



An enhanced approach for optimizing mathematical and structural problems by combining PSO, GSA and gradient directions

Farsad Salajegheh¹ · Eysa Salajegheh¹ · Saeed Shojaee¹

Accepted: 14 March 2022 / Published online: 16 April 2022

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Abstract

In this paper, the combination of particle swarm optimization (PSO) and gravitational search algorithm (GSA) is enhanced by the first-order gradient method and a new optimization algorithm is introduced as GPSG. In metaheuristic methods, some search directions are randomly selected and the resulting information gradually progresses toward the optimal solution. Since along the gradient direction usually yields the largest decrease in the desired function, it is added to the GSA and PSO process to allow for faster and more accurate convergence. By integrating the metaheuristic methods with the gradient directions, a powerful method for optimizing functions has been made possible. A novel approach is introduced by merging two metaheuristic methods with the randomly generated steepest decent directions. Numerous examples of unconstrained problems of mathematical functions of CEC2005 and CEC2017 together with some constrained examples of stress and displacement structural design problems have been chosen to demonstrate the reliability and capability of the presented method. Comparison of the numerical results with some methods indicates that the average rank of the proposed technique is better.

Keywords Particle swarm optimization · Gravitational search algorithm · Gradient directions · CEC2005 and 2017 · Structural design

1 Introduction

The optimization methods are divided into two main groups. The traditional mathematical programming techniques belong to this category (Vanderplaats 1999; Rao 2009; Haftka et al. 1990). Most of the techniques are based on choosing some search directions employing the first and higher-order derivatives of the functions under consideration. The search directions and the step lengths are modified to reach the desired optimal solution. The final results may not lead to global optimum for multimodal functions.

The methods are referred to as gradient-based approaches (GBA).

The second type of method is modern optimization methods that are based on statistical search directions and derived from different behaviors in nature (Yang 2010; Parmee 2001; Gandomi et al. 2013; Du and Swamy 2016; Yang et al. 2016; Siddique and Adeli 2017; Zhou et al. 2013; Akhtar et al. 2020). In these methods, the relevant variables are randomly selected in the design space and with intelligent computational methods, the results gradually move toward the optimal design. As all the design space is explored, it is possible to calculate the near-global optimal design (Osińska et al. 2013). There are several intelligent methods based on the social life of creatures, like particle swarm optimization (PSO) (Kennedy and Eberhart 1995), artificial immune systems (AIS) (Dasgupta 2006; Farmer et al. 1986), ant colony search algorithm (Dorigo and Stützle 2004) and harmony search algorithm (Geem 2010; Geem et al. 2001). Another category of science-based principles inspired by different disciplines like physics and chemistry such as simulated

✉ Eysa Salajegheh
eysasala@uk.ac.ir

Farsad Salajegheh
farsad.salajegheh@eng.uk.ac.ir

Saeed Shojaee
saeed.shojaee@uk.ac.ir

¹ Civil Engineering Department, Shahid Bahonar University of Kerman, Kerman, Iran

annealing (Kirkpatrick et al. 1983; Aarts and Korst 1989), quantum computing (Benioff 1980), central force optimization (Formato 2007, 2008), gravitational search algorithm (Rashedi et al. 2009, 2018) and chemical reaction optimization (Guggenheim and Modern 1967; Lam and Li 2010).

Among the heuristic optimization methods, the PSO method is attractive that has been studied by many researchers (Kashani et al. 2020). Different variants of PSO have been successfully presented in the literature (Kumar et al. 2020, 2021; Das et al. 2021). Another interesting approach is the gravitational search algorithm (GSA) that has been recently presented by researchers at the Shahid Bahonar University of Kerman with various modifications (Ebrahimi Mood et al. 2015).

The weakness of the standard random metaheuristic methods is the slow convergence and the approaches require a high number of particles in the design space with many iterations. If these methods are merged with deterministic methods such as gradient-based approaches (GBA), the optimal results will be achieved more efficiently with rapid convergence.

In this paper, the PSO and GSA methods with the GBA are combined and a new innovative method called GPSG (GSA + PSO + GBA) is introduced. To evaluate the performance of the approach, 25 mathematical optimization functions of CEC2005 (Suganthan et al. 2005) and 29 complicated multimodal functions of CEC2017 (Awad et al. 2017) are examined. Besides, three truss design problems from the literature are chosen to verify the convergence of the approach. The numerical results of PSO, GSA and GPSG are compared and it is observed that the performance of GPSG is much better than other approaches. In the next sections, first, a brief description of the methods of PSO and GSA are outlined and then the details of GPSG are presented. The numerical results of the three approaches are compared with some of the methods in the literature.

2 Optimization algorithms

This section presents the basic ideas of PSO, GSA, GBA and the proposed GPSG. The pseudo-code of the approach is outlined to clarify the main steps of the approach.

2.1 Particle swarm optimization (PSO)

Kennedy and Eberhart (1995) developed a metaheuristic optimization method based on a random search. In this algorithm, a random initial population with a certain number of particles is generated in the design space as indicated in (1).

$$\mathbf{X}_i = (x_i^1, \dots, x_i^d, \dots, x_i^n) \text{ for } i = 1 : NP, \quad (1)$$

where \mathbf{X}_i is the vector of the design variables of the particle i , n is the number of design variables, d denotes the dimension of the problem, and NP is the number of all particles.

The particles share their information with other particles. So each particle can adjust its position according to its previous experience and makes the best use of its own and its neighbors.

As a result, in the progress of optimization, over time to obtain the best possible response, the movement of each particle is based on self-awareness and the intelligence of the group particles.

In the PSO method, the particle velocity can be calculated according to (2).

$$\mathbf{V}_i^{t+1} = \omega \mathbf{V}_i^t + c_1 r_1 (\mathbf{P}_i^t - \mathbf{X}_i^t) + c_2 r_2 (\mathbf{P}_g^t - \mathbf{X}_i^t), \quad (2)$$

where \mathbf{V}_i^t is the velocity and \mathbf{X}_i^t is the positions of any particle at time t . The vectors \mathbf{P}_i^t (Pbest) are the best particle position i and \mathbf{P}_g^t (Gbest) are the best particle position in the whole society and the index g stands for global. The parameter ω is the weight of inertia to apply the importance of the velocity of the preceding iterations that gradually decreases linearly from 0.9 to 0.4 overtime. The scalars c_1 and c_2 are coefficients to determine the significance of Pbest and Gbest, respectively. In this study, an experimental value of 0.5 is considered for both coefficients. The coefficients of r_1 and r_2 are random scalars with a uniform distribution in the interval of zero and one to maintain the randomness of the algorithm. Note that initially, all particle velocities are set to zero. The first part of (2) is a portion of the speed of the previous iteration. The second and third parts are the effects of the particle in question and the whole group particles, respectively, from the beginning of the path to the moment t . PSO keeps the memory of all the best results of the previous iterations.

The particles are updated according to (3).

$$X_i^{t+1} = X_i^t + V_i^{t+1}. \tag{3}$$

By repeating the process, the optimal solution to the problem can be obtained.

2.2 Gravitational search algorithm (GSA)

To minimize the objective function, a set of particles is randomly assigned in the design space and updated over time. The position of each particle is defined as (1). The gravitational search algorithm is inspired by the law of gravity in nature using Newton’s laws. In summary, the acceleration vector of the *i*th particle in iteration *t* can be specified as (Rashedi et al. 2009, 2018);

$$a_i^t = G(t) \sum_{j=1}^n \left[\text{rand}_j \frac{M_j(t)}{R_{ij}(t) + \epsilon} (X_j^t - X_i^t) \right], \tag{4}$$

where *G* is the gravitational constant. *M_j* represents the mass of the *j*th particle and can be evaluated from the objective functions of particles (Rashedi et al. 2009). *R_{ij}* is the distance between the particles of *i* and *j*. *rand_j* is a random scalar with uniform distribution in the interval of zero and one, and *ε* is a small number to prevent numerical errors.

The gravitational constant *G₀* is defined as (Rashedi et al. 2009);

$$G(t) = G_0 e^{-\alpha t}, \tag{5}$$

where the parameters *G₀* and *α* are two constant coefficients. *t* represents the current iteration and *T* is the maximum number of iterations.

The updated mass of the particles is evaluated by (6) and normalized according to the relation (7).

$$m_i(t) = \frac{F_i(t) - \text{worst}(t)}{\text{best}(t) - \text{worst}(t)}, \tag{6}$$

$$M_i(t) = \frac{m_i(t)}{\sum_{j=1}^{NP} m_j(t)}, \tag{7}$$

in which

$$\text{best}(t) = \min F_i(t) \text{ for } i = 1 : NP, \tag{8}$$

$$\text{worst}(t) = \max F_i(t) \text{ for } i = 1 : NP, \tag{9}$$

where the fitness value (objective function) of each of the *i*th particles is evaluated as *F_i(t)* at time *t*.

The updated gravitational velocity vector is calculated from (10), assuming a one-second interval between the iterations.

$$V_i^{t+1} = \text{rand}_i \cdot V_i^t + a_i^t. \tag{10}$$

Then, the position of the particles is updated according to (3).

2.3 The first order gradient-based algorithm (GBA)

Using the Taylor series, retaining the first-order terms, the position of the updated particles is obtained as (11). The direction of the search is referred to as the gradient based-method (GBM) (Vanderplaats 1999; Rao 2009; Haftka et al. 1990).

$$X_i^{t+1} = X_i^t - \Upsilon \nabla F(X_i^t), \tag{11}$$

in which *Υ* is the step length and the operator *∇* is the gradients. By employing (11), the direction of search is in the negative gradients of the function under consideration that is referred to as steepest descent resulting in the most reduction in the function. Special care should be taken in choosing the step length *Υ*. The gradient directions are randomized for compatibility with the metaheuristic methods as explained in the next section.

2.4 Hybrid method (GPSG)

The metaheuristic methods such as PSO and GSA have a good capability of exploring the whole design space. The combination of PSO and GSA improves the quality of exploration (Tsai et al. 2013). However, all the heuristic approaches or their combination have low power of exploitation (local search). On the other hand, the GBA is

powerful for exploitation and weak in exploration (global search) that may be trapped in local optima. Thus the merging of the three approaches is a good idea for obtaining a fast and powerful method. The heuristic methods are random but the gradient methods are deterministic. In the combination approaches, the idea of randomization must be employed. Besides, a fraction of the speed in each method should be combined.

The velocity of the particles for PSO, GSA and GBA is given in (12), (13) and (14), respectively, with some modifications.

$$V_PSO_i^{t+1} = c_1 r_1 (P_i^t - X_i^t) + c_2 r_2 (P_g^t - X_i^t), \tag{12}$$

$$V_GSA_i^{t+1} = rand_i \cdot V_GPSG_i^t + a_i^t, \tag{13}$$

$$V_GBA_i^{t+1} = \frac{-\nabla F(X_i^t)}{|\nabla F(X_i^t)|} \cdot sv. \tag{14}$$

The parameter sv is given by

$$sv = |V_PSO_i^{t+1} + V_GSA_i^{t+1}|. \tag{15}$$

The velocity of GBA is normalized to achieve a unit vector along the negative gradient direction. Then, it is multiplied by sv to adjust the length of the search direction of the GBA corresponding to the resultant of the PSO and GSA algorithms. On the other hand, sv is a step length for the unit vector of the negative gradients.

Comparing (12) and the original PSO velocity indicates that the first term of (2) is omitted because its effects are considered in the velocity of the GSA (13).

Finally, the velocity of the combined approach (GPSG) is obtained by (16).

$$V_GPSG_i^{t+1} = C_i (V_PSO_i^{t+1} + V_GSA_i^{t+1} + C_g \cdot r_3 \cdot V_GBA_i^{t+1}). \tag{16}$$

In this formulation, r_3 is a random number between zero and one. $C_g = 2$ is a statistically appropriate coefficient as the average of $C_g * r_3$ tends to one. Therefore, the magnitude of the GBA (sv) does not change much.

The value of C_i is considered as 0.5 to prevent statistically increasing the resultant of the magnitude of the three vectors corresponding to the algorithms.

Finally, the position of each particle is updated by the GPSG velocity presented in (17).

$$X_i^{t+1} = X_i^t + V_GPSG_i^{t+1}. \tag{17}$$

The main idea of the proposed method is that for minimization problems, in the direction of negative gradient of the objective function (GBA), the reduction of the function is more than any other direction. However, the drawback of the gradient direction is that the optimal result falls in a local solution. Thus, the direction of the gradient vector is randomized and its length is normalized for compatibility with the resultant directions generated by PSO and GSA. In each iteration, the resultant of the PSO, GSA and GBA (GPSG) are employed for the optimization process. The fast convergence of numerical results with a small number of the initial population indicates the high ability of the exploration and exploitation of the proposed GPSG method.

The steps of the GPSG hybrid method are presented in the following pseudo-code (comments for more information represented with %);

Pseudo-code of GPSG algorithm

```

Set the initial parameters, such as  $NP$  (the number of particles),  $n$  (the number of design variables) and the design space
Generate initial random population:  $\mathbf{X}_{i=1:NP}^{t=1}$ 
for  $t = 1:T$  % (maximum number of iterations)
  Evaluate the objective function of all particles:  $F_{i=1:NP}(t)$ 
  % Find Pbest ( $\mathbf{P}_i^t$ ) and Gbest ( $\mathbf{P}_g^t$ ) among saved information of all particles up to the present iteration  $t$ 
  for  $i = 1:NP$ 
    if  $F(\mathbf{X}_i^t) \leq F(\mathbf{P}_i^t)$ 
       $\mathbf{P}_i^t = \mathbf{X}_i^t$ 
    end if
    if  $F(\mathbf{X}_i^t) \leq F(\mathbf{P}_g^t)$ 
       $\mathbf{P}_g^t = \mathbf{X}_i^t$ 
    end if
  end for
  % Find the best and worst in the present iteration  $t$  (8, 9):
   $best(t) = \min(F_{i=1:NP}(t))$ 
   $worst(t) = \max(F_{i=1:NP}(t))$ 
  % Update the normalized mass (7):
  for  $i = 1:NP$ 
     $m_i(t) = (F_i(t) - worst(t)) / (best(t) - worst(t))$ 
  end for
   $M_i(t) = m_i(t) / \text{sum}(m_i(t))$ 
  % Update gravitational constant (5):
   $G(t) = G_0 \cdot \exp(-\alpha \cdot t/T)$ 
  % Calculate the acceleration vector of particles (4):
  for  $i = 1:NP$ 
     $sum = \text{zeros}(n, 1)$ 
    for  $j = 1:NP$ 
       $R_{ij}(t) = \text{norm}(\mathbf{X}_j^t - \mathbf{X}_i^t)$ 
       $sum = sum + \text{rand} \cdot M_j(t) / (R_{ij}(t) + \text{eps}) \cdot (\mathbf{X}_j^t - \mathbf{X}_i^t)$ 
    end for
     $\mathbf{a}_i^t = G(t) \cdot sum$ 
  end for
  % Find the speed of PSO ( $\mathbf{V}_{PSO}_i^{t+1}$ ) and GSA ( $\mathbf{V}_{GSA}_i^{t+1}$ ) of particles (12 and 13):
  for  $i = 1:NP$ 
     $\mathbf{V}_{PSO}_i^{t+1} = c_1 \cdot \text{rand} \cdot (\mathbf{P}_i^t - \mathbf{X}_i^t) + c_2 \cdot \text{rand} \cdot (\mathbf{P}_g^t - \mathbf{X}_i^t)$  % ( $c_1=c_2=0.5$ )
     $\mathbf{V}_{GSA}_i^{t+1} = \text{rand} \cdot \mathbf{V}_{GPSG}_i^t + \mathbf{a}_i^t$ 
  end for
  Calculate the negative gradient of particles:  $-\nabla F(\mathbf{X}_{i=1:NP}^t)$ 
  % Find the speed of GBA ( $\mathbf{V}_{GBA}_i^{t+1}$ ) of particles (14):
  for  $i = 1:NP$ 
     $|\nabla F(\mathbf{X}_i^t)| = \text{norm}(\nabla F(\mathbf{X}_i^t))$ 
    if  $|\nabla F(\mathbf{X}_i^t)| = 0$ 
       $|\nabla F(\mathbf{X}_i^t)| = 1$ 
    end if
     $sv = \text{norm}(\mathbf{V}_{PSO}_i^{t+1} + \mathbf{V}_{GSA}_i^{t+1})$ 
     $\mathbf{V}_{GBA}_i^{t+1} = -\nabla F(\mathbf{X}_i^t) / |\nabla F(\mathbf{X}_i^t)| \cdot sv$ 
  end for
  % Update the speed of GPSG of particles with move limits (16):
   $\mathbf{V}_{GPSG}_{i=1:NP}^{t+1} = C_t (\mathbf{V}_{PSO}_{i:NP}^{t+1} + \mathbf{V}_{GSA}_{i:NP}^{t+1} + C_g \cdot \text{rand} \cdot \mathbf{V}_{GBA}_{i:NP}^{t+1})$  % ( $C_t=0.5, C_g=2$ )
  % Update position of particles, considering side limits (17):
   $\mathbf{X}_{i=1:NP}^{t+1} = \mathbf{X}_{i=1:NP}^t + \mathbf{V}_{GPSG}_{i=1:NP}^{t+1}$ 
   $\mathbf{X}_{i=1:NP}^{t+1} = \max(\mathbf{X}_{i=1:NP}^{t+1}, x_{min})$ 
   $\mathbf{X}_{i=1:NP}^{t+1} = \min(\mathbf{X}_{i=1:NP}^{t+1}, x_{max})$ 
  %  $t=t+1$  and go to the next iteration
end for

```

Fig. 1 Convergence history for CEC2005 with $NP = 5$

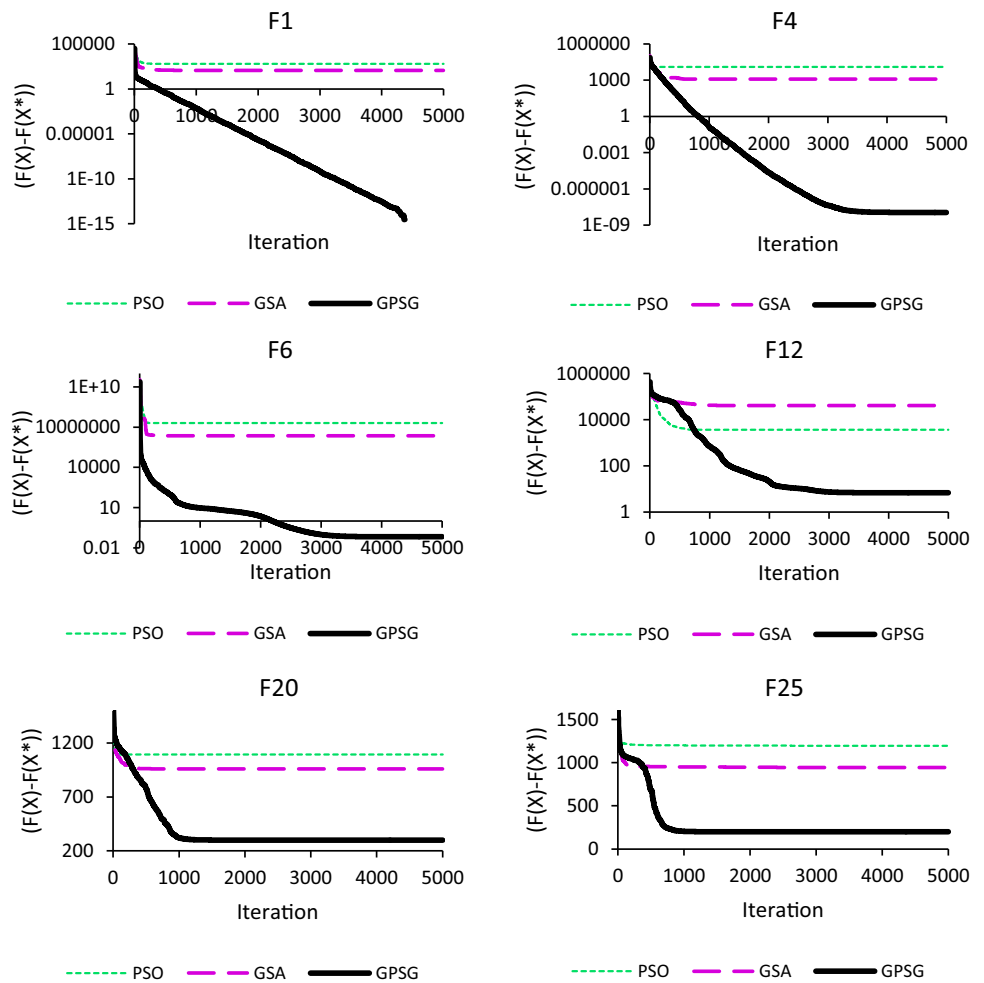


Table 1 Scaling parameters

Parameters	G_0 (Rasgedi 2009)	α (Rashedi 2009)	T	n	NP	Runs
CEC2005	100	20	5000	10	5, 10, 20, 30	30
CEC2017	100	20	7500	30	40	30

2.5 Optimization problem formulation

The general form of a constrained optimization problem can be specified as follows:

Minimize : $f(\mathbf{X})$, (18)

Subject to : $g_k(\mathbf{X}) \leq 0 \quad k = 1 : K$, (19)

where $f(\mathbf{X})$ and $g_k(\mathbf{X})$ represent the objective function and constraints, respectively. The value of K represents the number of constraints.

To convert the constrained structural problems into the unconstrained functions, the penalty function should be used as (Salajegheh and Salajegheh 2019);

$F(\mathbf{X}) = cf(\mathbf{X})$, (20)

$c = 1 + \sum_{i=1}^K \psi(i)q(i)^{\lambda(i)} \quad i = 1 : K$, (21)

$\psi(i) = \mu e^{1+q(i)}$, (22)

$q(i) = \max(g_i, 0)$, (23)

Fig. 2 Convergence history for F1 by algorithms with different number of particles

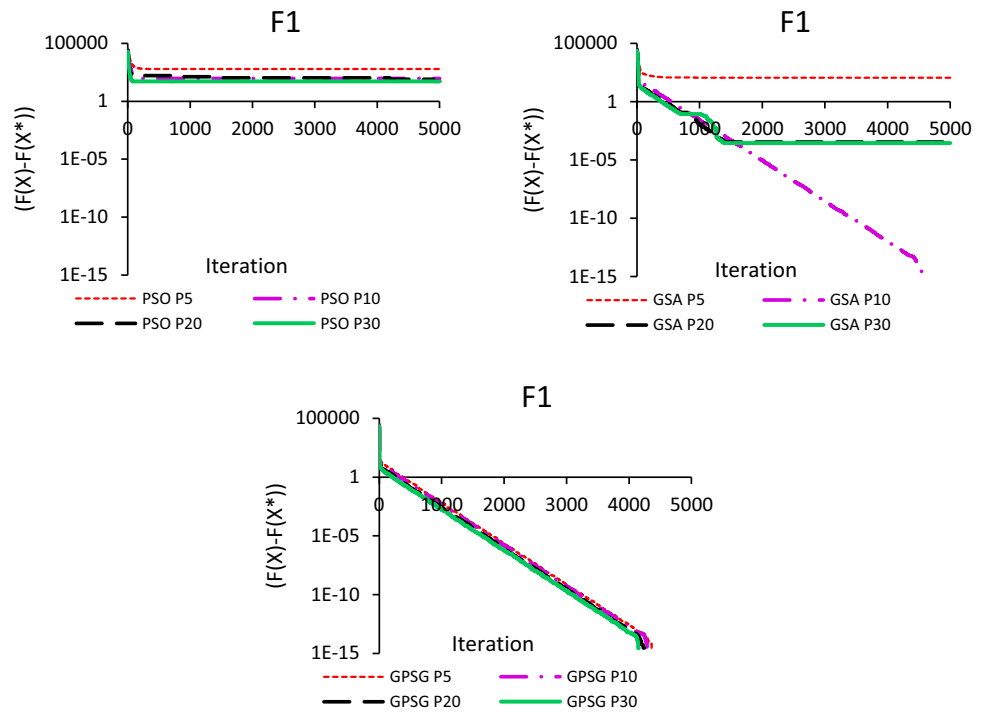


Fig. 3 Convergence history for F17 by algorithms with different number of particles

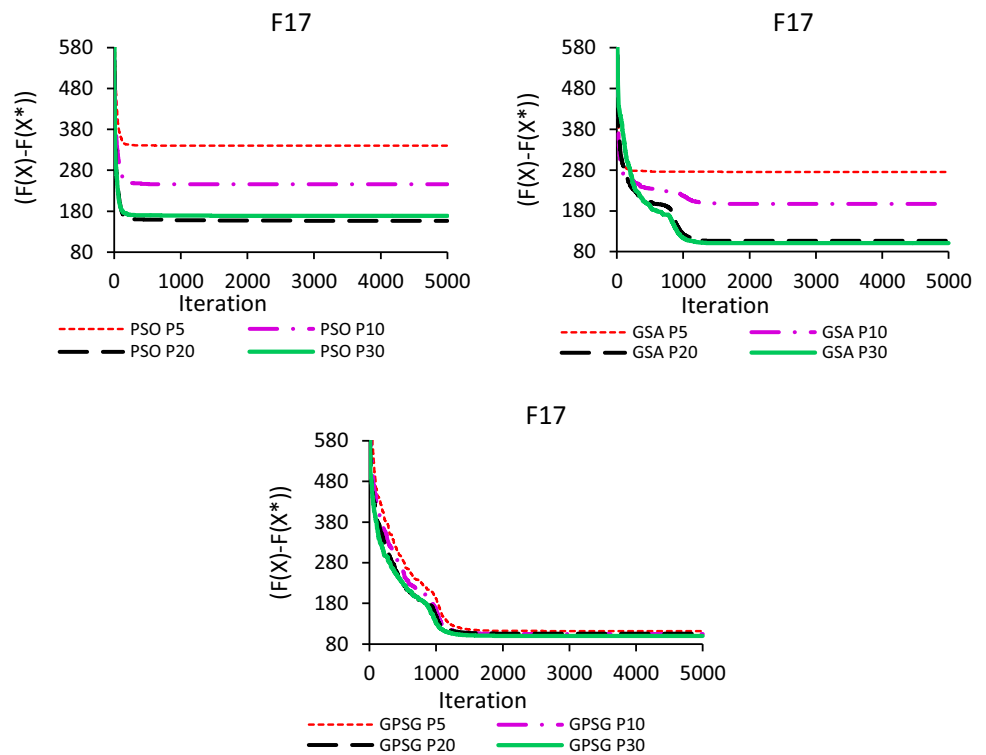
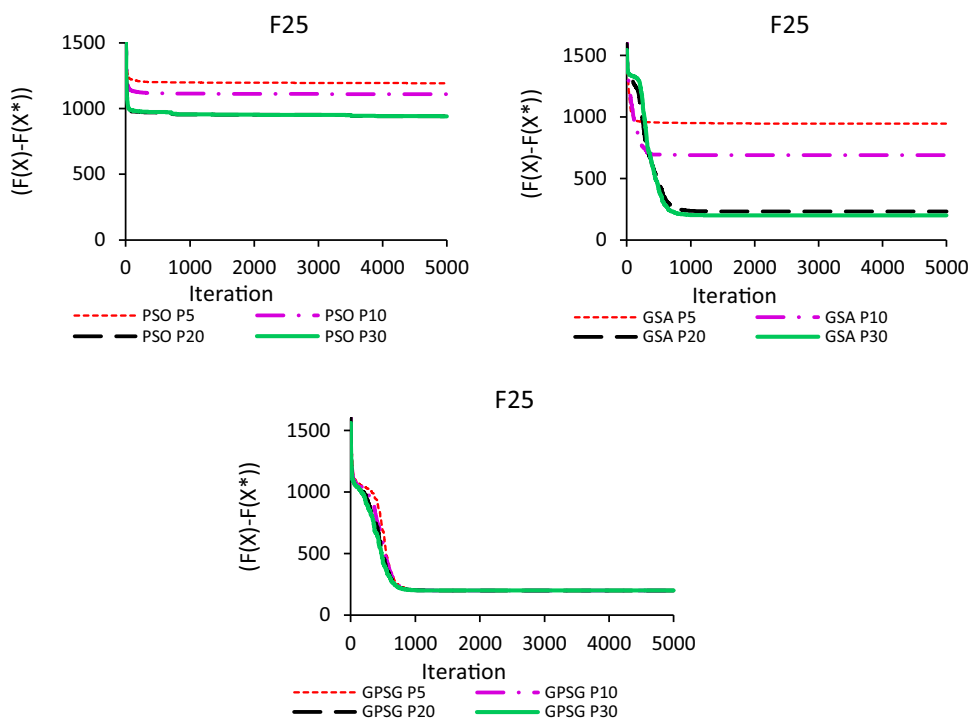


Fig. 4 Convergence history for F25 by GSA algorithm with different number of particles



$$\lambda(i) = \begin{cases} 1 & \text{if } q(i) \leq 1 \\ 2 & \text{if } q(i) > 1 \end{cases}, \tag{24}$$

where c is a scalar coefficient for penalties that increase the objective function if the constraints are violated. $F(\mathbf{X})$ is called the penalized objective function. The parameters μ and λ are the coefficients needed to calculate the value of c . In this study, μ is considered as 0.5.

3 Numerical investigation

In this research, the mathematical functions of CEC2005 (Suganthan et al. 2005) with 10 variables ($n = 10$) and CEC2017 (Awad et al. 2017) with 30 variables are used to explore the capabilities of the proposed approach. In addition, three standard benchmark structural problems are considered for the validation of the GPSG algorithm. These are discussed as follows:

3.1 Results of CEC2005 mathematical functions

The results of the methods of PSO, GSA and GPSG for a population of 5 (NP) are presented graphically for some of the functions in Fig. 1. The required data in the process of optimization are presented in Table 1.

The vertical axis represents the difference between the obtained results and the exact solution (\mathbf{X}^*) at each iteration. Each graph is the outcome of the average of 30 independent runs.

The two methods of PSO and GSA have very poor convergence and the methods trap in a local optimum for some of the cases. But in the combined GPSG method, the convergence of the optimization process is smooth with much better results.

Besides, the effects of the number of the initial population are considered for the methods. Populations of 5, 10, 20 and 30 are examined. The results are presented in Figs. 2, 3 and 4. It can be observed that the methods of PSO and GSA are very sensitive to the number of population. However, in the GPSG, the population does not affect the results much. With a small population, the enhanced method behaves well.

Table 2 (continued)

Function	Criteria	PSO					GSA					GPSG				
		N/P	5	10	20	30	5	10	20	30	5	10	20	30		
F8	Avg.	20.32	20.29	20.24	20.27	20.63	20.44	20.19	20.15	20.13	20.17	20.16	20.15			
	Rank	2.00	2.00	3.00	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00			
	SD.	0.07	0.08	0.07	0.06	0.09	0.06	0.07	0.06	0.07	0.06	0.06	0.05			
	Med.	20.34	20.29	20.24	20.29	20.64	20.45	20.21	20.17	20.14	20.17	20.17	20.15			
	Best	20.16	20.16	20.10	20.13	20.46	20.30	20.03	20.04	20.02	20.02	20.03	20.03			
F9	Avg.	41.24	32.26	20.97	19.10	55.82	33.67	8.85	14.99	59.61	51.64	7.91	3.83			
	Rank	1.00	1.00	3.00	3.00	2.00	2.00	2.00	2.00	3.00	3.00	1.00	1.00			
	SD.	9.80	9.67	6.74	4.65	5.10	4.99	3.38	2.85	15.06	7.50	5.62	1.42			
	Med.	40.37	32.86	18.90	19.90	55.85	34.50	9.03	15.55	54.22	48.75	6.96	3.98			
	Best	22.89	8.95	9.95	9.95	48.35	24.74	3.09	9.02	21.11	46.76	1.99	0.99			
F10	Avg.	66.55	30.16	25.92	17.76	62.21	30.72	7.38	5.40	5.17	4.93	3.28	3.83			
	Rank	3.00	2.00	3.00	3.00	2.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00			
	SD.	16.28	11.28	9.42	7.41	5.77	8.45	2.26	1.44	2.27	1.75	0.97	1.59			
	Med.	65.59	33.33	24.38	17.41	63.46	33.35	7.14	5.59	4.97	5.47	3.48	3.98			
	Best	23.93	13.93	12.93	5.97	52.76	12.56	3.23	2.13	0.99	1.99	0.99	0.99			
F11	Avg.	6.74	6.33	5.22	4.48	9.35	5.67	0.68	2.89	3.09	2.89	2.96	2.33			
	Rank	2.00	3.00	3.00	3.00	3.00	2.00	1.00	2.00	1.00	1.00	2.00	1.00			
	SD.	1.00	0.73	0.99	1.12	0.49	1.36	0.12	0.47	1.67	1.88	1.60	2.13			
	Med.	6.69	6.35	5.33	4.89	9.30	6.13	0.65	3.04	3.20	3.23	3.06	2.02			
	Best	5.12	4.25	3.08	1.78	8.50	3.43	0.53	1.65	0.18	0.19	0.25	0.16			
F12	Avg.	3.70E + 03	1.91E + 03	3.48E + 02	5.32E + 02	4.16E + 04	1.15E + 03	44.64	32.28	6.95	3.68	1.48E + 02	1.15E + 02			
	Rank	2.00	3.00	3.00	3.00	3.00	2.00	1.00	1.00	1.00	1.00	2.00	2.00			
	SD.	2.08E + 03	1.03E + 03	4.87E + 02	5.67E + 02	2.33E + 04	1.22E + 03	32.45	23.09	6.29	4.40	2.90E + 02	2.58E + 02			
	Med.	3.66E + 03	1.94E + 03	1.46E + 02	2.90E + 02	5.30E + 04	7.12E + 02	37.73	23.41	10.01	1.78	10.01	10.01			
	Best	7.94E + 02	3.02E + 02	7.22	2.43	9.96	0.00	5.30	6.12	0.00	0.00	0.00	0.00			
F13	Avg.	2.35	1.11	0.89	0.82	5.03	0.90	0.67	0.34	1.23	1.23	0.96	1.03			
	Rank	2.00	2.00	2.00	2.00	3.00	1.00	1.00	1.00	1.00	3.00	3.00	3.00			
	SD.	0.91	0.26	0.23	0.21	1.20	0.18	0.28	0.13	0.42	0.30	0.18	0.26			
	Med.	2.28	1.06	0.86	0.88	5.18	0.86	0.63	0.37	1.26	1.24	0.94	1.05			
	Best	0.67	0.47	0.52	0.34	0.71	0.64	0.20	0.12	0.56	0.53	0.68	0.37			
F14	Avg.	3.88	3.59	3.37	3.20	4.28	4.20	4.08	4.22	3.74	3.45	3.40	3.09			
	Rank	2.00	2.00	1.00	2.00	3.00	3.00	3.00	3.00	1.00	1.00	2.00	1.00			
	SD.	0.25	0.35	0.36	0.31	0.14	0.19	0.22	0.26	0.24	0.36	0.37	0.35			
	Med.	3.89	3.62	3.50	3.23	4.28	4.24	4.10	4.29	3.75	3.49	3.48	3.06			
	Best	3.20	2.41	2.36	2.32	4.06	3.83	3.60	3.59	3.42	2.74	2.77	2.42			

Table 2 (continued)

Function	Criteria	PSO						GSA						GPSG															
		5		10		20		30		5		10		20		30		5		10		20		30					
		<i>N/P</i>	Avg.	Rank	SD.	Med.	Best	Avg.	Rank	SD.	Med.	Best	Avg.	Rank	SD.	Med.	Best	Avg.	Rank	SD.	Med.	Best	Avg.	Rank	SD.	Med.	Best		
F15	Avg.	4.69E + 02	3.80E + 02	2.51E + 02	3.04E + 02	6.18E + 02	3.79E + 02	1.90E + 02	1.59E + 02	3.99E + 02	3.95E + 02	3.97E + 02	3.54E + 02	2.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	3.00	3.00	3.00	3.00		
	Rank	2.00	2.00	2.00	2.00	3.00	1.00	1.00	1.00	1.00	3.00	1.00	1.00	3.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	3.00	3.00	3.00	3.00	3.00		
	SD.	1.25E + 02	1.58E + 02	90.15	1.23E + 02	69.56	87.55	58.24	22.46	7.29	9.00	7.41	82.74	4.53E + 02	3.41E + 02	2.48E + 02	2.77E + 02	3.56E + 02	1.87E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	4.00E + 02	
	Med.	2.13E + 02	1.54E + 02	1.28E + 02	1.14E + 02	5.12E + 02	2.41E + 02	1.07E + 02	1.14E + 02	3.79E + 02	3.80E + 02	3.80E + 02	3.80E + 02	1.81E + 02	2.85E + 02	1.81E + 02	1.76E + 02	1.60E + 02	1.71E + 02	1.02E + 02	1.02E + 02	1.02E + 02	1.02E + 02	96.59	94.93	94.93	94.93	94.93	
	Avg.	3.00	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	2.00	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	
	Rank	75.40	23.60	35.33	25.28	25.50	23.99	33.28	22.46	4.10	4.00	3.16	3.91	2.99E + 02	1.77E + 02	1.76E + 02	1.59E + 02	1.75E + 02	1.04E + 02	1.02E + 02	1.02E + 02	1.02E + 02	1.02E + 02	99.25	97.64	95.27	95.27	95.27	
F16	Avg.	1.49E + 02	1.52E + 02	1.08E + 02	1.17E + 02	2.20E + 02	1.21E + 02	0.69	0.24	91.60	89.64	91.44	84.69	3.41E + 02	2.46E + 02	1.56E + 02	1.68E + 02	1.97E + 02	1.06E + 02	1.12E + 02	1.05E + 02	1.06E + 02	1.06E + 02	1.06E + 02	1.06E + 02	1.06E + 02	1.06E + 02	1.06E + 02	
	Rank	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00	3.00	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
	SD.	105.25	101.11	25.68	26.80	20.93	14.76	8.52	3.92	9.36	8.53	5.80	3.62	3.25E + 02	2.19E + 02	1.60E + 02	1.71E + 02	2.00E + 02	1.08E + 02	1.13E + 02	1.07E + 02	1.05E + 02	1.05E + 02	1.05E + 02	1.05E + 02	1.05E + 02	1.05E + 02	1.05E + 02	
	Med.	2.09E + 02	1.42E + 02	1.02E + 02	1.24E + 02	2.31E + 02	1.64E + 02	74.88	91.82	97.19	80.13	92.30	93.39	1.07E + 02	1.04E + 03	1.00E + 03	1.00E + 03	9.23E + 02	7.20E + 02	3.29E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
	Avg.	1.07E + 03	1.04E + 03	1.00E + 03	1.00E + 03	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	3.00E + 02	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Rank	56.81	52.71	48.87	52.58	1.08E + 02	6.18	0.27	0.13	1.31E + 02	0.00	0.00	0.00	3.62	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
F17	Avg.	1.06E + 03	1.05E + 03	1.02E + 03	1.01E + 03	8.91E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.06E + 03	1.05E + 03	1.02E + 03	8.91E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	
	Rank	9.00E + 02	9.08E + 02	8.94E + 02	8.00E + 02	7.41E + 02	7.14E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
	SD.	1.11E + 03	1.03E + 03	9.79E + 02	9.69E + 02	9.57E + 02	7.39E + 02	3.17E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.11E + 03	1.03E + 03	9.79E + 02	9.69E + 02	9.57E + 02	7.39E + 02	3.17E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
	Med.	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	3.00E + 02	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Avg.	54.53	55.25	68.54	79.56	97.71	42.13	71.51	0.09	0.00	0.00	0.00	0.00	54.53	55.25	68.54	79.56	97.71	42.13	71.51	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Rank	1.11E + 03	1.05E + 03	1.01E + 03	9.94E + 02	9.95E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.11E + 03	1.05E + 03	1.01E + 03	9.94E + 02	9.95E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
F18	Avg.	1.00E + 03	8.78E + 02	8.00E + 02	8.00E + 02	7.39E + 02	7.14E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.00E + 03	8.78E + 02	8.00E + 02	8.00E + 02	7.39E + 02	7.14E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	
	Rank	1.09E + 03	1.02E + 03	9.78E + 02	9.96E + 02	9.59E + 02	7.27E + 02	3.40E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.09E + 03	1.02E + 03	9.78E + 02	9.96E + 02	9.59E + 02	7.27E + 02	3.40E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	
	SD.	40.12	52.85	72.02	36.22	1.04E + 02	25.23	99.54	0.14	0.00	0.00	0.00	0.00	40.12	52.85	72.02	36.22	1.04E + 02	25.23	99.54	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Med.	1.09E + 03	1.04E + 03	1.01E + 03	1.01E + 03	9.97E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.09E + 03	1.04E + 03	1.01E + 03	1.01E + 03	9.97E + 02	7.19E + 02	3.01E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
	Avg.	1.03E + 03	8.12E + 02	8.00E + 02	9.11E + 02	7.65E + 02	7.14E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	1.03E + 03	8.12E + 02	8.00E + 02	9.11E + 02	7.65E + 02	7.14E + 02	3.01E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02	3.00E + 02
	Rank	1.29E + 03	1.15E + 03	1.01E + 03	9.62E + 02	1.26E + 03	1.06E + 03	8.02E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	1.29E + 03	1.15E + 03	1.01E + 03	9.62E + 02	1.26E + 03	1.06E + 03	8.02E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	
F19	Avg.	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	3.00	3.00	3.00	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
	Rank	8.65E + 01	1.24E + 02	2.67E + 02	2.75E + 02	43.95	88.63	0.33	0.18	0.00	0.00	0.00	8.65E + 01	1.24E + 02	2.67E + 02	2.75E + 02	43.95	88.63	0.33	0.18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
	SD.	1.32E + 03	1.20E + 03	1.14E + 03	1.08E + 03	1.27E + 03	1.06E + 03	8.02E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	1.32E + 03	1.20E + 03	1.14E + 03	1.08E + 03	1.27E + 03	1.06E + 03	8.02E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	
	Med.	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02
	Avg.	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02
	Rank	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	1.06E + 03	8.43E + 02	4.10E + 02	3.00E + 02	1.11E + 03	8.09E + 02	8.01E + 02	8.01E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02	5.00E + 02

Table 2 (continued)

Function	Criteria	PSO			GSA			GPSG					
		5	10	20	30	5	10	20	30	5	10	20	30
F22	Avg.	9.60E + 02	8.87E + 02	8.52E + 02	8.43E + 02	8.81E + 02	7.62E + 02	7.64E + 02	7.63E + 02	7.50E + 02	7.46E + 02	7.43E + 02	7.43E + 02
	Rank	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00
	SD.	67.48	71.85	56.14	52.87	24.49	11.51	5.82	4.66	7.48	6.98	7.79	6.41
	Med.	9.46E + 02	8.92E + 02	8.52E + 02	8.53E + 02	8.73E + 02	7.61E + 02	7.66E + 02	7.63E + 02	7.50E + 02	7.48E + 02	7.44E + 02	7.44E + 02
	Best	8.27E + 02	7.77E + 02	7.77E + 02	7.60E + 02	8.42E + 02	7.45E + 02	7.48E + 02	7.50E + 02	7.34E + 02	7.27E + 02	7.32E + 02	7.28E + 02
F23	Avg.	1.26E + 03	1.13E + 03	1.09E + 03	9.46E + 02	1.24E + 03	1.08E + 03	9.50E + 02	9.71E + 02	1.15E + 03	7.18E + 02	5.59E + 02	5.59E + 02
	Rank	3.00	3.00	3.00	2.00	2.00	2.00	2.00	3.00	1.00	1.00	1.00	1.00
	SD.	1.81E + 02	1.89E + 02	2.62E + 02	2.78E + 02	51.74	1.08E + 02	91.91	0.00	1.39E + 02	1.28E + 02	0.00	0.00
	Med.	1.33E + 03	1.20E + 03	1.19E + 03	1.04E + 03	1.26E + 03	1.13E + 03	9.71E + 02	9.71E + 02	1.20E + 03	8.28E + 02	5.59E + 02	5.59E + 02
	Best	5.51E + 02	6.69E + 02	4.25E + 02	5.59E + 02	1.12E + 03	8.28E + 02	5.59E + 02	9.71E + 02	8.28E + 02	5.59E + 02	5.59E + 02	5.59E + 02
F24	Avg.	1.16E + 03	1.03E + 03	9.08E + 02	8.57E + 02	9.75E + 02	7.77E + 02	2.54E + 02	2.67E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02
	Rank	3.00	3.00	3.00	3.00	2.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00
	SD.	1.93E + 02	1.13E + 02	1.33E + 02	1.79E + 02	35.55	82.85	75.53	1.23E + 02	0.00	0.00	0.00	0.00
	Med.	1.24E + 03	9.94E + 02	9.64E + 02	9.50E + 02	9.68E + 02	7.62E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02
	Best	5.27E + 02	8.03E + 02	5.52E + 02	5.02E + 02	9.51E + 02	6.04E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02
F25	Avg.	1.19E + 03	1.11E + 03	9.43E + 02	9.40E + 02	9.44E + 02	6.89E + 02	2.31E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02
	Rank	3.00	3.00	3.00	2.00	2.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00
	SD.	1.38E + 02	1.37E + 02	1.72E + 02	1.23E + 02	45.74	68.64	63.18	0.05	0.00	0.00	0.00	0.00
	Med.	1.26E + 03	1.06E + 03	9.64E + 02	9.63E + 02	9.63E + 02	7.11E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02
	Best	9.65E + 02	9.22E + 02	3.55E + 02	6.03E + 02	7.88E + 02	5.04E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02	2.00E + 02

Table 3 Average rank of methods with different populations

Algorithms	PSO	GSA	GPSG
5 particle	3	2	1
10 particle	3	2	1
20 particle	3	2	1
30 particle	3	2	1

The summary of the results is given in Table 2. For all the problems, mean, rank, standard deviation, median and

best response for the final iteration are given. The rank is evaluated based on the results of the average of the final iteration of the 30 runs, for the same population.

From the statistical point of view, the standard deviation (SD.) indicates that the diversity of the final results of the independent runs are lower for the proposed approach, which shows the superiority of the method.

The mean values of the average of the 25 functions are found and then their ranks are evaluated for each population. The final results are given in Table 3. It is seen that the GPSG possesses the first rank in all the cases.

Table 4 Comparison of GPSG with variants of GSA for CEC2005

Function	Ebrahimi Mood et al. (2015)				Present work			Rank GPSG
	GSA	CGSA	SSGSA	BSGSA	PSO	GSA	GPSG	
F1	0	1.59E - 12	8.0193E - 15	2.6328E - 15	54.05	0	0	1
F2	0	3.13E - 12	1.2764E - 14	5.9829E - 15	0	0	0	1
F3	1.93E + 05	2.02E + 05	9.5887E + 04	1.4268E + 05	2.96E + 05	1.88E + 05	8.56E + 04	1
F4	3.75E + 03	3.08E + 03	1.8194E - 14	7.6216E - 15	304	0.71	0	1
F5	2.53E + 03	3.34E + 03	319.4057	436.0698	6.32	0.81	0	1
F6	87.97	13.38	24.8792	54.3535	3.90E + 05	17.75	0.05	1
F7	2.23E + 03	1.60E + 03	0.0019	0.0039	15.06	0.11	0.02	3
F8	20.11	20.08	20.0571	20.0563	20.24	20.19	20.16	5
F9	3.78	4.62	4.4574	4.2584	20.97	8.85	7.91	5
F10	3.7	3.46	3.9798	4.2186	25.92	7.38	3.28	1
F11	1.39E - 04	4.94E - 04	0.0021	0.0015	5.22	0.68	2.96	6
F12	230.16	158.9900	9.1565	8.9871	3.48E + 02	4.46E + 01	1.48E + 02	4
F13	1.30	1.25	1.3188	1.3798	0.89	0.67	0.96	3
F14	4.82	4.79	3.6653	4.0158	3.37	4.08	3.4	2
F15	199.11	197.32	276.0382	173.9696	2.51E + 02	1.90E + 02	3.97E + 02	7
F16	92.40	84.62	96.1282	88.6387	1.76E + 02	95.51	96.59	6
F17	99.79	103.29	98.4660	100.4505	1.56E + 02	1.06E + 02	1.06E + 02	5
F18	941.70	880	913.9566	934.5902	1.00E + 03	3.01E + 02	3.00E + 02	1
F19	946.52	896	917.1538	924.1029	9.79E + 02	3.17E + 02	3.00E + 02	1
F20	950.68	880	906.2861	914.8380	9.78E + 02	3.40E + 02	3.00E + 02	1
F21	800	800	800.0000	800.0000	1.01E + 03	8.02E + 02	5.00E + 02	1
F22	763.36	756.32	747.4972	748.5580	8.52E + 02	7.64E + 02	7.43E + 02	1
F23	1.08E + 03	1.07E + 03	975.2348	970.5031	1.09E + 03	9.50E + 02	5.59E + 02	1
F24	602.87	628.47	276.0000	358.9453	9.08E + 02	2.54E + 02	2.00E + 02	1
F25	1.33E + 03	1.33E + 03	296.0000	388.0000	9.43E + 02	2.31E + 02	2.00E + 02	1
Average rank	4.44	4.24	3.48	3.44	5.84	3.44	2.44	
Rank	6	5	4	2	7	2	1	

Table 5 Comparison of GPSG with other methods for CEC2017

Function	Askarzadeh (2016)		Mirjalili et al. (2014)		Gandomi et al. (2012)		Karaboga and Basturk (2007)		Storn and Price (1997)		Civicioglu (2013)		Mirjalili (2016)		Salajegheh and Salajegheh (2019)		Present work		Rank
	CSA	GWO	GWO	KH	KH	ABC	ABC	DE	BSA	SCA	PSOG	Average	Best	SD	GPSG	Best	SD	GPSG	
F1	2540	8.87E + 08	1.72E + 09	435	4334.44	492	1.18E + 10	2340	535.75	137.55	337.26	3							
F3	475	2.50E + 04	4.48E + 04	1.10E + 05	2.21E + 04	2.86E + 04	3.50E + 04	462	2.20E + 04	1.80E + 04	2.76E + 03	3							
F4	502	536	505	431	519.42	495	1400	419	402.41	400.00	2.16	1							
F5	616	587	644	585	737.79	556	771	563	554.92	547.76	5.86	1							
F6	620	603	639	600	652.58	600	649	610	602.86	601.30	0.89	3							
F7	824	822	827	807	962.59	802	1120	810	741.17	739.78	0.85	1							
F8	894	873	905	895	967.25	861	1050	870	846.37	844.77	1.13	1							
F9	1330	1230	3160	2110	7878.78	901	5520	900	900.00	900.00	1.40E - 10	1							
F10	4480	3850	5230	3510	4536.99	5490	8120	3680	3194.90	2985.76	124.59	1							
F11	1250	1330	1620	1750	1184.63	1150	2190	1230	1160.09	1143.76	9.91	2							
F12	1.60E + 06	2.52E + 07	4.27E + 08	9.47E + 05	3.18E + 05	1.57E + 05	1.21E + 09	3.26E + 04	1.13E + 05	8.17E + 04	2.52E + 04	2							
F13	2.34E + 04	4.67E + 06	2.71E + 08	3.65E + 04	1.88E + 04	9220	4.07E + 08	8.43E + 04	2.01E + 04	1.78E + 04	1.71E + 03	3							
F14	1580	1.16E + 05	3.15E + 05	1.41E + 05	5502.16	1470	1.19E + 05	7390	2071.08	1637.80	288.46	3							
F15	4520	1.90E + 05	1.90E + 04	9560	2484.69	1630	1.56E + 07	4.36E + 04	1.03E + 04	9192.58	1.23E + 03	5							
F16	2380	2350	3190	2210	2827.01	2220	3640	1860	2062.18	2011.40	40.15	2							
F17	1960	1940	2220	1890	2604.53	1820	2420	1870	1764.99	1745.42	11.21	1							
F18	1.74E + 04	5.33E + 05	5.26E + 05	3.39E + 05	9.42E + 04	7840	2.80E + 06	8.68E + 04	4.39E + 04	3.14E + 04	8.48E + 03	3							
F19	7180	2.42E + 05	3.33E + 05	1.78E + 04	3010.24	2030	2.48E + 07	3.17E + 04	1.90E + 04	1.69E + 04	2.13E + 03	5							
F20	2330	2330	2540	2250	2864.83	2150	2610	2330	2207.72	2184.99	19.40	2							
F21	2400	2380	2430	2300	2504.78	2360	2560	2360	2338.58	2332.96	5.10	2							
F22	2300	4420	2710	2320	5655.57	2500	8250	2300	2300.00	2300.00	3.43E - 07	1							
F23	2840	2740	3020	2720	3572.97	2710	2990	2720	2715.06	2709.46	3.71	2							
F24	2950	2890	3250	2710	3290.7	2890	3160	2860	2857.09	2854.98	1.96	2							
F25	2910	2940	2920	2890	2946.71	2890	3200	2890	2886.87	2886.83	3.63E - 02	1							
F26	3190	4450	5920	2900	6756.37	4030	6870	3590	2800.00	2800.00	3.07E - 07	1							
F27	3360	3230	3460	3210	3998.88	3210	3390	3220	3220.61	3215.66	3.86	4							
F28	3230	3340	3250	3220	3326.26	3390	3780	3100	3100.00	3100.00	5.11E - 09	1							
F29	3860	3590	4230	3530	4115.19	3490	4620	3820	3599.44	3550.32	3.71E + 01	4							
F30	1.49E + 05	3.97E + 06	1.98E + 08	2.26E + 04	3900.83	7200	7.44E + 07	6.47E + 04	3.71E + 04	3.54E + 04	1.10E + 03	4							
Average rank	4.66	5.69	7.28	3.69	6.38	2.69	8.48	3.34	2.24										
Rank	5	6	8	4	7	2	9	3	1										

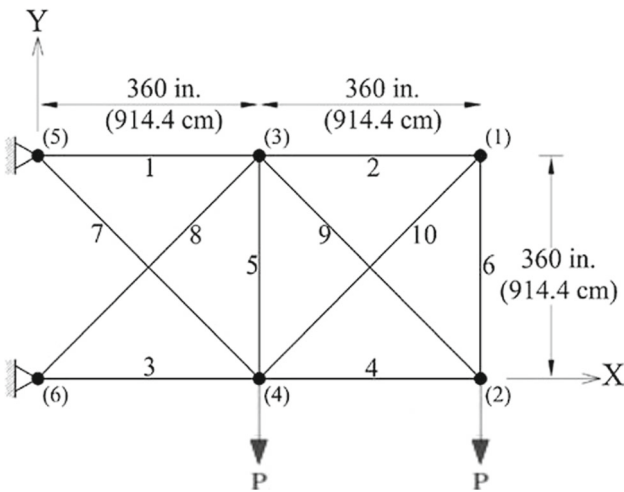


Fig. 5 10-bar plane truss

Table 6 Information for the 10-bar plane truss

Properties	Values
External loading, P	100 kips
Elasticity modulus	10,000 ksi
density	0.1 lb/in ³
Area lower bound	0.1 in ²
Area upper bound	35 in ²
Allowable displacement in all directions	± 2.0 in
Allowable stress	± 25 ksi

3.2 Comparison of the proposed method with several metaheuristic algorithms

The outlined approach with 20 particles is compared with different variations of GSA for the CEC2005 (Ebrahimi et al. 2015). The required initial parameters are chosen similarly. The numerical results are presented in Table 4. It can be observed that 15 functions have the first rank and the average rank of all the 25 functions is better than variants of GSA.

For CEC2017 the average, best and standard deviation (SD.) results for each function are indicated in Table 5. The average results of the proposed approach compared with 8 other methods, according to the available information. The

Table 7 Results of 10-member truss algorithms with different populations

NP	PSO			GSA			GPSG					
	5	10	20	30	5	10	20	30	5	10	20	30
Truss 10 member	7.25E + 03	6.56E + 03	5.51E + 03	5.46E + 03	5.91E + 03	5.12E + 03	5.07E + 03	5.07E + 03	5.07E + 03	5.06E + 03	5.06E + 03	5.06E + 03
Avg. (lb)												
Rank	3	3	3	3	2	2	2	2	1	1	1	1
SD. (lb)	4.59E + 02	3.99E + 02	2.68E + 02	2.93E + 02	5.33E + 02	5.00E + 01	1.71E + 00	2.47E + 00	8.84E - 01	8.47E - 01	4.93E - 01	5.89E - 01
Med. (lb)	7.32E + 03	6.43E + 03	5.42E + 03	5.42E + 03	6.04E + 03	5.10E + 03	5.07E + 03	5.07E + 03	5.07E + 03	5.06E + 03	5.06E + 03	5.06E + 03
Best. (lb)	6.13E + 03	5.85E + 03	5.12E + 03	5.12E + 03	5.18E + 03	5.07E + 03	5.06E + 03	5.06E + 03	5.06E + 03	5.06E + 03	5.06E + 03	5.06E + 03

Fig. 6 Convergence history for the 10-bar truss with different number of particles

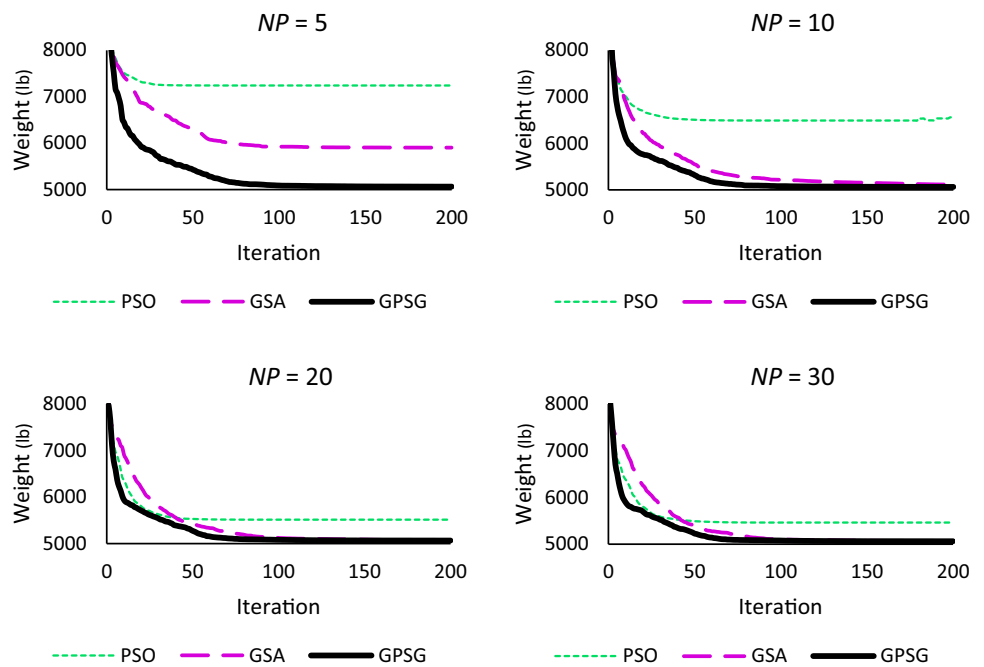


Table 8 Average ranking with different populations for 10-bar plane truss

Algorithms	PSO	GSA	GPSG
Average Mean (lb)	6193.62	5289.54	5063.95
Average Rank	3	2	1

superiority of the GPSG among the others is observed according to the average rank. Also, the same number of function evaluations is chosen for all methods. The standard deviations (SD.) are obtained for GPSG and the other methods, the results of SD. are not available for comparison.

3.3 Structural problems

The optimal design of structures is the main topic among structural engineers (Mashayekhi et al. 2012, 2016; Gholizadeh 2013; Khatibinia and Yazdani 2018; Bhullar et al. 2020). In this section, three design problems are chosen for truss structures. The weight of the structures is taken as the

objective function and the constraints are bounds on member stresses and joint displacements. The cross-sectional areas are continuous design variables. In all the problems, the value of α in (5) and the maximum iterations (T) are chosen as 4 and 200, respectively.

3.3.1 10-bar plane truss

The 10-bar truss is optimized as shown in Fig. 5. The required information for the truss is given in Table 6.

The results are given in Table 7. The numerical results indicate that the best results are obtained with the combined GPSG method, in which for all the number of particles, similar results are approximately achieved.

The convergence trend for different populations is illustrated in Fig. 6. It is concluded that the GPSG method yields better results which demonstrates the efficiency of this method.

The ranking of the three algorithms is given in Table 8. The ranking of the GPSG is first.

Fig. 7 72-bar truss

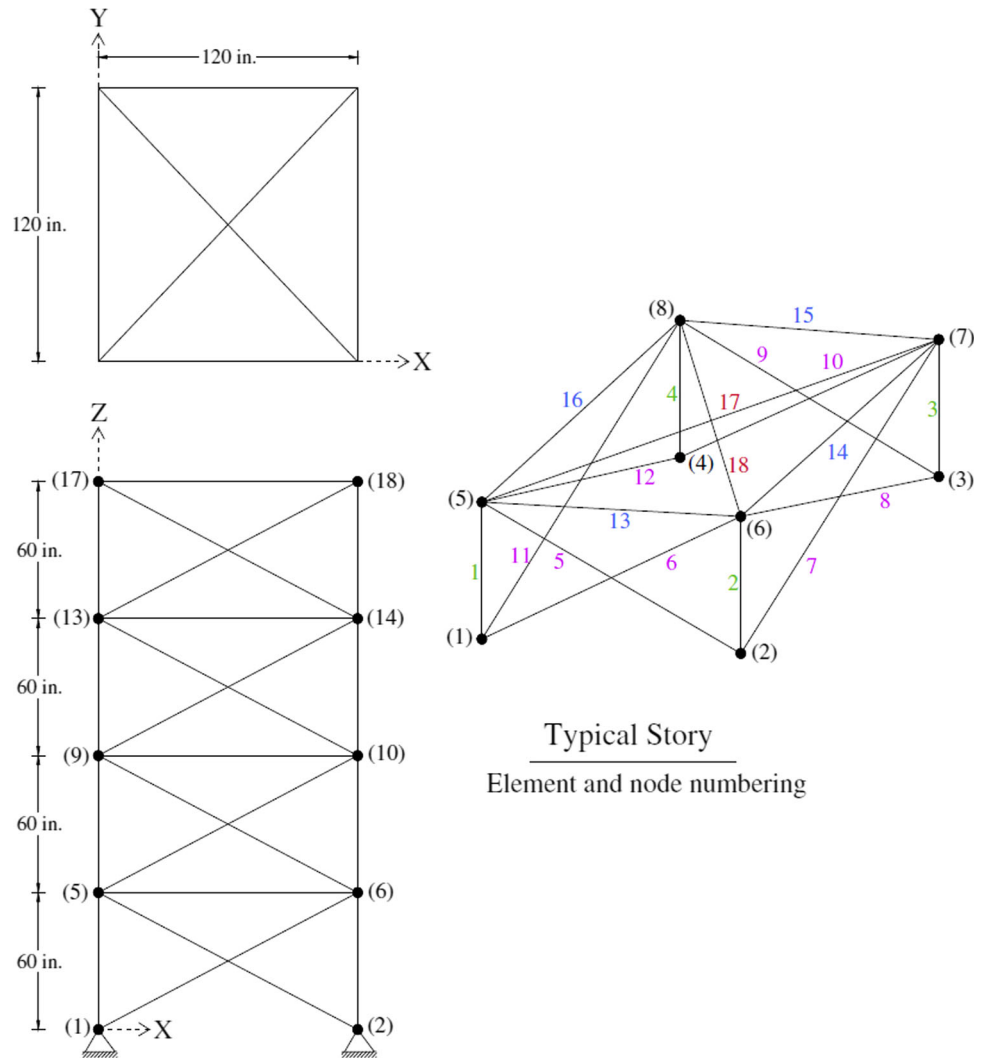


Table 9 Information of the 72-bar truss

Properties	Values
External loading, P on node 17	$P_x = 5$ kips $P_y = 5$ kips $P_z = -5$ kips
Elasticity modulus	10,000 ksi
density	0.1 lb/in ³
Area lower bound	0.01 in ²
Area upper bound	4 in ²
Allowable displacement in all directions	± 0.25 in
Allowable stress	± 25 ksi

3.3.2 72-bar truss

The 72-member truss shown in Fig. 7 consists of 16 member types due to geometrical shape. The aim is to minimize the weight of the structure. All of the specifications of the structure are given in Table 9.

The results are presented in Table 10. It can be concluded that the GPSG hybrid method has the most favorable results. The number of the initial population does not affect the results. The average of the hybrid method with only five particles is better than the PSO and GSA methods with 30 particles.

Table 10 Results of 72-member algorithms with different populations

NP	PSO	GSA			GPSG								
		5	10	20	30	5	10	20	30				
Truss 72 member	Avg. (lb)	1.04E + 03	9.14E + 02	7.32E + 02	6.42E + 02	8.14E + 02	4.78E + 02	4.73E + 02	4.78E + 02	4.20E + 02	3.89E + 02	3.79E + 02	3.72E + 02
	Rank	3	3	3	3	2	2	2	2	1	1	1	1
	SD. (lb)	1.31E + 02	8.53E + 01	8.62E + 01	7.88E + 01	8.67E + 01	5.51E + 01	4.27E + 01	3.86E + 01	3.25E + 01	2.05E + 01	1.45E + 01	1.00E + 01
	Med. (lb)	1.05E + 03	9.17E + 02	7.34E + 02	6.25E + 02	8.43E + 02	5.88E + 02	4.74E + 02	4.77E + 02	4.19E + 02	3.86E + 02	3.77E + 02	3.72E + 02
	Best. (lb)	6.78E + 02	7.29E + 02	5.44E + 02	5.10E + 02	6.00E + 02	4.64E + 02	3.89E + 02	4.15E + 02	3.61E + 02	3.66E + 02	3.59E + 02	3.58E + 02

The convergence history of the methods is shown in Fig. 8. The GPSG method yields better results that demonstrate its effectiveness.

The ranking of the three algorithms is shown in Table 11 and the GPSG method is ranked first.

3.3.3 120-member dome under asymmetric vertical load

The 120-member dome shown in Fig. 9 is composed of 7 member types due to the existing geometric symmetry. Therefore, the number of design variables is reduced from 120 to 7. Stress constraints have been used following AISC-ASD regulations. The permissible tensile and compressive stresses are given in (25 and 26), respectively.

$$\sigma_T = 0.6F_y, \tag{25}$$

$$\sigma_c = \frac{\left[F_y \left(1 - \frac{\lambda_i^2}{2C_c^2} \right) \right]}{\frac{5}{3} + \frac{3\lambda_i}{8C_c} - \frac{\lambda_i^3}{8C_c^3}} \quad \text{if } \lambda_i < C_c \text{ (for inelastic buckling),} \tag{26a}$$

$$\sigma_c = \frac{12 \pi^2 E}{23 \lambda_i^2} \quad \text{if } \lambda_i \geq C_c \text{ (for elastic buckling),} \tag{26b}$$

where E is the modulus of elasticity, F_y is the yield stress of steel, and C_c is the boundary value between the elastic and inelastic buckling states. The effective length coefficient $k=1$, and r_i is the radius of gyration of each member, evaluated as (26). The asymmetric vertical load is applied to the free nodes in the z -direction according to Table 12.

$$C_c = \sqrt{\frac{2\pi^2 E}{F_y}}, \tag{27}$$

$$\lambda_i = \frac{kL_i}{r_i}, \tag{28}$$

$$r_i = aA_i^b, \tag{29}$$

For hollow pipe section : $a = 0.4993, b = 0.6777.$ (30)

The required specifications for the 120-member dome are given in Table 13.

The results are presented in Table 14. The best results correspond to the combined GPSG method, in which the deviation between different performances is low.

Fig. 8 Convergence history for the 72-member truss with different number of particles

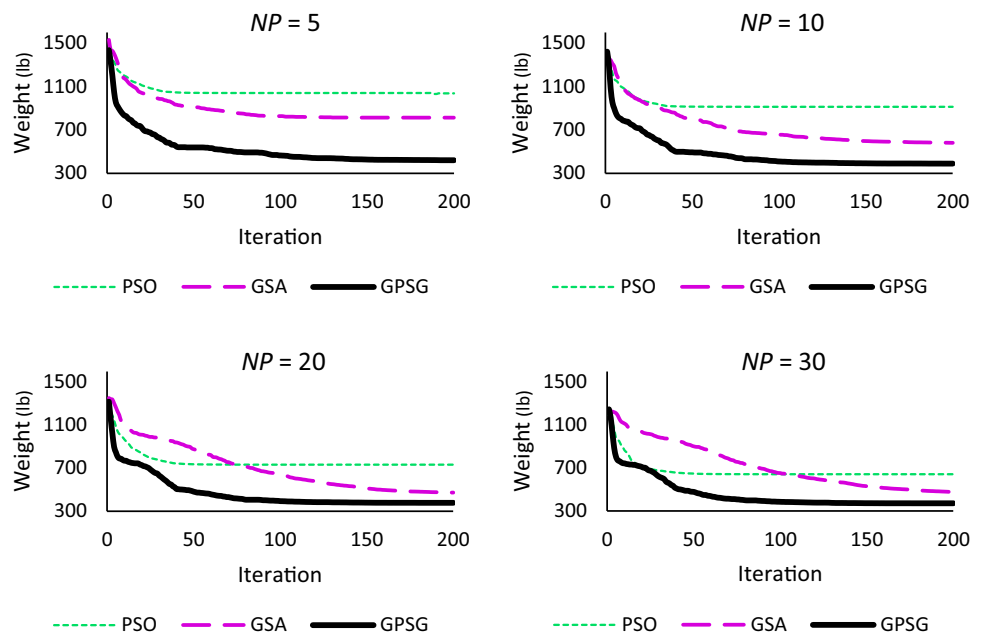


Table 11 Average ranking with different populations for 72-member truss

Algorithms	PSO	GSA	GPSG
Average mean (lb)	$8.32E + 02$	$5.86E + 02$	$3.90E + 02$
Average rank	3	2	1

The convergence trend of the results is presented in Fig. 10. The results show that for different populations, the GPSG is the most appropriate method.

The rankings of the three GSA, PSO and GPSG algorithms are presented in Table 15. Similar to the previous examples, the first rank belongs to the suggested new method of GPSG.

4 Conclusions

In advanced methods of optimization, the main goal is to find the optimal solution of multimodal functions efficiently. There are two main categories in this field. The

traditional gradient-based methods (GBM) start from a pre-assigned solution and move along a search direction using the gradients of the function under consideration. The GBM methods are reliable, efficient and fast for unimodal functions but may trap into a local optimum for multimodal functions and the initial point is important for the convergence. The second category is referred to as multipoint metaheuristic approaches. These methods are based on a number of the initial population and the search directions are made on some statistical ideas. The methods lead to finding the global point if enough initial population is chosen and the search directions are organized logically. However, the exploitation of the approaches is weak and unsatisfactory.

Based on these difficulties, in the present research, the two categories are combined to achieve a new successful approach. A compromise is made between the two categories in terms of their capabilities and shortcomings.

Among the vast number of metaheuristic techniques, the two rather successful methods of PSO and GSA are

Fig. 9 120-member dome

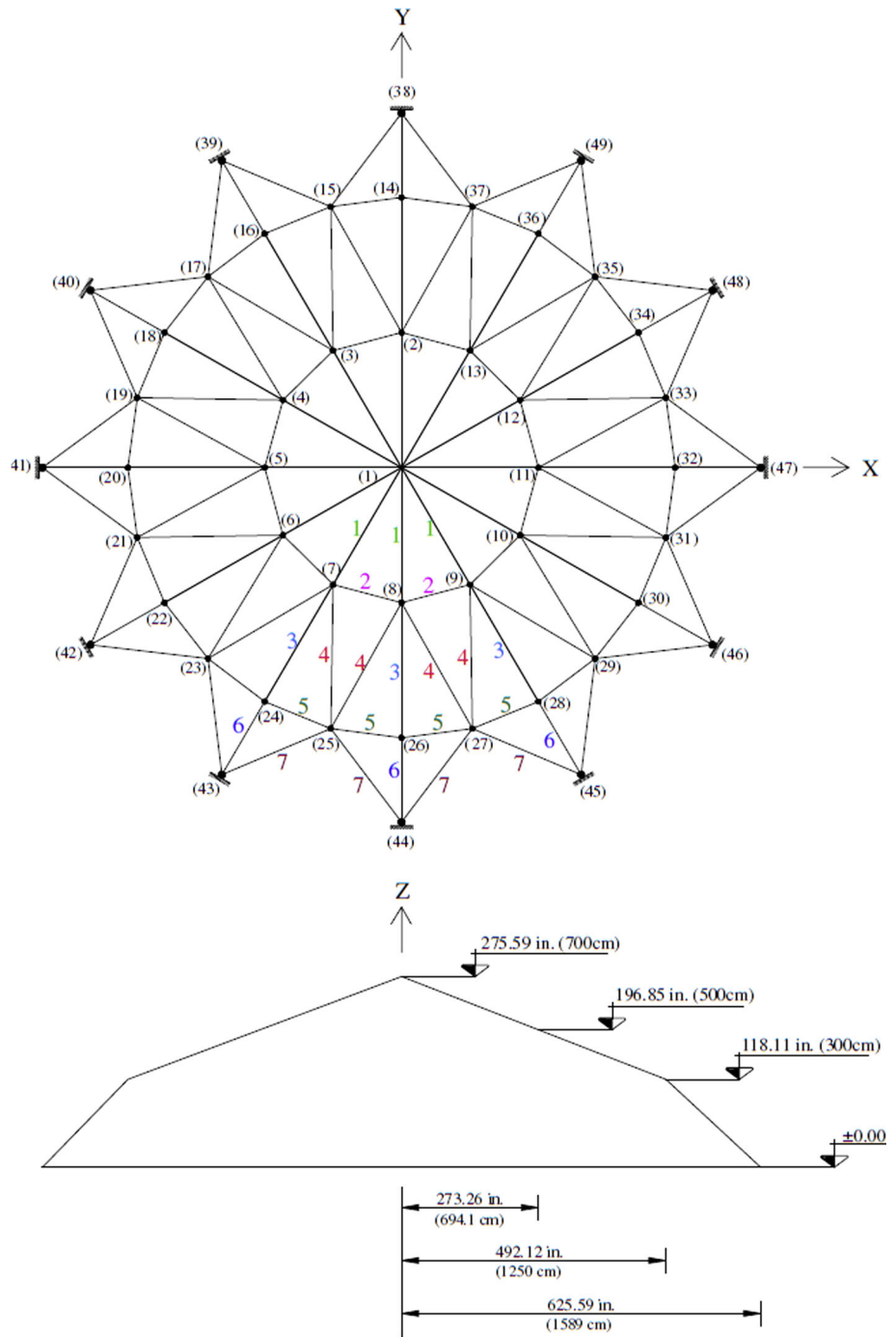


Table 12 External asymmetric forces applied to the 120-member dome

Node	External forces in the direction of the z-axis (kips)
1	- 13.49
2-14	- 6.744
15-37	- 2.248

Table 13 Properties of the 120-member dome

Properties	Values
Elasticity modulus	30,450 ksi
density	0.288 lb/in ³
Yield stress of steel	58.0 ksi
Area lower bound	0.775 in ²
Area upper bound	20 in ²
Allowable displacement in all directions	± 0.1969 in

Table 14 Results of 120-member algorithms with different populations

NP	PSO			GSA			GPSG						
	5	10	20	30	5	10	20	30	5	10	20	30	
Truss 120 bar	Avg. (lb)	51,022.67	41,847.61	37,230.87	36,078.23	46,004.19	34,800.11	33,556.52	33,810.75	34,159.15	33,760.72	33,790.71	33,725.07
	Rank	3	3	3	3	2	2	2	2	1	1	1	1
	SD. (lb)	5485.122	3462.493	2199.561	1329.784	3441.853	769.8276	137.3718	280.2098	532.2426	188.7468	156.5461	135.0523
	Med. (lb)	51,573.86	41,578.95	36,927.25	35,974.15	46,739.93	34,857.27	33,561.27	33,791.94	34,023.41	33,837.54	33,812.28	33,717.31
	Best. (lb)	43,521.18	35,769.45	33,998.85	33,895.98	38,813.21	33,544.44	33,334.58	33,399.91	33,593	33,452.62	33,428.94	33,480.05

selected and their combination is merged with GBM. The integration of the three methods is called GPSG.

The resultant of the search directions of the three methods are made in such a way to control the overall speed of the GPSG with proper move limits, employing the multipoint initial population and the philosophy of the stochastic ideas.

To verify the proposed method, 25 complicated multimodal functions of CEC2005 and 29 functions of CEC2017 from the literature as benchmark examples are tested. Besides, three structural design problems of two and three-dimensional truss structures with stress and displacement constraints are optimized for optimal weight.

The numerical results indicate the superiority of the proposed approach compared to both methods of PSO and GSA. In addition, the results of CEC2005 are compared with four variants of GSA and the results of CEC2017 are compared with eight other available methods. The first mean rank belongs to the proposed approach. The power of GPSG is investigated in terms of the exploration and exploitation demands. The new approach can reach the appropriate optimal solution with a less initial population with lower independent runs. The convergence history of the approach is smooth and the results are more efficient, reliable and stable.

It was found that the combination of GBA with either of the PSO and GSA works well; however, the efficiency of the integration of the three approaches is greatly enriched.

As the metaheuristic approaches are not suitable for all the optimization problems, the search is continuously under progress to reach more suitable approaches. It is intended to incorporate higher-order gradient directions with other variants in the future.

Fig. 10 Convergence history for the 120-member truss with different number of particles

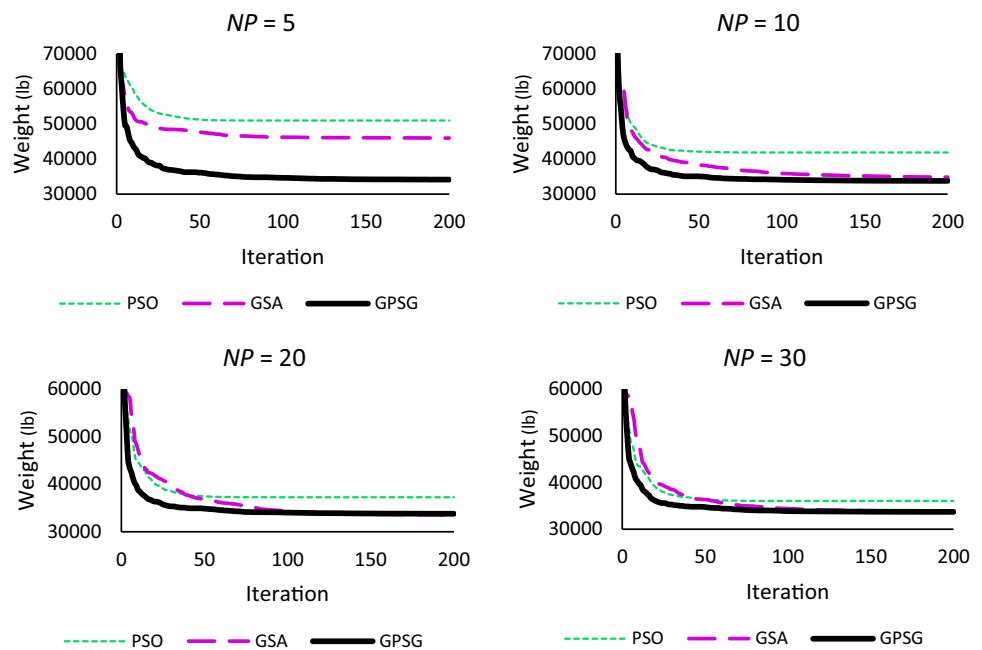


Table 15 Average ranking with different populations for 120-member Truss

Algorithms	PSO	GSA	GPSG
Average mean (lb)	41,544.84	37,042.89	33,858.91
Average rank	3	2	1

Author contributions FS was involved in conceptualization, methodology, software, writing; ES helped in supervision, editing, reviewing; SS contributed to supervision, validation, reviewing.

Funding No funding was received to assist with the preparation of this manuscript.

Data availability Enquiries about data availability should be directed to the corresponding author.

Declarations

Conflict of interest Authors declare that they have no conflict of interest.

Ethical approval This article does not contain any studies with human participants or animals performed by any of the authors.

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