



A novel method for improving the accuracy of MR-derived patient-specific vascular models using X-ray angiography

John D. Horn¹ · Zbigniew Starosolski^{2,3} · Michael J. Johnson⁴ · Avner Meoded^{2,3} · Shaolie S. Hossain^{1,4} 

Received: 27 December 2021 / Accepted: 27 May 2022 / Published online: 27 June 2022
© The Author(s), under exclusive licence to Springer-Verlag London Ltd., part of Springer Nature 2022

Abstract

MR imaging, a noninvasive radiation-free imaging modality commonly used during clinical follow-up, has been widely utilized to reconstruct realistic 3D vascular models for patient-specific analysis. In recent work, we used patient-specific hemodynamic analysis of the circle of Willis to noninvasively assess stroke risk in pediatric Moyamoya disease (MMD)—a progressive steno-occlusive cerebrovascular disorder that leads to recurrent stroke. The objective was to identify vascular regions with critically high wall shear rate (WSR) that signifies elevated stroke risk. However, sources of error such as insufficient resolution of MR images can negatively impact vascular model accuracy, especially in areas of severe pathological narrowing, and thus diminish clinical relevance of simulation results, as local hemodynamics are sensitive to vessel geometry. To improve the accuracy of MR-derived vascular models, we have developed a novel method for adjusting model vessel geometry utilizing 2D X-ray angiography (XA), which is considered the gold standard for clinically assessing vessel caliber. In this workflow, “virtual angiographies” (VAs) of 3D MR-derived vascular models are conducted, producing 2D projections that are compared with corresponding XA images to guide the local adjustment of modeled vessels. This VA-comparison-adjustment loop is iterated until the two agree, as confirmed by an expert neuroradiologist. Using this method, we generated models of the circle of Willis of two patients with a history of unilateral stroke. Blood flow simulations were performed using a Navier–Stokes solver within an isogeometric analysis framework, and WSR distributions were quantified. Results for one patient show as much as 45% underestimation of local WSR in the stenotic left anterior cerebral artery (LACA), and up to a 56% underestimation in the right anterior cerebral artery when using the initial MR-derived model compared to the XA-adjusted model. To evaluate whether XA-based adjustment improves model accuracy, vessel cross-sectional areas of the pre- and post-adjustment models were compared to those seen in 3D CTA images of the same patient. CTA has superior resolution and signal-to-noise ratio compared to MR imaging but is not commonly used in the clinic due to radiation exposure concerns, especially in pediatric patients. While the vessels in the initial model had normalized root mean squared deviations (NRMSDs) ranging from 26 to 182 and 31 to 69% in two patients with respect to CTA, the adjusted vessel NRMSDs were comparatively smaller (32–53% and 11–42%). In the mildly stenotic LACA of patient 1, the NRMSDs for the pre- and post-adjusted models were 49% and 32%, respectively. These findings suggest that our XA-based adjustment method can considerably improve the accuracy of vascular models, and thus, stroke-risk prediction. An accurate, individualized assessment of stroke risk would be of substantial help in guiding the timing of preventive surgical interventions in pediatric MMD patients.

Keywords Computer-aided design · Image-based modeling · Segmentation · Stroke · Wall shear rate

1 Introduction

Patient-specific modeling of vascular networks has proven to be a valuable tool in the research of vascular pathologies and their treatment. Researchers have used patient-specific vascular modeling to detect coronary artery disease [1], to inform treatment planning via optimization of graft placement [2], surgical intervention [3] and nanoparticulate drug

✉ Shaolie S. Hossain
shossain@texasheart.org

Extended author information available on the last page of the article

delivery [4, 5], and to assess aneurysms and their treatments [6]. In previous work [7, 8], we have used patient-specific modeling to evaluate the hemodynamics within the circle of Willis (CoW) of pediatric patients with Moyamoya disease (MMD). MMD is a chronic cerebrovascular disease characterized by progressive (non-atherosclerotic) narrowing of the major vessels of the CoW that can result in recurring stroke events [9]. Since there are no known treatments to reverse or slow the vessel narrowing caused by MMD, current clinical interventions focus on addressing the complications of the disease (e.g., recurrent stroke, brain volume loss). These include neurosurgical strategies that allow blood flow to bypass areas of stenosis, thereby reducing stroke risk. Therefore, an individualized assessment of stroke risk, as a means of guiding the timing of preventive interventions, would be of great clinical benefit. It has been postulated that local wall shear rate (WSR) in the CoW arteries may be an indicator for disease progression and elevated stroke risk in pediatric MMD patients [7, 10]. Critically high local WSR values above a 5000 s^{-1} limit could result in thrombus formation leading to ischemic stroke [11, 12]. Thus, by evaluating WSR, stroke risk in MMD patients can be assessed, and clinicians can plan individualized patient follow-up and surgical strategies.

Computational fluid dynamics (CFD) simulation has been successfully used to evaluate hemodynamic quantities in the major arteries of the CoW [7, 13, 14]. As variations in vessel architecture can strongly influence local hemodynamics including WSR [7, 15], it is critically important that computational modeling accurately captures a patient's vascular anatomy. Computed tomography angiography (CTA) is often utilized to create three-dimensional (3D) patient-specific vascular models for CFD studies, and many segmentation techniques have been developed to improve model accuracy [16]. While CTA imaging is generally desirable for this purpose, it is not commonly collected during pediatric MMD patient follow-up because of the significant radiation burden associated with CTA imaging in children. MR time of flight (MR TOF), which does not require ionizing radiation, is an alternative for reconstructing 3D patient-specific models that is more commonly used during clinical follow-up of young MMD patients. Given tradeoffs between resolution and imaging time—an important factor since pediatric patients must be sedated during image collection—MR TOF data often have coarse voxel resolution. This can affect geometric accuracy, particularly in pediatric patient models, where some vessels of interest may only be one or two voxel widths in diameter (vessel diameters as small as 1 mm vs. voxel widths near 0.5 mm). Further, important vessel features, such as severe MMD-caused vessel narrowing, can sometimes go unresolved by MR TOF which produces insufficient signal in areas of slow blood flow

[17]. In addition, vessels oriented parallel to the imaging slice plane can be poorly resolved. Therefore, the accuracy of MR-derived models may not be adequate to reliably predict stroke risk in pediatric MMD patients. X-ray angiography (XA), a minimally invasive imaging tool, is also commonly used to visualize a patient's vasculature during clinical evaluation and follow-up. While the 2D projections obtained from XA cannot be used alone for 3D geometry reconstruction, they offer accurate depictions of vessel diameter and MMD-related vessel narrowing is typically well resolved. Lumen boundaries are also generally better defined in 2D XA images than 3D MR or CTA images.

Given the need for accurate vascular models for stroke risk assessment in MMD patients, we have developed a method of 3D vascular model reconstruction that uses a combination of MR and XA patient imaging data. We hypothesize that by using 2D XA images as a reference for correct vessel caliber, MR-derived 3D models can be adjusted to improve accuracy. Our method involves computing 2D projections of the MR-derived 3D models onto a virtual detector plane using geometric parameters that mimic the clinical XA imaging setup (i.e., patient position in relation to the X-ray source and detector). The 2D projections are compared to the XA images and vessels in the 3D model are locally adjusted until the two agree. The effectiveness of the proposed adjustment methods in improving geometric accuracy is evaluated by comparing the resulting CoW models to 3D CTA images that were also available in the patient records. Treating the CTA images as a more accurate 3D representation of the patient's vascular anatomy compared to MR [18], we then assess if the MR-derived models have improved accuracy after XA-based adjustment.

2 Methods

In this work, we generated CoW models from de-identified imaging data of two patients who were retrospectively selected from a Texas Children's Hospital database under an institutional review board-granted waiver of written authorization for consent. The selection criteria were (1) the availability of MR TOF, XA, and CTA imaging data in patient history, and (2) a history of stroke with visible vascular narrowing in the affected side. Patient 1 is diagnosed with MMD and presented with a stroke involving the right middle cerebral artery (RMCA). Patient 2 is a non-MMD patient, who suffered a right-side stroke. Evidence of severe occlusion in the RMCA was found on imaging. While unresolved, dehydration, inflammation, and viral infection including possible COVID infection, were suggested as potential causes for the stroke in patient 2.

2.1 Vascular model creation

To create patient-specific models of the CoW suitable for blood flow simulations, we employ a four-stage process whereby an initial representation is segmented from clinical MR TOF patient data and adjusted using clinical XA imaging data. This model creation process is summarized in Figs. 1 and 2 and detailed in the following sections.

2.1.1 Generating the initial 3D model

We start with MR TOF data output as an image stack in a .NRRD file format. Prior to segmenting the CoW from the image stack, 3D Slicer (version 4.10.2) is used to resample the volume to yield voxel sizes with linear dimensions reduced by at least one half. This improves the segmentation results, especially in smaller vessels that are at most one or two voxels in diameter prior to the resampling. 3D Slicer is then used to segment the resampled image stack using intensity thresholding and other manual methods. The segmented label map is then exported as a triangulated surface mesh as a .STL file. The surface mesh is then post-processed using MeshMixer (version 3.5, Autodesk Inc., San Rafael, CA,

USA) to locally smooth the segmented surface and repair any mesh errors resulting from the segmentation process. The resulting triangulated surface mesh is exported as a new .STL and is considered the initial model or mesh (Fig. 1A).

2.1.2 Aligning the 3D model with XA imaging axis

To compare vessel geometry of the CoW model to that seen on XA images, we must align the model to the XA imaging view. Metadata from XA imaging including “distance source to patient”, “distance source to detector”, “positioner primary angle”, and “positioner secondary angle” are used to define the imaging axis in a virtual space, mimicking the XA setup for each XA image. Centerlines, extracted from the CoW model, are used to find a position and orientation, relative to the imaging axis and virtual X-ray source, such that the CoW model centerlines align with the XA image when projected along the imaging axis onto the virtual detector plane (Fig. 1B). This is done by selecting a set of reference points on the model centerlines at vessel intersections and target points on the XA images that correspond to the same vessel intersections. Using custom algorithms implemented in Matlab

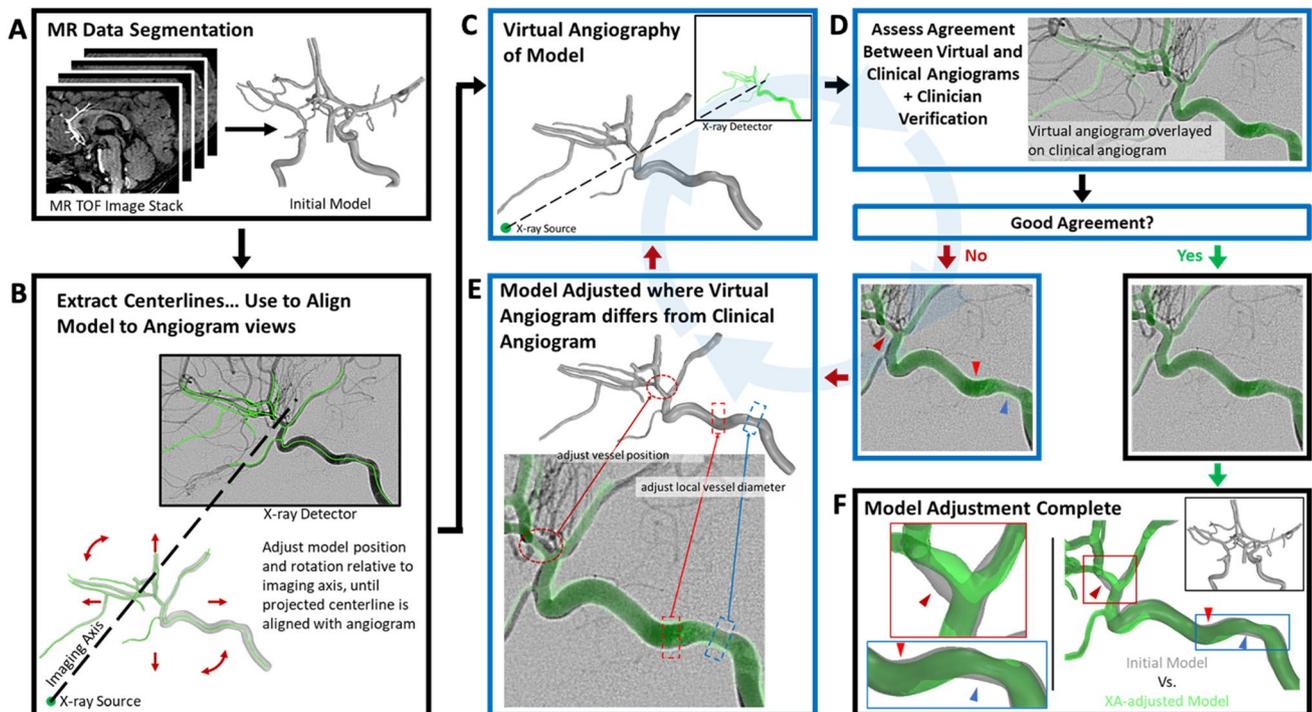


Fig. 1 Graphical flow chart showing processes for model creation and XA-based adjustment. **A** An initial model is created by segmenting an MR TOF image stack. **B** Model centerlines are used to align the model relative to a virtual X-ray source and detector mimicking clinical XA image acquisition. **C** A virtual angiogram is computed of the model and **D** compared to the corresponding clinical XA image. If

the virtual angiogram of the model and the clinical angiogram differ, the model is locally adjusted (**E**), and a new virtual angiogram is computed. The adjust–virtual angiography–compare steps (**C–D–E**) are iteratively repeated until there is good agreement between the two angiograms. **F** Comparison of final adjusted model (green) to initial model (color figure online).

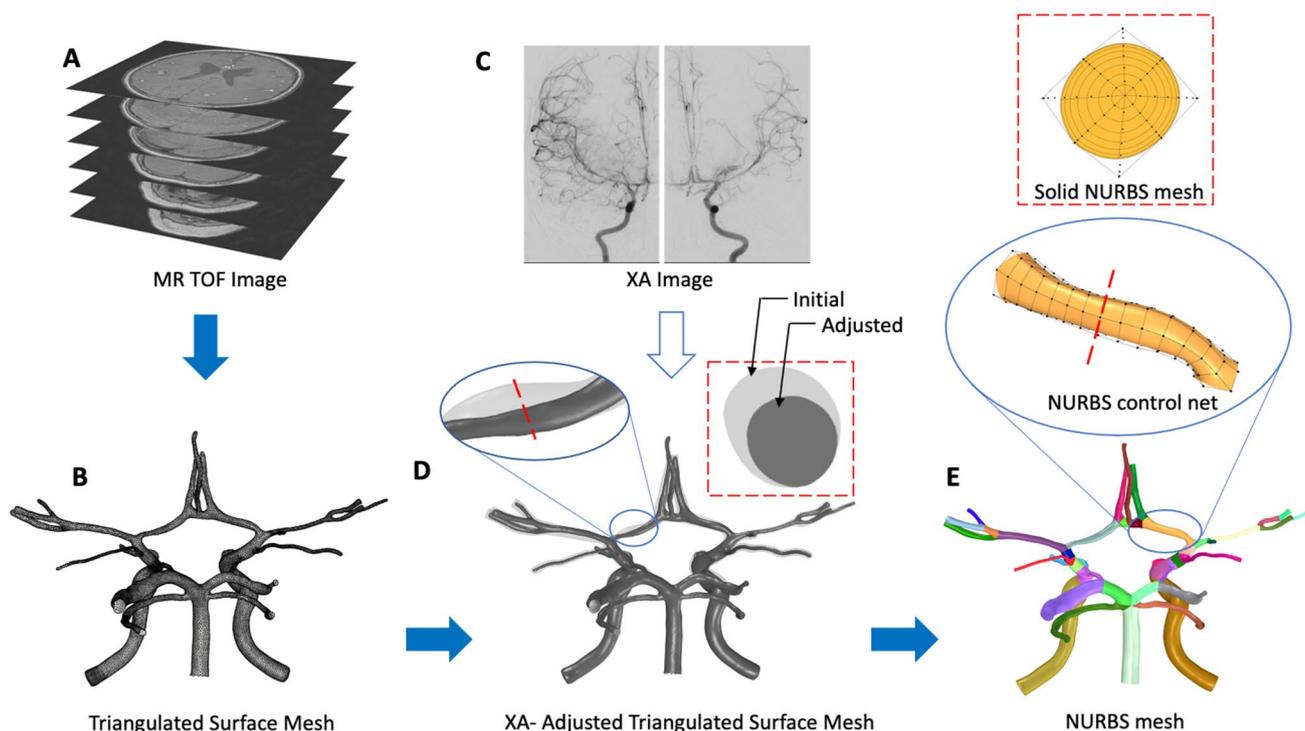


Fig. 2 The vascular modeling pipeline. The circle of Willis vasculature is segmented from MR TOF images (**A**) as a triangulated surface mesh (**B**) using 3D Slicer. 2D projections of the segmented mesh are registered to (**C**) XA images. The vessel diameters along the mesh are locally adjusted to match XA images. **D** The adjustments made

across the entire mesh. Adjustments made along the LACA are highlighted in the insets. The adjusted surface mesh is used to generate the solid NURBS mesh (**E**). Each vessel corresponds to a volumetric NURBS patch. The insets show the NURBS patch, control net, and a cross-section for the RACA (color figure online).

(version 2019b, The MathWorks Inc, Natick, MA, USA), a range of rotations and translations about the three coordinate axes are then tested to determine which model orientation and position produces the best alignment. This is done by optimizing a cost metric, C , defined as the root mean square of the distances between the projected reference points and their corresponding target points where P_n and T_n are the n th projected reference point and target point, respectively, and N is the total number of reference/target pairs considered:

$$C = \sqrt{\frac{1}{N} \sum \|P_n - T_n\|^2}$$

Initially, a 3D domain of rotations about each axis is systematically sampled, with uniform spacing, over a wide range of values and the resulting cost metric for each orientation is computed. We chose a spacing density of 31 in each dimension resulting in 31^3 rotational orientations tested for each iteration. For subsequent iterations, the test range is reduced in size and centered about the orientation that previously produced the minimum cost metric. For each XA image, between 10 and 15 iterations are typically required

to determine the optimal alignment. Using this process, the model is aligned to each of the XA images.

2.1.3 Algorithmic adjustment of 3D model geometry using XA images

After determining the alignment of the initial model for each XA image, Rhino and Grasshopper (version 6, Robert McNeel & Associates, Seattle, WA, USA) are used to apply algorithmic adjustment to the CoW model based on each XA image. In this process, local vessel diameters of the CoW model are measured at set intervals along each vessel. After superimposing the clinical XA image on the virtual detector plane, vessel lumen edges are manually delineated on the XA images and confirmed by an expert neuroradiologist, and target vessel diameters are determined. The model diameters are then projected onto the virtual detector plane (Fig. 1C) and compared to the target diameters to generate scale factors that are used to locally expand or contract the 3D model radially about the vessel centerline. This process is repeated for each XA image. After adjustment in all six views—that is coronal and sagittal views of both the left

ICA (LICA) and right ICA (RICA), and coronal and sagittal views of the basilar artery (BA)—the mesh is manually adjusted using Meshmixer to smooth out any unwanted artifacts from the algorithmic adjustment and to manually adjust at vessel intersections where the algorithmic process cannot be applied.

2.1.4 Manual adjustment of 3D model geometry to achieve agreement with XA images

Finally, a series of manual adjustments are made to the 3D model to improve its agreement with the XA images. Virtual angiographies of the adjusted model onto the detector plane of each XA image are computed after orientating the model to the imaging axis based on the alignments determined earlier. The virtual angiographies result in 2D projections of the model which are overlaid onto the XA images enabling comparison of the model's vessel geometry to the vessel geometry shown on the XA images (Fig. 1D). The model is manually adjusted using Meshmixer in areas where the projection does not agree with the vessel geometry as depicted on the XA image (Fig. 1E). This involves locally adjusting the vessel boundaries using Meshmixer's mesh editing tools to either expand or reduce the vessel radius, make slight adjustments to vessel curvature, and correct the geometry at vessel junctions. This manual adjustment-projection-compare process is iteratively repeated for each area of concern until good agreement is achieved, as confirmed by an expert neuroradiologist. This process typically takes 5–10 iterations for each focus area in each XA image. Overall, the manually adjustment process can take up to several hours depending on the amount of deviation between the model and the XA images. The final adjusted model (Fig. 1F) is then exported as a surface mesh and processed for nonuniform rational B-spline (NURBS) mesh generation.

2.1.5 Reconstruction of solid NURBS model

The adjusted surface mesh from the previous step is used to generate a volumetric NURBS reconstruction of the CoW (Fig. 2). This is done according to the procedures defined in a previous report [19]. The NURBS generation uses a template-based vascular modeling [20] software built with the computer-aided design (CAD) package Rhinoceros 3D. First, a skeletonization algorithm is applied to the surface mesh to extract the vessel centerlines and topology. Along each centerline, a set of minimal torsion perpendicular frames are constructed at regular intervals. At branch points, where multiple vessel centerlines intersect, the frames are folded to define conforming NURBS patch interfaces. The fold angle is interpolated along a length of the centerline to avoid self-intersection and provide a higher quality parameterization. A closed intersection curve between the mesh

and each frame is computed and interpolated with a NURBS curve. The control points of the NURBS curves are then lofted together to create the control net for the multi-patch NURBS surface reconstruction of the adjusted surface mesh. Finally, the surface control points are extruded in the radial direction to the centerline to obtain a volumetric NURBS reconstruction of the CoW that is used for analysis. Element sizes and refinements are chosen according to mesh independence studies [7, 8]. Each branch in the vasculature is a quadratic NURBS solid with 16 elements in the circumferential direction and 17 elements in the radial direction. The element size in the radial direction is graded such that there are more elements near the boundary to resolve the boundary layer in the blood flow simulation. The NURBS geometry is maximally smooth in the radial and axial directions and contains four C^0 knot lines in the circumferential direction corresponding to the folding axes.

2.2 Blood flow simulations

Figure 3 illustrates the simulation setup. The details of the governing equations and solution strategy can be found in previous works [7, 8] and references therein. Briefly, blood flow is assumed to be governed by the unsteady Navier–Stokes equations subjected to boundary conditions as follows. A pulsatile inflow condition [21] is imposed at the three inlets: LICA, RICA, and BA, with a parabolic inflow profile [22] (Fig. 3E). A no-slip Dirichlet boundary condition is set on the vessel wall, and a traction-free boundary condition is prescribed at all the outlets for simplicity [7]. Blood is assumed to be a Newtonian fluid with a density of 1060 kg/m^3 and a dynamic viscosity of $0.0035 \text{ Pa}\cdot\text{s}$. The system of equations is solved by implementing a residual-based variational multiscale method using a Newton–Raphson procedure with a multistage predictor–corrector algorithm applied at each time step. The generalized-alpha method is used for time advancement. Within an isogeometric analysis framework [23], quadratic NURBS are used to describe both the geometry and the solution space. The CoW model of patient 1 and patient 2 has 138,720 and 149,600 volumetric quadratic NURBS elements and is divided into 40 and 34 subdomains, respectively, where each subdomain is assigned to a compute core [7]. WSR is computed from the equation of wall shear stress vector: $\boldsymbol{\tau} = (\boldsymbol{\sigma} \cdot \mathbf{n}) - ((\boldsymbol{\sigma} \cdot \mathbf{n}) \cdot \mathbf{n})\mathbf{n}$, where $(\boldsymbol{\sigma} \cdot \mathbf{n})$ is the traction vector, $\boldsymbol{\sigma}$ is the stress tensor, and \mathbf{n} is the unit normal.

2.3 Assessment of model accuracy

To determine if the XA-adjustment process described above improves accuracy of the reconstructed CoW geometry, we use CTA imaging data as a reference. For our analysis, the working assumption is that CTA images provide a more

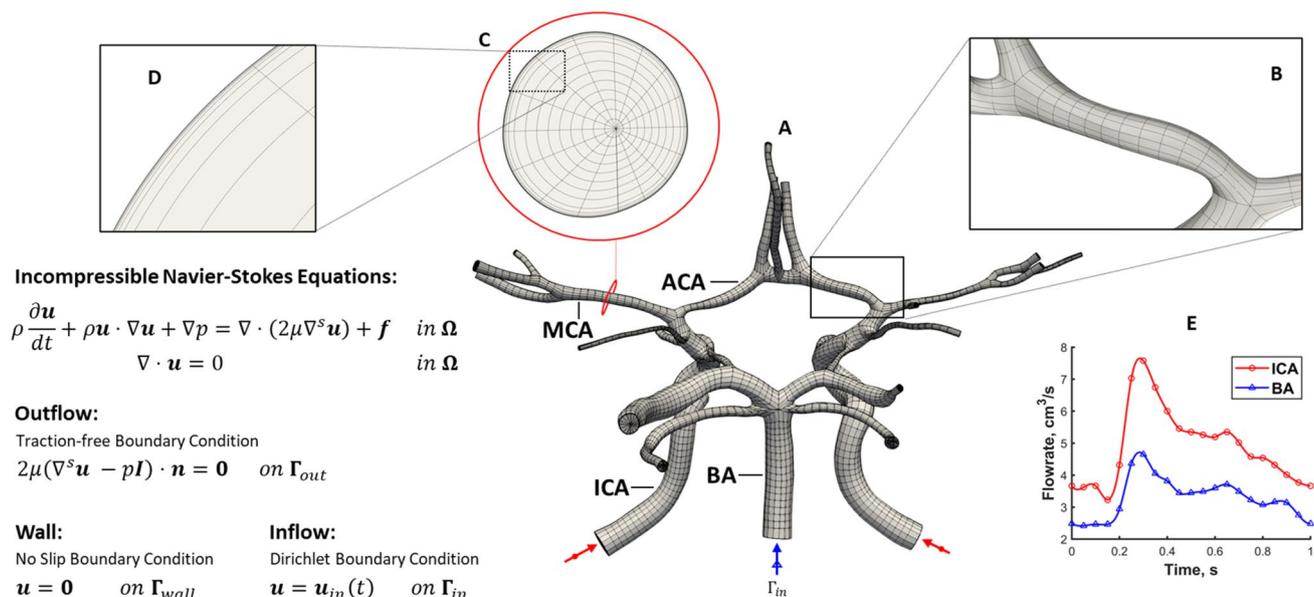


Fig. 3 A volumetric NURBS mesh of the CoW (A) is generated from the adjusted CoW surface mesh. A close-up of a bifurcation (B) is shown to highlight the mesh quality and refinement used in the computation. The cross-section of the NURBS mesh (C) is shown to highlight the boundary layer refinement (D) used in the simulation. The equations and boundary conditions for the blood-flow simulation is presented, where \mathbf{u} represents velocity, p is pressure, \mathbf{f} is the

accurate 3D representation of vessel caliber, especially in areas of vessel narrowing compared to MR TOF [18]. Thus, by comparing the MR-derived XA-adjusted models of a patient's CoW to corresponding CTA imaging, we can determine whether the XA-adjusted model more closely represents the patient's geometry than the MR-derived initial model. To do this, we quantify how much deviation exists between vessel cross-sectional areas taken from the models (initial and adjusted) and the corresponding vessel cross-sectional areas extracted from the CTA images. For our analysis, we focus on the major vessels of the anterior circulation: terminal internal carotid arteries (ICAs), proximal middle cerebral arteries (MCAs), and proximal anterior cerebral arteries (ACAs) [24].

2.3.1 MR and CTA volume co-registration

First, we co-register the CTA image stack and the MR image stack from which the initial 3D model was segmented. This brings the vessels in the 3D model in approximate alignment with the CTA images and allows for direct comparison between the two. Prior to co-registration, regions of interest in each set of images were defined to isolate the vessels of interest in the CoW and reduce vessel misalignment related to high pixel intensities corresponding to boney structures. Rigid co-registration (translation and rotation only) was

performed in 3D slicer using the built-in general registration module that optimizes alignment using a Mattes Mutual Information cost metric.

external force, μ is dynamic viscosity, ρ is density, t is time, and \mathbf{n} is the unit normal. A pulsatile inflow condition [21] is prescribed at the three inlets. The inflow at the two ICAs and BA are given by the red and blue waveforms, respectively. A no-slip boundary condition is imposed along the vessel walls, and a traction-free boundary condition is applied at each outlet

2.3.2 Vessel cross-sections

Vessel cross-sections are obtained from the initial and adjusted models using planes perpendicular to the respective vessel centerlines (Fig. 4A). These are taken at an interval of 0.1 mm along each centerline. These planes are then used to extract slices from the co-registered CTA volume resulting in perpendicular cross-sections of each vessel that correspond to the model cross-sections.

2.3.3 Detection of lumen boundary on CTA

With the goal of comparing cross-sectional lumen areas between the CoW model geometry and the CTA images, we extract the lumen boundary from each cross-sectional slice along the vessel centerline (Fig. 4B). The lumen boundary is detected based on an analysis of CTA pixel intensity taken along a line extending from the center of the vessel (greatest intensity) to beyond the lumen boundary (least intensity). The inflection point of this pixel intensity profile is identified along with the amplitude between the peak intensity and the lowest intensity. The lumen boundary is taken as the point where the pixel intensity is equal to the inflection point plus

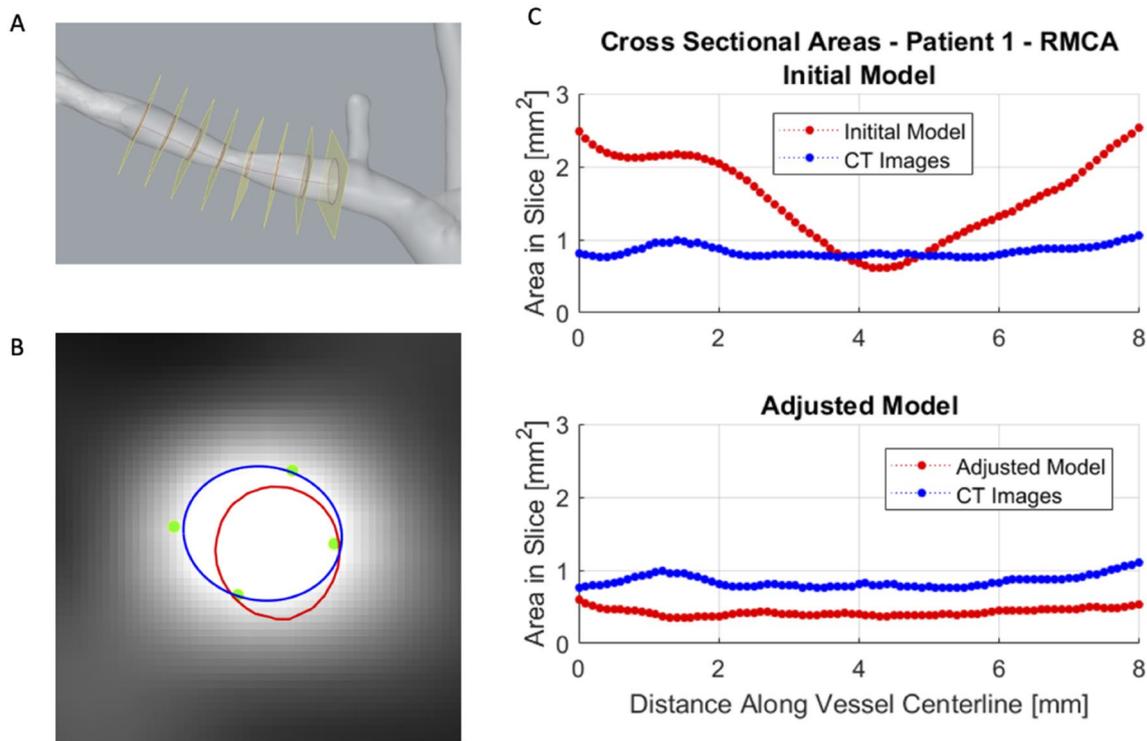


Fig. 4 Overview of XA-adjustment verification strategy. **A** Several planes (yellow) along the length of a vessel of the 3D model (RMCA of the initial patient 1 model shown), perpendicular to its centerline, are used to extract vessel cross-sections (red curves). **B** An example CTA slice corresponding to one of the perpendicular planes in (**A**). The cross-section of the model superimposed on the CTA slice is shown by the red curve. Determination of the vessel lumen boundary on the CTA slice (blue curve) is guided by assessment of lumen

extent provided by a trained neuroradiologist (green dots). **C** Cross-sectional areas of the model vessel and CTA vessel are computed in each slice and plotted against the position along the vessel centerline. The top plot compares the initial model (red curve) to the CTA-extracted lumen area (blue curve) and the bottom plot compares the adjusted model (red curve) to the CTA images (blue curve). These curves are used to compute the RMSD for each vessel (color figure online).

an offset value. This offset value, defined as a percentage of the profile amplitude, is calibrated using neuroradiologist input. This process is repeated at several angular positions relative to the center of the vessel producing a series of points outlining the lumen. To calibrate the offset value, a sample set of vessel cross-sections was provided to an expert pediatric neuroradiologist who estimated vessel caliber from clinical CTA images. The neuroradiologist marked 3–5 points on each image corresponding to his visual estimate of the lumen boundary (Fig. 4B). Calibration of the offset value is achieved by determining the offset value that produces the lumen boundary with the least average distance to the points marked by the neuroradiologist. The optimal offset value is identified for each slice, and a mean offset for each vessel is calculated and used for detecting the lumen boundary.

2.3.4 Comparison of cross-sectional areas

Cross-sectional areas of the initial and adjusted models are found by computing the areas enclosed by the rings produced by intersecting the perpendicular planes with

the model surface meshes. Likewise, corresponding cross-sectional areas are computed using the detected lumen boundaries on CTA. As an example, Fig. 4C shows these cross-sectional areas for one vessel (patient 1—RMCA) plotted against the position along the vessel centerline. To compare the cross-sectional areas of the models to the cross-sections extracted from CTA images, along the length of each vessel, the root means squared deviation (RMSD) was computed:

$$RMSD_{\text{vessel}} = \sqrt{\frac{\sum_{n=1}^N (A_{\text{model},n} - A_{\text{CTA},n})^2}{N}}$$

where $A_{\text{model},n}$ and $A_{\text{CTA},n}$ are the cross-sectional areas in the n th slice taken from the model and CTA images, respectively, and N is the total number of slices taken for that vessel. The RMSD values are then normalized by the mean cross-sectional area, taken from the CTA images, for a given vessel. The normalized RMSD (NRMSD) is then given by

$$\text{NRMSD}_{\text{vessel}} = \frac{\text{RMSD}_{\text{vessel}}}{\text{mean}(A_{\text{CTA},\text{vessel}})}$$

3 Results

Clinical imaging data, including XA and MR TOF, were used to create two patient-specific CoW models. The initial models, derived from the MR TOF volumetric data alone, were adjusted using XA images and the procedures outlined above. A comparison of the initial and adjusted models for the two patients can be seen in Fig. 5. The XA-based adjustment of patient 1's CoW model generally resulted in vessels with reduced caliber. In contrast, the XA-based adjustment

of the patient 2 model resulted in larger vessel calibers in general.

In recent work [7, 8], we have used CoW models derived from pediatric MMD patient imaging data to assess stroke risk through blood flow simulation and an analysis of predicted WSR distributions. We conducted similar simulations using the initial and XA-adjusted CoW models for the two patients included in the present study and compared the WSR distributions of the pre- and post-adjustment models (Fig. 6). The maximum WSRs in each vessel of interest from the initial and XA-adjusted models for both patients are shown in Table 1. For patient 1, the initial model resulted in a surface-averaged peak systolic WSR of 5290 s^{-1} and the adjusted model produced a surface-averaged peak WSR of 9827 s^{-1} . The adjusted model produced focal areas with greater maximum WSR at peak systole than the initial

Fig. 5 Comparison of initial (blue) and XA-adjusted models (green) for patient 1 (top panels) and patient 2 (bottom panels) shown in posterior (left) and anterior views (right)

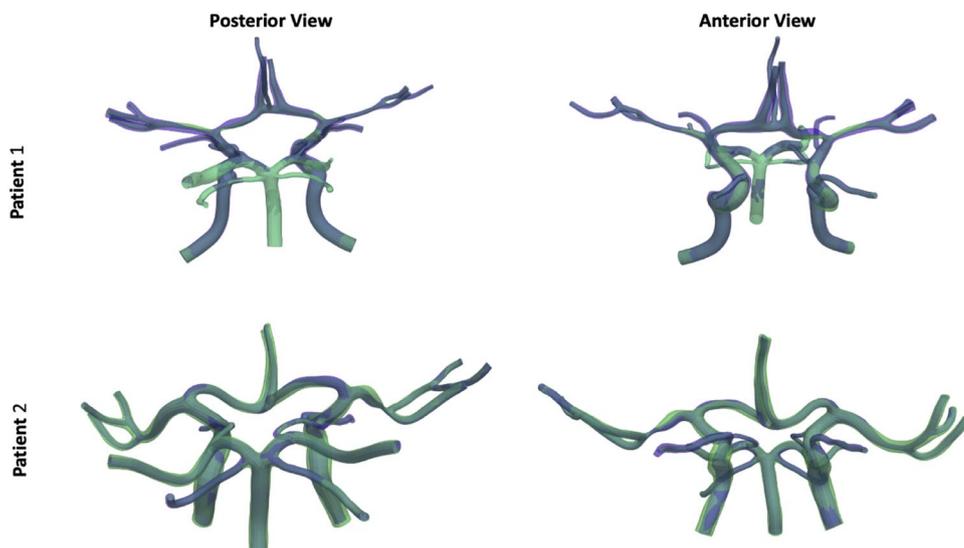


Fig. 6 Comparison of predicted WSR (above 5000 s^{-1} coagulation limit) distributions for the initial (left panels) and XA-adjusted (right panels) models of patient 1 (top) and patient 2 (bottom) (color figure online).

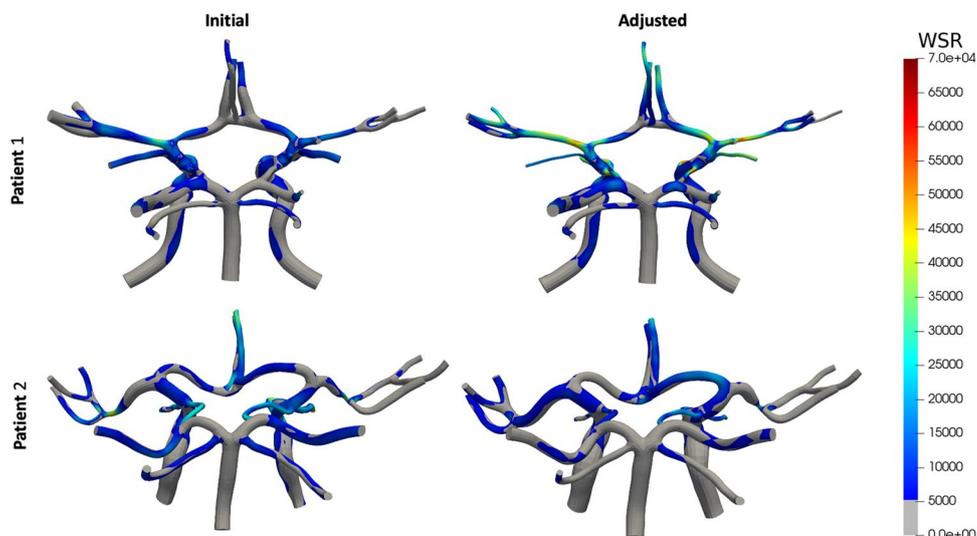


Table 1 A summary of simulation (maximum WSR) results and model accuracy (NRMSD) for initial and adjusted models

Vessel	Maximum WSR (s^{-1})		NRMSD (%)	
	Initial model	Adjusted model	Initial model	Adjusted model
<i>Patient 1</i>				
LACA	20,364	37,013	49	32
LMCA	37,778	50,370	31	44
LICA	18,217	28,522	81	35
RACA	19,550	44,932	182	28
RMCA	17,829	54,198	82	53
RICA	17,335	37,631	26	32
<i>Patient 2</i>				
LACA	10,885	20,181	45	30
LMCA	43,402	10,251	69	42
LICA	10,112	10,576	36	11
RACA	14,734	26,211	37	22
RMCA	50,887	43,291	48	21
RICA	16,492	12,981	31	36

model. Of note, the proximal left MCA (LMCA) and left ACA (LACA) of the adjusted model had maximum WSRs of $50,370 s^{-1}$ and $37,013 s^{-1}$, whereas the corresponding vessels of the initial model had maximum WSRs of $37,788 s^{-1}$ and $20,364 s^{-1}$, respectively. On the other hand, in proximal right ACA (RACA) and right MCA (RMCA), maximum WSRs of $19,550 s^{-1}$ and $17,829 s^{-1}$ were predicted in the initial models, respectively, and maximum WSRs of $44,932 s^{-1}$ and $54,198 s^{-1}$ were predicted in the adjusted models, respectively. For patient 2, the initial model resulted in a surface-averaged peak systolic WSR of $7942 s^{-1}$ and the adjusted model produced a surface-averaged peak WSR of $4763 s^{-1}$. In the initial model, the LMCA saw a peak WSR of $43,402 s^{-1}$, while the same vessel in the adjusted model saw a maximum WSR of $10,251 s^{-1}$. The RACA in the initial model had a peak WSR of $14,734 s^{-1}$, while the adjusted RACA had a peak WSR of $26,211 s^{-1}$. (color figure online).

To determine if the XA-based adjustments of the two patients' CoW models improve model accuracy, we compared the geometries to clinical CTA data that was available for each patient. Specifically, cross-sectional areas taken from each model were compared with cross-sectional areas extracted from corresponding CTA slices, and the deviations between the two were quantified. Figure 7 shows NRMSDs between the model cross-sectional areas and CTA lumen areas along each vessel for the initial and adjusted models for both patients. In most of the vessels considered for the two patients, the adjusted model shows less deviation from the cross-sectional areas suggested by the CTA images (see Table 1). For four of six vessels in patient 1 and five of six vessels of patient 2, XA-adjustment resulted in reduced

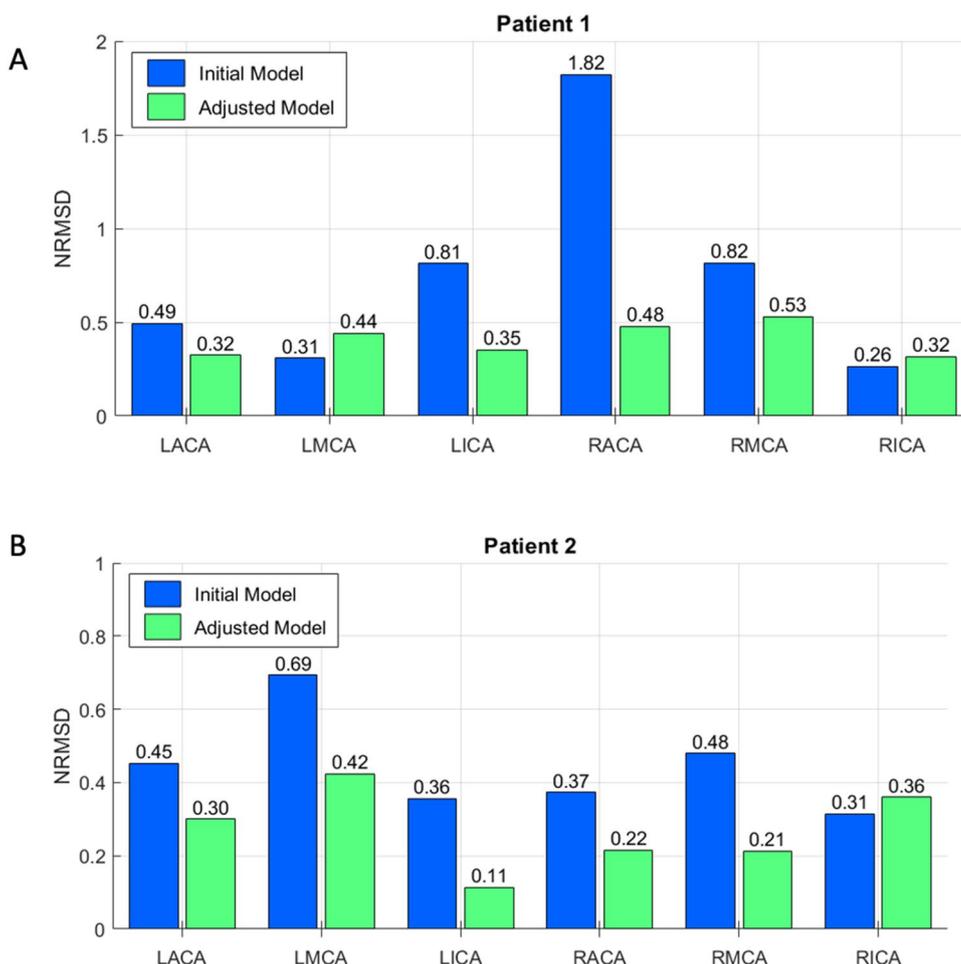
NRMSD. Of note, the NRMSD for the RACA in patient 1 (Fig. 7A) decreased from 182 (of the average CTA area in the RACA) to only 48% after adjustment. However, two of the six vessels of interest for patient 1 had more deviation from the CTA images after adjustment. The NRMSD increased from 31 to 44% for the LMCA after adjustment and it increased from 26 to 32% for the RICA. In patient 2 (Fig. 7B), all the vessels of interest exhibited smaller NRMSD in the adjusted model vessels compared to the initial model with the exception of the RICA that had increased NRMSD after adjustment (36 vs. 31% in the initial model).

4 Discussion

With growing focus on expanding personalized medicine, patient-specific geometries have been increasingly used to make personalized assessments of disease status and enable tailored planning of treatment strategies. Recently, we performed patient-specific hemodynamic analysis of the CoW with the goals of assessing stroke risk in pediatric MMD patients and potentially aiding clinicians in determining if surgical intervention may be required [7]. A common, and often preferred, source for patient-specific vascular geometries is clinically obtained CTA volumetric data that is segmented to create 3D cerebrovascular models. However, from a retrospective study of 50 patients we conducted in a previous work [7], this type of imaging is not generally used in the pediatric MMD patient population as part of standard clinical follow-up practice because of radiation exposure concerns. Instead, 3D MR TOF imaging, which is radiation-free and noninvasive, is typically employed. This imaging modality has inherent challenges that make it susceptible to insufficient image quality, which can compromise the accuracy of any 3D vascular model created from it. Complex and/or slow flow patterns are usually insufficiently resolved which can introduce inaccuracies in areas of vessel narrowing—a major clinical feature of interest in MMD. To improve the accuracy of patient-specific models derived from MR TOF data, we have developed a method to locally correct vessel geometry using 2D XA imaging data that is often collected during MMD patient evaluation.

Using the XA-based adjustment process, we can generate 3D vascular models that show improved agreement with 2D XA images, the current reference standard for evaluating neurovascular lesions [25]. In the present study, we have adopted this approach for two patients selected based on the availability of clinical data using all three of the following imaging modalities: MR TOF, XA, and CTA. The goal is to compare the XA-adjusted CoW model to CTA images of the same patient. Given the rarity of such cases, only patient 1 is a pediatric MMD patient. Patient 2 is a non-MMD patient who presented with clinical symptoms of right sided stroke

Fig. 7 Comparison of NRMDS values for each vessel before (blue bars) and after XA-based adjustment (green bars) for **A** patient 1 and **B** patient 2 (color figure online).



and whose imaging revealed evidence of a focal high-grade stenosis in the RMCA. When we compare patient-specific geometries before and after XA-based adjustment, we see significant changes in local vessel geometry including more accurate representations, relative to XA images, of vessels that exhibit MMD-related vessel narrowing as noted by the patient's history. For example, patient 1's RMCA and LACA were identified by clinicians as exhibiting narrowing and both vessels are significantly impacted by the XA-adjustment process where the average vessel diameters were reduced by 48% and 30% after adjustment in the two vessels respectively. In patient 2, one of the most impacted vessels was the LMCA which increased in local diameter by 132% where the initial model was the narrowest.

We performed hemodynamic simulations on the initial and adjusted geometries of both patients and demonstrated that the distribution and magnitudes of WSR values in the CoW can be highly sensitive to geometric variations with potential implications for clinical relevance of the results. The simulation results show that, following adjustment, the surface-averaged WSR in the full CoW models at peak systole increased by 86% in patient 1 (from 2.1× that of a

healthy control case [7] to 3.9× the control) and decreased by 40% in patient 2 (from 3.1× to 1.9× that of the control) relative to the initial models. Furthermore, in these two patients the maximum WSR in several vessels of interest at peak systole changed by more than 70% after adjustment. For patient 1, the presence of focal regions of critically high WSRs at least 120% greater than seen in the previously simulated control in 5 of 6 vessels of interest of the adjusted model may be an indicator of impending secondary stroke contralateral to the primary stroke event. However, the results from the initial model, with fewer areas of severe WSR (only one vessel with max WSR greater than 20% of the that seen in the control), might not indicate stroke risk at all, thus negatively impacting preventive intervention measures. This underscores the need for accurate patient-specific geometries in noninvasive assessment of stroke risk in pediatric cerebrovascular disease and guiding the timing of surgical intervention.

While XA-based adjustment allows us to locally correct a 3D vascular model such that it agrees with the vessel geometry depicted on XA images, we currently do not know if the adjusted model is more representative of the patient's 3D

vessel anatomy than the initial MR-segmented model. To verify that our adjustment methods improve vascular model accuracy, we use CTA imaging as an additional reference for comparison. CTA is widely used for 3D vascular model reconstruction and provides stronger signal in the vasculature, particularly in narrowed vessels, than MRI data [26, 27]. Thus, we consider the CTA volume a more accurate 3D representation of the patient's CoW compared to MR TOF and examine if the adjusted model more closely matches the CTA images than the initial MR-derived model. The agreement between model and CTA was assessed by comparing the cross-sectional areas of the vessels of the model and of the vessels depicted in the CTA volume. Cross-sectional areas were collected at several points throughout the vessel and a NRMSD was calculated for each vessel of the initial and adjusted models. The NRMSD for a vessel gives a measure of how much, on average, the local vessel size in the model deviates from what the CTA images suggest the vessel size should be. For all vessels of interest (in both patients) except for three, the NRMSD is reduced following adjustment. This indicates that overall, the adjusted models more closely match the CTA images than the initial models and is evidence that the XA-based adjustment procedure may improve accuracy of MR-derived vascular models.

While these results are promising and support the effectiveness of our proposed adjustment procedures, the verification approach used herein has limitations. For our purposes, the CTA volumetric data are considered as accurate representations of the patient-specific vascular anatomy. While CTA is commonly used to this end in computational studies, whether the CTA data provides a good “ground truth” of target geometries is unknown. Cerebrovascular lesions in pediatric patients are particularly challenging to image [25]. Factors such as insufficient slice resolution, low contrast in smaller vessels, bone artifacts, and suboptimal synchronization between the contrast injection and image acquisition may negatively impact the accuracy of the vessel representations in the CTA volume. In addition, to extract the vessel cross-sectional areas from the CTA slices, we use algorithmic lumen boundary detection guided by the input of an expert pediatric neuroradiologist. These algorithms rely on image pixel intensity which can vary from vessel to vessel within the same CTA volume and among different CTA volumes. Thus, defining a standard method for identifying the lumen boundary is challenging. Furthermore, the clinician's assessment of vessel caliber was done solely based on visual inspection where subjectivity and factors such as image brightness and contrast can impact the consistency of the results slice to slice. To minimize human error, a more comprehensive analysis should be performed utilizing inputs from multiple trained neuroradiologists.

The above challenges in assessing the accuracy of MR-derived and XA-adjusted models all originate from the need

of a known target geometry for comparison. In the future, additional verification of our XA-based adjustment method using known CoW geometries is planned. The goal is to generate multiple physical 3D printed CoW models of known geometry, collecting MR TOF and XA imaging data of the physical models while mimicking the clinical settings for patient imaging, and reconstructing XA-adjusted MR-derived vascular models from the imaging data following the procedures discussed here. These models can then be directly compared to the corresponding known geometries to determine how well the XA-based adjustment performs and whether it produces a more accurate model.

Planned future work also includes implementation of a more sophisticated scheme for ensuring optimum alignment of the 3D models to the XA imaging axis (see Sect. 2.1.2) using, for example, genetic algorithms [28] or gradient descent algorithms [29]. In addition, techniques for the direct registration of the 3D MR volume to 2D XA image to determine the model orientation prior to segmentation will also be investigated. Recent work in this widely researched area has demonstrated a radon-based approach for 2D/3D registration that eliminates the need to compute 2D projections at each candidate model orientation [30].

In this study, segmentation of MR TOF imaging data involved using manual techniques. Machine learning algorithms have recently been used to significantly automate this process. These approaches have been adopted to produce 2D segmentations of coronary arteries from XA images [31] and 3D segmentations of the coronary network from CTA images [32], significantly speeding up the image-based vascular model creation pipeline. For example, automated methods of segmenting multirow detector CTA data have been used to efficiently calculate the fractional flow reserve metric (FFR_{CT}) to noninvasively assess coronary disease severity [33, 34] in clinic. Neural network-based algorithms have also been applied to the segmentation of neurovascular aneurysms using 3D rotational XA images [35]. Of interest to our work, given our reliance on MR TOF as the most common volumetric data associated with MMD treatment, Kandil et al. [36] used automated algorithms to segment MR TOF images of MMD patients. They achieved high segmentation accuracy when compared to segmentations manually generated by experienced experts. Replacing the manual segmentation steps in our process with these automated approaches in the future could result in significant time savings and potentially improve accuracy of the initial MR-segmented model. However, in the context of pediatric MMD studies, where only MR TOF imaging is commonly available, XA-based model adjustment may still be warranted regardless of how the initial MR-segmentation is generated. Sugino et al. [18] compared the use of CTA imaging versus MR imaging for the evaluation of MMD patients. They concluded that CTA is a more reliable technique for

assessing MMD given that MR was shown to overestimate the degree of stenosis in diseased vessels. This uncertainty in the underlying MR imaging data and the previously mentioned challenges associated with MR-segmentation motivated the XA-based adjustment approach presented in this work. To our knowledge, this is the first time 2D XA and 3D MR TOF imaging are combined to improve cerebrovascular model accuracy.

In summary, patient-specific modeling of vascular networks has proven to be a valuable tool in the research of vascular pathologies. In previous work, we showed how patient-specific hemodynamic analysis of the CoW and WSR can be used to noninvasively assess stroke risk in pediatric MMD, potentially resulting in earlier diagnosis of disease progression with reduced stroke burden and improved clinical outcome. These analyses rely on geometrically authentic 3D vascular models that can be reconstructed using volumetric CTA or MR imaging data, the latter of which is the more likely imaging modality for pediatric MMD patients due to radiation exposure concerns with CTA. However, MR imaging can be suboptimal for 3D model reconstruction because of limitations such as insufficient image resolution. We developed a method where virtual angiographies of 3D MR-derived vascular models are conducted and the resulting 2D projections are compared to corresponding 2D XA images, which are commonly used to clinically assess vessel narrowing. The 3D model is then locally adjusted until its 2D projections and XA images are in agreement. Through blood flow simulations, we demonstrated that local WSR distributions in an initial MR-derived model are considerably different from the XA-adjusted model which can lead to incorrect stroke risk assessments. A comparative analysis with patients' CTA imaging data suggests that XA-based adjustment can improve vascular model accuracy and enable more accurate assessments of stroke risk, thereby potentially improving individualized treatment and monitoring of pediatric MMD patients.

Acknowledgements The authors gratefully acknowledge Texas Advanced Computing Center (TACC) for providing high-performance computing resources.

Funding This work was supported by NIH Grant R03NS110442 awarded to SH.

Declarations

Conflict of interest ZS is a stockholder in Alzeca Biosciences and a consultant for InContext.ia. All the other authors declare that they have no conflict of interest.

Ethical approval There was no direct involvement of human subjects or protected health information (PHI). All patient imaging data used in analysis and modeling were collected retrospectively from medical records and de-identified at Texas Children's Hospital. Institutional

review board (IRB) approval was obtained with a waiver of written authorization for consent.

References

1. Taylor CA, Fonte TA, Min JK (2013) Computational fluid dynamics applied to cardiac computed tomography for noninvasive quantification of fractional flow reserve: scientific basis. *J Am Coll Cardiol* 61(22):2233–2241. <https://doi.org/10.1016/j.jacc.2012.11.083>
2. Rogers C, Tseng DY, Squire JC, Edelman ER (1999) Balloon–artery interactions during stent placement. *Circ Res* 84(4):378–383. <https://doi.org/10.1161/01.RES.84.4.378>
3. Marsden AL, Feinstein JA (2015) Computational modeling and engineering in pediatric and congenital heart disease. *Curr Opin Pediatr* 27(5)
4. Hossain SS, Hossainy SFA, Bazilevs Y, Calo VM, Hughes TJR (2012) Mathematical modeling of coupled drug and drug-encapsulated nanoparticle transport in patient-specific coronary artery walls. *Comput Mech* 49(2):213–242. <https://doi.org/10.1007/s00466-011-0633-2>
5. Hossain SS, Hughes TJ, Decuzzi P (2014) Vascular deposition patterns for nanoparticles in an inflamed patient-specific arterial tree. *Biomech Model Mechanobiol* 13(3):585–597. <https://doi.org/10.1007/s10237-013-0520-1>
6. Horn JD, Maitland DJ, Hartman J, Ortega JM (2018) A computational thrombus formation model: application to an idealized two-dimensional aneurysm treated with bare metal coils. *Biomech Model Mechanobiol* 17(6):1821–1838. <https://doi.org/10.1007/s10237-018-1059-y>
7. Hossain SS, Starosolski Z, Sanders T, Johnson MJ, Wu MCH, Hsu M-C et al (2021) Image-based patient-specific flow simulations are consistent with stroke in pediatric cerebrovascular disease. *Biomech Model Mechanobiol* 20(6):2071–2084. <https://doi.org/10.1007/s10237-021-01495-9>
8. Horn JD, Johnson MJ, Starosolski Z, Meoded A, Milewicz DM, Annapragada A, et al. (2022) Patient-specific modeling could predict occurrence of pediatric stroke. *Front Physiol*. <https://doi.org/10.3389/fphys.2022.846404>
9. Nagiub M, Allarakhia I (2013) Pediatric Moyamoya disease. *Am J Case Rep* 14:134–138. <https://doi.org/10.12659/AJCR.889170>
10. Lee WJ, Jeong SK, Han KS, Lee SH, Ryu YJ, Sohn CH et al (2020) Impact of endothelial shear stress on the bilateral progression of unilateral Moyamoya disease. *Stroke* 51(3):775–783. <https://doi.org/10.1161/STROKEAHA.119.028117>
11. Casa LD, Deaton DH, Ku DN (2015) Role of high shear rate in thrombosis. *J Vasc Surg* 61(4):1068–1080. <https://doi.org/10.1016/j.jvs.2014.12.050>
12. Scott RM, Smith ER (2009) Moyamoya disease and Moyamoya syndrome. *N Engl J Med* 360(12):1226–1237. <https://doi.org/10.1056/NEJMra0804622>
13. Rashad S, Saqr KM, Fujimura M, Niizuma K, Tominaga T (2020) The hemodynamic complexities underlying transient ischemic attacks in early-stage Moyamoya disease: an exploratory CFD study. *Sci Rep* 10(1):3700. <https://doi.org/10.1038/s41598-020-60683-2>
14. Grinberg L, Cheever E, Anor T, Madsen JR, Karniadakis GE (2011) Modeling blood flow circulation in intracranial arterial networks: a comparative 3D/1D simulation study. *Ann Biomed Eng* 39(1):297–309. <https://doi.org/10.1007/s10439-010-0132-1>
15. Hossain SS, Zhang Y, Liang X, Hussain F, Ferrari M, Hughes TJ et al (2013) In silico vascular modeling for personalized

- nanoparticle delivery. *Nanomedicine (Lond)* 8(3):343–357. <https://doi.org/10.2217/nmm.12.124>
16. Lesage D, Angelini ED, Bloch I, Funka-Lea G (2009) A review of 3D vessel lumen segmentation techniques: models, features and extraction schemes. *Med Image Anal* 13(6):819–845. <https://doi.org/10.1016/j.media.2009.07.011>
 17. Urchuk SN, Plewes DB (1992) Mechanisms of flow-induced signal loss in MR angiography. *J Magn Reson Imaging* 2(4):453–462. <https://doi.org/10.1002/jmri.1880020415>
 18. Sugino T, Mikami T, Ohtaki S, Hirano T, Iihoshi S, Houkin K et al (2013) Assessment of Moyamoya disease using multidetector row computed tomography. *J Stroke Cerebrovasc Dis* 22(5):644–649. <https://doi.org/10.1016/j.jstrokecerebrovasdis.2012.01.014>
 19. Urlick BY, Sanders TJ, Hossain S, Zhang Y, Hughes TJ (2019) Review of patient-specific vascular modeling: template-based isogeometric framework and the case for CAD. *Arch Comput Methods Eng* 26:381–404
 20. Zhang Y, Bazilevs Y, Goswami S, Bajaj CL, Hughes TJR (2007) Patient-specific vascular NURBS modeling for isogeometric analysis of blood flow. *Comput Methods Appl Mech Eng* 196(29):2943–2959. <https://doi.org/10.1016/j.cma.2007.02.009>
 21. Wahlin A, Ambarki K, Birgander R, Wieben O, Johnson KM, Malm J et al (2013) Measuring pulsatile flow in cerebral arteries using 4D phase-contrast MR imaging. *AJNR Am J Neuroradiol* 34(9):1740–1745. <https://doi.org/10.3174/ajnr.A3442>
 22. Hossain SS, Zhang Y, Fu X, Brunner G, Singh J, Hughes TJ, et al. (2015) Magnetic resonance imaging-based computational modeling of blood flow and nanomedicine deposition in patients with peripheral arterial disease. *J R Soc Interface*. <https://doi.org/10.1098/rsif.2015.0001>
 23. Hsu M-C, Akkerman I, Bazilevs Y (2011) High-performance computing of wind turbine aerodynamics using isogeometric analysis. *Comput Fluids* 49(1):93–100. <https://doi.org/10.1016/j.compfluid.2011.05.002>
 24. Kelly ME, Bell-Stephens TE, Marks MP, Do HM, Steinberg GK (2006) Progression of unilateral moyamoya disease: a clinical series. *Cerebrovasc Dis* 22(2–3):109–115
 25. Latchaw RE, Alberts MJ, Lev MH, Connors JJ, Harbaugh RE, Higashida RT et al (2009) Recommendations for imaging of acute ischemic stroke. *Stroke* 40(11):3646–3678. <https://doi.org/10.1161/STROKEAHA.108.192616>
 26. Hamdan A, Asbach P, Wellnhofer E, Klein C, Gebker R, Kelle S, et al (2011) A prospective study for comparison of MR and CT imaging for detection of coronary artery stenosis. *JACC: Cardiovasc Imaging* 4(1):50–61. <https://doi.org/10.1016/j.jcmg.2010.10.007>
 27. Anzidei M, Napoli A, Zaccagna F, Di Paolo P, Saba L, Cavallo Marincola B et al (2012) Diagnostic accuracy of colour Doppler ultrasonography, CT angiography and blood-pool-enhanced MR angiography in assessing carotid stenosis: a comparative study with DSA in 170 patients. *Radiol Med (Torino)* 117(1):54–71. <https://doi.org/10.1007/s11547-011-0651-3>
 28. Tabassum M, Mathew K (2014) A genetic algorithm analysis towards optimization solutions. *Int J Digit Inform Wirel Commun (IJDIWC)* 4(1):124–142
 29. Li XL (2018) Preconditioned stochastic gradient descent. *IEEE Trans Neural Netw Learn Syst* 29(5):1454–1466. <https://doi.org/10.1109/TNNLS.2017.2672978>
 30. Frysck R, Pfeiffer T, Rose G (2021) A novel approach to 2D/3D registration of X-ray images using Grangeat's relation. *Med Image Anal* 67:101815. <https://doi.org/10.1016/j.media.2020.101815>
 31. Yang S, Kweon J, Roh J-H, Lee J-H, Kang H, Park L-J et al (2019) Deep learning segmentation of major vessels in X-ray coronary angiography. *Sci Rep* 9(1):16897. <https://doi.org/10.1038/s41598-019-53254-7>
 32. Huang W, Huang L, Lin Z, Huang S, Chi Y, Zhou J, et al. (2018) Coronary artery segmentation by deep learning neural networks on computed tomographic coronary angiographic images. In: 2018 40th annual international conference of the IEEE engineering in medicine and biology society (EMBC), pp 608–611
 33. Min JK, Taylor CA, Achenbach S, Koo BK, Leipsic J, Nørgaard BL, et al. (2015) Noninvasive fractional flow reserve derived from coronary CT angiography. *JACC: Cardiovasc Imaging* 8(10):1209–22. <https://doi.org/10.1016/j.jcmg.2015.08.006>
 34. Schaap M, Walsum Tv, Neeffjes L, Metz C, Capuano E, Bruijne Md, et al. (2011) Robust shape regression for supervised vessel segmentation and its application to coronary segmentation in CTA. *IEEE Trans Med Imaging* 30(11):1974–1986. <https://doi.org/10.1109/TMI.2011.2160556>
 35. Liu X, Feng J, Wu Z, Neo Z, Zhu C, Zhang P et al (2021) Deep neural network-based detection and segmentation of intracranial aneurysms on 3D rotational DSA. *Interv Neuroradiol* 27(5):648–657. <https://doi.org/10.1177/15910199211000956>
 36. Kandil H, Soliman A, Fraiwan L, Shalaby A, Mahmoud A, ElTanboly A, et al. (2018) A novel MRA framework based on integrated global and local analysis for accurate segmentation of the cerebral vascular system. In: 2018 IEEE 15th international symposium on biomedical imaging (ISBI 2018). pp 1365–1368

Publisher's Note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Authors and Affiliations

John D. Horn¹ · Zbigniew Starosolski^{2,3} · Michael J. Johnson⁴ · Avner Medded^{2,3} · Shaolie S. Hossain^{1,4} 

¹ Molecular Cardiology Research Laboratory, Texas Heart Institute, 6770 Bertner Avenue, Houston, TX 77030, USA

² Department of Radiology, Texas Children's Hospital, Houston, TX, USA

³ Department of Radiology, Baylor College of Medicine, Houston, TX, USA

⁴ Oden Institute for Computational Engineering and Sciences, University of Texas at Austin, Austin, TX, USA