OPTIMIZATION

Optimization of the different controller parameters via OBL approaches based artificial ecosystem optimization involving fitness distance balance guiding mechanism for efficient motor speed regulation of DC motor

Evren Isen^{[1](https://orcid.org/0000-0002-1091-125X)} **D** · Serhat Duman¹ **D**

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Abstract

This study proposes a new optimization approach, which is called as artificial ecosystem optimization algorithm with fitness-distance balance guiding mechanism by using opposite based learning methods (FDBAEO_OBLs) for the speed regulation of direct current (DC) motor. The performance of the proposed FDBAEO_OBL algorithm is tested in two different experimental studies. In the first experimental study, the proposed approach is tested in the CEC2020 benchmark test functions and the FDBAEO algorithm, which included the best OBL approach, is determined using non-parametric Wilcoxon and Friedman statistical analysis methods. Second, the parameters of proportional integral derivative (PID), tilt integral derivative (TID), proportional integral derivative with filter (PIDF), tilt integral derivative with filter (TIDF), fractional-order proportional integral derivative (FOPID), fractional-order proportional integral derivative with filter (FOPIDF), proportional integral derivative with fractional-order filter (PIDFF) and fractional-order proportional integral derivative with fractional-order filter (FOPIDFF) controller structures to be used in DC motor closed loop speed control are determined with FDBAEO_OBL, and the performances of the controllers are investigated. Integral absolute error (IAE), integral time absolute error (ITAE), integral time squared error (ITSE) and integral squared error (ISE) performance indices are used as the objective function of the operation process in which the control parameters are determined. According to the comparative step response results of the controller structures, the four best controller structures for DC motor speed regulation are determined. The performances of these controllers are examined under different simulation conditions and according to the results obtained, it is seen that the best controller structure is FOPIDFF. The FDBAEO_OBL algorithm, which is used in both benchmark test functions and DC motor speed regulation, shows an effective, durable and superior performance in finding the optimal solution values during the optimization.

Keywords Artificial ecosystem optimization · Benchmark test functions · DC motor speed regulation · Fitness-distance balance guiding mechanism - Opposite-based learning methods

1 Introduction

DC motor is a type of motor that is frequently used in many applications due to its ease of use, low cost, and durability. It is preferred in robot arms in industrial applications,

 \boxtimes Evren Isen eisen@bandirma.edu.tr household electrical appliances, and electric vehicles in daily life. Depending on the requirements at the point of use of the DC motor, which converts electrical energy into motion energy, closed-loop speed control is widely used in motor control. It is expected that the motor speed settles to the determined reference value as quickly as possible, with minimum overshoot, and without error. To meet these conditions, the controller used must be well designed.

PID controller is widely used in closed-loop speed control used in motor speed regulation. It generates the required control signal to reduce the applied error signal to

¹ Electrical Engineering, Engineering and Natural Sciences Faculty, Bandirma Onyedi Eylul University, Bandirma, Turkey

zero. The gain coefficient (K_p) , integral coefficient (K_i) and derivative coefficient (K_d) in the PID controller, which consists of gain, integral and derivative operations, determine the performance of the controller. The K_p coefficient ensures that the output settles to the reference quickly. However, if it is not selected at the appropriate value, it causes an overshoot from the reference value. In addition, the K_p coefficient helps to reduce the steady-state error. The integrator in the controller ensures that the steady state error is reduced to zero by continuously adding the error. The negative effect of the integrator is that it can cause oscillation in the control signal when the sign of error signal changes. The derivative expression, which is the other part of the controller, calculates the slope of the error and provides to reduce settling time and the percentage of overshoot.

PID controller, which is used as a controller in many system controls such as voltage regulation (Hemeida et al. [2023\)](#page-25-0), temperature control (Xu and Liu [2022](#page-26-0)), inverter control in grid-connected photovoltaic systems (Malarvili and Mageshwari [2022\)](#page-26-0), DC–DC boost converter (Li et al. [2023\)](#page-26-0), zeta converter (Arun and Manigandan [2021](#page-24-0)), is also widely used in motor applications (Baidya et al. [2023](#page-25-0); Viaene et al. [2022](#page-26-0); Jeon et al. [2018](#page-25-0); Liu et al. [2021](#page-26-0); Choi et al. [2015;](#page-25-0) Zhang and Gao [2022](#page-26-0)). A well-designed controller is required for the motor to achieve the desired reference value (speed, torque, and position) (Hasanhendoei et al. [2023](#page-25-0); Amyal et al. [2023\)](#page-24-0) and to maintain the speed value despite the disturbances. At this point, the controller coefficients gain importance. Various traditional methods such as Ziegler–Nichols (Ziegler and Nichols [1942\)](#page-26-0), Cohen–Coon (Cohen and Coon 1953), Gain and Phase Method (Astrom and Hägglund [1984\)](#page-24-0) are used to determine the controller coefficients. Beetle antennae search algorithm (Mourtas et al. [2023](#page-26-0)), gazelle simplex optimizer (Ekinci et al. [2023a](#page-25-0)), hybrid Lévy flight distribution and Nelder-Mead algorithm (Izci [2021](#page-25-0)), slime mould algorithm (Izci and Ekinci [2021](#page-25-0)), particle swarm optimization (PSO) (Feng et al. [2021\)](#page-25-0), ant colony optimization (Liang et al. [2019\)](#page-26-0) and gray wolf optimization (Sahoo and Panda [2018\)](#page-26-0) are also different optimization methods used lately. ITAE, ITSE, ISE and IAE are used as objective functions in determining the coefficients in optimization methods (Veinovic et al. [2022](#page-26-0); Zeng et al. [2020;](#page-26-0) Bouakkaz et al. [2020;](#page-25-0) Isen [2022\)](#page-25-0). PID controller has been widely used as a controller in many applications until recent years. Different controllers, though, have been developed and are being utilized to attain performance above that of this controller, nowadays. The most commonly used one is FOPID controller (Xia et al. [2023](#page-26-0); Izci et al. [2022a](#page-25-0)). FOPIDF controller is obtained by adding N constant first order filter to the FOPID controller. Here the filter is used to eliminate noise and harmonics (Tripathy et al. [2021\)](#page-26-0). In addition, TID controller (Ahmed et al. [2022\)](#page-24-0) used in high

frequency control is a fractional order controller type. TIDF controller, which has a similar structure to PIDF, has a fractional integrator and tilt coefficient instead of proportional coefficient. It provides simpler adjustment, a higher rate of interference prevention, and less sensitivity to changes in system parameters (Sahu et al. [2016\)](#page-26-0). Unlike the PID controller, the PIDF controller has a derivative filter coefficient. This filter is used to reduce the derivative kick (Singh et al. [2021](#page-26-0); Sahu et al. [2014\)](#page-26-0). With the combination of PID with filter N and PD with filter N controllers, a dual-stage controller structure is created (Singh et al. [2023\)](#page-26-0).

In recent years, advances in technology and rapid developments in computer architectures have increased the applicability of digital controller structures. Parameters of digital controllers determined according to user experience and classical calculation methods may not perform adequately in systems. The parameters of the controller structures are chosen using the optimization techniques recently presented in the literature to overcome these drawbacks resulting from user experience and conventional calculation methods. Zhao et al. ([2020\)](#page-26-0) recently introduced the artificial ecosystem optimization (AEO) method to the literature as a new population-based optimization algorithm that is motivated by the life process features of living species in the ecosystem. Since 2020, this method has been employed in more than 280 academic works, drawing the interest of several scientists from other disciplines. In these studies, it has been shown that the performance of the AEO algorithm is better than other optimization algorithms. Stated differently, its good exploration/exploitation capabilities in finding the global solution, its remarkable ability to converge to the optimum solution and its success in solving large-scale optimization problems make the AEO algorithm more valuable, important and preferable than other algorithms. Sonmez et al. [\(2022](#page-26-0)) developed the optimal solution and convergence capability of the AEO algorithm by using the selection method based on the fitness-distance balance (FDB) guiding mechanism. The authors named the algorithm they developed with the proposed FDB method as the FDB artificial ecosystem optimization (FDBAEO) algorithm.

In different studies in the literature, opposition-based learning (OBL) strategies have been used in the initial population to improve the performance of optimization algorithms and in local search operators that will enable the algorithms to avoid local solution traps. The FDB guidance mechanism plays an important role in identifying solution candidates that do not improve the search process in optimization algorithms and removing them from the solution space. Moreover, it reduces the risk of premature convergence, a phenomenon that can occur depending on the design steps of the algorithm. The FDB mechanism helps algorithms in avoiding local solution traps, encouraging an

increase in the diversity of solutions within the solution space. Considering the advantages of both design operators presented in the literature to improve the performance of optimization algorithms, the FDBAEO algorithm, which includes AEO and OBL strategies containing these two design operators, has been presented to the literature for the first time. In this study, the use of OBL strategies in the initial population enabled the proposed algorithm to increase the solution diversity in the solution space and its ability to search for the optimal solution. Moreover, the FDB method is used to update the value of the solution candidate's position in the next iteration, thus reducing the risk of premature convergence of the algorithm. In other words, it enables the algorithm to get rid of local solution traps and contributed to its rapid convergence to the global solution point. In particular, the performances of both basic AEO and FDBAEO algorithms have been improved by using the advantages and superior features of these two design operators together. FDBAEO algorithm developed using OBL strategies is used to determine the parameters of different controller structures used in closed-loop speed control of the DC motor. In DC motor speed control, the two main criteria are the controller design and optimization algorithms used for adjusting the controller parameters to their optimum values. When the recent studies are examined, optimization algorithms are seen as one of the most effective system parameters in determining the parameters of the controller structures used in different fields of science and increasing the performance of the controllers. Eight different controller topologies with presented controller performance in various systems are used in this study to regulate the speed of a DC motor. While these controllers can improve system performance according to system operating conditions, controller parameters determined based on user experience or mathematical approaches may sometimes be insufficient to improve system performance. Considering this situation, the parameters of eight different controller structures used to improve the quality of the work and the performance of the controllers are adjusted using the proposed FDBAEO_OBL algorithm.

The specific main contributions of the study can be summarized as follows:

FDBAEO_OBL is introduced as a new, improved and powerful optimization algorithm. The performance of the proposed algorithm and its success in finding the optimal solution have been demonstrated by simulation studies on CEC 2020 benchmark test functions. In order for the FDBAEO algorithm developed using OBL methods to converge or find the optimal solution value in the benchmark test functions, the efficiency of the exploration and balanced search features used in the algorithm design has been demonstrated by testing in different dimensional search spaces and populations.

- The utilization of opposite-based learning (OBL) strategies in generating contrasting solutions within the initial population of the FDBAEO algorithm has enhanced its capability to converge toward optimal solutions. The incorporation of OBL strategies has improved the algorithm's ability to converge while also improving the balance between exploration and exploitation characteristics. The introduction of the FDBAEO_OBL algorithm was presented to the literature for the first time in this study.
- The results derived from non-parametric Wilcoxon and Friedman tests prove that the FDBAEO_OBL algorithm is an effective and robust algorithm in solving optimization problems in various disciplines.
- In this study the operational effectiveness of eight different controller structures—PID, FOPID, TID, TIDF, PIDF, FOPIDF, PIDFF, and FOPIDFF—whose parameters were optimized using the FDBAEO_OBL method, is thoroughly examined. Moreover, this study focuses on the speed regulation of a DC motor using optimized controller structures, and the results are thoroughly analyzed and discussed. This research concept is presented for the first time in this study for DC motor speed regulation.
- The comparative findings of the system's transient and dynamic responses across several simulation studies demonstrate the FOPIDFF controller's superior structure, durability, and effectiveness above other controller structures created with the proposed FDBAEO_OBL algorithm.

This study is presented in seven sections with subsections after the introduction. These sections are prepared as follows.

- The electrical and mechanical description of the DC motor structure is given in the second section.
- In the third section, the controller structures used to improve system performance are introduced.
- Section [4](#page-7-0) and subsections describe the improved FDBAEO algorithm using four different OBL methods in detail.
- Information on the statistical evaluation of the results obtained from the standards, benchmark test functions and algorithms taken into account in the implementation of experimental studies is given in detail in Sect. [5.](#page-11-0)
- To highlight the effectiveness, efficiency, and robustness of the proposed FDBAEO OBL algorithm in obtaining the ideal solution, a thorough examination of the outcomes of two separate experimental experiments is presented in Sect. [6.](#page-12-0)
- The results are finally explained in Sect. [7](#page-20-0) along with suggestions for additional research.

2 Definition of DC motor structure

The equivalent circuit model of the externally-excited type DC motor that is considered in this paper is seen in Fig. 1. It has an armature circuit and an exciting circuit as shown in the figure (Izci et al. [2021\)](#page-25-0).

Equation (1) is obtained when the electrical equations of the armature circuit of the motor is written. In this equation, R_a and L_a is armature resistance and inductance, i_a is armature current, e_b is back-emf voltage, and e_a is armature voltage.

$$
e_a(t) = R_a i(t) + L_a \frac{di(t)}{dt} + e_b(t)
$$
\n⁽¹⁾

The back-emf voltage is calculated depending on (2) which is obtained with K_b electromotor force constant and ω angular speed. Also, e_b changes with derivative of θ theta depending on the time as seen in Eq. (2).

$$
e_b = K_b \omega = K_b \frac{d\theta}{dt} \tag{2}
$$

The torque T that is given in (3) is the sum of inertia and friction torques. It is calculated with J inertia torque of motor, ω angular speed and B motor friction constant. The torques is also calculated depending on K motor torque constant and i_a armature current.

$$
T = J\frac{d\omega}{dt} + B\omega = Ki_a \tag{3}
$$

If the angle is used to calculated the torque, (4) can be used as seen below.

$$
T = J\frac{d^2\theta}{dt^2} + B\omega\tag{4}
$$

The open-loop transfer function of the motor that is derived from (1) to (3) is given in (5) .

$$
\frac{\omega(s)}{E_a(s)} = \frac{K}{J L_a s^2 + (R_a J + B L_a)s + (K K_b + R_a B)}
$$
(5)

The block diagram of the transfer function is seen Fig. 2. The input of the model is the applied voltage to motor terminals whereas the output is speed of shaft. In this

block diagram, T_L defines load torque, and it is assumed zero in the transfer function.

The values of motor parameters that are seen in (5) are given in Table [1](#page-4-0). They are used in the simulation studies in the paper.

3 The controller structures used for improving the system performance

The closed-loop speed control of the system is seen in Fig. [3](#page-4-0). The voltage required to reduce the error between the speed reference and the measured speed to zero is calculated by the controller. The calculated voltage E_a is applied to the motor model shown in Fig. 2 and the DC motor runs. Thus, the speed control of the motor is provided.

In this system, motor speed control is provided by the controller. Therefore, the performance of the controller is very important. Many structures are used as controllers in the literature. The block diagrams of the controllers examined in this study and used in the system are shown in Fig. [4](#page-5-0).

The PID controller seen in Fig. [4](#page-5-0)a is the most frequently used controller from past to present (Ekinci et al. [2023b](#page-25-0); Izci et al. [2023](#page-25-0)). The controller which mathematical expression is given in (6) consists of proportional, integral and derivative terms. Each has coefficient called K_p , K_i , and K_d that impacts the controller performance. These parameters determine the settling time, percentage of overshoot, and the steady-state error of the system at transition moments. As seen in Fig. [4](#page-5-0)a, the block diagram of the conventional PID controller is given in Fig. [4a](#page-5-0). The error signal is given to the proportional, integral and derivative controller and the results are summed to obtain the PID output.

$$
TF_{PID}(s) = K_p + \frac{K_i}{s} + K_d s \tag{6}
$$

When the PID controller in Fig. [4a](#page-5-0) is added as a controller to the system structure seen in Fig. [3,](#page-4-0) the transfer function of the entire system is seen in (7). This 3rd order transfer function is used in system simulation and controller optimization.

Fig. 1 DC motor model **Fig. 2 DC** motor block diagram

Fig. 3 Block diagram of DC motor control system

$$
TF_{STS}(s) = \frac{KK_d s^2 + KK_p s + KK_i}{s^3 J L + (JR + BL + KK_d)s^2 + (BR + K^2 + KK_p)s + KK_i}
$$
\n(7)

Tilt integral derivative controller has three components as PID controller. The difference between the two controllers is that TID controller proportional term (K_t) is multiplied by a transfer function as seen in (8). The parameter of n is a real number different from zero (Topno and Chanana [2016](#page-26-0); Rai and Das [2022](#page-26-0)).

$$
TF_{TID}(s) = \frac{K_t}{s^{1/n}} + \frac{K_i}{s} + K_d s \tag{8}
$$

The block diagram is seen in Fig. [4b](#page-5-0). The input of the controller is an error signal and the output is the control signal. The transfer function depending on the motor and TID controller parameters is given in (9).

$$
A_1 = (JR + BL + KK_d)
$$

\n
$$
A_2 = (BR + KK_d)
$$

\n
$$
TK_d s^{2+(1/n)} + KK_f s + KK_f s^{1/n}
$$

\n
$$
TF_{SYS}(s) = \frac{KK_d s^{2+(1/n)} + KK_f s + KK_f s^{1/n}}{s^{(3+(1/n))} + A_1 s^{(2+(1/n))} + A_2 s^{(1+(1/n))} + KK_f s + KK_f s^{1/n}}
$$
\n(9)

$$
C_1 = (JR + BL + JLN)
$$

$$
C_2 = (BR + KK_b + JRN + BLN + KK_dN)
$$

$$
C_3 = (BRN + KK_bN + KK_i)
$$

$$
TF_{SYS} = \frac{KK_dNs^{2+(1/n)} + KK_is^2 + KK_is^{1+(1/n)} + KK_iN_s + KK_iNs^{1/n}}{s^{4+(1/n)}IL + C_1s^{3+(1/n)} + C_2s^{2+(1/n)} + KK_is^2 + C_3s^{1+(1/n)} + KK_iNs}
$$

PI controller is preferred in many applications because of its simple structure and applicability. In order for the system to respond quickly in transient situations, the PID controller obtained by adding a derivative component to the PI controller is used. The derivative component, however, may produce unfavorable outcomes in practical applications if there is noise and a rapid change in the signal that the controller receives. The PIDF controller shown in (10) is produced for this situation by adding a filter to the derivative component. In the controller, which has a similar structure to the PID controller, N refers to the filter coefficient of derivative (Guha et al. [2017](#page-25-0)).

$$
\text{TF}_{\text{PIDF}}(s) = K_p + \frac{K_i}{s} + K_d s \frac{N}{s + N} \tag{10}
$$

The transfer function of the DC motor speed control system using the PIDF controller, which block diagram is seen in Fig. [4](#page-5-0)c, is given in (11).

$$
B_1 = (JR + BL + JLN)
$$

\n
$$
B_2 = (BR + K^2 + JRN + BLN + KK_p + KK_dN)
$$

\n
$$
B_3 = (BRN + K^2N + KK_pN + KK_i)
$$

\n
$$
TF_{SYS}(s) = \frac{(KK_p + KK_dN)s^2 + (KK_pN + KK_i)s + KK_iN}{s^4JL + B_1s^3 + B_2s^2 + B_3s + KK_iN}
$$
\n(11)

Tilt integral derivative with filter controller, which transfer function is seen in (12) , is like the combination of PID and FOPID. It has the advantages of both controllers. The controller in the block diagram shown in Fig. [4](#page-5-0)d differs from the other two controllers in that it immediately suppresses the disturbances (Chiranjeevi et al. [2021](#page-25-0)).

$$
TF_{TIDF}(s) = \frac{K_t}{s^{1/n}} + \frac{K_i}{s} + K_d s \frac{N}{s+N}
$$
\n(12)

The transfer function of the system using the DC motor model and the controller model applied for speed control is seen in (13) .

FOPID controller is an extended version of PID controller (Izci and Ekinci [2023\)](#page-25-0). In the PID controller, the

 (13)

Fig. 4 Block diagrams of the controllers a PID, b TID, c PIDF, d TIDF, e FOPID, f FOPIDF, g PIDFF, h FOPIDFF

integrator and derivative components are of the 1st order. Controller performance is adjusted by coefficients only. In the FOPID controller, whose transfer function is given in (14) and the block diagram is given in Fig. 4e, λ and μ parameters also affect the controller performance. Depending on the 0 and 1 condition of these coefficients, the controller becomes P, PI, PD and PID controller (Divya et al. [2022;](#page-25-0) Tang et al. [2012](#page-26-0)).

$$
TF_{FOPID}(s) = K_p + \frac{K_i}{s^{\lambda}} + K_d \frac{s^{\lambda + \mu}}{s^{\lambda}}
$$
(14)

The transfer function of the system obtained by using FOPID controller and DC motor model is given in (15). As can be seen, besides circuit parameters and controller coefficients, λ and μ parameters are included in the system transfer function and affect the performance.

$$
D_1 = (JR + BL)
$$

\n
$$
D_2 = (BR + K^2 + K_p K)
$$

\n
$$
TF_{SYS} = \frac{KK_d s^{\mu + \lambda} + K_p K s^{\lambda} + K_i K}{s^{2 + \lambda} JL + D_1 s^{1 + \mu} + D_2 s^{\lambda} + K_d K s^{\lambda + \mu} + K_i K}
$$
\n(15)

The FOPIDF controller is obtained by filtering the derivative component in the FOPID controller as seen in Fig. [4](#page-5-0)f. This feature improves the performance of the FOPID controller and filters out high-frequency noise in the control signal. The derivative filter not only reduces noise but also ensures that the transfer function is appli-cable (Dey et al. [2022\)](#page-25-0). N, μ and λ parameters determine the filter performance in the FOPIDF controller, which transfer function is given in (16) and transfer function of the whole system to which it is applied in (17).

$$
TF_{FOPIDF}(s) = K_p + \frac{K_i}{s^2} + K_d s^{\mu} \frac{N}{s+N}
$$
(16)
\n
$$
E_1 = (JR + BL + JLN)
$$

\n
$$
E_2 = (BR + K^2 + K_p K + JRN + BLN)
$$

\n
$$
E_3 = (BRN + K^2 N + KK_p N)
$$

\n
$$
TF_{SYS}(s)
$$

\n
$$
= \frac{KK_p s^{1+\lambda} + K_p KN s^{\lambda} + K_i K s + KK_i N + KK_d N s^{\lambda+\mu}}{s^{3+\lambda} JL + s^{2+\lambda} E_1 + E_2 s^{\lambda+1} + E_3 s^{\lambda} + KK_d N s^{\lambda+\mu} + sKK_i + KK_i N}
$$
(17)

The block diagram and transfer function of the PIDFF controller, which is obtained by adding a fractional order filter to the derivative component in the PID controller, is shown in Fig. [4g](#page-5-0) and (18). As you can see, unlike the PID

$$
F_1 = (BR + K^2 + KK_p)
$$

\n
$$
F_2 = (JRN + BLN + KK_dN)
$$

\n
$$
F_3 = (NBR + K^2N + KK_pN)
$$

\n
$$
F_4 = (JR + BL)
$$

\n
$$
TF_{SYS}(s)
$$

\n
$$
= \frac{KK_p s^{1+\lambda_f} + NK_d s^2 K_f KK_i s^{\lambda_f} + K_pKNs + KK_iN}{s^{3+\lambda_f}JL + s^{2+\lambda_f}F_4 + s^{1+\lambda_f}F_1 + s^3JLN + s^2F_2 + sF_3 + KK_i s^{\lambda_f} + KK_iN}
$$
\n(19)

The fractional-order PID with fractional filter controller is the final controller and has the most complicated structure among all the controllers employed. Figure [4](#page-5-0)h shows its block diagram. There is a fractional-order integral and derivative component, just like in the FOPID controller, and a fractional-order filter in the derivative component, like in the PIDFF controller. As seen in (20), the number of parameters that need to be optimized is more than FOPID and PIDFF controllers, and it is 7 in total. The transfer function of the system using FOPIDFF is also given in (21) and it has a very complex structure.

$$
TF_{FOPIDFF}(s) = K_p + \frac{K_i}{s^{\lambda}} + K_d s^{\mu} \frac{N}{s^{\lambda_f} + N}
$$
\n(20)

$$
G_1 = (jR + BL)
$$

\n
$$
G_2 = (BR + K^2 + KK_p)
$$

\n
$$
G_3 = (JRN + BLN)
$$

\n
$$
G_4 = (BRN + K^2N + KK_pN)
$$

\n
$$
G_5 = JLN
$$

\n
$$
G_6 = KK_dN
$$

\n
$$
G_7 = KK_iN
$$

\n
$$
G_8 = KK_i
$$

\n
$$
TF_{SYS}(s)
$$

\n
$$
= \frac{KK_p s^{\lambda + \lambda_f} + KK_pNs^{\lambda} + KK_dNs^{\lambda + \mu}}{s^{2 + \lambda_f} + G_1 s^{\lambda + \lambda_f} + G_1 s^{\lambda + \lambda_f} + G_2 s^{\lambda + \lambda_f} + G_3 s^{\lambda + 1} + G_6 s^{\lambda + \mu} + G_4 s^{2\lambda} + G_8 s^{\lambda_f} + G_7}
$$
\n(21)

controller, there is a filter with fractional order (λ_f) and gain (N). Apart from the coefficients in the classical PID controller, these parameters also need to be optimized (Sahin [2019\)](#page-26-0).

$$
\text{TF}_{\text{PDFF}}(s) = K_p + \frac{K_i}{s} + K_d s \frac{N}{s^{\lambda_f} + N} \tag{18}
$$

As seen in (19) , a complex transfer function appears when the controller is used together with the system.

The optimizable parameters of the controllers and number of them are given in Table [2.](#page-7-0) FOPIDFF controller has maximum optimizable control parameters of 7, whereas PID has three parameters among the controllers studied in the paper.

Table 2 Optimizable parameters of the controllers

Controller	Optimizable Parameters	Number	
PID.	K_n, K_i, K_d	3	
TID	K_t , K_i , K_d , n	4	
PIDF	K_p, K_i, K_d, N	4	
TIDF	K_i , K_i , K_d , n , N	5	
FOPID	$K_n, K_i, K_d, \lambda, \mu$	5	
FOPIDE	$K_n, K_i, K_d, \lambda, \mu, N$	6	
PIDFF	$K_p, K_i, K_d, \lambda_f, N$	5	
FOPIDFF	$K_n, K_i, K_d, \lambda, \lambda_f, \mu, N$		

4 Improved artificial ecosystem optimization algorithm with fitnessdistance balance guiding mechanism by using opposite based learning methods

4.1 Artificial ecosystem optimization algorithm

The AEO algorithm was presented to the literature in 2020 by Zhao et al. ([2020\)](#page-26-0) as a new population-based metaheuristic optimization algorithm inspired by the behavior of living organisms in the ecosystem, production, consumption, and decomposition characteristics. AEO has been used in nearly 200 scientific studies since 2020 to solve real-world engineering problems and different fields of science. While the production phase in the AEO algorithm aims at the discovery and usage trends of the optimization process, the consumption phase aims to develop the discovery feature of the algorithm in the optimization process. Decomposing is defined as a process used to improve the use process of the algorithm. AEO follows

Fig. 5 The ecosystem of AEO algorithm

some rules stated below to search for the most appropriate solution in the solution process of an optimization problem.

- (1) The ecosystem including the producer, consumer, decomposer organisms should be defined as the population.
- (2) It should contain only one producer and one decomposer in the population.
- (3) Consumers selected as carnivores, herbivores, or omnivores should each have the same probability of generating other solution candidates in the population.

The ecosystem of the AEO algorithm is shown in Fig. 5. In the ecosystem constituting the population, the producer with the highest energy level $X₁$, which constitutes the population in the ecosystem is determined as the solution candidate and the decomposer with the lowest energy level X_n (best individual) is determined as the solution candidate. The producer with the highest energy level is determined as X_1 the solution candidate and the decomposer with the lowest energy level is determined as X_n (best individual) the solution candidate in the ecosystem that constitutes population Consumers representing equally distributed carnivorous, herbivorous, and omnivorous organisms for other solution candidates in the population are shown in detail in Fig. 5. The producer, consumer and decomposer processes of the algorithm are explained as follows (Zhao et al. [2020](#page-26-0); Sonmez et al. [2022](#page-26-0); Yousi et al. [2020;](#page-26-0) Rizk-Allah et al. [2021](#page-26-0)).

4.1.1 Production phase

In the optimization process of the AEO algorithm, balancing the discovery and usage trends of the algorithm to find the best value is expressed as the purpose of the production phase. The producer (the worst solution candidate) in the population is updated as in (22) using an individual (X_{rand}) that is constituted with usage of the best individual (X_n) and limit values of the variables in the population. The solution candidate, which is updated during the search process, directs the other solution candidates in the population to search in different regions of the solution space of the problem (Zhao et al. [2020](#page-26-0); Sonmez et al. [2022](#page-26-0); Topno and Chanana [2016](#page-26-0); Rai and Das [2022;](#page-26-0) Guha et al. [2017](#page-25-0); Chiranjeevi et al. [2021](#page-25-0); Divya et al. [2022](#page-25-0); Tang et al. [2012](#page-26-0); Dey et al. [2022](#page-25-0); Sahin [2019](#page-26-0); Yousi et al. [2020](#page-26-0); Rizk-Allah et al. [2021](#page-26-0)). The equations of σ ve X_{rand} parameters used in (22) are given in (23) and [\(24](#page-8-0)).

$$
X_1(t+1) = (1-\sigma)X_n(t) + \sigma X_{rand}(t)
$$
\n(22)

$$
\sigma = (1 - \frac{t}{T_{\text{max}}})r_1 \tag{23}
$$

$$
X_{rand} = r(U - L) + L \tag{24}
$$

Here *n* is defined as the population size. σ is expressed as a linear weight coefficient used to move the individual to the best individual. t and T_{max} represent the current iteration and maximum iteration numbers, respectively. r_l is a random number between $[0,1]$. *r* is a random number vector generated depending on the number of variables between [0,1]. U and L are specified as the upper and lower limits of the variables in the optimization problem.

4.1.2 Consumption phase

After the production process is completed in the ecosystem, the consumption operator is used in the algorithm for the consumers in the system. In the consumption operator, each consumer is fed by eating consumers with lower energy levels, producers, or both to obtain food energy and complete the energy flow in the ecosystem. This feeding process is simulated as the discovery process of the AEO algorithm. This process can be explained as (25) with a consumption factor with similar properties to Lévy Flight as a random walk without any parameters (Zhao et al. [2020;](#page-26-0) Sonmez et al. [2022;](#page-26-0) Topno and Chanana [2016;](#page-26-0) Rai and Das [2022](#page-26-0); Guha et al. [2017;](#page-25-0) Chiranjeevi et al. [2021](#page-25-0); Divya et al. [2022](#page-25-0); Tang et al. [2012;](#page-26-0) Dey et al. [2022;](#page-25-0) Sahin [2019;](#page-26-0) Yousi et al. [2020;](#page-26-0) Rizk-Allah et al. [2021\)](#page-26-0).

$$
C = \frac{1}{2} \frac{v_1}{|v_2|} \quad v_1 \sim N(0, 1), \quad v_2 \sim N(0, 1) \tag{25}
$$

Different types of consumers show different consumption behaviors in the consumption process. If the randomly selected individual from the population is herbivore, it feeds only on producer X_1 like consumers X_2 and X_5 , as can be seen in Fig. [5.](#page-7-0) This process is expressed mathematically as in (26).

$$
X_i(t+1) = X_i(t) + C(X_i(t) - X_1(t)), \quad i \in [2, ..., n]
$$
\n(26)

If the solution candidate selected from the population is carnivorous, it is fed with a consumer with a higher energy level than its own energy level, as seen in Fig. 5 (as in X_4) and X_6 consumers). The consumption behavior of the solution candidate carnivore can be defined by (27).

$$
X_i(t+1) = X_i(t) + C(X_i(t) - X_j(t)), \quad i \in [3, ..., n], \quad j
$$

= $randi([2, i - 1])$ (27)

If the i_{th} solution candidate selected from the population is omnivorous, it is fed by both the producer X_l and another

consumer with a higher energy level than its own. The consumption behavior of the omnivorous consumer is mathematically formulated as in (28).

$$
\begin{cases}\nX_i(t+1) = X_i(t) + C(r_2X_i(t) - X_1(t)) + (1 - r_2) \\
i \in [3, ..., n], \quad j = randi([2, i - 1])\n\end{cases}
$$
\n(28)

Here, r_2 is defined as a random number between 0 and 1.

4.1.3 Decomposition phase

Decomposition can be expressed as the most important process in terms of the functioning of the ecosystem, where when an individual dies, its remains are decomposed by decomposers such as bacteria or fungi. This process is simulated mathematically with the parameters D (*dissociation factor*) and, e and h (weighting coefficients) in the algorithm, as in (29) . In the parsing process, the position of the i_{th} solution candidate is updated via the position of the X_n parser. It also ensures that the next position of each solution candidate in the search space is located around the parser X_n (best individual), and this process is formulated as follows (Zhao et al. [2020](#page-26-0); Sonmez et al. [2022;](#page-26-0) Topno and Chanana [2016](#page-26-0); Rai and Das [2022;](#page-26-0) Guha et al. [2017](#page-25-0); Chiranjeevi et al. [2021](#page-25-0); Divya et al. [2022](#page-25-0); Tang et al. [2012](#page-26-0); Dey et al. [2022](#page-25-0); Sahin [2019](#page-26-0); Yousi et al. [2020](#page-26-0); Rizk-Allah et al. [2021\)](#page-26-0).

$$
X_i(t+1)) = X_n(t) + D \cdot (e \cdot X_n(t) - h \cdot X_i(t)), \ \forall \ i \in n
$$

$$
D = 3u, \ N(0,1), \ e = r_3 \cdot randi([12]) - 1, \ h = 2 \cdot r_3 - 1
$$
 (29)

4.2 AEO algorithm involving fitness-distance balance guiding mechanism

The FDBAEO algorithm, which includes a fitness-distance balance guiding mechanism, was presented to the literature by Sonmez et al [\(2022](#page-26-0)) in 2022. The performance of the algorithm has been increased by using the FDBAEO algorithm in the parsing process, which is one of the most important stages of the ecosystem. The FDB method aims to select the solution candidate from the population that can contribute the most to the search process after the best individual X_n used in the parsing process of the AEO. Thus, it was stated by the authors that the basic AEO algorithm provided a better balance between discovery and exploitation processes (Sonmez et al. [2022](#page-26-0)). The FDB method, which can be adapted to all optimization algorithms and creates solution diversity in the search space of algorithms, was first introduced to the literature in 2020 by Kahraman et al. ([2020\)](#page-25-0). This method has been adapted to optimization algorithms and has been used in the solution

of different science fields and engineering problems in nearly 70 scientific studies since 2020. FDB has two important features that consider the fitness values of the solution candidates and the distances from the best solution candidate (P_{best}) in the population. The implementation steps in which the FDB guidance mechanism is introduced can be expressed as follows. (Aras et al. [2021;](#page-24-0) Guvenc et al. [2021;](#page-25-0) Duman et al. [2021](#page-25-0), [2022](#page-25-0); Kahraman et al. [2022;](#page-25-0) Bakir et al. [2022](#page-25-0); Cengiz et al. [2021;](#page-25-0) Suicmez et al. [2021\)](#page-26-0).

(i) i. In meta-heuristic optimization algorithms, *n*-unit solution candidates are created in the search space within the specified limit values of the control variables according to the determined population number (n) . The vector (P) of the created solution candidates and their fitness values vector (F) can be expressed by the (30) below.

$$
P = \begin{bmatrix} p_1 \\ \vdots \\ p_2 \end{bmatrix} = \begin{bmatrix} x_{11} & \cdots & x_{1m} \\ \vdots & \ddots & \vdots \\ x_{n1} & \cdots & x_{nm} \end{bmatrix}_{n \times m}, \quad F = \begin{bmatrix} f_1 \\ \vdots \\ f_n \end{bmatrix}_{n \times 1}
$$
(30)

(ii) In a solution space with the number of solution candidates (n) and the number of variables (m) in the population, the Euclid distance of the i_{th} solution candidate p_i to the best solution candidate of the population (p_{best}) is formulated in (31).

$$
\begin{aligned} & \sum_{i=1}^{n} \forall P_i, D_{p_i} \\ &= \sqrt{\left(p_{i[1]} - p_{\text{best}[1]}\right)^2 + \left(p_{i[2]} - p_{\text{best}[2]}\right)^2 + \ldots + \left(p_{i[m]} - p_{\text{best}[m]}\right)^2} \end{aligned} \tag{31}
$$

(iii) D_P is defined by (32) as a row vector containing numerical values representing the distance of solution candidates in the population from p_{best} .

$$
D_p \equiv \begin{bmatrix} d_1 \\ \cdot \\ \cdot \\ \cdot \\ d_n \end{bmatrix}_{n \times 1} \tag{32}
$$

(iv) While calculating the FDB score values of the solution candidates in the population, the fitness values vector (F) and the distance vector (D_n) are used. It is desired that these two parameters do not dominate each other in the calculation of the FDB value. Therefore, FDB values (S_n) of possible solution candidates are calculated as in (33) by normalizing F and D_p between [0,1].

$$
{i=1}^{n} \forall P{i}, \quad S_{p_{[i]}} = w \cdot normF_{[i]} + (1 - w) \cdot normD_{p_{[i]}} \quad (33)
$$

The weight coefficient w which is set to 0.5, is used to determine the effects of normalized fitness and distance values on the FDB score.

(i) The n-dimensional vector of FDB scores (S_n) in which the solution candidates are represented in the search space is shown in (34)

$$
S_p \equiv \begin{bmatrix} s_1 \\ \cdot \\ \cdot \\ \cdot \\ s_n \end{bmatrix}_{n \times 1} \tag{34}
$$

After the S_p vector showing the FDB scores of the possible solution candidates in the search space is created, the selection of individuals from the population can be done using the greedy or probabilistic selection method. The solution candidate with the highest FDB score value is used in the selection process.

The pseudocode of the steps of applying the FDB selection method in the algorithm is shown in Algorithm 1.

4.3 FDBAEO algorithm including opposite based learning methods

This section discusses the improvement of the FDBAEO algorithm using opposition-based learning (OBL) methods. Such approach strategies take into account the position that is opposed to the current solution candidate's position. By using the values of the fitness function of the solution candidates, it is determined whether the inverse is better than the current solution candidate and the best ones are selected for use in the next generations (Tizhoosh [2005](#page-26-0); Elaziz et al. [2017;](#page-25-0) Elaziz and Mirjalili [2019](#page-25-0); Ewees et al. [2018](#page-25-0); Ekinci et al. [2022\)](#page-25-0). OBL methods focus on increasing the rate of convergence to the optimal solution by improving the exploration capability of the FDBAEO algorithm. The OBL strategies used for the proposed algorithm in this study are described mathematically below.

i. In the method presented by Tizhoosh [\(2005](#page-26-0)) to the literature, $x \in [L, U]$ is defined as the inverse of the real number \bar{x} , as seen in (35).

$$
\overline{x} = L + U - x \tag{35}
$$

The definition of x in the multidimensional search space can be formulated with generalization as seen in (36) (Tizhoosh [2005\)](#page-26-0).

$$
\bar{x}_j = L_j + U_j - x_j
$$
, $x \in R^{nn}$, $j = 1, 2, ..., nn$ (36)

Here, j represents the number of variables in the solution candidate. The size of the solution candidate in the search space is defined as nn .

ii. Rahnamayan et al. ([2007\)](#page-26-0) presented the Quasi-OBL (QBL) method to the literature to improve the performance of the differential evolution algorithm with the help of the following mathematical equation. The quasi-opposite solution (\overline{x}_q) of solution candidate x is generated as a random solution candidate uniformly distributed between the midpoint (*mid*) and the opposite solution (\bar{x}) as shown in (37).

 $\overline{x}_q = mid + (mid - \overline{x}) \times rand$ (37)

$$
mid = (U + L)/2
$$

$$
\overline{x}_{qr} = U + (mid - \overline{x}) \times rand
$$
 (38)

iv. Kaucic [\(2013](#page-26-0)) provided the convergence of the particle swarm optimization algorithm to the global solution by using super-opposite based learning method in 2013. The performance of the algorithm proposed by the author has been verified by testing 100 global optimization problems.

iii. Ergezer et al ([2009\)](#page-25-0) proposed the Quasi-Reflection OBL (QROBL) method to improve the convergence rate of the biogeography-based optimization algorithm. In this method, the quasi-reflected solution (\overline{x}_{qr}) of the x solution candidate is mathematically defined as a uniformly distributed random solution as in (38).

Equation (39) represents the uniformly distributed superopposite solution (\overline{x}_{so}) of the solution candidate x.

$$
\overline{x}_{so} = \begin{cases} \overline{x} + (U - \overline{x}) \times \text{rand} & \text{if } \overline{x} > \text{mid} \\ L + (\overline{x} - L) \times \text{rand} & \text{otherwise} \end{cases}
$$
(39)

The pseudocode of OBL methods showing the application steps in the FDBAEO algorithm is shown in Algorithm 2.

Algorithm 2 The pseudo code of the FDBAEO algorithm including OBL strategies

5 Experimental settings of the study

An experimental study is conducted to verify the success of the OBL-based FDBAEO algorithm, which is developed for the speed control of the DC motor from electrical machines, in convergence and finding the optimal solution. The FDBAEO algorithm based on OBL methods is defined as follows.

- FDBAEO_OBL1: FDBAEO algorithm based on the classical OBL method
- FDBAEO_OBL2: FDBAEO algorithm based on Quasi-OBL method
- FDBAEO_OBL3: FDBAEO algorithm based on Quasi-Reflection OBL method
- FDBAEO_OBL4: FDBAEO algorithm based on Super OBL method

Comparison of the performances of FDBAEO algorithms based on the above mentioned OBL methods, classical AEO and FDBAEO algorithms is performed under the conditions described below.

- (a) CEC2020 benchmark test is used to test the global solution search performance of FDBAEO algorithms based on AEO, FDBAEO and OBL methods.
- (b) 10000*D maximum function evaluations (maxFEs) are used as termination criteria in the search space. Thus, a fair comparison environment is created for the algorithms to search for the global solution during the optimization.
- (c) To evaluate the convergence performance of the algorithms to the general solution in different search spaces, experimental studies are carried out in the

Benchmark test system for the dimensions of 5/10/ 15/20/30/50/100.

(d) 30 independent trials are conducted for each test problem in the CEC2020 benchmark test system. Statistical analysis studies are carried out to make the results obtained from these experimental studies more meaningful. In these studies, non-parametric Wilcoxon pairwise and Friedman statistical test methods are used.

The performances of FDBAEO algorithms, classical AEO and FDBAEO algorithms based on the proposed OBL methods are described as follows in two different experimental studies.

- (i) First subsection: the successful performances of the proposed method and other algorithms are investigated in the CEC2020 (Yue et al. [2019\)](#page-26-0) benchmark test functions.
- (ii) The parameters of the controllers used in the speed control of the DC motor are optimized by using the most successful algorithm among the FDBAEO algorithms based on OBL methods. Thus, it is aimed to design the most suitable controller for the speed control problem of the DC motor.

6 Simulation studies

6.1 Identifying the best FDBAEO algorithm based on OBL methods in CEC 2020 Benchmark Test Functions

CEC 2020 benchmark test functions are used to test the success and ability of the FDBAEO algorithm designed according to four different OBL strategies in finding the global solution point in these test functions. In order to make a fair comparison between the proposed approach, AEO and FDBAEO algorithms, the adjustment parameters of the algorithms determined according to the user experience are accepted as presented in the literature in the basic AEO algorithm and simulation studies are carried out.

6.1.1 Statistical analysis

In the statistical analysis subsection, the Friedman method is used to statistically analyze the results obtained from the experimental studies of the FDBAEO_OBL, AEO and FDBAEO algorithms. By means of this non-parametric method, the algorithm that successfully finds the global solution point is determined. The problem size in each of the benchmark test functions in CEC 2020 has been

determined as 5/10/15/20/30/50 and 100. In addition, two different case studies are determined as population numbers of 100 and 200. The Friedman results and the success ranking of the algorithms according to the statistical analysis of the results obtained from the simulation studies on these problem sizes and population numbers are presented in detail in Tables [3](#page-13-0) and [4](#page-13-0), respectively.

The Friedman values from 14 different trials are presented in Table [3](#page-13-0). According to these values, different population numbers and mean values of Friedman results for each algorithm are demonstrated in Table [4](#page-13-0). The last row in Table [4](#page-13-0) shows the Friedman overall mean values and the ranking of the algorithms based on these values. Under the simulation conditions determined for the CEC 2020 benchmark test functions, it is clearly seen that the best performing algorithm compared to its competitors in finding the global solution is FDBAEO_OBL3 (FDBAEO algorithm based on Quasi-Reflection OBL method). Also, the algorithm with the worst performance is the FDBAEO algorithm. In addition, according to the results in Table [4,](#page-13-0) it is seen that each of the FDBAEO algorithms designed according to the OBL strategies is better than the AEO and FDBAEO algorithms.

The results obtained from the CEC2020 benchmark test functions are used in the Wilcoxon pairwise test to compare the classical AEO algorithm with other algorithms and the Wilcoxon results of the algorithms against the AEO algorithm are given in Table [5.](#page-14-0)

At the end of the optimization process, in order for the Wilcoxon binary test results to be statistically meaningful, the victory of the algorithm against the AEO algorithm is defined with the " $+$ " symbol, the draw with the " $=$ " symbol, and the defeat with the "-" symbol. The FDBAEO_OBL3 algorithm, which ranked first among the algorithms according to the Friedman test results, is evaluated for the situation where the population number is 100 in the CEC 2020 benchmark test functions. According to the evaluation results, FDBAEO_OBL3 performed 4/8/7/1/ 1 times better than the classical AEO algorithm in 5/10/15/ 20/50 problem sizes. The proposed approach and the AEO algorithm in these problem sizes have obtained similar results 2/2/2/9/9 times. In the 30- and 100-dimensional search space, the proposed approach and the AEO algorithm converged to a similar result 10/10 times. For the 5/10/15/20/30/50/100-dimensional search space, when the population number is 200, the FDBAEO_OBL3 algorithm victories the AEO algorithm 1/4/4/6/5/4/4 times. Moreover, the proposed approach is drawn 3/5/3/1/3/5/2 times and defeated 6/1/3/3/2/1/4 times with the AEO algorithm. In other words, the FDBAEO_OBL3 algorithm has been compared with the AEO algorithm 140 times in the simulation studies conducted with different populations and sizes, and according to the results of the comparison, 49

Table 3 Freidman test results of the optimization algorithms

Table 4 Friedman test ranking of the optimization algorithms

The color was used to show the best results

wins, 66 draws and 25 losses have been achieved. To better understand and evaluate these results, the percentage comparison of wins, draws and defeats in test functions against the AEO algorithm of the proposed approach is given in Table [6](#page-14-0). According to the results in Table [6,](#page-14-0) where wins, draws and defeats are evaluated as percentages, it is clearly seen that the FDBAEO_OBL3 algorithm is superior to the AEO algorithm in 9 of 14 different simulation studies.

6.1.2 Convergence analysis

This subsection presents the convergence curves and boxplot figures of the OBL variants of the AEO, FDBAEO and FDBAEO algorithms. Convergence and boxplot analysis aims to better understand and interpret optimization algorithms for search and convergence to the global solution point in different problem types. Convergence curves and boxplot graphs in cases where the population numbers of test problems selected from the CEC 2020 benchmark test functions are 100 and 200 are shown in Figs. [6](#page-15-0) and [7,](#page-16-0) respectively. Figures [6](#page-15-0) and Fig. [7a](#page-16-0), d and g show the variation of the error value obtained depending on the convergence of the algorithms to the optimal solution value according to the maximum fitness function evaluation criterion. The graphs showing the change in convergence values of the best fitness values obtained depending on the iteration are shown in Figs. [6](#page-15-0) and [7b](#page-16-0), e and h. The performance of all optimization algorithms is tested by performing 30 independent trials for each simulation case. Boxplot plots are given in Figs. [6](#page-15-0) and [7c](#page-16-0), f and i for better interpretation of the results from these independent runs. Boxplot plots show the limits of the best fitness values that the optimization algorithms found in independent trials. In other words, it gives information about the frequency of convergence of the algorithm to the optimal solution after

Table 5 Wilcoxon pairwise comparison results for the

optimization algorithms

Table 6 Comparison of FDBAEO_OBL3 algorithm against AEO algorithm as a percentage of victory, draw and defeat

	CEC 2020						
FEBAEO OBL3 vs. AEO	Pop size= 100						
	$D=5$	$D=10$	$D=15$	$D=20$	$D=30$	$D=50$	$D=100$
Victory $(\%)$	40	80	70	10	-	10	
Draw $(\%)$	20	20	20	90	100	90	100
Defeat $(\%)$	40		10				
	Pop size= 200						
FEBAEO OBL3 vs. AEO	$D=5$	$D=10$	$D=15$	$D=20$	$D=30$	$D=50$	$D=100$
Victory $(\%)$	10	40	40	60	50	40	40
Draw $(\%)$	30	50	30	10	30	50	20
Defeat $(\%)$	60	10	30	30	20	10	40

The color was used to show the best results

30 trials. It is clear from the boxplot graphs that depending on the problem type, the proposed FDBAEO_OBL3 algorithm always converges to the optimal solution value of the problem or closer value to optimal solution. Moreover, these graphs confirm the results of both Friedman and Wilcoxon non-parametric statistical analysis.

6.2 Application of the FDBAEO_OBL3 algorithm in controller design of DC motor

The speed control of the DC motor is realized in MATLAB/Simulink environment with the developed FDBAEO_OBL3 algorithm. Figure [8](#page-17-0) displays the flow diagram or block diagram illustrating the optimization procedure whereby the controller parameters utilized for DC motor speed control are optimized via the use of the proposed algorithm. The speed error between the reference speed and the measured actual speed in the control structure is computed and provided to the controller whose parameters are optimized, as can be seen in the block diagram in Fig. [8.](#page-17-0) The speed control of the motor is achieved by applying the signal that makes the error produced by the controller to zero to the DC motor. PID, FOPID, TID, TIDF, PIDF, FOPIDF, PIDFF, and FOPIDFF controllers are used to provide speed regulation of the DC motor. The optimization algorithm's objective functions are created based on the performance indices. The optimized controller parameters are represented in the

Fig. 6 Convergence and boxplot shapes of algorithms for Pop_size = 100

optimization process by the solution candidate with the lowest objective function value. The DC motor speed regulation circuit tests these parameters and the outcomes are examined.

6.2.1 Using performance indices as objective functions during optimization

The performance indices that are commonly used in the literature are IAE (Ghith and Tolba [2023\)](#page-25-0), ISE (Izci et al. [2022a](#page-25-0)), ITAE (Majhi et al. [2021\)](#page-26-0) and ITSE (Barakat et al. [2022\)](#page-25-0). The equations of the indices that are used as the objective functions are presented in Eqs.(40)–(43). They are used in the study to evaluate the performance of the controllers that are optimized.

$$
IAE = \int_0^T |e(t)|dt
$$
\n(40)

$$
ISE = \int_{0}^{t} e^{2}(t)dt
$$
 (41)

T

$$
ITAE = \int_{0}^{T} t|e(t)|dt
$$
\n(42)

$$
ITSE = \int_{0}^{T} te^{2}(t)dt
$$
\n(43)

6.2.2 Evaluation of simulation results obtained according to performance indices

In Table [7,](#page-18-0) rise time, settling time, overshoot, peak value, peak time and steady-state error values of the controllers optimized with the FDBAEO_OBL3 method based on IAE, ITAE, ITSE and ISE performance indices are shown.

Fig. 7 Convergence and boxplot shapes of algorithms for Pop_size = 100

As a result of these data, the best performance indices of each controller in different performance parameters are determined and highlighted. In the PID controller, all the best results are obtained with the ITSE index, while in the FOPID controller, the best rise time is obtained with the IAE index and the other best results are obtained with the ITSE index. As seen in the table, these determinations are made for all controller and performance indices.

Table 8 is created by ranking $1-4$ from the best to the worst in the performance results seen in Table [7.](#page-18-0) The best result is represented by 1, while 4 is used for the worst result. Then, the scores of the parameters are averaged and the average values are obtained. Based on these values, the average value ranking is made. Thus, the performance index with the best score is determined for each controller. According to this method, as seen in Table [8](#page-19-0), ITAE for PID controller, ITSE for FOPID, ISE for TID, IAE for TIDF, ITAE for PIDF, IAE for FOPID, ITAE for PIDFF and IAE for FOPIDFF are the best performance indices. They are highlighted in the table.

Table [9](#page-19-0) is obtained depending on Table [8.](#page-19-0) The best performance index for each controller is determined based on ''Ranking of mean values'' in Table [8](#page-19-0), and the best transient response values are given in Table [9](#page-19-0) for each controller. In addition, the best controller for each transient response parameter is determined by scoring the controllers. The best controller for transient response is selected by averaging the scores of the controllers. As seen in Table [9](#page-19-0), the first and best performance controller is FOPIDFF. The best four controllers that are FOPIDFF, FOPID, FOPIDF and PID between eight controllers are determined depending on the Table [9](#page-19-0) and they are used for the performance analysis in the rest of the work. The step performance of the controllers is seen Fig. [9](#page-20-0). As seen in Fig. [9](#page-20-0)a, all controllers settle to the reference value with successful steady-state response. The maximum overshoot occurs in FOPIDF controller while the minimum overshoot occurs in FOPID controller. The minimum settling time and rise time belongs to FOPIDFF and FOPIDF, respectively. The results can be seen in Table [9](#page-19-0) and Fig. [9b](#page-20-0).

Fig. 8 Flowchart of the optimization process of the proposed FDB-AEO-OBL algorithm

FOPID and FOPIDFF controllers have almost the same response, but FOPIDFF has little higher performance.

In this study, eight distinct controller structures with different design parameters were used to ensure speed regulation of the DC motor and to contribute the motor operate more steadily under changing operating conditions. Stated differently, appropriate determination of the parameters in a controller structure ensures that the systems can operate stable and reliably. In light of this circumstance, Table [10](#page-20-0) provides a detailed display of the parameters that were acquired by applying the proposed FDBAEO-OBL technique to identify the most suitable controller settings. Additionally, Table [10](#page-20-0) displays the optimal parameter values of the top four controller architectures, based on the outcomes of several objective functions. Four controller structures that differ from each other in terms of computational complexity demonstrated more effective performance than TID, TIDF, PIDF and PIDFF controllers in providing speed regulation of the DC motor. Determining the parameters of a controller structure using optimization algorithms affects the calculation time of the optimization algorithm during the optimization process. The quantity of parameters in the controller structures that need to be optimized is the cause of this. The computational complexity of controller structures with fewer parameters is lower than that of controller structures with more parameters when controller structures with optimized parameters are assessed in terms of application. Nonetheless, the sampling frequency needs to be determined in accordance with the controller structure with the highest computational complexity if it is intended to test the performance of controllers in systems equitably.

To examine the dynamic response of the controllers depending on the speed reference change of the motor, five different speed refences are applied to the controllers in different time intervals that are given in Table [11](#page-20-0). The start-up speed reference is set to 1, and it increases to 1.2 and 1.5 in the next two intervals. In the last two intervals, the speed reference decreases to 0.6 and 0.8.

Table 7 Performance criteria of the controllers FDBAEO_OBL3

	Transient		Performance Indices				Transient Controller		Performance Indices		
Controller	responses	IAE	ITAE	ITSE	ISE		responses	IAE	ITAE	ITSE	ISE
	Rise time (s)	0.064	0.0606	0.0663	0.0704		Rise time (s)	0.0526	0.0513	0.0551	0.0573
	Settling time (s)	0.462	0.318	0.492	0.675		Settling time (s)	0.498	0.361	0.674	1.16
PID	Overshoot $(\%)$	23	18.7	26.6	35.7	PIDF	Overshoot $(\%)$	46.9	40.3	54.5	65.2
	Peak value (V)	1.23	1.19	1.27	1.36		Peak value (V)	1.47	1.4	1.54	1.65
	Peak time (s)	0.161	0.153	0.166	0.177		Peak time (s)	0.143	0.137	0.15	0.162
	SS Error (V)	Ω	Ω	$\mathbf{0}$	0		SS Error (V)	$\mathbf{0}$	Ω	$\bf{0}$	0
	Rise time (s)	0.00536	0.0402	0.0241	0.0155		Rise time (s)	0.0147	0.0335	0.0153	0.00626
	Settling time (s)	0.0794	0.189	0.0503	0.143		Settling time (s)	0.0848	0.165	0.083	
FOPID	Overshoot $(\%)$		12.5		0.268	FOPIDF	Overshoot $(\%)$	21.6	24.5	19.4	32.9
	Peak value (V)	0.995	1.13	0.993	1.00268		Peak value (V)	1.22	1.25	1.19	1.33
	Peak time (s)	0.225	0.0939	0.078	0.547		Peak time (s)	0.0358	0.0854	0.0367	0.0166
	SS Error (V)	0.005	θ	Ω	0		SS Error (V)	$\mathbf{0}$	0.01	$\mathbf{0}$	0.02
	Rise time (s)	0.07666	07674		0.07675 0.07617		Rise time (s)	0.0518	0.0502	0.054	0.0567
	Settling time (s)	0.566	0.566	0.566	0.566		Settling time (s)	0.95	0.441	1.52	3.14
TID	Overshoot $(\%)$	12	12	12	12	PIDFF	Overshoot $(\%)$	63.3	44.8	69.8	77.9
	Peak value (V)	1.12	1.12	1.12	1.12		Peak value (V)	1.63	1.45	1.7	1.78
	Peak time (s)	0.258	0.259	0.259	0.258		Peak time (s)	0.146	0.134	0.156	0.16
	SS Error (V)	Ω	$\mathbf{0}$	$\mathbf{0}$	$\overline{0}$		SS Error (V)	$\mathbf{0}$	Ω	$\bf{0}$	0
	Rise time (s)	0.0742	0.0766	0.0769	0.076		Rise time (s)	0.0224	0.0369	0.0243	0.00434
	Settling time (s)	1.93	2.22	3.09	3.74	FOPIDFF	Settling time (s)	0.0416	0.167	0.043	0.146
TIDF	Overshoot $(\%)$	72.9	75.5	79.8	83.7		Overshoot $(\%)$	0.661	4.62	0.734	2.85
	Peak value (V)	1.73	1.75	1.8	1.84		Peak value (V)	1.00661	1.05	1.00734 1.03	
	Peak time (s)	0.206	0.215	0.218	0.218		Peak time (s)	0.07	0.0898	0.0713	0.00876
	SS Error (V)	0	$\mathbf{0}$	$\mathbf{0}$	θ		SS Error (V)	0.003	0.01	0.007340	

The color was used to show the best results

Figure [10](#page-22-0) shows the dynamic response of the controllers for five different speed references. All the controllers have good steady-state response by settling the reference value. The dynamic response of the controllers in Region 1– Region 5 is shown in detail in Fig. [10b](#page-22-0)–f. As can be seen from the figures, the FOPID and FOPIDFF controller shows good performance in terms of settling time, overshoot and steady state response. The controllers have similar responses as in Fig. [9.](#page-20-0) A Bode diagram of the controllers can be seen in Fig. [11.](#page-22-0)

Four different scenarios are created to examine how the system responded at different motor parameters. In the scenarios created, the motor armature resistance is 0.75 and 1.25, and the torque constant is 0.0184 and 0.0276. The scenarios created using these values are given in Table [12.](#page-22-0)

When Scenario I in Table [12](#page-22-0) is applied, the change in the response of the system can be seen in Fig. [12.](#page-22-0) When compared with the response obtained from the basic motor parameters used in the study, it is seen that there is a decrease in the overshoot value of the FOPIDF controller. The time to reach steady state of the PID controller has increased, however, the controller is successful in the steady state response. The numerical expressions of the response performances of the controllers are shown in Table [13](#page-22-0).

In the second scenario, the moment constant is increased by keeping the armature resistance constant. In this case, the step responses of the controllers and the transient response at the beginning are seen in Fig. [13.](#page-23-0) The numerical values of the response performances of the

controllers in these changes are given in Table [14](#page-23-0). As can be seen from the response curves, the overshoot of the PID controller decreases while the overshoot of the FOPIDF controller increases. When examined in terms of steadystate response, the PID controller enabled the system to settle in a shorter time. Other transient response performance values are given in Table [13](#page-22-0). When examined in terms of steady state, all controllers ensured that the system is set to the reference value despite the parameter change.

The third scenario is created by increasing the motor armature resistance and using the torque constant at the value used in Scenario I. The performance data of the controllers of Scenario III, whose step response is seen in Fig. [14](#page-23-0), are given in Table [15](#page-23-0). While the PID controller overshoot performance is the same as in Scenario II, the FOPIDF overshoot value is the least compared to Scenario I and Scenario II. FOPIDFF controller response reached the reference value in the shortest time. In the steady state response, all controllers reached the reference value. Performance values are given in detail in Table [15](#page-23-0).

In Scenario IV, which is the last scenario, the moment constant is increased while the armature resistance is kept constant. When the response changes and performance values seen in Fig. [15](#page-24-0) and Table [16](#page-24-0) are examined, the PID controller result improved in terms of overshoot and the FOPIDF controller response worsened. While FOPIDFF gives the best result in terms of settling time, the time is shortened compared to Scenario III. In the steady state response, all the controllers ensured that the system is set to the reference value.

Table 8 Performance scoring of the controllers

The color was used to show the best results

The color was used to show the best results

6.2.3 Computational complexity of the proposed algorithm

Computational complexity in optimization algorithms tells researchers how long it takes for an algorithm to solve a given problem; this time varies depending on the program's design parameters. In the literature, computational complexity is expressed in a variety of ways. To help readers better comprehend computational complexity, the methodology used in related articles (Ekinci et al. [2022](#page-25-0); Izci et al. [2023\)](#page-25-0) is applied to the discussion of computational complexity in this study. The computational complexity of the baseline AEO and intended FDBAEO-OBL algorithms is calculated considering three main criteria. These can be expressed as initializing the solution space,

Fig. 9 Step response of the controllers a Step response, b Transient response at start

Table 10 Optimized parameter values of the four best controllers

Parameter	PID.	FOPID	FOPIDF	FOPIDFF
K_p	49.9854	30.7432	26.4429	25.1659
K_i	0.3459	9.3411	9.1942	9.8338
K_d	3.9757	16.0164	18.4174	16.2685
λ		1.0011	0.4823	0.1537
μ		1.0203	1.0206	1.0203
\overline{N}			121.7686	146.8065
λ_f			1	0.2517

 $4 \le t$ 0.8

calculating the fitness function of each solution candidate in the solution space depending on the design steps, and updating the positions of the solution candidates. The computational complexity of the AEO algorithm can be computed using these three criteria. $CC(ABO) = CC(N) + CC(N \times t_{max})$ -

+ CC($N \times d \times t_{\text{max}}$), where, N, t_{max} , and d can be expressed as the size of the solution space, the maximum number of iterations, and the dimension of the problem, respectively. However, the computational complexity of the proposed FDBAEO_OBL algorithm can be given as $CC(FDBAEO_O) = CC(AEO) + CC(N \times t_1)$ -

+ CC(2 \times N \times t_{max}). CC(N \times t₁) shows the effect of

OBL strategies used in the initial population on the computational complexity. $CC(2 \times N \times t_{max})$ represents the additional computational load brought about by the FDB guiding mechanism. The proposed FDBAEO_OBL algorithm appears to have an additional computational overhead, both because it is used in the initial population of OBL strategies and because the FDB guidance mechanism is used in updating solution candidates. Although this may seem to be a disadvantage of the algorithm in terms of calculation time, improving the ability to find the optimal solution, quickly converge to the optimal solution, and avoid local solution traps are expressed as the biggest advantages of the algorithm.

7 Conclusion

This study aims to improve the performance of the FDBAEO algorithm by using classical OBL, Quasi-OBL, Quasi-Reflection OBL and Super OBL methods. These four different OBL methods are used to increase the solution diversity to find the global point of the solution space created in the initial population of the optimization algorithm and their performance is tested in different simulation studies. In the first simulation study, variations of the FDBAEO algorithm based on OBL methods are investigated in different dimensional search spaces and population numbers in terms of their ability to converge to the optimal solution, exploration, exploitation, and avoidance of problem-based local solution traps, using the CEC2020 benchmark test functions. According to the experimental results obtained from different simulation scenarios, non-parametric Wilcoxon and Friedman tests are applied to statistically evaluate the optimal solution search performance of the algorithm. According to statistical

b Fig. 10 Dynamic response of the controllers a normal version, b zoom of region 1, c zoom of region 2, d zoom of region 3, e zoom of region 4, f zoom of region 5

Fig. 11 Bode plots of the controllers

results, FDBAEO algorithm based on Quasi-Reflection OBL (FDBAEO_OBL3) method is more successful than FDBAEO algorithms with other OBL versions, basic AEO and FDBAEO algorithms.

Table 13 The performances of the controller in Scenario I

Transient responses	Controllers						
	PID	FOPID	FOPIDE	FOPIDFF			
Rise time (s)	0.0695	0.0308	0.0178	0.0279			
Settling time (s)	0.489	0.142	0.0903	0.0535			
Overshoot $(\%)$	22.3	0.0236	14.9	0.107			
Peak value (V)	1.223	1.000236	1.149	1.00107			
Peak time (s)	0.177	0.142	0.0413	0.0954			

The proposed FDBAEO_OBL3 method is used in the second simulation study to set the controller parameters used for speed regulation of DC motors which is electrical machine used in many electrical engineering applications. The parameters of eight different controller structures are determined by the proposed optimization algorithm and their performances are tested in different simulation scenarios. Depending on the rise time, settling time, overshoot and peak time values, the performances of the controllers are evaluated with statistical scoring values according to the results obtained from different objective functions. Based on these statistical scoring results, the four best controller structures for DC motor speed regulation are determined. To evaluate the performance of these

Fig. 12 Step response of the controller for Scenario I a Step response, b Transient response at start

Fig. 13 Step response of the controller for Scenario II a Step response, b Transient response at start

Transient responses	Controllers						
	PID	FOPID	FOPIDE	FOPIDFF			
Rise time (s)	0.0519	0.0188	0.0126	0.0159			
Settling time (s)	0.292	0.0372	0.0975	0.0314			
Overshoot $(\%)$	18.6	θ	29.2	0			
Peak value (V)	1.18		1.29				
Peak time (s)	0.135	0.07	0.0323	0.06			

Table 14 The performances of the controller in Scenario II

Table 15 The performances of the controller in Scenario III

Transient responses	Controllers						
	PID	FOPID	FOPIDE	FOPIDFF			
Rise time (s)	0.0728	0.0325	0.0181	0.0294			
Settling time (s)	0.356	0.0775	0.0989	0.0689			
Overshoot $(\%)$	18.7		13.3				
Peak value (V)	1.187	0.989	1.13	0.991			
Peak time (s)	0.183	0.14	0.0411	0.15			

controllers in detail, simulation studies are carried out under different scenarios. According to the comparative results obtained from the simulation studies, it is clearly seen that the FOPIDFF controller, whose parameters are adjusted using the proposed FDBAEO_OBL3 method, exhibits a more successful and superior performance than

Fig. 14 Step response of the controller for Scenario III a Step response, b Transient response at start

Fig. 15 Step response of the controller for Scenario IV a Step response, b Transient response at start

Transient responses	Controllers						
	PID	FOPID	FOPIDF	FOPIDFF			
Rise time (s)	0.054	0.0195	0.0127	0.0164			
Settling time (s)	0.295	0.0445	0.0777	0.037			
Overshoot $(\%)$	16		27.7				
Peak value (V)	1.16	0.989	1.27	0.989			
Peak time (s)	0.137	0.07	0.0322	0.06			

Table 16 The performances of the controller in Scenario IV

other controller structures. All the simulation studies show that the controller coefficients that provides the desired high performance in DC motor speed control can be determined with the optimization method.

The FDBAEO_OBL3 method can be used in solving optimization problems in different fields of science and especially in solving power systems planning and operation problems such as optimal power flow, economic dispatch, combined heat and power economic dispatch, energy management of micro-grid and transmission expansion planning.

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Data availability There is no additional data associated with this manuscript.

Declarations

Conflict of interest The authors declare that they have no conflict of interest.

Ethical approval This article does not contain any studies with human participants or animals performed by any of the authors.

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