### **ORIGINAL PAPER**



# **Role of electrode temperature in anodic growth of sulfuric acid alumina flms**

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#### **Abstract**

Studies of the self-organized growth of nanoporous anodic aluminum oxide (AAO) flms and anodization parameters have been the subject of decades of research and various theories. At the same time, temperature, being one of the most important parameters in anodizing treatments of aluminum, has been investigated only as a function of electrolyte temperature. This paper presents the results of studying the growth kinetics and morphology of AAO formed by anodization processes in 1 M  $H_2SO_4$  at different anode temperatures. The activation energy of ionic conductivity for AAO determined in this study was 0.41 eV for sulfuric acid, which was greater than the activation energy of 0.34 eV for oxalic acid. The efect of anode temperature on the pore diameter ( $d_{\text{pore}}$ ) and the interpore distance ( $D_{\text{inter}}$ ) was studied. It was demonstrated that in the temperature range from 10 to 40 °C, the  $d_{pore}$  and  $D_{inter}$  did not change with the anode temperature, with values equal to  $12.5\pm0.1$  nm and  $52.5\pm0.2$  nm, respectively. However, when the anode (aluminum) temperature was increased to 60 °C, the  $d_{\text{more}}$  increased to 16 nm. The results obtained show that by increasing the temperature of the anode from 20 to 40 °C, it is possible to increase the ionic conductivity of AAO and thus achieve a greater than threefold increase in the the rate of AAO growth, without altering the porous morphology of the anodic flms.

**Keywords** Anodic alumina · Sulfuric acid · Electrode temperature · Ionic conductivity · Activation energy

### **Introduction**

Anodic aluminum oxide (AAO) is widely used for the production of nanoporous membranes with high structural perfection. The possibility of obtaining an ordered porous structure has driven the growth in the use of AAO for fabrication of nanostructures used in electronic, magnetic, and photonic devices and in various radioelectronics products  $[1–5]$  $[1–5]$ . The technology for producing nanoporous AAO is characterized by a high degree of control over its properties through appropriate selection of anodization parameters including composition and electrolyte temperature, anodizing voltage, current density, and anodization time [[6–](#page-6-1)[8\]](#page-6-2). The parameters of the porous structure of anodic flms, such as

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<sup>2</sup> Belarussian State University of Informatics and Radioelectronics, P.Brovki 6, 220013 Minsk, Belarus pore diameter and interpore distance, can be controlled by varying the anodizing voltage [[9](#page-6-3), [10](#page-6-4)].

A critical parameter, in addition to anodizing voltage, that allows us to achieve control over the porous structure of AAO flms is temperature [[11](#page-6-5), [12](#page-6-6)]. For example, an increase in electrolyte temperature has a noticeable effect on both the rate of aluminum anodization and the increase in the surface microrelief of porous anodic oxide flms.

The infuence of electrolyte temperature has been studied in many works [\[13](#page-6-7)–[17\]](#page-6-8). However, the infuence of another important parameter—anode (aluminum) temperature—on the growth of porous AAO is still poorly investigated. The results of such studies are of great value, since they provide information about the ion transfer processes in AAO. This is because the mass transfer caused by migration of  $Al^{3+}$ cations and  $O^{2-}$  anions under the effect of an electric field has a noticeable efect on the growth rate of AAO.

In order to provide precise temperature control for this kind of experiment, a thermoelectric Peltier device can be used. In [\[18](#page-6-9)], the infuence of the aluminum substrate temperature was investigated with respect to the porous structure and thickness of anodic flms formed in oxalic acid at a

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constant voltage. The results obtained using a solution-fow type microdroplet cell design showed that the pore diameter of AAO for anodized strips increased with increasing substrate temperature. In this case, the interpore distance in anodic flms did not change. These results, however, have limited application due to the small volume of electrolyte used in the design of a solution-fow-type microdroplet cell for anodizing aluminum. In [\[19\]](#page-6-10), the aluminum substrate temperature was controlled in the temperature range of 5–65 °C using a thermoelectric Peltier device. Porous AAO was formed at constant current in an aqueous solution of sulfuric acid with the addition of  $Al_2(SO_4)_3$ . However, the choice of aluminum anodizing modes at constant current does not allow one to evaluate the efect of the substrate temperature on the morphology of anodic flms, which limits the value of such results.

We have previously studied the effect of anode temperature on the formation of porous AAO in oxalic acid [[20](#page-6-11)]. The results confrmed that in order to obtain high growth rates while maintaining the quality and microstructure of the formed anodic flms, a higher anode temperature can be used for the aluminum anodization process. The purpose of the present work was to study the efect of anode temperature on the growth rate and microstructure of porous AAO (interpore distance and pore diameter) and to determine the nature of ionic conductivity in AAO in the case of anodization of aluminum in sulfuric acid.

### **Experimental**

High-purity aluminum foils (99.999% Al, Alfa Aesar) with thickness of 25 and 100 μm were used as starting material. Analytical-grade chemicals and distilled water were employed for the preparation of all experimental solutions.

The aluminum samples were frst degreased in acetone. They were then pretreated in a hot solution of 1.5 M NaOH for 15 s, neutralized in 1.5 M HNO<sub>3</sub> for 2 min, and carefully rinsed in distilled water and dried with warm air.

AAO was formed by two-stage anodization of 25-μm-thick aluminum foil in 1.0 M sulfuric acid at an electrolyte temperature of 20 °C and voltage of 20 V. The frst anodization was carried out on both sides of the samples at 20 V and at an electrolyte temperature of 20 °C for 30 min. After this operation, the porous  $Al_2O_3$  layer was completely removed by dissolving it in a mixture of  $H_3PO_4 + CrO_3$  at 75 °C for 2 h. The second anodization was carried out at a constant electrolyte temperature of 20 °C and anode temperature ranging from 5 to 70 °C until the aluminum was completely oxidized. The design of the electrochemical cell that was used is described in detail in our previous works [\[20](#page-6-11), [21](#page-6-12)]. A polytetrafuoroethylene (PTFE) electrochemical cell, consisting of two main parts, was used to study the temperature effects and to control the anodization processes. The frst part included an electrochemical cell with a tank for the electrolyte, and with a heat exchanger and electrolyte temperature control. The aluminum substrate under study was placed at the bottom, on the base of the electrochemical cell. The second part contained a heating module. A thermoelectric Peltier device was used to control the aluminum substrate temperature. The electrolyte temperature was kept constant using a cryostat and electrolyte stirring. It is known that the thermal conductivity of aluminum changes from 236 to 238 W/(K·m) when the temperature rises from 0 to 70 °C. On the other hand, the thermal conductivity of porous oxide layers obtained in a sulfuric acid solution stays in the range from 1.0 to 0.5  $W/(K \cdot m)$  when the temperature increases from 0 to 40  $\degree$ C [\[22](#page-6-13), [23](#page-6-14)], which is close to that of sulfuric acid solution (from 0.316 to 0.584 W/[K·m] for temperatures from 5 to 70 °C, respectively) [\[24](#page-6-15)]. The thermal resistance of aluminum oxide resulted in temperature gradients between the electrolyte and the aluminum. The temperature gradient, therefore, is mainly concentrated in the oxide layer. The value of this gradient depended on the heating power of the aluminum substrate, which was set by the thermoelectric Peltier device.

Single-sided anodization was carried out on an aluminum surface area of  $2.54 \text{ cm}^2$  using a platinum cathode. A Voltcraft (Germany) DC power supply (40 V/5 A) was used for the anodization process. Transient currents during anodizing were measured and recorded on a computer in real time using a UNI-T UT71E digital multimeter with a data sampling rate of 60 points/min. After anodization, porous AAO flms were thoroughly washed with distilled water and dried with warm air.

The nanoporous morphology of anodic flms obtained at diferent anode temperatures was studied by scanning electron microscopy (SEM) using a LEO DSM 982 instrument (Germany). The pore size and interpore distance were determined from SEM images of the surface morphology of anodic flms using ImageJ software.

### **Results and discussion**

#### **Efect of anode temperature on transient currents**

Figure [1](#page-2-0) shows a plot of the anodic current density versus Al anodization time for the range of anode temperature from 5 to 60 °C. Three stages of growth of anodic  $Al_2O_3$ can be distinguished. The frst stage lasts about 1 min and is associated with a sharp increase in current density until a stationary value is reached. For anode temperatures up to 40 °C, the current curves reveal a clearly defned plateau



<span id="page-2-0"></span>**Fig. 1** Current transients for porous anodic alumina formation at different anode temperatures of 10–60 °C in a 1.0 M sulfuric acid solution  $(20 °C)$ 

(second stage), which is associated with the stationary growth of AAO.

With an increase in anode temperature from 10 to 60 °C, the anodic current density in the second stage increases by approximately one order of magnitude (from 9 to 95 mA $\cdot$ cm<sup>-2</sup>), with a decrease in the duration of this stage. When the anode temperature is above 50 °C, the process accelerates and the aluminum foil is anodized in less than 5 min, and therefore no plateau is observed. For this reason, studies with anode temperatures of 60 and 70 °C were additionally repeated with aluminum foil of greater thickness.

It is worth mentioning that due to the presence of slight irregularities in the thickness, there are separate, thicker areas on aluminum foil that take longer to anodize. This results in a gradual decrease in the detected current during the third stage due to the progressively decreasing surface area of the aluminum at the fnal stage of the anodization process. The time for complete anodization of aluminum foil (the end of the third stage) is decreased 5.5-fold with an increase in anode temperature from 10 to 60 °C.

It is also important to evaluate the electrical power required for anodization of aluminum. Specifcally, for complete anodization of aluminum with an area of  $1 \text{ cm}^2$ :

$$
\int_{0}^{t} J(t)dt, \mathbf{C} \cdot \mathbf{cm}^{-2}
$$
 (1)

where *j* is anodic current density and *t* is the time of complete anodization of aluminum. The electrical power is defned as the area under the *J*–*t* curve in Fig. [1](#page-2-0). It is observed that *Q* passes through a maximum of about 50 C·cm<sup>-2</sup> in the anode temperature range of [2](#page-2-1)0–30 °C (Fig. 2).



<span id="page-2-1"></span>Fig. 2 The effect of anode temperature on specific quantity of electricity of oxide layer

According to Faraday's law of electrolysis, one can expect that oxidation of samples with equal amounts of aluminum would consume the same amount of electricity. Therefore, the higher values of Q at temperatures below 40 °C indicate that in addition to aluminum oxidation, a competitive reaction occurs. The most frequently discussed competing reaction during anodization is the oxygen evolution reaction [[25](#page-6-16)]. Release of oxygen takes place according to the following reaction:

$$
2H_2O \to O_2 + 4H^+ + 4e^-
$$
 (2)

This is unlikely during anodization of high-purity aluminum because electron transfer from the flm/electrolyte interface to the metal through the high-resistance barrier layer is negligible  $[26]$ . On the other hand, at sufficiently high electric fields,  $O^{2-}$  ions of aluminum oxide can provide an alternative source of oxygen:

$$
20^{2-} \to O_2 + 4e^-
$$
 (3)

This reaction occurs at the metal/oxide interface and is more likely when metal impurities are present in anodizing aluminum or in the case of aluminum alloys [[26](#page-6-17), [27](#page-6-18)]. The reaction of oxygen release, however, has been proven to occur with pure aluminum as well, and is the basis of the oxygen bubble model for the formation of pores in AAO [[28,](#page-6-19) [29\]](#page-6-20).

It is also well known that high temperature favors the transfer of  $Al^{3+}$  to the oxide/electrolyte interface, and the

anodization rate increases [[30](#page-6-21)]. When the temperature of the aluminum substrate is higher than 40 °C, as will be shown later in the paper,  $Al^{3+}$  ions will form at a higher rate than the rate of AAO growth. As a result, the oxygen released at the electrolyte/oxide interface will interact with  $Al^{3+}$  ions on the surface to form aluminum oxide. Therefore, for the electrochemical oxidation of aluminum in this case, a smaller quantity of electricity (Q) will be needed. This explains the decrease in  $Q$  at higher temperatures, where the efficiency of the anodization process approaches 100%.

## **Efect of anode temperature on ionic**  conductivity of anodic Al<sub>2</sub>O<sub>3</sub>

Figure [3](#page-3-0) shows anodic current density  $(J_a)$  versus anode temperature  $(T_{\text{anode}})$  plots for stage II. As can be seen, with increasing anode temperature, anodic current density increases exponentially. It is worth mentioning that anodic current during aluminum anodization is almost entirely ionic current. The conductivity of AAO in this case is, therefore, ionic in nature. The result of ion transfer under the effect of a strong electric field in anodic oxide,  $O^{2-}$  anions to the Al<sub>2</sub>O<sub>3</sub>/Al interface and Al<sup>3+</sup> cations to the electrolyte/Al<sub>2</sub>O<sub>3</sub> interface is the formation of new layers of aluminum oxide at these boundaries. Consequently, the electrochemical characteristics of such systems are determined primarily by the characteristics of ion transport. The temperature dependence of ionic conductivity has an Arrhenius character and is described by the following formula [[31\]](#page-6-22):



<span id="page-3-0"></span>**Fig. 3** The average current density during aluminum steady-state anodization at an electrolyte temperature of 20  $^{\circ}$ C in 1.0 M H<sub>2</sub>SO<sub>4</sub> and in 0.4 M oxalic acid at 20 and 40 V, respectively, as a function of anode temperature

<span id="page-3-1"></span>
$$
\sigma = \frac{\sigma_0}{T} \exp\left(-\frac{E_a}{kT}\right) \tag{4}
$$

where  $\sigma$  is ionic conductivity,  $E_a$  is the activation energy of ionic conductivity, *T* is the absolute temperature, and  $\sigma_0$  is a constant.

The electrical conductivity of dielectrics depends on their chemical composition and structure and is determined by the migration of ions. The electrical conductivity of the dielectric σ is given by the expression

$$
\sigma = c q \mu \tag{5}
$$

where  $c$  is the concentration of mobile ions,  $q$  is the ionic charge, and *μ* is the ion mobility. The concentration *c* and mobility  $\mu$  of ions depend on the temperature. Consequently, the electrical conductivity  $\sigma$  of the dielectric is a function of temperature. In general, the current density  $J_a$  is related to the conductivity  $\sigma$  in the dielectric by the following equation:

$$
J_a = \sigma E \tag{6}
$$

In the case of porous anodization of aluminum in potentiostatic mode, the electric feld strength in the barrier layer of AAO remains constant. Therefore, it is possible to use the ionic current density  $J_a$  instead of conductivity  $\sigma$  in Eq. ([4](#page-3-1)).

Plotted in Arrhenius coordinates, the ionic conductivity versus temperature curve has the form of a straight line (Fig. [4\)](#page-3-2). The activation energy for ionic conductivity calculated for AAO formed in sulfuric acid is 0.41 eV. This value is in good agreement with the activation energy of 0.48 eV, which was obtained in [\[32](#page-6-23)] from the results of direct electrical measurements for AAO formed in sulfuric acid.



<span id="page-3-2"></span>**Fig. 4** Ionic conductivity of anodic aluminum oxide vs. anode temperature plotted in Arrhenius coordinates for sulfuric and oxalic acid

It is important to compare the results obtained for sulfuric acid with the same parameters for Al anodization in oxalic acid using the data from [\[20](#page-6-11)]. As can be seen in Fig. [4,](#page-3-2) the ionic conductivity versus temperature plot in Arrhenius coordinates has the same form. According to the graph, the activation energy of ionic conductivity for AAO in oxalic acid is 0.34 eV.

It is known that the activation energy of ionic conductivity for polycrystalline and amorphous dielectrics increases with deviations from stoichiometry. This is explained by the peculiarity of ion migration in a dielectric in the presence of defects such as impurities. Due to their small radii, the cations are more mobile than the anions. The incorporation of anionic impurities with a radius larger than the radius of oxygen ions into the structure of AAO leads to a change in the potential interaction energy of cations and, as a consequence, to an increase in the activation energy of ionic conductivity. The lower activation energy of ionic conductivity in the case of oxalic acid relative to sulfuric acid may indicate that the composition of AAO obtained in oxalic acid contains a smaller amount of electrolyte anion residues (impurities).

This is in good agreement with the data on the percentage of anions incorporated into the porous oxide layer of  $Al_2O_3$  for sulfuric acid (10–13%) and oxalic acid  $(2-3\%)$  [\[33](#page-6-24)]. It is also evidenced by the formulas calculated in [[34](#page-6-25)] for the composition of AAO, taking into account the following content of impurities: for sulfuric acid,  $(Al_2O_{2.77})_{100}(SO_4)_{19}(OH)_{8}$  39H<sub>2</sub>O; for oxalic acid,  $\text{(Al}_2\text{O}_{2.92}\text{)}_{100}\text{(C}_2\text{O}_4)\text{_6}\text{(OH)}_4\text{ }26\text{H}_2\text{O}.$ 

### Surface morphology of porous anodic Al<sub>2</sub>O<sub>3</sub> **with diferent anode temperatures**

SEM images of the surface morphology of the porous AAO films formed in the anode temperature range of  $10-60$  °C are shown in Fig. [5](#page-4-0).

The SEM data show  $d_{\text{pore}}$  and  $D_{\text{inter}}$  values of  $12.5 \pm 0.1$  nm and  $52.5 \pm 0.2$  nm, respectively, which were found to be independent of anode temperature in the range from 10 to 40 °C. When the anode temperature increased from 50 to 60 °C, a decrease in the interpore distance from



<span id="page-4-1"></span>**Fig. 6** Variation in the average pore diameter and average interpore distance of self-ordered anodic alumina obtained by anodization in 1.0 M sulfuric acid (20 °C) at 20 V as a function of anode temperature

<span id="page-4-0"></span>**Fig. 5** SEM images of surface morphology of self-ordering of anodic alumina formed at different anode temperatures of (a) 10 °C, (b) 20 °C, (c) 30 °C, (d) 40 °C, (e) 50 °C, and (f) 60 °C at 20 V, in 1.0 M sulfuric acid solution  $(20 °C)$ 





<span id="page-5-1"></span>**Fig. 7** Change in the thickness reduction rate of aluminum and in the rate of anodic aluminum oxide growth with anode temperature

51.8 nm (50 °C) to 43.5 nm (60 °C) was observed (Fig. [6\)](#page-4-1). In this case, the pore diameter increased from 12.5 nm (40 °C) to 16.2 and 15.8 nm (50 and 60  $\degree$ C, respectively).

It is important to consider the nature of the change in the proportionality coefficient  $(D<sub>inter</sub>/U)$  for anodic films with anode temperatures of 50 and 60 °C. Data from the analysis show that the value of the proportionality coefficient  $(D<sub>inter</sub>/U)$  decreases from 2.59 to 2.18 when the anode temperature increases from 50 to 60 °C. In accordance with  $[25]$ , this indicates a decrease in mechanical stress in the anodic oxide flm with an anode temperature of 60 °C. In turn, a decrease in mechanical stress should lead to an increase in the porosity of the AAO flm in order to maintain a balance in the stress–strain state of the  $A1-A1_2O_3$  system. The changes in the pore diameter are plotted in Fig. [6](#page-4-1) to confrm this result.

Figure [7](#page-5-1) presents a graph showing the rate of thickness reduction of aluminum (according to Fig. [1;](#page-2-0) the duration of anodization corresponds to the plateau stage of anodic current) and the rate of AAO (AAO) growth (according to Fig. [1;](#page-2-0) the duration of  $Al_2O_3$  formation corresponds to the stage of anodic current until it completely declines) as a function of anode temperature. The behavior of the two lines is in good agreement up to a temperature of 40 °C. However, at higher temperatures, a dramatic divergence in their behavior is observed, which may be due to chemical dissolution.

As can be seen from the graph in Fig. [7](#page-5-1), the thickness reduction rate for aluminum is clearly divided into two different stages. As the anode temperature increases from 20 to 40 °C, a gradual increase in the thickness reduction rate for aluminum is observed (frst stage), while the porous structure of the formed anodic flms remains unchanged. When the anode temperature increases above 40  $\degree$ C, a sharp increase in the rate of thickness reduction is observed (second stage), which is accompanied by a change in the porous structure of the anodic flms (Fig. [6\)](#page-4-1). The data for the frst stage show that by increasing the temperature of the anode, it is possible to increase the rate of ionic transfer in AAO, achieving a greater than threefold increase in the rate of AAO growth with an increase in temperature from 20 to 40 °C, without altering the porosity morphology of the anodic flms.

### **Conclusions**

The growth kinetics and surface morphology of AAO were studied for anodization processes in 1 M  $H_2SO_4$  at different anode temperatures. To determine the ionic conductivity as a function of temperature, it was proposed to consider that ionic conductivity is directly proportional to ionic current. A plot of ionic conductivity versus anode (aluminum) temperature in Arrhenius coordinates exhibited a straight line. According to the results, the activation energy of ionic conductivity of AAO for sulfuric acid was 0.41 eV, which was greater than that of 0.34 eV for oxalic acid. The higher activation energy for sulfuric acid in this case was explained by a large deviation from stoichiometry for AAO due to the introduction of anionic impurities in the electrolyte.

The effect of anode temperature on the pore diameter  $(d_{\text{pore}})$  and the interpore distance  $(D_{\text{inter}})$  was also investigated. It was demonstrated that in the temperature range from 10 to 40 °C, the  $d_{\text{pore}}$  and  $D_{\text{inter}}$  did not change with anode temperature, exhibiting values equal to  $12.5 \pm 0.1$  nm and  $52.5 \pm 0.2$  nm, respectively. When the anode temperature (aluminum) increased to 60 °C,  $d_{\text{pore}}$  increased to 16 nm.

These results show that by increasing the temperature of the anode (aluminum) from 20 to 40  $^{\circ}$ C, it is possible to increase the ionic conductivity of AAO and thus achieve a greater than threefold increase in the rate of AAO growth, without altering the porous morphology of the anodic flms.

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