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Underwater acoustic positioning based on the robust zero‑diference Kalman flter

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Abstract

The accuracy of underwater acoustic positioning is greatly infuenced by both systematic error and gross error. Aiming at these problems, the paper proposes a robust zero-diference Kalman flter based on the random walk model and the equivalent gain matrix. The proposed algorithm takes systematic error as a random walk process, and estimates it together with the position parameters by using zero-diference Kalman flter. In addition, the equivalent gain matrix based on the robust estimation of Huber function is constructed to resist the infuence of gross error. The proposed algorithm is verifed by the simulation experiment and a real one for underwater acoustic positioning. The results demonstrate that the robust zerodiference Kalman flter can control both the efects of systematic error and gross error without amplifying the infuence of the observation random noise, which is obviously superior to the zero-diference least squares (LS), the single-diference LS and zero-diference Kalman flter in underwater acoustic positioning.

Keywords Systematic error · Gross error · Kalman flter · Zero-diference positioning · Robust estimation

1 Introduction

With the development of the national marine strategy and the marine resource exploration, accurate ocean navigation and positioning technology are needed to obtain the highprecision, large-scale marine environmental information [\[1–](#page-15-0)[3\]](#page-15-1). Sound waves, rather than electromagnetic waves or light waves, are mainly used to estimate the position of the underwater target. The reason is that sound waves can spread hundreds of kilometers in the water while electromagnetic waves and light waves decay quickly [[4](#page-15-2)]. The classical acoustic-based approaches for underwater target positioning include long baseline (LBL), short baseline (SBL), ultrashort baseline (USBL) and underwater global positioning system (GPS) according to the acoustic baseline range [[5,](#page-15-3) [6](#page-15-4)]. The shipborne acoustic positioning generally adopts the voyage positioning mode, which is afected by the geometric

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structure of trajectory and the measurement error related to the time delay as well as the sound speed [\[7](#page-15-5), [8](#page-15-6)].

For underwater acoustic positioning, there inevitably exist the gross error, the random error and the systematic error caused by the marine environment and the observation instrument. Many studies have been dedicated to improve the underwater positioning model and the error correction method. Xu et al. [[9](#page-15-7)] first proposed the underwater difference positioning algorithm including the single diference algorithm between the observation epochs and the double diference algorithm which can greatly improve the accuracy of seafloor deformation measurement. Zhao et al. [[10\]](#page-15-8) proposed a ship-board difference positioning method based on selecting weight iteration. Although the diference positioning algorithm can weaken the efects of the systematic errors, it enlarges the infuence of random errors, which decreases the accuracy of the underwater acoustic positioning. Aiming at the time delay error, a positioning model considering the apparent time delay error as unknown parameter is proposed [\[11](#page-15-9)]. Yan et al. [[12\]](#page-15-10) proposed a long baseline positioning algorithm for moving buoy by estimating the uncertain sound speed as an unknown parameter. However, even though the time delay error or the unknown sound speed is estimated as a fxed systematic parameter, it is hard to be accurately estimated since it changes with the

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change of the marine environment. In the global navigation satellite system (GNSS) positioning, Paziewski and Wielgosz [[13](#page-15-11)] used the random walk model to estimate the intersystem biases as the unknown parameters, which inspires us to apply this method to estimate the systematic error in underwater acoustic positioning. As for gross errors, Zhou [\[14\]](#page-15-12) proposed the IGG robust estimation method based on the equivalence weight. On this basis, Yang et al. [\[15](#page-15-13)] developed the bi-factor equivalence weight based on the robust estimation for correlation observation. Xu et al. [\[16\]](#page-15-14) proposed a robust estimation method based on the symbol constraint. Wang et al. [[17\]](#page-15-15) proposed a robust extended Kalman flter using W-test statistics based on fltering residuals to eliminate the efect of gross errors on GNSS navigation solutions. Yang et al. [[18](#page-15-16)] proposed the robust M–M unscented Kalman fltering for GPS/IMU navigation. The applications of the robust estimation in GPS navigation and positioning have been widely adopted and tested [[19\]](#page-15-17). Wang et al. [\[20\]](#page-15-18) proposed an adaptive robust unscented Kalman filter for autonomous underwater vehicle (AUV) acoustic navigation, which constructs the judgment factor and adaptive factor by the prediction residual to balance the contribution between the observation information and AUV motion state information.

The zero-diference (ZD) least squares (LS) is rarely adopted for the high precision underwater positioning due to the efects of systematic error as well as gross error. At the same time, the single-diference (SD) LS of adjacent epoch enlarges the infuence of random errors and even the gross errors while it suppresses the efects of systematic errors. To solve the aforementioned problems, this paper proposes a robust zero-diference Kalman flter based on the random walk model and the equivalent gain matrix to resist the efects of systematic errors and gross errors in underwater acoustic positioning. The proposed method involves a robust estimation method based on the prediction residual as well as the observation variance, and an improved KF with systematic error compensation, which has obvious diferences compared to the method of reference [[20](#page-15-18)].

The paper is organized as follows. We frstly present an improved zero-diference positioning function model as well as the zero-diference Kalman flter by estimating the systematic error as the random walk process in Sect. [2.](#page-1-0) Then Sect. [3](#page-3-0) introduces the theoretical derivation and algorithm implementation of the robust zero-diference Kalman flter. The robust zero-diference Kalman flter is verifed and analyzed by the simulation experiment and a real one for underwater acoustic positioning in Sect. [4](#page-4-0). Finally, we sum-marize the significant conclusions in Sect. [5.](#page-10-0)

2 Method

2.1 Zero‑diference positioning function model

The transducer under the survey ship can continuously send sound waves to the transponder to get the signal propagation time $[21]$ $[21]$ $[21]$; therefore, the range between the transducer and the transponder at the diferent time and position can be obtained by the travel time and the sound speed structure [[22\]](#page-15-20).

As shown in Fig. [1,](#page-1-1) assuming that the transducer at position \mathbf{X}_k and time t_k transmits an acoustic signal to the transponder to get the slant range ρ_k , the transponder coordinates can be obtained through the intersection positioning method, which can be regarded as a prototype of the underwater zerodiference positioning, since there are no diferential operations on observations between epochs and transponder stations. The observation model of underwater zero-diference positioning can be expressed as

$$
\rho_k = f(\mathbf{X}_k, \mathbf{X}_o) + \delta \rho_{d_k} + \delta \rho_{v_k} + \varepsilon_k, \tag{1}
$$

$$
f(\mathbf{X}_k, \mathbf{X}_o) = \sqrt{(x_k - x_o)^2 + (y_k - y_o)^2 + (z_k - z_o)^2},
$$
 (2)

$$
\rho_k = ct_k,\tag{3}
$$

where $X_{\rho} = (x_{\rho}, y_{\rho}, z_{\rho})$ is the unknown position vector of the transponder, and $\mathbf{X}_k = (x_k, y_k, z_k)$ is the position vector of

Sea bottom

Fig. 1 The geometric diagram of underwater zero-diference positioning

transducer under the ship, which can be directly calculated from the kinematic GNSS. $f(\mathbf{X}_k, \mathbf{X}_o)$ is the theoretical range between the transponder and the transducer. $\delta \rho_{d_k}$ is the systematic error due to the time delay in re-transmitting the received signal from the transponder back to the transducer, $\delta \rho_{v_k}$ is the systematic error due to the spatial and temporal variation in the sound speed structure, ε_k is the random ranging error. t_k is the travel time between the transducer and the transponder, and *c* is the sound speed.

In the actual underwater acoustic positioning, the sound speed error is afected by the ocean internal wave and has a periodic variation. In addition, the systematic error related to time delay for the same transponder is approximately equal [[23,](#page-15-21) [24\]](#page-15-22). Therefore, the systematic error related to the time delay and the sound speed can be estimated as an unknown parameter and the observation Eq. [1](#page-1-2) can be rewritten as

$$
\rho_k = f(\mathbf{X}_k, \mathbf{X}_o) + \delta \rho_k + \varepsilon_k,\tag{4}
$$

where $\delta \rho_k$ is the estimated parameter of the systematic error. Equation [4](#page-2-0) is linearized as

$$
\rho_k - f(\mathbf{X}_k, \mathbf{X}_o^0) - \delta \rho_k^0 = a_k d\mathbf{X}_o + d\delta \rho_k + \varepsilon_k + b_k \varepsilon_{\mathbf{X}_k},\qquad(5)
$$

where \mathbf{X}_{o}^{0} , $\delta \rho_{k}^{0}$ are approximate values for \mathbf{X}_{o} and $\delta \rho_{k}$. $d\mathbf{X}_{o}$ and $d\delta\rho_k$ are the unknown coordinate correction vector and the systematic error correction vector to be estimated with $\mathbf{X}_o = \mathbf{X}_o^0 + d\mathbf{X}_o$ and $\delta \rho_k = \delta \rho_k^0 + d\delta \rho_k$, respectively. a_k and b_k are the first-order partial derivatives with respect to \mathbf{X}_o and \mathbf{X}_k , respectively, and $\epsilon_{\mathbf{X}_k}$ is the random errors of the survey ship positions.

When combining all the measurements, the linear observation equation of underwater zero-diference positioning can be expressed as:

$$
\mathbf{Z} = \mathbf{H}d\mathbf{X}'_o + \mathbf{V},\tag{6}
$$

$$
\mathbf{H} = \begin{bmatrix} \frac{\partial f_1}{\partial x} & \frac{\partial f_1}{\partial y} & \frac{\partial f_1}{\partial z} & 1\\ \frac{\partial f_2}{\partial x} & \frac{\partial f_2}{\partial y} & \frac{\partial f_2}{\partial z} & 1\\ \frac{\partial f_3}{\partial x} & \frac{\partial f_3}{\partial y} & \frac{\partial f_3}{\partial z} & 1\\ \vdots & \vdots & \vdots & \vdots\\ \frac{\partial f_n}{\partial x} & \frac{\partial f_n}{\partial y} & \frac{\partial f_n}{\partial z} & 1 \end{bmatrix},
$$
\n(7)

$$
\mathbf{Z} = \begin{bmatrix} \rho_1 - f(\mathbf{X}_1, \mathbf{X}_0^0) - \delta \rho_1^0 \\ \rho_2 - f(\mathbf{X}_2, \mathbf{X}_0^0) - \delta \rho_2^0 \\ \rho_3 - f(\mathbf{X}_3, \mathbf{X}_0^0) - \delta \rho_3^0 \\ \vdots \\ \rho_n - f(\mathbf{X}_n, \mathbf{X}_0^0) - \delta \rho_n^0 \end{bmatrix},
$$
\n(8)

where $\mathbf{X}'_o = (x_o, y_o, z_o, \delta \rho_k)$, **Z** is the constant term, **H** is the coefficient matrix of observation equation, and **V** is the observation residual vector.

2.2 Zero‑diference Kalman flter

The observation and state equations using zero-diference Kalman filter for underwater acoustic positioning can be expressed as [\[25](#page-15-23)]:

$$
\mathbf{Z}_{k} = \mathbf{H}_{k} d\mathbf{X}'_{o,k} + \mathbf{V}_{k},
$$
\n(9)

$$
\mathbf{X'}_{o,k} = \mathbf{\varphi}_{k,k-1} \mathbf{X'}_{o,k-1} + \mathbf{\omega}_{k-1},\tag{10}
$$

where $\mathbf{X}'_{o,k} = (x_{o,k}, y_{o,k}, z_{o,k}, \delta \rho_k)$ denotes the estimated parameter vector of the transponder position and the systematic error at time t_k , \mathbf{Z}_k is the observation vector with covariance matrix \mathbf{R}_k , assumed to be white, \mathbf{H}_k is the coefficient matrix of observation equation and V_k is the observation residual vector. $\varphi_{k,k-1}$ is the state transition matrix from epoch t_{k-1} to t_k . $\mathbf{\omega}_{k-1}$ is the process noise vector with covariance matrix \mathbf{Q}_k , assumed to be white.

The discrete first-order Gauss–Markov process [\[26\]](#page-15-24) describes the epoch state changes of related parameters, and the mathematical expression is as follows:

$$
\begin{cases}\n\mathbf{X'}_{o,k} = e^{-\frac{\Delta t}{\tau}} \mathbf{X'}_{o,k-1} + \mathbf{\omega}_{k-1}, & \mathbf{\omega}_{k-1} = \int_{t_{k-1}}^{t_k} e^{-\frac{\Delta t}{\tau}} \mathbf{\omega} dt \\
E(\mathbf{\omega}_k \mathbf{\omega}_{k-1}) = \frac{1}{2} \tau (1 - e^{-\frac{2\Delta t}{\tau}}) \delta\n\end{cases}
$$
\n(11)

where $\Delta t = t_k - t_{k-1}$, τ is the time constant, and δ is Dirac function.

When $\tau \to \infty$, the state of Eq. [11](#page-2-1) is the random walk process

$$
\begin{cases}\n\mathbf{X'}_{o,k} = \mathbf{X'}_{o,k-1} + \mathbf{\omega}_{k-1} \\
E(\mathbf{\omega}_k \mathbf{\omega}_{k-1}) = \sigma_{\mathbf{w}}^2 \delta\n\end{cases} .
$$
\n(12)

When $\tau \to 0$, the state of Eq. [11](#page-2-1) is the white noise

$$
\begin{cases}\n\mathbf{X}'_{o,k} = \mathbf{\omega}_{k-1} \\
E(\mathbf{\omega}_k \mathbf{\omega}_{k-1}) = \sigma_{\mathbf{w}}^2 \delta\n\end{cases} (13)
$$

where σ_w^2 is the variance of the state parameters.

The unknown parameters of the zero-diference Kalman flter are the transponder position and the systematic error. Since the transponder position parameters are constants and the systematic error parameter changes regularly with time, the state transition matrix and the state noise matrix of Eq. [10](#page-2-2) are given by

$$
\mathbf{\varphi}_{k,k-1} = \mathbf{I}_{4\times 4},\tag{14}
$$

$$
\mathbf{Q}_{k} = \begin{bmatrix} 0 & & \\ & 0 & \\ & & \\ & & \sigma_{\omega_{\delta\rho}}^{2} \end{bmatrix},\tag{15}
$$

where $\mathbf{I}_{4\times4}$ is a unit array of four rows and four columns, and $\sigma_{\omega_{\delta\rho}}^2$ is the variance of the systematic error parameter.

The covariance propagation equation is given by

$$
\mathbf{P}_{k,k-1} = \mathbf{\varphi}_{k,k-1} \mathbf{P}_{k-1} \mathbf{\varphi}_{k,k-1}^T + \mathbf{Q}_{k-1}.
$$
 (16)

The solutions for the estimated state vector, the Kalman flter gain matrix and the covariance matrix of the estimated state can be obtained as [\[25](#page-15-23)]

$$
\mathbf{X'}_{o,k} = \mathbf{X'}_{o,k-1} + \mathbf{K}_k [\mathbf{Z}_k - \mathbf{H}_k d \mathbf{X'}_{o,k-1}],
$$
\n(17)

$$
\mathbf{K}_k = \mathbf{P}_{k,k-1} \mathbf{H}_k^T [\mathbf{H}_k \mathbf{P}_{k,k-1} \mathbf{H}_k^T + R_k]^{-1},
$$
\n(18)

$$
\mathbf{P}_k = [\mathbf{I} - \mathbf{K}_k \mathbf{H}_k] \mathbf{P}_{k,k-1}.
$$
\n(19)

3 Robust zero‑diference Kalman flter

In underwater acoustic positioning, when the observation contains the gross error, the measurement equation should be

$$
\rho_k = f(\mathbf{X}_k, \mathbf{X}_o) + \delta \rho_k + \mathbf{B}_k \Delta_k + \varepsilon_k,
$$
\n(20)

where \mathbf{B}_k is the interference matrix of gross error, and $\mathbf{\Delta}_k$ is the gross error.

If the standard Kalman flter is still used for calculation, the prediction residual with the gross error is as follows:

$$
\tilde{V}_k = \rho_k - f(\mathbf{X}_k, \mathbf{X}_o) - \delta \rho_k = V_k + \mathbf{B}_k \Delta_k,
$$
\n(21)

where V_k and \tilde{V}_k are the prediction residual vector without the gross error and with the gross error respectively.

The gross error is fully refected in the prediction residual, then the state vector is

$$
\mathbf{X}'_k = \mathbf{X}'_{k,k-1} + \mathbf{K}_k \tilde{V}_k. \tag{22}
$$

According to Eq. [22](#page-3-1), the gross error in the observation affects the state vector \mathbf{X}'_k through the gain matrix \mathbf{K}_k . To resist the infuence of gross error, a robust zero-diference Kalman flter is adopted based on the equivalent gain matrix. By using the prediction residual and the observation variance to construct the judgment factor S_k , the gross error in the observation equation can be efficiently detected. Based on the idea of equivalent gain matrix [[20](#page-15-18)] and equivalent weight function of Huber $[27, 28]$ $[27, 28]$ $[27, 28]$ $[27, 28]$, the equivalent gain

matrix related to the constant k_0 is constructed to reduce the infuence of gross error. The equivalent gain matrix is

$$
\overline{\mathbf{K}}_{k} = \begin{cases} \mathbf{K}_{k} & |S_{k}| < k_{0} \\ \mathbf{K}_{k} \frac{k_{0}}{|S_{k}|} & |S_{k}| \ge k_{0} \end{cases} \tag{23}
$$

where k_0 is a constant, generally, $k_0 = 1 \sim 2$.

expressed as

$$
S_k = V_k / \sqrt{\mathbf{D}_{V(k)}},\tag{24}
$$

$$
\mathbf{D}_{V(k)} = [\mathbf{I} - \mathbf{H}_k \mathbf{K}_k] R_k, \tag{25}
$$

where V_k is the prediction residual vector, and $\mathbf{D}_{V(k)}$ is the covariance matrix of observation vector.

When there exists gross error in the observations, the corresponding \mathbf{K}_k will be decreased and the influence of gross error on KF will be reduced.

To resist the efects of both systematic error and gross error, a robust zero-diference Kalman flter based on the random walk model and the equivalent gain matrix is proposed. The fowchart of the proposed algorithm is shown in Fig. [2](#page-3-2). The detailed steps of the algorithm are explained as follows:

Fig. 2 The fowchart of the robust zero-diference Kalman flter

• Transp

• The trajectory of the ship

 250

 $20₀$ 150

 $10($

 50

 -50

 -100

 -150

 -200 -250
 -300

 -200

 -100

 $Y(m)$

Fig. 3 The diagram of simulated ship and transponder

- 1. The initial state vector $\mathbf{X'}_{o,1} = (x_{o,1}, y_{o,1}, z_{o,1}, \delta \rho_1)$ including the transducer position and the systematic error is given.
- 2. The state vector $\mathbf{X'}_{o,k}$ and the corresponding covariance matrix $P_{k,k-1}$ are calculated by Eqs. [10](#page-2-2) and [16.](#page-3-3)
- 3. The gain matrix of the Kalman filter \mathbf{K}_k is computed by Eq. [18.](#page-3-4) The equivalent gain matrix $\overline{\mathbf{K}}_k$ based on robust estimation is calculated by Eq. [23.](#page-3-5)
- 4. The state vector and the error covariance matrix are estimated by Eqs. [26](#page-4-1) and [27](#page-4-2).

$$
\mathbf{X'}_{o,k} = \mathbf{X'}_{o,k-1} + \overline{\mathbf{K}}_k [Z_k - \mathbf{H}_k d\mathbf{X'}_{o,k-1}],
$$
 (26)

$$
\mathbf{P}_k = [\mathbf{I} - \overline{\mathbf{K}}_k \mathbf{H}_k] \mathbf{P}_{k,k-1}.
$$
 (27)

4 Simulation and real experimental analysis

4.1 Simulation analysis

Simulation analysis on the acoustic positioning based on the proposed method is conducted in this paper. As shown in Fig. [3,](#page-4-3) the four transponders are located at the positions of the asterisk symbol with the diferent underwater depth of 30 m, 100 m, 500 m and 3000 m. The trajectories of the ship are circles with the radius of 100 m, 200 m, 800 m and 3000 m as well as the linear track with the grid shape. The sampling interval is 2 s and the speed of the survey ship is

100

200

300

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× l,

Fig. 4 The observation residuals of LS, SD and KF at diferent depths

Fig. 5 The results of the estimated systematic errors by KF at diferent depths

Fig. 6 The underwater positioning results of diferent algorithms at diferent depths

Table 1 The positioning result statistics of diferent algorithms

Depth (m)	Method	Mean RMS-X (m)	Mean RMS-Y (m)	Mean RMS-Z (m)	$3D-RMS$ (m)
30	LS	0.061	0.059	0.447	0.455
	SD	0.014	0.013	0.062	0.065
	ΚF	0.011	0.012	0.045	0.048
100	LS	0.032	0.065	0.373	0.380
	SD	0.014	0.015	0.084	0.087
	ΚF	0.010	0.013	0.041	0.044
500	LS	0.034	0.038	0.403	0.406
	SD	0.016	0.020	0.086	0.090
	ΚF	0.012	0.011	0.036	0.040
3000	LS	0.039	0.051	0.500	0.504
	SD	0.029	0.018	0.105	0.110
	КF	0.014	0.014	0.062	0.065

about 1 m/s. The measured sound speed profle of 3000 m is adopted for the calculation of sound speed. The layered ray acoustic tracking algorithm is used to simulate the travel time, and the systematic error [\[29\]](#page-15-27) is simulated based on Eq. [28](#page-8-0) proposed in Xu et al. [\[9](#page-15-7)]. The slant range error caused by the random error is 0.1 m; therefore, the initial measurement noise variance is $R = 0.01 \text{ m}^2$. The initial system noise matrix is **Q** = diag[0 0 0 0.001] m^2 .

and the real value of the transponder respectively. *N* is the number of the transponder.

As shown in Figs. [4](#page-5-0) and [5](#page-6-0), the SD can effectively reduce the effects of systematic errors compared with the LS. However, the SD produces larger random errors compared with the KF. The KF can efectively estimate systematic error parameters, together with position parameter without enlarging the infuence of random errors. Therefore, the KF can signifcantly improve the underwater positioning accuracy.

As shown in Fig. [6](#page-7-0) and Table [1](#page-8-1), when there exist random errors, systematic errors and no gross errors in the acoustic observations, the LS cannot resist the efects of the systematic errors on the positioning result, especially in the Z direction of coordinates. The SD and KF can both reduce the infuence of the systematic errors and greatly improve the positioning accuracy. For the case of underwater 30 m depth, the three-dimension (3D) RMSs of SD and KF are 0.065 m and 0.048 m, respectively, compared to LSs 0.455 m, with the improvement of 85.7% and 89.4%. For the case of 100 m depth, they are 0.087 m and 0.044 m, respectively, compared to LSs 0.380 m, with the improvement of 77.1% and 88.4%. For the case of 500 m depth, they are 0.090 m and 0.040 m, respectively, compared to LSs 0.406 m, with the improvement of 77.8% and 90.1%. For the case of 3000 m depth, they are 0.110 m and 0.065 m, respectively, compared to LSs 0.504 m, with the improvement of 78.2% and 87.1%. In addition, the KF can further enhance the positioning accu-

$$
\delta \rho_{v} = c_{1} + c_{2} \sin \left(\frac{2(t - t_{0})}{T_{S}} \pi \right) + c_{3} \sin \left(\frac{(t - t_{0})}{T_{L}} \pi \right) + c_{4} \left[1 - \exp \left\{ -\frac{1}{2} \left\| \mathbf{X}_{o} - \mathbf{X} \right\| / (2 \text{km})^{2} \right\} \right],
$$
\n(28)

where the constant term is $c_1 = 0.1$ m, the short-period internal wave error term is $c_2 = 0.12$ m, the long-period error term is $c_3 = 0.3$ m, the term related to the measurement range is $c_4 = 0.02$ m, the short period of internal wave is $T_s = 15 * 60$ s (equal to 15 min) and the long period of internal wave is $T_L = 12 * 3600$ s (equal to 12 h). $||\mathbf{X}_o - \mathbf{X}||$
is the distance between the transducer and the transponder is the distance between the transducer and the transponder.

The zero-diference least squares (LS), the single-difference least squares (SD), the zero-difference Kalman flter (KF), the robust zero-diference least squares(R-LS), the robust single diference least squares (R-SD) and the robust zero-diference Kalman flter (R-KF) are conducted and compared for underwater acoustic positioning. Firstly, the proposed algorithm is validated in the case without gross error. The observation residuals of LS, SD and KF as well as the estimated systematic errors by KF are shown in Figs. [4](#page-5-0) and [5.](#page-6-0) Monte Carlo experimental simulation with 100 times is conducted, the root mean squares (RMS) of the transponder position calculated at the diferent depth and the diferent algorithm is shown in the Fig. [6](#page-7-0). In calculating the formula of RMS, $X_{o,k}$ and $\hat{X}_{o,k}$ are the calculation value racy with about 5–12% improvement compared to the SD.

Secondly, to further verify the performance of LS, SD and KF in the case of the ship trajectories with irregular curve, the transponders with the diferent underwater depth of 30 m, 100 m, 500 m and 3000 m are positioned by the simulated trajectories as shown in Fig. [7](#page-9-0). Table [2](#page-10-1) presents the RMSs of diferent algorithms and depths. For the case of underwater 30 m depth, the 3D RMSs of SD and KF are 0.079 m and 0.057 m compared to the 0.362 m of LS, with the improvement of 78.2% and 84.3%. For the case of 100 m depth, they are 0.175 m and 0.082 m compared to the 0.304 m of LS, with the improvement of 42.4% and 73.0%. For the case of 500 m depth, they are 0.127 m and 0.061 m compared to the 0.373 m of LS, with the improvement of 66.0% and 83.6%. For the case of 3000 m depth, they are 0.223 m and 0.165 m compared to the 0.442 m of LS, with the improvement of 47.3% and 62.7%. Therefore, the performance of KF is also better than that of LS and SD in the case of the ship trajectories with irregular curve.

100

150

2000

3000

200

Fig. 7 The diagram of the simulated ship and transponder in diferent depths

Finally, the time delay observation is added to the gross errors based on normal distribution with zero mean and standard deviation of 0.05 s, and the gross errors are added in the acoustic observations every 50 s. Figure [8](#page-11-0) shows the result of the estimated systematic error by the R-KF. At the same time, the positioning results of the non-robust estimation and the robust estimation are shown in Figs. [9](#page-12-0), [10,](#page-12-1) [11](#page-13-0) and [12](#page-13-1).

Figure [8](#page-11-0) shows that the R-KF can resist the infuence of gross errors on the position and systematic error parameter based on the equivalent gain matrix. As shown in the Figs. [9,](#page-12-0) [10](#page-12-1), [11](#page-13-0) and [12](#page-13-1), the accuracy of the SD is signifcantly reduced compared with the LS and the KF due to the efects

of the gross errors. The R-SD can also resist the infuences of the gross errors by the robust estimation and reduce the infuence of the systematic errors to improve the accuracy of the underwater positioning compared with the R-LS. However, the R-SD has also the disadvantage of enlarging the effects of random errors, which leads to the positioning accuracy lower than that of the R-KF. The R-KF can estimate the systematic errors by the random walk process without enlarging the infuence of the random errors, and provide robust solutions by using the equivalent gain matrix, which has higher precision and stability than those of the other two algorithms.

Table 2 The positioning result statistics of diferent algorithms

Depth (m)	Method	Mean RMS-X (m)	Mean RMS-Y (m)	Mean RMS-Z (m)	$3D-RMS$ (m)
30	LS	0.047	0.066	0.353	0.362
	SD	0.020	0.017	0.074	0.079
	КF	0.015	0.013	0.054	0.057
100	LS	0.022	0.045	0.299	0.304
	SD	0.021	0.019	0.172	0.175
	КF	0.014	0.014	0.079	0.082
500	LS	0.037	0.037	0.369	0.373
	SD	0.027	0.023	0.122	0.127
	ΚF	0.019	0.012	0.056	0.061
3000	LS	0.039	0.049	0.437	0.442
	SD	0.023	0.017	0.221	0.223
	ΚF	0.018	0.014	0.163	0.165

The means of RMS for 100 times of each algorithm are shown in Table [3](#page-14-0). From Table [3](#page-14-0), it can be seen that the positioning accuracy of the LS, SD and KF is greatly decreased by gross errors, especially for the SD due to the enlarged gross errors. R-LS, R-SD and R-KF can obviously improve the positioning by using robust estimation to resist the infuence of the gross errors. For the case of underwater 30 m depth, the three-dimension (3D) RMSs of R-SD and R-KF are 0.076 m and 0.045 m, respectively, compared to R-LSs 0.463 m, with the improvement of 83.5% and 90.3%. For the case of 100 m depth, they are 0.103 m and 0.051 m, respectively, compared to LSs 0.378 m, with the improvement of 72.7% and 86.5%. For the case of 500 m depth, they are 0.099 m and 0.040 m, respectively, compared to LSs 0.406 m, with the improvement of 75.6% and 90.1%. For the case of 3000 m depth, they are 0.137 m and 0.062 m, respectively, compared to LSs 0.504 m, with the improvement of 72.8% and 87.7%. In addition, the R-KF can further enhance the positioning accuracy with about 7–15% improvement compared to R-SD.

4.2 Real experiment analysis

The in situ data were collected from an experiment conducted at Lingshan Island in Dec. 2017. Lingshan Island is located in Qingdao City, Shandong Province in China with longitude and latitude about 120° 13' 02" E, and 35° 46′ 53″ N, respectively. The single transponder is located at the ocean bottom, and the trajectory of the voyage move is centered around the transponder with a radius of about 50 m. The ultrashort baseline response mode is used for underwater positioning, and GPS receiver, attitude sensor and sound velocity profler are auxiliary installed.

After preprocessing the measured data, LS, SD, KF, R-LS, R-SD and R-KF are used for the positioning calculation and then compared. The observation noise and the system noise of Kalman filter are set as $R = 1 \text{ m}^2$ and $Q = \text{diag}[0 \ 0 \ 0 \ 0.001] \text{ m}^2$, respectively. Since the position of the underwater transponder in the experimental area is unknown, the positioning accuracy cannot be directly evaluated. To verify the accuracy of the algorithm, as shown in Fig. [13](#page-14-1), the observations that are not involved in positioning calculation on the trajectory are selected to calculate the residuals, namely the observation ranges minus computation/theory ranges (O–C).

As shown in Table [4,](#page-14-2) the RMS of the validated residuals of the SD is lower than that of the LS and the KF. The reason may be that: (1) since the experiment is conducted in shallow sea, the infuence of the systematic errors is relatively small; (2) the systematic error between the adjacent epochs are not exactly equal in the actual observations, and the SD cannot totally eliminate the systematic errors; (3) SD enlarges the infuence of random errors. When using robust estimation, all the RMSs of the three methods decrease, which indicates that robust estimation can efficiently control the influence of gross errors. Compared with the R-LS and the R-SD, the RMS of the validated residuals of the R-KF is greatly reduced from 1.63 m and 1.81 m, respectively, to 0.85 m, which proves the higher precision of R-KF. From Fig. [14,](#page-15-28) it can be seen that both the KF and the R-KF need some certain epochs to make the fltering solution convergence. There is a bias between the solutions of R-KF and KF, since the former uses robust estimation to reduce the infuence of the gross errors on the systematic error parameter, while the latter has no action on gross errors and inevitably brings the deviation of solution for underwater positioning.

5 Conclusion

To reduce the efects of the systematic error and the gross error on the underwater positioning, this paper proposes a robust zero-diference Kalman flter based on the random walk model and the equivalent gain matrix. After the validation from the simulation experiment and a real example, the following conclusions can be drawn.

1. Compared with the zero-diference LS, the single-difference LS between the observation epochs can reduce the infuence of the systematic error. However, it also enlarges the infuence of the random errors and the gross errors. Although the robust single-diference LS can eliminate the infuence of the gross errors by the robust estimation, its accuracy of underwater position-

Fig. 8 The results of the estimated systematic errors by R-KF at diferent depths

a The non-robust estimation of the different algorithm

Fig. 9 The positioning results at the depth of underwater 30 m

a The non-robust estimation of the different algorithm

Fig. 10 The positioning results at the depth of underwater 100 m

b The robust estimation of the different algorithm

b The robust estimation of the different algorithm

Fig. 11 The positioning results at the depth of underwater 500 m

a The non-robust estimation of the different algorithm

Fig. 12 The positioning results at the depth of underwater 3000 m

ing is greatly reduced by the enlarged random errors and the remained systematic errors. The accuracy of zerodiference Kalman flter can be signifcantly improved compared to the zero-diference LS and the single-diference LS. At the same time, the zero-diference Kalman

b The robust estimation of the different algorithm

b The robust estimation of the different algorithm

flter has the better performance in the case of the ship trajectories with irregular curve.

2. The proposed robust zero-difference Kalman filter can estimate the systematic error by the random walk model without enlarging the infuence of the random

Table 3 The positioning result statistics of different algorithms

Fig. 13 The trajectory of ship and checkpoint

Table 4 The residuals statistics of the 20 epochs

Method	RMS(m)	Max(m)	Min(m)
LS	1.73	2.16	0.99
SD	1.91	2.59	1.39
ΚF	1.24	2.12	0.51
$R-I.S$	1.63	2.17	0.92
$R-SD$	1.81	2.55	1.26
$R-KF$	0.85	1.69	0.04

errors, and resist the infuence of the gross error by the equivalent gain matrix. In the simulating experiment, the positioning accuracy of the proposed algorithm is obviously superior to that of robust zero-diference LS and robust single-diference LS with the improvement of about 86–90% and about 5–15%, respectively. In the real data experiment, the RMS of the validated residuals of the robust zero-diference Kalman flter

Fig. 14 The positioning result of epoch by epoch (blue line represents KF and red line is R-KF)

is about 0.8 m, and obviously less than that of robust zero-diference LS and the robust single-diference LS, which proves that the proposed algorithm has higher accuracy and stability.

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