prediction capability of the model. Accordingly, a database that consists of case records, each of which carry information at least on w/c, D_r , P, FC, as well as the grain size distribution of the host soil and the grout is used to develop a robust ANN model.

Using the test setup shown in Figs. 2 and 3, Tekin (2004) investigated the penetrability of the microfine cement Rheocem 900 into sand specimens with a variety of grain size distributions. A total of fifteen tests were conducted under 100 kPa grouting pressure for sands prepared at a $D_{\rm r}$ of about 30%. These are presented as case records 57 to 71 in Table 1. To obtain a database that includes case records with more diverse properties, the same experimental setup was utilized to perform sixteen additional tests for the current study, numbered 72 to 87 in Table 1. The new tests were conducted at a higher grouting pressure and with different grain size distributions and FC for the host soil, using a finer cement grout, and with various values of D_r , as summarized in Table 1. These results were supplemented with data compiled from the literature: case records numbered from 1 to 38 in Table 1 being from Akbulut and Saglamer (2002), and 39 to 56 from Zebovitz et al. (1989). As seen in Table 1, the ANN was based on a total of 87 case records including w/c, Dr, P, FC, D10 and D_{15} of soil, and d_{85} , d_{90} , and d_{95} of grout and the experimental results of the grouting.

Implementation of the ANN model

The neural network toolbox of MATLAB was used to develop the ANN model, which comprised five neurons in the input layer (i.e., w/c, D_r , P, FC, and $(D_{15})_{\text{base soil}}/(d_{85})_{\text{cement grout}}$, and one neuron in the output layer

Fig. 2 Schematic diagram of test setup







Fig. 3 Grouting test setup

(groutability decision), where the binary number 1 represents successful grouting and 0 represents unsuccessful grouting. The range of the model input and output parameters are given in Table 2. As suggested by Demuth et al. (2009), for a more effective learning phase, the input and output data were normalized to a range of -1.0 to 1.0using the pre-processing functions:

$$y = \frac{(y_{\max} - y_{\min})(x - x_{\min})}{(x_{\max} - x_{\min})} y_{\min}$$
(6)

in which, for a *N* x *Q* sized matrix *X*, where *N* = number of ANN model parameters, and *Q* = number of samples, x = actual value, $y_{max} =$ maximum value for each row of *X*, $y_{min} =$ minimum value for each row of *X*, $x_{min} =$ minimum value of matrix *X*, and $x_{max} =$ maximum value of matrix *X*.

Division of data is another aspect of ANN modeling which requires careful attention. To divide the data into two subsets, namely training and testing, can result in overfitting, i.e., memorization rather than generalization, especially if the training data are noisy (Shahin et al. 2008). Consequently, a separate validation set is needed to ensure that the model can generalize within the range of the data used during training. For the current study, the dataset given in Table 1 was randomly categorized into three subsets of training, testing and validation. In the literature, there are no hard and fast rules concerning the relative ratios of these subsets. Hammerstrom (1993) suggested two-thirds of the data should be used for model training and testing and one-third for model validation. Shahin et al. (2004) investigated the impact of the proportion of data used in the various subsets in a study on estimating the settlement of shallow foundations, and found that there is no clear relationship between the proportion of data for training, testing and validation and model performance. However, they observed that the model performed best when 20% of the data were used for validation and the remaining data were divided into 70% for training and 30% for testing. For the model developed in this study, about 60% of the data, i.e., 53 of the case records, were used for training with the remaining data divided equally into testing and validation sets. The cross-validation technique proposed by Stone (1974) was used as the stopping criteria in order to overcome premature model stopping or overtraining

There is no unified approach regarding determination of an optimal ANN architecture. For multilayer perceptrons (MLPs), also used in the current study, the number of layers representing the input and output variables are each fixed at one. It has been shown that one hidden layer is sufficient to approximate any continuous function provided that sufficient connection weights are given. Accordingly, for the MLP feedback ANN model in the current study, a single hidden layer was used. After many trials, the number of neurons within the hidden layer was selected to be fifteen. As a result, the model consists of three layers (input, hidden, and output) with 5, 15 and 1 neurons, respectively.

No	w/c	Dr (%)	P (kPa)	FC (%)	$D_{10 \text{ soil}} (\text{mm})$	$D_{15 \text{ soil}} (\text{mm})$	$d_{85 \text{ grout}} \text{ (mm)}$	$d_{90 \text{ grout}} (\text{mm})$	$d_{95 \text{ grout}} (\text{mm})$	Groutability	
										Experimental	ANN
1	1	80	50	1	2.50	2.70	0.03100	0.04000	0.06000	Yes	1
2	1	80	100	1	1.28	1.40	0.03100	0.04000	0.06000	Yes	1
3	1	80	100	1	0.60	0.65	0.03100	0.04000	0.06000	Yes	1
4	1	80	100	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
5	1	80	150	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
6	1	80	250	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
7	2	30	100	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
8	2	30	200	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
9	1	80	100	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
10	1	80	150	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
11	1	80	200	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
12	2	30	100	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
13	2	30	200	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
14	1	80	100	33	0.70	0.85	0.03100	0.04000	0.06000	Yes	1
15	1	80	100	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
16	1	80	150	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
17	1	80	200	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
18	1	30	200	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
19	2	30	200	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
20	1	80	100	15	0.54	0.60	0.03100	0.04000	0.06000	No	0
21	2	30	200	15	0.54	0.60	0.03100	0.04000	0.06000	No	0
22	1	80	100	10	0.60	0.73	0.03100	0.04000	0.06000	No	0
23	1	80	100	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
24	1	80	100	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
25	1	80	150	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
26	1	80	200	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
27	1	30	200	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
28	2	30	100	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
29	2	30	100	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
30	3	30	100	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
31	2	30	200	100	0.32	0.35	0.03100	0.04000	0.06000	No	0
32	2	30	200	34	0.37	0.44	0.03100	0.04000	0.06000	No	0
33	1	80	200	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
34	2	30	200	15	0.48	0.60	0.03100	0.04000	0.06000	No	0
35	1	80	100	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
36	1	80	150	5	0.76	0.88	0.03100	0.04000	0.06000	No	0
37	1	80	200	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
38	1	30	200	5	0.76	0.88	0.03100	0.04000	0.06000	Yes	1
39	4	70	517	100	0.15	0.17	0.00600	0.00640	0.00800	Yes	1
40	4	70	517	100	0.14	0.16	0.00600	0.00640	0.00800	Yes	1
41	4	70	517	100	0.13	0.15	0.00600	0.00640	0.00800	Yes	1
42	4	70	690	100	0.13	0.15	0.00600	0.00640	0.00800	No	0
43	4	70	690	100	0.12	0.13	0.00600	0.00640	0.00800	No	0
44	4	70	483	25	0.35	0.43	0.00600	0.00640	0.00800	Yes	1
45	4	70	517	25	0.32	0.40	0.00600	0.00640	0.00800	Yes	1
46	4	70	690	25	0.12	0.15	0.00600	0.00640	0.00800	Yes	1
47	4	70	690	25	0.30	0.35	0.00600	0.00640	0.00800	No	0

Table 1 continued

Experimental ANN 48 2 70 655 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 49 4 70 517 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 50 6 70 345 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 51 4 70 552 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 55 4 70 552 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 55 4 70 552 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.0160 0.01500 Yes 1 57 1 30 <th>No</th> <th>w/c</th> <th>Dr (%)</th> <th>P (kPa)</th> <th>FC (%)</th> <th>$D_{10 \text{ soil}} (\text{mm})$</th> <th>$D_{15 \text{ soil}} (\text{mm})$</th> <th>d_{85 grout} (mm)</th> <th>d_{90 grout} (mm)</th> <th>d_{95 grout} (mm)</th> <th colspan="2">Groutability</th>	No	w/c	Dr (%)	P (kPa)	FC (%)	$D_{10 \text{ soil}} (\text{mm})$	$D_{15 \text{ soil}} (\text{mm})$	d _{85 grout} (mm)	d _{90 grout} (mm)	d _{95 grout} (mm)	Groutability	
											Experimental	ANN
49 4 70 517 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 50 6 70 345 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 52 4 70 483 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 54 2 70 552 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 100 0.10 0.12 0.00800 0.0100 0.01500 Yes 1 58 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 23	48	2	70	655	100	0.15	0.17	0.00600	0.00640	0.00800	Yes	1
50 6 70 345 100 0.15 0.17 0.00600 0.00640 0.00800 Yes 1 51 2 70 532 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 53 6 70 241 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 54 2 70 552 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 55 4 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 10 0.12 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 23 <t< td=""><td>49</td><td>4</td><td>70</td><td>517</td><td>100</td><td>0.15</td><td>0.17</td><td>0.00600</td><td>0.00640</td><td>0.00800</td><td>Yes</td><td>1</td></t<>	49	4	70	517	100	0.15	0.17	0.00600	0.00640	0.00800	Yes	1
51 2 70 552 65 0.19 0.22 0.00600 0.00840 0.00800 Yes 1 52 4 70 483 65 0.19 0.22 0.00600 0.00840 0.00800 Yes 1 54 2 70 552 25 0.35 0.43 0.00600 0.00840 0.00800 Yes 1 55 4 70 448 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 244 25 0.35 0.43 0.00680 0.01100 0.01500 Ne 1 57 1 30 100 10 0.10 0.12 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1	50	6	70	345	100	0.15	0.17	0.00600	0.00640	0.00800	Yes	1
52 4 70 483 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 55 6 70 241 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 54 2 70 448 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 100 0.10 0.12 0.00880 0.01100 0.01500 Yes 1 59 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Ne 1 61 1 30 100 <	51	2	70	552	65	0.19	0.22	0.00600	0.00640	0.00800	Yes	1
53 6 70 241 65 0.19 0.22 0.00600 0.00640 0.00800 Yes 1 54 2 70 552 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 55 4 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 100 0.10 0.12 0.00880 0.01100 0.01500 Ne 0 58 1 30 100 20 1.04 1.07 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Ne 0 65 1 30 100 <t< td=""><td>52</td><td>4</td><td>70</td><td>483</td><td>65</td><td>0.19</td><td>0.22</td><td>0.00600</td><td>0.00640</td><td>0.00800</td><td>Yes</td><td>1</td></t<>	52	4	70	483	65	0.19	0.22	0.00600	0.00640	0.00800	Yes	1
54 2 70 552 2.5 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 55 4 70 448 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 58 1 27 100 20 1.04 1.07 0.00880 0.01100 0.01500 Yes 1 60 1 32 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 61 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 62 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 <td< td=""><td>53</td><td>6</td><td>70</td><td>241</td><td>65</td><td>0.19</td><td>0.22</td><td>0.00600</td><td>0.00640</td><td>0.00800</td><td>Yes</td><td>1</td></td<>	53	6	70	241	65	0.19	0.22	0.00600	0.00640	0.00800	Yes	1
55 4 70 448 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 100 0.12 0.00880 0.01100 0.01500 Yes 1 59 1 30 100 29 0.23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 29 0.23 0.36 0.01800 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Ne 0 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 Ne 1	54	2	70	552	25	0.35	0.43	0.00600	0.00640	0.00800	Yes	1
56 6 70 241 25 0.35 0.43 0.00600 0.00640 0.00800 Yes 1 57 1 30 100 100 0.10 0.12 0.00880 0.01100 0.01500 No 0 58 1 27 0.00 23 0.26 0.51 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 29 0.23 0.36 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 64 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 Yes 1	55	4	70	448	25	0.35	0.43	0.00600	0.00640	0.00800	Yes	1
57 1 30 100 100 0.10 0.12 0.00880 0.01100 0.01500 Yes 1 58 1 27 100 20 1.04 1.07 0.00880 0.01100 0.01500 Yes 1 60 1 32 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 60 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 67 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1	56	6	70	241	25	0.35	0.43	0.00600	0.00640	0.00800	Yes	1
58 1 27 100 20 1.04 1.07 0.00880 0.01100 0.01500 Yes 1 59 1 30 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 61 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 <	57	1	30	100	100	0.10	0.12	0.00880	0.01100	0.01500	No	0
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60 1 32 100 23 0.28 0.40 0.00880 0.01100 0.01500 No 0 61 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 No 0 62 1 30 90 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 67 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0	59	1	30	100	19	0.36	0.51	0.00880	0.01100	0.01500	Yes	1
61 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 No 0 62 1 30 90 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 1	60	1	32	100	23	0.28	0.40	0.00880	0.01100	0.01500	Yes	1
62 1 30 90 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 1	61	1	30	100	29	0.23	0.30	0.00880	0.01100	0.01500	No	0
63 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 64 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 23 0.22 0.00880 0.01100 0.01500 Yes 1 71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 72 1 30 490 100 0.10 0.11 0.0075 0.0080 0.00120 Yes 1 71 <td>62</td> <td>1</td> <td>30</td> <td>90</td> <td>19</td> <td>0.36</td> <td>0.51</td> <td>0.00880</td> <td>0.01100</td> <td>0.01500</td> <td>Yes</td> <td>1</td>	62	1	30	90	19	0.36	0.51	0.00880	0.01100	0.01500	Yes	1
64 1 30 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 67 1 30 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 71 1 30 100 0.10 0.11 0.00075 0.0080 0.00120 Yes 1 73 <td>63</td> <td>1</td> <td>30</td> <td>100</td> <td>23</td> <td>0.28</td> <td>0.40</td> <td>0.00880</td> <td>0.01100</td> <td>0.01500</td> <td>Yes</td> <td>1</td>	63	1	30	100	23	0.28	0.40	0.00880	0.01100	0.01500	Yes	1
65 1 30 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 66 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 67 1 30 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 71 1 30 490 100 0.10 0.11 0.0075 0.00880 0.00120 Yes 1 73 1 30 490 69 0.11 0.13 0.0075 0.00880 0.00120 Yes 1 <t< td=""><td>64</td><td>1</td><td>30</td><td>100</td><td>29</td><td>0.23</td><td>0.30</td><td>0.00880</td><td>0.01100</td><td>0.01500</td><td>Yes</td><td>1</td></t<>	64	1	30	100	29	0.23	0.30	0.00880	0.01100	0.01500	Yes	1
66 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 67 1 30 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 71 1 30 490 100 0.10 0.11 0.0075 0.0080 0.00120 Yes 1 73 1 30 490 69 0.11 0.13 0.0075 0.0080 0.00120 Yes 1 74 1 30 490 62 0.12 0.14 0.0075 0.0080 0.00120 Yes 1	65	1	30	100	33	0.20	0.27	0.00880	0.01100	0.01500	No	0
67 1 30 100 19 0.36 0.51 0.00880 0.01100 0.01500 Yes 1 68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 No 0 71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.0120 Yes 1 73 1 30 490 100 0.10 0.11 0.0075 0.0080 0.00120 Yes 1 74 1 30 490 69 0.11 0.13 0.0075 0.0080 0.00120 Yes 1 75 1 30 490 64 0.14 0.20 0.0075 0.0080 0.00120 Yes 1	66	1	30	100	38	0.17	0.22	0.00880	0.01100	0.01500	No	0
68 1 30 100 23 0.28 0.40 0.00880 0.01100 0.01500 Yes 1 69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 Yes 1 71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 72 1 30 490 100 0.10 0.11 0.0075 0.0080 0.0120 Yes 1 73 1 30 490 69 0.11 0.13 0.0075 0.0080 0.0120 Yes 1 74 1 30 490 62 0.12 0.14 0.0075 0.0080 0.0120 Yes 1 75 1 30 490 64 0.14 0.20 0.0075 0.0080 0.00120 Yes 1	67	1	30	100	19	0.36	0.51	0.00880	0.01100	0.01500	Yes	1
69 1 28 100 29 0.23 0.30 0.00880 0.01100 0.01500 Yes 1 70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 Yes 1 71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 72 1 30 490 100 0.10 0.11 0.00075 0.00880 0.00120 Yes 1 73 1 30 490 69 0.11 0.12 0.00075 0.0080 0.00120 Yes 1 74 1 30 490 62 0.12 0.14 0.00075 0.0080 0.00120 Yes 1 75 1 30 490 54 0.13 0.15 0.00075 0.0080 0.00120 Yes 1 76 1 30 490 52 0.57 0.00075 0.0080 0.00120 Yes 1 78	68	1	30	100	23	0.28	0.40	0.00880	0.01100	0.01500	Yes	1
70 1 31 100 33 0.20 0.27 0.00880 0.01100 0.01500 Yes 1 71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 72 1 30 490 100 0.10 0.11 0.00075 0.00080 0.00120 Yes 1 73 1 30 490 69 0.11 0.12 0.00075 0.00080 0.00120 Yes 1 74 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 75 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 76 1 30 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 77 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1	69	1	28	100	29	0.23	0.30	0.00880	0.01100	0.01500	Yes	1
71 1 30 100 38 0.17 0.22 0.00880 0.01100 0.01500 No 0 72 1 30 490 100 0.10 0.11 0.00075 0.0080 0.00120 Yes 1 73 1 30 490 77 0.10 0.12 0.00075 0.0080 0.00120 Yes 1 74 1 30 490 69 0.11 0.13 0.0075 0.0080 0.00120 Yes 1 75 1 30 490 62 0.12 0.14 0.00075 0.0080 0.00120 Yes 1 76 1 30 490 54 0.13 0.15 0.00075 0.0080 0.00120 Yes 1 77 1 30 490 46 0.14 0.20 0.00075 0.0080 0.00120 Yes 1 78 1 30 490 62 0.12 0.14 0.00075 0.0080 0.00120 Yes 1	70	1	31	100	33	0.20	0.27	0.00880	0.01100	0.01500	Yes	1
72 1 30 490 100 0.10 0.11 0.00075 0.00080 0.00120 Yes 1 73 1 30 490 77 0.10 0.12 0.00075 0.00080 0.00120 Yes 1 74 1 30 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 75 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 76 1 30 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 77 1 30 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 78 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 79 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1	71	1	30	100	38	0.17	0.22	0.00880	0.01100	0.01500	No	0
73130490770.100.120.000750.000800.00120Yes174130490690.110.130.000750.000800.00120Yes175130490620.120.140.000750.000800.00120Yes176130490540.130.150.000750.000800.00120Yes177130490460.140.200.000750.000800.00120Yes178130490620.120.140.000750.000800.00120Yes179130490620.120.140.000750.000800.00120Yes180130490620.120.140.000750.000800.00120Yes181130490690.110.130.000750.000800.00120Yes181130490770.100.120.000750.000800.00120Yes182150490540.130.150.000750.000800.00120Yes183150490620.120.140.000750.000800.00120Yes184150490690.110.130.000750.00080<	72	1	30	490	100	0.10	0.11	0.00075	0.00080	0.00120	Yes	1
74130490690.110.130.000750.000800.00120Yes175130490620.120.140.000750.000800.00120Yes176130490540.130.150.000750.000800.00120Yes177130490460.140.200.000750.000800.00120Yes178130490620.520.570.000750.000800.00120Yes179130490620.120.140.000750.000800.00120Yes180130490620.120.140.000750.000800.00120Yes181130490620.120.140.000750.000800.00120Yes181130490540.130.150.000750.000800.00120Yes181130490540.130.150.000750.000800.00120Yes182150490540.130.150.000750.000800.00120Yes183150490620.120.140.000750.000800.00120Yes184150490690.110.130.000750.00080<	73	1	30	490	77	0.10	0.12	0.00075	0.00080	0.00120	Yes	1
75130490620.120.140.000750.000800.00120Yes176130490540.130.150.000750.000800.00120Yes177130490460.140.200.000750.000800.00120Yes178130490230.520.570.000750.000800.00120Yes179130490620.120.140.000750.000800.00120Yes180130490690.110.130.000750.000800.00120Yes181130490540.130.150.000750.000800.00120Yes182150490540.130.150.000750.000800.00120Yes183150490620.120.140.000750.000800.00120Yes184150490620.120.140.000750.000800.00120Yes184150490690.110.130.000750.000800.00120Yes185160490460.140.200.000750.000800.00120Yes1	74	1	30	490	69	0.11	0.13	0.00075	0.00080	0.00120	Yes	1
76130490540.130.150.000750.000800.00120Yes177130490460.140.200.000750.000800.00120Yes178130490230.520.570.000750.000800.00120Yes179130490620.120.140.000750.000800.00120Yes180130490690.110.130.000750.000800.00120Yes181130490770.100.120.000750.000800.00120Yes182150490540.130.150.000750.000800.00120Yes183150490620.120.140.000750.000800.00120Yes184150490690.110.130.000750.000800.00120Yes184150490690.110.130.000750.000800.00120Yes185160490460.140.200.000750.000800.00120Yes1	75	1	30	490	62	0.12	0.14	0.00075	0.00080	0.00120	Yes	1
77130490460.140.200.000750.000800.00120Yes178130490230.520.570.000750.000800.00120Yes179130490620.120.140.000750.000800.00120Yes180130490690.110.130.000750.000800.00120Yes181130490770.100.120.000750.000800.00120Yes182150490540.130.150.000750.000800.00120Yes183150490620.120.140.000750.000800.00120Yes184150490690.110.130.000750.000800.00120Yes185160490460.140.200.000750.000800.00120Yes1	76	1	30	490	54	0.13	0.15	0.00075	0.00080	0.00120	Yes	1
78 1 30 490 23 0.52 0.57 0.00075 0.00080 0.00120 Yes 1 79 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 80 1 30 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 81 1 30 490 77 0.10 0.12 0.00075 0.00080 0.00120 Yes 1 82 1 50 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1	77	1	30	490	46	0.14	0.20	0.00075	0.00080	0.00120	Yes	1
79 1 30 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 80 1 30 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 81 1 30 490 77 0.10 0.12 0.00075 0.00080 0.00120 Yes 1 82 1 50 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.20 0.00075 0.00080 0.00120 Yes 1	78	1	30	490	23	0.52	0.57	0.00075	0.00080	0.00120	Yes	1
80 1 30 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 81 1 30 490 77 0.10 0.12 0.00075 0.00080 0.00120 Yes 1 82 1 50 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	79	1	30	490	62	0.12	0.14	0.00075	0.00080	0.00120	Yes	1
81 1 30 490 77 0.10 0.12 0.00075 0.00080 0.00120 Yes 1 82 1 50 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	80	1	30	490	69	0.11	0.13	0.00075	0.00080	0.00120	Yes	1
82 1 50 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1 83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	81	1	30	490	77	0.10	0.12	0.00075	0.00080	0.00120	Yes	1
83 1 50 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1 84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	82	1	50	490	54	0.13	0.15	0.00075	0.00080	0.00120	Yes	1
84 1 50 490 69 0.11 0.13 0.00075 0.00080 0.00120 Yes 1 85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	83	1	50	490	62	0.12	0.14	0.00075	0.00080	0.00120	Yes	1
85 1 60 490 46 0.14 0.20 0.00075 0.00080 0.00120 Yes 1	84	1	50	490	69	0.11	0.13	0.00075	0.00080	0.00120	Yes	1
	85	1	60	490	46	0.14	0.20	0.00075	0.00080	0.00120	Yes	1
86 1 60 490 54 0.13 0.15 0.00075 0.00080 0.00120 Yes 1	86	1	60	490	54	0.13	0.15	0.00075	0.00080	0.00120	Yes	1
87 1 60 490 62 0.12 0.14 0.00075 0.00080 0.00120 Yes 1	87	1	60	490	62	0.12	0.14	0.00075	0.00080	0.00120	Yes	1

For obtaining the best performance in the learning phase, tangent-sigmoid (Orbani and Fajdiga 2003) and logistic sigmoid (Sakellariou and Ferentinou 2005) transfer functions are used in the hidden and output layers, respectively. A shortened version of the ANN code prepared in Matlab is given in "Appendix".

Performance assessment of ANN model and comparison with existing methods

The accuracy of the ANN model is examined by comparing the model predictions with the groutability results obtained in the experimental programs (Table 1). These results are

Table 2 The range of ANN model input and output parameters

ANN parameters	Minimum	Maximum	
Input parameters	Output parameter	value	value
w/c		0.8	6.0
$D_{\rm r}$ (%)		27	80
Pressure, P (kPa)		50	690
Finer content, FC (%)		1	100
D_{15}/d_{85}		10	762
	Groutability	0	1



Fig. 4 ANN model performance on groutability prediction

also summarized in Fig. 4 for all data, including the training, testing and validation data sets. It can be seen that, overall, the ANN model correctly predicted the groutability for 83 of the 87 cases. For the validation data set (17 cases), all the ANN predictions were successful. Note that the validation data set can be regarded as the real test for the performance of the model, because it is used for applying the trained algorithm to a separate dataset which has not been introduced to the network previously (Hanna et al. 2007). In general, the results shown in Table 1 and Fig. 4 indicate the significant potential of the proposed ANN model in successfully predicting the groutability of granular soils by cement grouts.

The overall comparison of the performance of the ANN model with that of the commonly-used empirical methods for estimating groutability is shown in Table 3. Note that the number of cases that could be considered by each empirical model varies, as no definite groutability prediction can be performed for borderline situations. For example, with case number 23, using the Burwell (1958) method, the numerical value of N obtained by Eq. 1 is greater than 25, which means that Eq. 2 should subsequently be applied. As the value given by Eq. 2 is ten, the method requires that in situ tests should be performed to determine if the soil is groutable with cement-based grouts. In addition, the performance of the Akbulut and Saglamer (2002) method is assessed twice, using all the data and a subset of it. As this method was originally developed using 38 of the cases in Table 1, to avoid any bias a separate performance analysis should be performed excluding these data, as given in Table 3.

The Burwell (1958) and Akbulut and Saglamer (2002) methods have high success rates exceeding 90%. However, the Burwell (1958) method could only give predictions for 62% of the cases and the success rate of the Akbulut and Saglamer (2002) method was only 86% when the 38 cases used to develop the model are excluded from the analysis. As seen in Table 3, the highest ratio of successful predictions to the total number of case records considered (95.4%) is obtained by the ANN model.

Summary and conclusions

In this study, an ANN model was developed to predict the groutability of granular soils using cement-based grouts. A total of 87 laboratory case records were used to develop, test and validate the model. Sixteen of these experiments were specifically performed for this study. The proposed model uses w/c, D_r , P, FC, and $(D_{15})_{\text{base soil}}/(d_{85})_{\text{cement grout}}$ as input parameters.

The results obtained using the proposed ANN model compared very well with the groutability results determined experimentally. For 95% of the cases in the

Table 3 Comparison of the
performance of groutability
prediction methods

Method	Case records	Correct predictions	Success rate (%)
DeBeer (1970)	87	51	58.6
Burwell (1958), Mitchell (1981)	54	50	92.6
Incecik and Ceren (1995)	86	64	74.4
Akbulut and Saglamer (2002): all data	85	77	90.6
Akbulut and Saglamer (2002): excluding own data	49	43	86.0
ANN model (all data)	87	83	95.4
ANN model (verification set)	17	17	100

compiled database, the model correctly predicted the groutability result, with no error for the validation data set. Furthermore, a comparison of the performance of the ANN model with the results using empirical methods from the literature indicated the relative superiority of the proposed ANN model.

It is concluded that the proposed ANN model provides a viable groutability assessment tool that can assist the geo-professionals in making accurate and reliable predictions.

Appendix

Matlab 7.8.0 source code for ANN

clear all % clear all data

 $p = [...]; \%5 \times 87 \text{ sized input matrix (not shown)}$ $t = [...]; \%1 \times 87 \text{ sized target matrix (not shown)}$ % input layer: 5 neurons % hidden layer: 15 neurons % output layer: 1 neuron net = newff(p, t, [15,1], {'tansig','logsig'},'trainlm'); net.trainParam.epochs = 10000; net.trainParam.mu = 1; net.trainParam.mu_dec = 0.8; net.trainParam.mu_inc = 1.5; net = train(net, p, t); Y = sim(net, p);

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