



# The role of wetting layer and QD-layers on the performance of 1.3 $\mu\text{m}$ QD-VCSEL

Sara Alaei<sup>1</sup> · Mahmood Seifouri<sup>2</sup> · Saeed Olyaei<sup>1</sup> · Gholamreza Babaabbasi<sup>3</sup>

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## Abstract

The purpose of this paper is to investigate the effect of the thickness of the wetting layer (WL) and the number of quantum dots (QDs) on the performance of 1.3  $\mu\text{m}$  QD vertical-cavity surface-emitting lasers (QD-VCSELs) using self-consistent model based on rate equations and thermal conduction equations. QD-VCSELs' output power and modulation bandwidth rolled-over due to self-heating. Results demonstrate that at the same bias current, the maximum achievable 3-dB modulation bandwidth and output power are not achieved, and the point of maximum 3-dB modulation bandwidth occurred at lower currents. In addition, the larger wetting layer thickness and the greater number of QD layers modify the self-heating and enhance the efficiency and output characteristics of the laser where the rolled-over of the laser happens at higher bias currents. Furthermore, since wetting-layer thickness and the number of QD layers increase, the self-heating phenomenon is modified and the efficiency and output characteristics of the QD-VCSELs are improved by the output power rollover at higher bias currents.

## 1 Introduction

Vertical-cavity surface-emitting lasers (VCSELs) are receiving a lot of attention due to the applications they may have in many fields, such as optical communications, optical signal processing, and high-speed data transmission [1, 2]. It was predicted that semiconductor quantum dot (QD) lasers would offer substantial advantages over lasers of a higher dimensionality, such as quantum wells, wires, and bulks. In the case of GaAs-based VCSELs with InAs-QD structures exist many benefits such as large differential gains, thermal stability, modulation bandwidths, spectrum linewidths, and higher optical gains that result from the delta function like the discrete density of states [3, 4]. Therefore, these properties make QD-VCSELs a promising candidate for 1.3  $\mu\text{m}$  advanced photonic networks [5]. The atom-like state

density in QDs active region with 3-D confinement of carrier leads to increase in optical gain, reduction of threshold current, limited thermal carrier distribution, narrow spectral linewidth, and large modulation bandwidth [6–9]. Therefore, QD-VCSELs are expected to show high power, but reports indicate that the output power of these devices is limited [1, 10–13]. Consequently, QD-VCSEL performance does not fully meet expectations, since carrier confinement is severely affected by self-heating [14], which further deteriorates QD efficiency and output power [15].

The self-heating effect in QD VCSELs occurs principally due to the small diameter of the oxide aperture and the weak confinement of holes in the QD layer [16, 17]. It was determined that poor hole confinement is one of the factors limiting the output power of QD-VCSELs [18]. According to the evidence, the weak confinement of holes in InAs/GaAs QDs is likely due to thin wetting layer (WL) and close energy spacings between the holes. However, small aperture devices have a high differential resistance and a high current density, causing severe self-heating [15]. A variety of methods have been reported [6] for improving the performance of QD VCSELs [4]. These include modifying the size and location of the oxide aperture, the number of QD layers ( $N_L$ ) [19], the doping concentration, and the size of the active area [15]. To improve the self-heating effect, one method is to increase the oxide aperture size [20]. Although, larger oxide apertures

✉ Saeed Olyaei  
s\_olyaei@sru.ac.ir

<sup>1</sup> Nano-Photonics and Optoelectronics Research Laboratory (NOR Lab), Shahid Rajaei Teacher Training University, Tehran, Iran

<sup>2</sup> Faculty of Electrical Engineering, Shahid Rajaei Teacher Training University, Tehran, Iran

<sup>3</sup> Faculty of Electrical Engineering, Islamic Azad University, Khorramabad, Iran

result in multimode-operation and a decrease in 3 dB modulation bandwidth of the VCSEL [21].

Another reason is due to the thin WL [15] and closely spaced hole energy levels in QDs, which can generate a self-heating effect that limits the output power [1, 15]. WL shape and thickness play a crucial role in the QD-VCSEL's performance [22–25]. So, when the active layer reaches a critical thickness and the pressure-induced growing layer begins to form 3-D islands (QDs) from 2-D monolayers, the strain is partially relaxed and the elastic energy is diminished [26]. Wetting layers (WL) are the initial monolayers that form. Thus, the 2-D WL is innately found in Stranski–Krastanov grown QD structures [27–30]. Therefore, the thin wetting layer can limit the power output in QD-VCSEL due to poor cavity confinement [15, 18]. Stranski–Krastanov (S-K) is a method for constructing In(Ga)As self-assembled QDs that has received considerable attention [31, 32]. In this method, there is an approximate 7% mismatch between InGaAs and GaAs [31, 33]. In actuality, the thickness of the WL ( $L_w$ ) depends both on materials and fabrication methods [34, 35]. As a result, self-assembled QDs have a similar size, high density, and high emission efficiency [36]. In other words, self-heating severely affects the output power performance of QD VCSELs, and therefore, further investigation is needed to better understand this issue. All QD-VCSEL structural parameters have been evaluated.

To analyze the effect of self-heating on the power output of QD VCSELs, in this paper, we examine the effects of both parameters, namely the  $L_w$  and ( $N_L$ ), on the performance of the 1.3  $\mu\text{m}$  wavelength. In this work, the main idea is to alter the thickness of WL and number of QD layers to reduce the effect of self-heating on the QD-VCSEL, in turn improving its performance both static and dynamic. To investigate the effect of self-heating, we apply

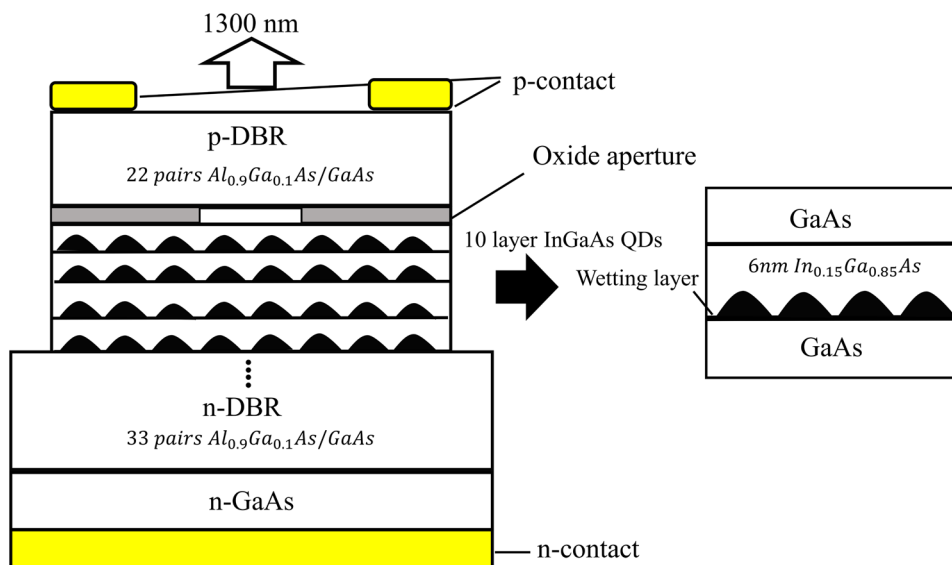
a self-consistent model based on rate equations (REs) and thermal conduction equations. By varying the number of QD layers and modifying the  $L_w$ , we can calculate the temperature increase of the active region due to the effect of self-heating as well as output power and modulation bandwidth.

## 2 Theoretical model

Figure 1 shows schematic cross-section diagram of QD-VCSEL emitting at 1.3  $\mu\text{m}$ . Self-assembled In(Ga)As QDs are grown on GaAs substrate using a GaAs buffer layer, as illustrated in Fig. 1. The QDs are placed between the top and bottom distributed Bragg reflectors (DBRs). The DBRs consist of 33 pairs of n-doped and 22 pairs of p-doped for the bottom and the top layer, respectively. DBRs can be formed by growing  $\text{Al}_{0.9}\text{Ga}_{0.1}\text{As}$  on GaAs substrate. Stranski–Krastanov growth method consists of self-assembled InGaAs QDs grown on GaAs and covered with an  $\text{In}_{0.15}\text{Ga}_{0.85}\text{As}$  layer of 6 nm thickness [15, 34, 37]. A GaAs layer is used to separate the QD layers. Moreover, QDs are assumed to consist of three distinct states, where the energy gap between InGaAs and GaAs is calculated using the formula in [38].

In the next section, the injection processes are discussed in greater detail. At first, when current is injected into the active area of the QD-VCSEL, the carriers are transported from the cladding layer to the WL. Afterward, the carriers are captured by the QDs and relaxed by intra-band relaxation to the ground state. On the basis of these processes, the Appendix A contains the rate equations.

Fig. 1 Schematic cross-sectional diagram of 1.3  $\mu\text{m}$  QD-VCSEL



### 2.1 Thermionic emission in the wetting layer

The following equation represents the carrier transport time from the cladding layer to the WL [39]:

$$t_r = \frac{L_s^2}{2D_{n,p}} \tag{1}$$

where  $L_s$  indicates the distance between the doped cladding layer and WL.  $D_n$  and  $D_p$  are the diffusion coefficient of electrons and holes, respectively, which can be calculated from the Einstein relation in [21].  $t_{bw}$  indicates the total transport time from the cladding layer to the WL and is equal to  $t_r + t_c$ , and  $t_c$  represents the carrier capture time of the WL. In our calculation,  $t_c$  is chosen as 0.3 ps [21]. In general, the carrier thermionic emission time in the WL is expressed as follows [40]:

$$L_w \left( \frac{2\pi m^*}{k_B T} \right)^{1/2} \exp\left( \frac{E_{bw}}{k_B T} \right), \tag{2}$$

where,  $E_{bw}$ ,  $m^*$ , and  $L_w$  are the effective energy barrier, effective mass of electrons, and the thickness of QW, respectively.  $T$  and  $k_B$  represent temperature and Boltzmann’s constant, respectively.

### 2.2 Carriers relaxation and escape in QDs

The capture, relaxation, and escape of carriers in QDs is governed by phonon-assisted carrier relaxation and Auger-assisted relaxation. Carrier capture is dominated by phonon-assisted relaxation, and fast intra-band relaxation of QDs is dominated by Auger-assisted relaxation [41, 42]. In addition, the complete model describes that all possible relaxation pathways. In contrast, the similar reverse pathways in the valence band corresponding to the hole relaxation [43]. Since the concentration of carriers within the wetting layer state strongly influences Auger recombination, the following formula is used to calculate the rate of carrier relaxation [41, 42]:

$$R_{ij} = A_{ij} + C_{ij} N_w \tag{3}$$

where the subscripts  $i, j = 0, 1, 2, w$  represent the ground state, first excited state, second excited state, and the lowest state in the WL, respectively.  $C_{ij}$ ,  $A_{ij}$ , and  $N_w$  illustrate the Auger-assisted relaxation coefficient between  $i_{th}$  and  $j_{th}$  level, the phonon-assisted relaxation rate, and carrier density in the WL(CL). The values of  $A_{ij}$ ,  $C_{ij}$ , and  $N_w$  can be calculated in [21]. Consequently, the rates of carrier escape can be obtained in the condition, which the system has reached a quasi-Fermi equilibrium. Under the condition of equilibrium, the rate of escape carrier have an exponential

relationship with the relaxation rates [44]. Therefore, the intra-band escape rate is calculated as follows [21]:

$$E_{sij}(i < j) = \frac{p_i}{p_j} \exp\left( -\frac{E_{ij}}{K_B T} \right) R_{ij} \tag{4}$$

The rate of escape carrier from  $i^{th}$  QD levels to WL (CL) is determined as:

$$E_{siw} = \frac{g_w}{2p_i \rho} \exp\left( -\frac{E_{iw}}{K_B T} \right) R_{wj}, \tag{5}$$

where,  $p_i$  and  $\rho$  are the degeneracy of the energy in the QD levels and the surface density of QDs, respectively.  $E_{i,j}$  is the energy separation between different QD energy levels, and  $E_{iw}$  is the energy difference between WL state and QD levels. The values of  $E_{i,j}$  and  $E_{iw}$  have been extracted from [45].  $R_{wi}$  is the relaxation rate from the WL(CL) to the QD levels.

The rate equations are established in

**Appendix A.** The parameters of the rate equations are presented in Table 1 in **Appendix A**. Due to the length of the cavity and the single longitudinal mode, only the central mode will be examined, and the other longitudinal modes will not be considered [15, 40]. Hence, in QD-VCSEL at 1.3 μm, the photon number  $S$  can be expressed as [15]:

$$\frac{ds}{dt} = \frac{v_g g_{max} (f_{0e} + f_{0h} - 1) S}{1 + \epsilon S} - \frac{S}{t_p} \tag{6}$$

where  $v_g$  and  $t_p$  denote the group velocity, the lifetime of output photon, respectively. The cavity photon lifetime is  $(v_g \times g_{th})^{-1}$ , where  $g_{th}$  (threshold gain) can be obtained through  $g_{th} = a_i + a_m$ ,  $a_i$  is the intrinsic losses and the mirror losses is  $a_m = \left( \frac{1}{2L_{cav}} \right) \ln\left( \frac{1}{R_t R_b} \right)$  in which  $L_{cav}$  is the cavity length and  $R_t$  and  $R_b$  are the of the top and bottom reflectivity Bragg mirrors, respectively.  $(f_{0e} + f_{0h} - 1)$  indicates the degree of population inversion.  $\epsilon = \frac{\epsilon_m}{\Gamma v_a}$ , where  $\Gamma$  and  $v_a$  are the optical confinement factor and the volume of all QDs.  $\epsilon_m$  is the coefficient of nonlinear gain which can be extracted from [46].  $g_{max}$  in Eq. (6) is the maximum model gain, which can be expressed as [3, 47]:

$$g_{max} = \frac{\hbar q}{c n_r m_0 \epsilon_0} \frac{|P_{cv}|^2}{m_0 E_L} \frac{\rho \Gamma_r}{d_D} \sqrt{2\pi} \left( \frac{2.35}{F_{in}} \right) \tag{7}$$

where  $|P_{cv}|^2$  is the transition matrix, which can be expressed in [3] and  $d_D$  and  $F_{in}$  represent the effective thickness of QD layer and the full-width at half-maximum (FWHM) of the inhomogenous broadening of QDs, respectively, where FWHM is dependent on  $\tau_p$  [16, 48]. Accordingly, the QD-VCSEL operates in a single mode (coherently) with an

**Table 1** Parameter used in the equations

Symbol	Meaning	Value
$f_i (i = B.w.0.1.2)$	Carrier occupation probability in the barrier, WL (CL), QD ground state, first excited state and second excited state, respectively	
$N_B$	Carrier concentration in the barrier layer	
$J$	Injected current density	
$q$	Electronic charge	$1.60 \times 10^{-19} \text{C}$
$b$	Total thickness of GaAs	191 nm
$n$	Number of QD layers	
$K_B$	Boltzmann's constant	$1.38 \times 10^{-5} \text{J/K}$
$T$	Temperature at the center of active region	
$p_i (i = 0.1.2)$	Degeneracy of QD levels	$p_0 = 1, p_1 = 2, p_2 = 4$
$S_a$	Area of active region	$78.53 \mu\text{m}^2$
$E_L$	Lasing energy	0.957 eV
$S$	Photon number in cavity	
$F_{in}$	FWHM of QD inhomogeneous broadening	24 meV
$F_{ho}$	FWHM of QD homogeneous broadening	15 meV
$g_w$	Parameter describing the carrier concentration in the WL (CL)	[21]
$t_{bw}$	Carrier transport time from cladding layer to the nearest WL (CL), which is a function of temperature	[21]
$t_c$	Carrier capture time	0.3 ps
$t_{ewb}$	Carrier escape time from WL (CL) to the GaAs barrier, which is a function of temperature	[21]
$g_{max}$	Maximum modal gain of QD laser	
$n_r$	Refractive index of active material	3.409
$m_0$	Rest mass of electron	$9.1 \times 10^{-31} \text{Kg}$
$h$	Planck's constant	$6.62 \times 10^{-34} \text{Js}$
$v_D$	Volume of one QD	$1.6 \times 10^{-24} \text{m}^3$
$t_p$	Photon lifetime	

FWHM of 24 meV and a sidemode suppression ratio of 28 dB [13].

### 2.3 Thermal conduction equation

In semiconductor lasers, many parameters are affected by temperature, so the thermal analysis is very complicated. One of the dominant heat sources in QD-VCSELs is the active region, where heat is generated by non-radiative recombination and spontaneous emission [49]. Therefore, the steady-state thermal density at the active region is expressed as [50, 51]:

$$Q_a(j) = \frac{V(T)(1 - \eta_{sp}f_{sp})}{nd_D} \{J_{th}(T) + [J - J_{th}(T)](1 - \eta_{QD})\} \quad (8)$$

where,  $\eta_{sp}$  and  $f_{sp}$  are the spontaneous quantum efficiency and spontaneous radiation escape factor [50].  $\eta_{QD}$  is the internal quantum efficiency of the device that can be obtained from [15].  $V(T)$  is the voltage at the center of the

active area, which can be calculated from the following equation [51]:

$$V(T) = \frac{2k_B T}{q} \left( \ln \frac{J}{J_s} + \frac{r_0}{r_{01}} \right) \quad (9)$$

where,  $J_s$  is the reversed saturation current density.  $r_0$  and  $r_{01}$  are the radius of the oxide aperture and the device radius, respectively.

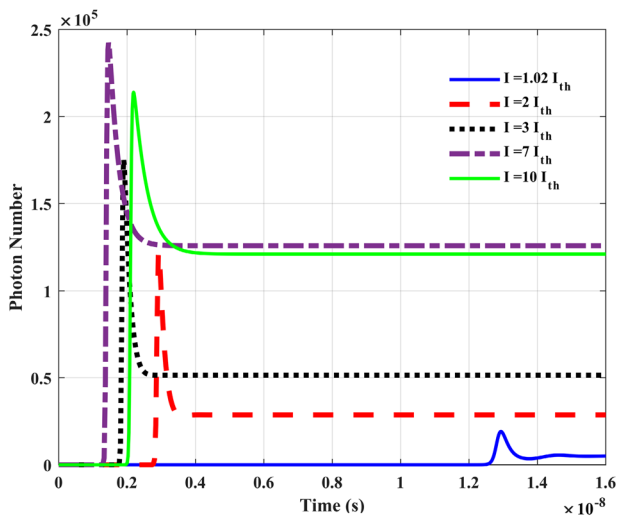
We assume that no heat escapes through the sides, the edge, or the top of the device. The temperature change with time ( $t$ ) in the device can be governed by three-dimensional dynamic thermal equation [52]:

$$(r.t) = \frac{1}{r} \frac{\partial}{\partial r} \left[ r \frac{\partial T(r.t)}{\partial r} \right] + \frac{1}{\lambda_i} Q(J.r.t), \quad (10)$$

where,  $k_i$ ,  $\lambda_i$ , and  $r$  represent the thermal diffusion coefficient, effective thermal conductivity, and radius, respectively. Equation (10) can be solved using Green's function [15, 52].

**Table 2** Physical properties of the structure

Symbol	Meaning	Value
$S_p$	Area of p-contact region	$3.77 \times 10^{-5} \text{cm}^2$
$S_n$	Area of n-contact region	$2.5 \times 10^{-3} \text{cm}^2$
$\rho_p$	Resistivity of p-doped DBR	$0.23 \text{ }\Omega\text{cm}$
$\rho_n$	Resistivity of n-doped DBR	$0.032 \text{ }\Omega\text{cm}$
$r_0$	Radius of oxide aperture	$6 \text{ }\mu\text{m}$
$r_{01}$	Radius of device	$40 \text{ }\mu\text{m}$
$f_{sp}$	Spontaneous radiation escape factor	$10 \text{ nm}$
$\eta_{sp}$	Spontaneous quantum efficiency	$0.667$
$\eta_{QD}$	Internal quantum efficiency of PhC-VCSEL	$0.5$
$k_i$	Thermal diffusion coefficient	
	GaAs	$0.267 \text{ cm}^2\text{s}^{-1}$
$\lambda_i$	Thermal conduction coefficient	
	GaAs	$44 \text{ WmK}$
$J_s$	Reverse saturation current density	$6 \times 10^{-5} \text{ Am}^{-2}$



**Fig. 2** The output photon number at different injection current values

Joule heating in the DBR stacks is another source of heat in QD-VCSELs, which leads to severe self-heating. The Joule heat density can be calculated according to [51]. The values of the used parameters are listed in Table 2 in Appendix A.

### 3 Results and discussion

In this section, the effects of parameters such as  $L_w$  and  $N_L$  on output power, the probability of carrier occupation, and the 3-dB modulation bandwidth are examined in more detail.

The number of output photons at different currents can be determined by simultaneously solving the rate equation and the thermal conduction equation for QD-VCSELs. As illustrated in Fig. 2, the number of output photons varies with different currents. The value of threshold current  $0.7 \text{ mA}$  was acquired at the  $N_L$  of 10, and the surface density of  $5 \times 10^{14} \text{ m}^{-2}$  at 300 K. Because the number of carriers is small at currents near the threshold, the turn-on delay is high. As should be emphasized, the reducing turn-on delay of QD-VCSELs is not permanent with increasing current. Threshold current increases with increasing injection current and temperature since the threshold current is strongly influenced by temperature. Therefore, increasing the threshold current leads to a delay in reaching the steady state and consequently causes a turn-on delay. According to Fig. 2, when the current becomes higher, the temperature rises and QD-VCSELs operate slower, which is because of the effect of self-heating and output power roll-over.

According to previous studies [15], it has been found that the confinement of holes depends on the thickness of the wetting layer, and therefore the thermionic emission time depends on the wetting layer thickness. Increasing the  $L_w$  leads to an increase in the number of holes in this layer as well as an increase in thermionic emission time.

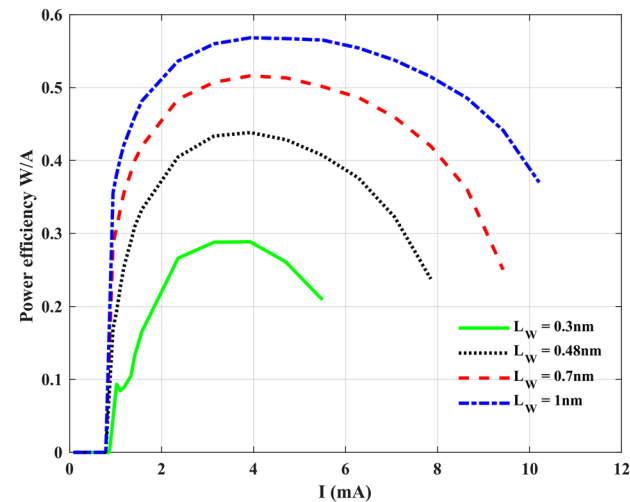
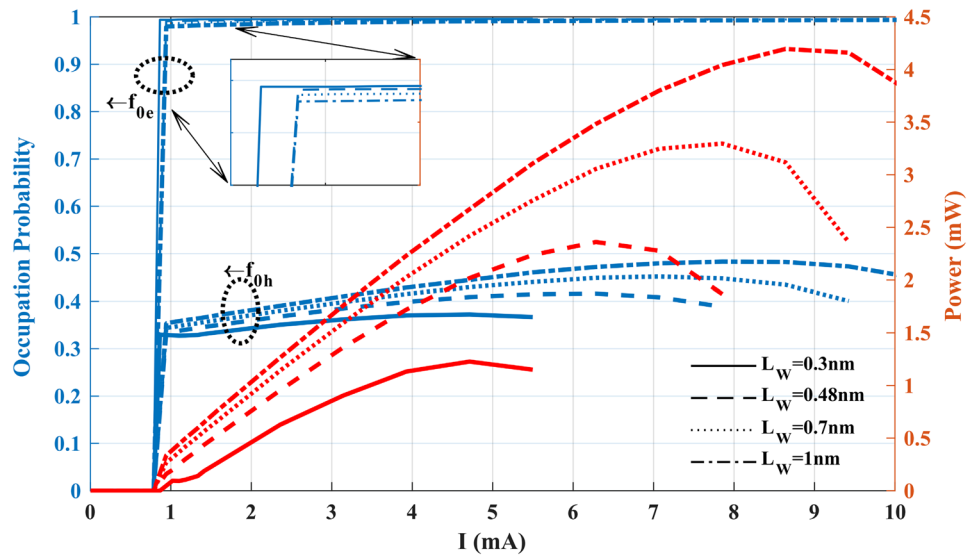
Figure 3 shows the characteristics of output power and the probability of electron and hole occupation at the ground state of QD-VCSELs as a function of current for varying  $L_w$ . According to our studies of the effect of  $L_w$  on the static behavior of the QD-VCSEL, increasing the wetting layer thickness delays the roll-over of output power at higher currents and output powers. Moreover, Fig. 3 illustrates how increasing the wetting layer thickness enhances the probability of holes occupation, and this causes power roll-over to occur over a broad range of currents, which results in improved output power.

Figure 4 shows the power efficiency as the function of the injection current for the different values of  $L_w$  with  $N_L=10$  at room temperature. The behavior of power efficiency for a different value of  $L_w$  is very similar to that of power roll-over, while in the maximum value of  $L_w$ , power efficiency increases. Consequently, the VCSEL with  $L_w=1 \text{ nm}$  has the highest power efficiency.

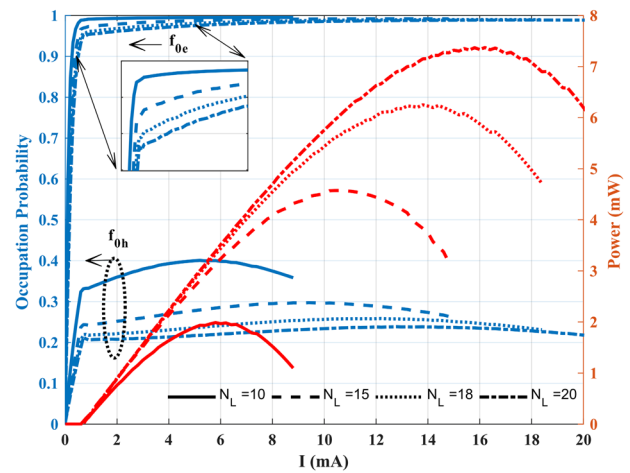
The effect of injection current on the temperature increase at the center of the active region is shown in Fig. 5. It can also be observed that, an increase in the  $L_w$  leads to increase thermionic emission in the wetting layer as well as greater confinement of holes. As a consequence, the temperature due to self-heating increases at a slower rate, which improves the effect of self-heating in the active area.

To examine the effect of the number of QD layers on the operation of the 1.3 μm QD-VCSEL,  $N_L$  is chosen to be 10, 15, 18, and 20 respectively. As shown in Fig. 6, the electron and hole occupation probabilities in the ground

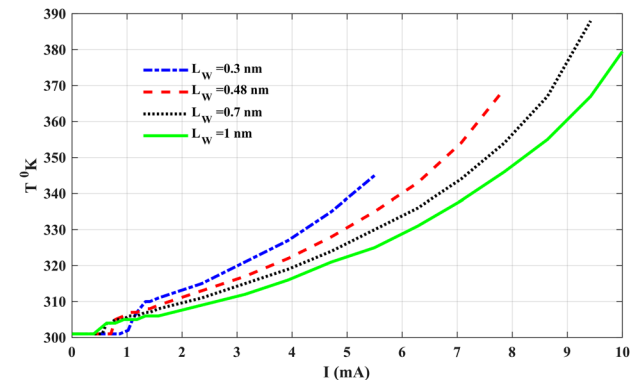
**Fig. 3** Effect of the  $L_w$  on the output power and occupation probability



**Fig. 4** The Power efficiency versus the current for a different values of  $L_w$  with  $N_L=10$  at the room temperature

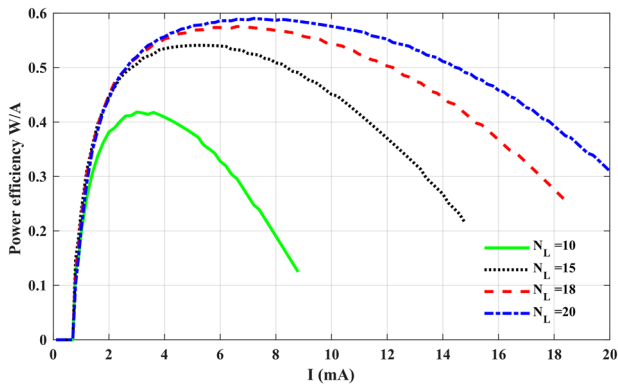


**Fig. 6** Effect of the  $N_L$  on the output power and occupation probability

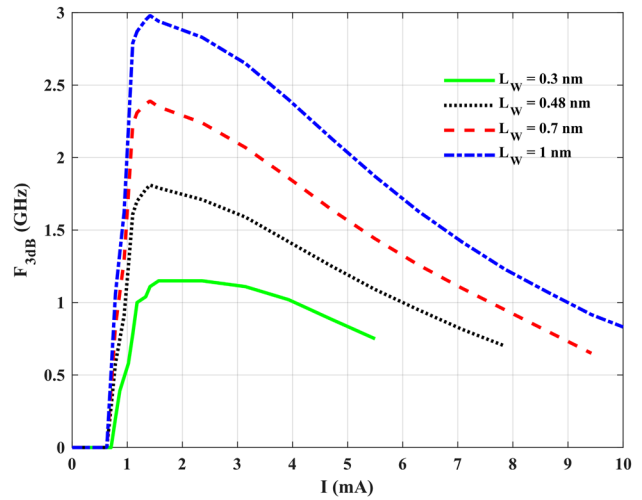


**Fig. 5** Effect of the  $L_w$  on the temperature increase of the 1.3  $\mu\text{m}$  VCSEL active region for different injection currents

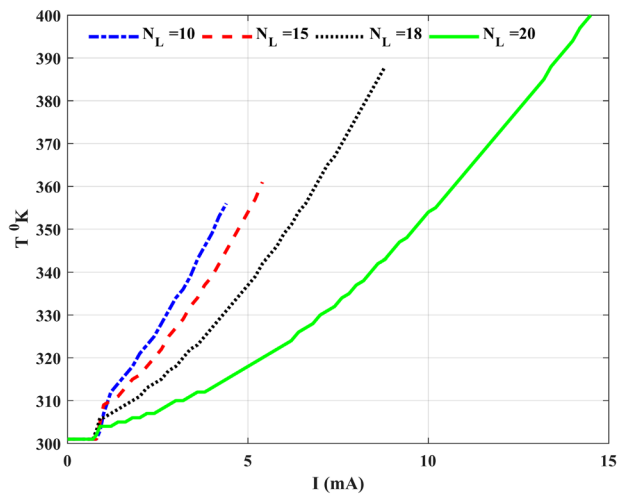
state, as well as output power are plotted as a function of the injected current for 1.3  $\mu\text{m}$  QD-VCSEL ( $F_0$ - $I$ - $P_{out}$ ). Here, we investigate the effect of  $N_L$  on self-heating. Therefore, output power ( $P_{out}$ ) could be calculated at different current, as shown in Fig. 6. According to the simulation, increasing the  $N_L$  in results to delaying the output power roll-over in the higher injection current, which is due to the improved self-heating effect. Due to the self-heating effect, there is also the roll-over of occupation probability in addition to the output power roll-over. Also, this figure illustrates the importance of the self-heating effect on carrier occupation probabilities in QD ground states. According to this figure, as the  $N_L$  increases, the occupation probability of holes decreases. Therefore, self-heating results in an increase in temperature in the active region, which leads to more carriers escaping,



**Fig. 7** The Power efficiency versus the current for a different values of  $N_L$  with  $L_w=0.48$  nm at the room temperature



**Fig. 9** Effect of  $L_w$  on the 3-dB modulation bandwidth of VCSELs at 1.3 μm as a function of the bias current



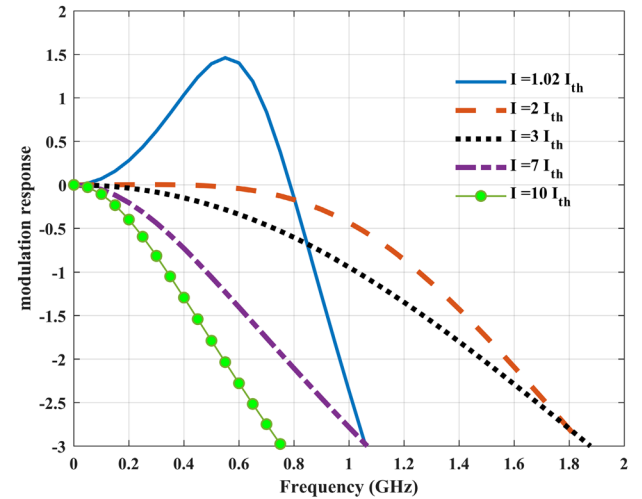
**Fig. 8** Effect of the  $N_L$  on the temperature increase of the 1.3 μm VCSEL active region for different injection currents

especially holes. From Fig. 6, it is evident that the effect of self-heating is greater on the occupation probability of holes than electrons.

In Fig. 7 power efficiency is shown as a function of injection current for different values of  $N_L$  with  $L_w=0.48$  nm at room temperature. In varying values of  $N_L$ , power efficiency behaves very similar to power rollover, and power efficiency increases at the maximum value of  $N_L$ . Consequently, the VCSEL with  $N_L=20$  has the highest power efficiency.

Figure 8 shows the calculation of the temperature of the active region as a function of the injection current for different numbers of QD layers. It is evident that increasing the  $N_L$  can significantly improve the effect of self-heating. The results show that when the  $N_L$  reach 20 layers, the self-heating effect occurs at a slower rate.

The modulation response of QD-VCSELs as a function of current considering the effect of self-heating at different  $L_w$

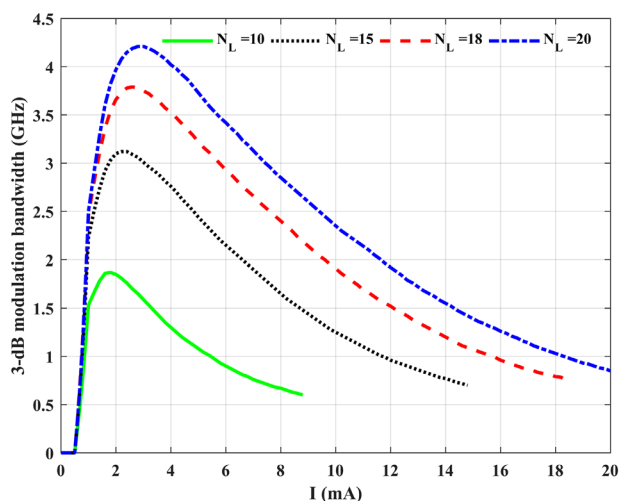


**Fig. 10** The modulation response at different injection current

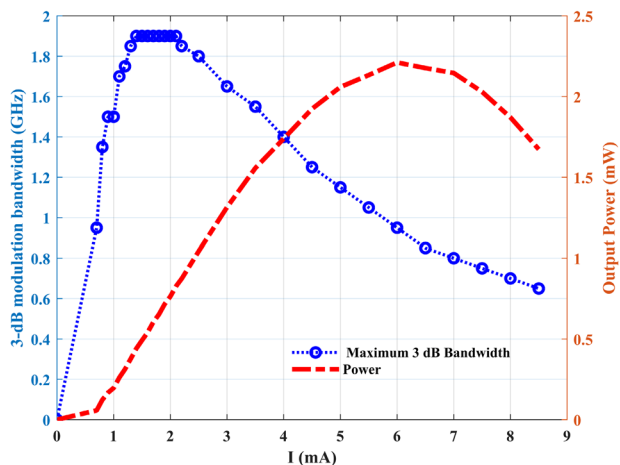
is depicted in Fig. 9. It is evident from Fig. 9 that increasing the  $L_w$  increases the maximum modulation bandwidth. As an example, when the current is between 1 and 2 mA and  $L_w = 1$  nm, the best frequency response occurs, which results in more power in the highest modulation response.

The modulation response of a QD-VCSEL is shown in Fig. 10 at various bias currents. It can be concluded that the maximum 3-dB bandwidth is obtained at bias currents about  $3I_{th}$ . Any further increase in bias current will lead to a deterioration of the 3-dB bandwidth of the QD-VCSEL.

Figure 11 shows the 3-dB modulation bandwidth of the QD-VCSEL as a function of the injection current with different QD layers. It is obvious that the maximum bandwidth



**Fig. 11** Effect of the  $N_L$  on the 3-dB modulation bandwidth of VCSELs at  $1.3 \mu\text{m}$  as a function of the bias current



**Fig. 12** The 3-dB modulation bandwidth and output power of the QD-VCSEL as a function of bias current

increases when the  $N_L$  increases. Consequently, the best modulation bandwidth occurs when  $N_L > 20$  and the injection current is between 2 and 4 mA.

To investigate the performance of the  $1.3 \mu\text{m}$  QD-VCSEL, we have calculated the maximum modulation bandwidth and output power as a function of the bias current for  $N_L = 10$  and  $L_w = 0.48 \text{ nm}$ . According to Fig. 12, as the injection current increases, the 3-dB modulation bandwidth also

increases and reaches its maximum value at  $\sim 3I_{th}$ . A further increase in bias current results in the reduction of 3-dB modulation bandwidth. However, the maximum output power can be achieved at higher bias currents (about  $6I_{th}$ ). Therefore, maximum power and modulation bandwidth cannot both be achieved simultaneously. This behavior can be attributed to the effect of QD-VCSELs self-heating, which drastically increases the escape rate of carriers especially the holes. Consequently, it can be seen that the threshold current increases sharply, which has a negative impact on the dynamic and static properties of QD-VCSELs. For example, at the highest output power, the 3-dB modulation response is as low as 1 GHz, and the maximum bandwidth corresponds to 0.6 mW output power, which limits the performance of the laser.

### 4 Conclusion

Due to self-heating and temperature increase, QD-VCSELs' output power and modulation bandwidth decrease. At the same bias current, the maximum achievable 3-dB modulation bandwidth and output power are not achieved, and the point of maximum 3-dB modulation bandwidth occurred at lower currents. As a result, the laser performance can be improved by a self-heating rein. Increasing the thickness of the wetting layer and the number of QD layers in the active region contribute to the enhancement of the self-heating of the laser, which allows the rollover to occur at higher bias currents. As the wetting layer thickness increases, the maximum output power increases from about 1.4 mW to 4.2 mW, while the maximum modulation bandwidth increases from about 1.2 GHz to 3 GHz. Furthermore, it resulted in improved laser characteristics due to a greater number of QD layers. An output power up to 7 mW and modulation bandwidth up to 3 GHz in 20 QD-layer structures can be achieved.

### Appendix A: rate equations

Here, the rate equations for the  $1.3 \mu\text{m}$  QD-VCSELs are listed [15, 21]. The parameters of the rate equations are demonstrated in Table 1.

$$\frac{dN_B}{dt} = \frac{J}{qb} + \frac{1}{t_{ewb}} \frac{g_w f_w}{\frac{b}{n}} (1 - f_B) - \left( \frac{1}{t_{bw}} + \frac{1}{t_{rB}} \right) N_B \quad (A1)$$



$$\frac{df_w}{dt} = \frac{(1-f_w) N_B b/n}{g_w t_{bw}} - \frac{f_w}{t_{ebw}} + \sum_{i=0}^{n_2} \left[ \frac{2P_i \rho}{g_w} E_{s_{iw}} f_i (1-f_w) - R_{wi} f_w (1-f_i) \right] - \frac{f_w}{t_{rw}} \tag{A2}$$

$$\frac{df_2}{dt} = \frac{g_w}{2p_2 \rho} R_{w2} f_w (1-f_2) - R_{s_{2w}} f_2 (1-f_w) + \sum_{i=0}^1 \left[ \frac{P_i}{p_2} E_{s_{i2}} f_i (1-f_2) - R_{2i} f_2 (1-f_i) \right] - \frac{f_2}{t_{r2}} \tag{A3}$$

$$\frac{df_1}{dt} = \frac{g_w}{2p_1 \rho} R_{w1} f_w (1-f_1) - E_{s_{1w}} f_1 (1-f_w) + \left[ \frac{p_2}{p_1} R_{21} f_2 (1-f_1) - E_{s_{12}} f_1 (1-f_2) \right] + \left[ \frac{p_0}{p_1} E_{s_{01}} f_0 (1-f_1) - R_{10} f_1 (1-f_0) \right] - \frac{f_1}{t_{r1}} \tag{A4}$$

$$\frac{df_0}{dt} = \sum_{i=1}^{2n} \left[ \frac{P_i}{p_0} R_{i0} f_i (1-f_0) - E_{s_{0i}} f_0 (1-f_i) \right] + \left[ \frac{g_w}{2p_0 \rho} R_{w0} f_w (1-f_0) - E_{s_{0w}} f_0 (1-f_w) \right] - \frac{f_0}{t_{r0}} - \frac{1}{2p_0 n S_a \rho} \frac{v_g g_{\max} (f_{0e} + f_{0h} - 1)}{1 + \epsilon S} \tag{A5}$$

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**Declarations**

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