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Particle size and concentration efect on thermal difusivity of water‑based ZnO nanofuid using the dual‑beam thermal lens technique

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Abstract

In the present work, we experimentally investigate the size and concentration dependence of the thermal difusivity of waterbased ZnO nanofuid. The results show an increase in thermal difusivity both by increasing the particle size from 5.6 to 16.6 nm as well as nanoparticle concentration in the range 0.02–0.1 mg/ml. It was also observed that there is a 4% enhancement in thermal difusivity of the nanofuid for an optimum value of nanoparticle size and concentration. The dependence of thermal difusivity on the particle size and concentration can give a great insight into the inter-particle interaction and the aggregation dynamics in nanofuid.

1 Introduction

Nanofuids are termed as a new class of heat transfer fuids that exhibits important thermophysical properties. It is well known that the nanoparticles of the order of 1–100 nm when suspended into the base fuids can enhance the heat transfer mechanism $[1-12]$ $[1-12]$. Nanofluids can be considered as next-generation heat transfer fuids, which have the potential to reduce the thermal resistance compared to conventional fuids as well as fuids containing micro-sized particles. Conventional liquids such as water, ethylene glycol, decene, silicon oil, and engine oil are normally used as heat transfer liquids. When micro-sized particles are suspended in such fuids, there is a chance that they settle down due to higher size and density. Since the above process introduces an additional fow resistance and erosion, micro-fuids have not yet been commercialized [[4,](#page-6-2) [10](#page-6-3), [12](#page-6-1), [13](#page-6-4)].

Nanoparticles possess larger surface area compared to conventional particles thereby signifcantly improving the stability and heat transfer capacity. Nanofuids are fnding applications in numerous felds such as microelectronics, microfluidics, medical, instrumentation, transportation, MEMS and HVAC systems [[2](#page-6-5), [5](#page-6-6), [6,](#page-6-7) [12](#page-6-1), [14\]](#page-6-8). Several possible

 \boxtimes M. Kailasnath kailas@cusat.ac.in mechanisms such as Brownian motion, fuid convection, liquid layering at the particle–fuid interface and cluster agglomeration can afect the heat transfer enhancement in nanofluids $[1, 6, 15]$ $[1, 6, 15]$ $[1, 6, 15]$ $[1, 6, 15]$ $[1, 6, 15]$ $[1, 6, 15]$.

Nanofuid is not a simple mixture of nanoparticles and base fuid. To prepare efective nanofuids, proper dispersion and stabilization of nanoparticles in the base fuid are essential. Homogenously dispersed nanofuids can be prepared using various techniques such as by (1) controlling the pH value of suspensions, (2) adding surfactants and (3) using ultrasonication. All the above techniques help to obtain stable suspensions by changing the surface properties of dispersed nanoparticles [[2,](#page-6-5) [6,](#page-6-7) [7,](#page-6-10) [13,](#page-6-4) [16\]](#page-7-0). Two techniques are most commonly used for synthesizing the nanofuids: a two-step technique and a one-step technique. In the two-step method, nanoparticles are synthesized using a physical or chemical route and the prepared powder form of nanoparticles is dispersed in the base fuid. The one-step method simultaneously synthesizes and disperses the nanoparticles into a base fuid [[2](#page-6-5), [7](#page-6-10), [8](#page-6-11), [16](#page-7-0)[–19](#page-7-1)].

Ceramics, metals, semiconductors, carbon nanotubes and composite materials are used for nanofuid preparation [[2](#page-6-5)]. Several parameters such as nanoparticle volume concentration, particle materials, size and morphology of materials, base fuid materials, temperature, and surfactants can afect the heat transfer characteristics of a nanofuid [\[5,](#page-6-6) [6,](#page-6-7) [8](#page-6-11), [20](#page-7-2), [21\]](#page-7-3). Thermal conductivity is the ability of the materials to transfer or conduct the heat, which is an important parameter responsible for heat

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transfer enhancement. Several theoretical models (Maxwell model, Hamilton–Crosser model, Yue–Choi model, Xue model, and Strauss–Pober model) have been proposed to explain the thermal conductivity in nanofluids $[2, 8, 8]$ $[2, 8, 8]$ $[2, 8, 8]$ $[2, 8, 8]$ $[2, 8, 8]$ [13](#page-6-4), [22](#page-7-4), [23](#page-7-5)]. In many existing models of thermal conductivity, experimental values are found to be deviated from theoretical values. To minimize these discrepancies to an extent, researchers measure other parameters such as viscosity and difusivity. Thermal conductivity and dynamic viscosity depend on the above-mentioned parameters that affect the heat transfer mechanism $[24, 25]$ $[24, 25]$ $[24, 25]$ $[24, 25]$ $[24, 25]$. There is no general correlation between thermal conductivity and dynamic viscosity established due to the lack of a common understanding mechanism of nanofuids.

Thermal conductivity (*k*) of nanofuid is directly related to its thermal diffusivity (*α*) by $\alpha = \frac{k}{\rho C_p}$ where ρ is the fluid density and C_p is the specific heat capacity. Hence, the measurement of thermal difusivity helps to determine the thermal conductivity. Thermal difusivity is a materialspecifc property, which describes how quickly the material reacts to the change in their thermal environment. Material with large thermal difusivity will react quickly to change in temperature than smaller thermal difusivity materials that take longer time to reach a new equilibrium condition. In most of the photonic applications, high thermal difusivity materials are required to dissipate the laserinduced heating [\[26\]](#page-7-8).

Several techniques such as transient techniques, steadystate techniques and thermal comparator have been adopted for measuring thermal conductivity of nanofuids $[20, 27-33]$ $[20, 27-33]$ $[20, 27-33]$ $[20, 27-33]$ $[20, 27-33]$. In comparison with the above methods, thermal lens techniques have many advantages. This is a very sensitive, accurate and less time-consuming technique which can be carried out at room temperature. Additional advantage of thermal lens technique includes the determination of d*n*/d*t*, which contains information about polarizability, refractive index, thermal expansion coefficient, viscosity, etc. $[34-42]$ $[34-42]$. In this technique, the nanofluid is irradiated with a laser source of appropriate frequency and a transient thermal lens signal is produced within the nanofuid. By monitoring these signals, we can estimate the thermal difusivity of nanofuid.

Zinc oxide (ZnO) is a wonderful semiconducting material with a wide range of unique properties and is used in numerous multidisciplinary felds [[43](#page-7-13)[–46\]](#page-7-14). In this paper, we discuss the synthesis of stable water-based ZnO nanofuids and its thermal difusivity measurement using thermal lens technique. To the best of our knowledge, this is the frst report on thermal lensing studies of ZnO nanoparticles dispersed in water. The thermal difusivity of nanocolloids mainly depends on size, concentration and shape of the suspended particles. Optimization of these

parameters is important to understand the heat conducting mechanism in the nanofluid. Hence, the effect of particle size and nanoparticle concentration in the solution on the thermal difusivity has been discussed.

2 Experimental

2.1 Synthesis of ZnO nanoparticles

Size-varied ZnO nanoparticles were synthesized using solution method incorporating ultrasound sonication at various temperatures. Detailed description of the synthesis method and characterization such as XRD, absorption, and TEM has been described in the previously published work [[47\]](#page-7-15). Particle size of the synthesized ZnO nanoparticles is 5.6 ± 0.61 nm, 7.5 ± 1.7 nm, 12.5 ± 1.4 nm and 16.6 ± 2.2 nm corresponding to the samples A, B, C and D [[47\]](#page-7-15). Figure [1](#page-2-0) shows the TEM images of synthesized ZnO nanoparticles.

2.2 Preparation of ZnO nanofuids

In the present work, nanofuids were prepared by a two-step method. The powder form of ZnO nanoparticles of sizes ranging from 5.6 to 16.6 nm in diferent volume fraction (0.02–0.1 mg/ml) was dispersed in water. To achieve good dispersion stability of ZnO nanoparticles in the water, ultrasonication (EQUITRON, SR.NO. 8442.030.53H.ACD:002) was employed with a frequency of 53 kHz and 100% of power factor for a period of 1 h at room temperature. Intensive ultrasonication intensively disperses the particles, reduces agglomeration and suppresses the tendency to form particle clusters. This method also helps to attain good stability for water-based ZnO nanofuids. Figure [2](#page-2-1) shows the flow chart for the preparation of ZnO nanofluids.

2.3 Theoretical background of thermal lens technique

The thermal lens (TL) technique is a well-known laser photothermal spectroscopy. Photothermal spectroscopy is a nondestructive technique where the information is deduced by the direct detection of change in the thermo-optical properties due to the absorption of radiation by the sample [\[40,](#page-7-16) [48](#page-7-17)[–50\]](#page-7-18). Photothermal techniques have two versions: (1) photothermal modulation spectroscopy (CW laser used for excitation) and (2) pulsed photothermal spectroscopy (pulsed laser used for excitation). In both cases, thermal waves are generated in the sample. Analysing time-dependent variation of the light intensity can gain information about thermooptical properties of the medium, such as temperature coefficient of refractive index and the thermal diffusivity.

Fig. 1 TEM image of ZnO nanoparticles [[47](#page-7-15)]

Fig. 2 Flow diagram of ZnO nanofuid preparation processes

In TL, the sample is irradiated by a laser beam of Gaussian intensity distribution (TEM $_{00}$) that generates a temperature gradient due to nonuniform heating [\[40](#page-7-16), [48\]](#page-7-17). Consequently, refractive index (*n*) of the medium is changed producing a lensing efect. In more general cases, the variation of refractive index is given by

$$
\Delta n = \left(\frac{\partial n}{\partial T}\right)_{\rm P} \Delta T + \left(\frac{\partial n}{\partial \rho}\right)_{\rm T} \Delta \rho.
$$

The thermal lensing effect is observable for a laser in milliwatt or microwatt range provided the sample is transparent [[40\]](#page-7-16). This effect can be generated using different pump or probe beam geometries. In 1965, Gordon et al. [\[38](#page-7-19)] used a single-beam geometry where generation and probing thermal lens signals were achieved using a single laser beam. Optical simplicity and ease of optical alignment are the main advantages of single-beam arrangement. The dual-beam optical confguration utilizes two laser beams. One beam that is used to excite the sample forms the thermal lens. A second laser beam probes the lens created in the sample. Usually a high-power CW/pulsed laser is used as the pump beam, while the probe beam is a relatively weaker CW laser [\[48\]](#page-7-17).

The dual-beam thermal lens instrumentation can be arranged in two confgurations, longitudinal (collinear) and transverse. In most of the cases, a collinear confguration is used. Mode-matched and mode-mismatched confgurations are also implemented in dual-beam technique. In the frst case, beam waists of both beams are made to coincide inside the sample. In the latter, the sample is placed in the beam waist of pump beam and the beam waists of the pump and probe beams are spatially separated.

In our thermal lens experimental setup as shown in Fig. [3,](#page-3-0) sample was pumped using a DPSS CW laser operating at 403 nm with maximum power 100mW. The detection of thermal lens signal was achieved by making use of a 4 mW CW He–Ne laser at 632.8 nm wavelength. Both pump and probe beams were aligned in a collinear mode-matched confguration. In collinear confguration, pump and probe beam propagate coaxially in the sample, which creates longer interaction length of the two beams providing a good sensitivity.

A mechanical chopper was used to modulate the pump beam intensity. By adjusting the chopping frequency and sample position, maximum intensity TL signal can be obtained. The chopping frequency is fxed at 3 Hz for all measurements. As the nonmodulated probe beam passes through the irradiated region, a diverging lens efect and thermal blooming occurs [\[15,](#page-6-9) [49,](#page-7-20) [51\]](#page-7-21). The change in probe beam intensity is measured using a photodetector–DSO system. Time-dependent probe-beam intensity is found to follow the expression [\[52\]](#page-8-0):

$$
I(t) = I(0) \left[1 - \frac{\theta}{1 + \frac{t_{\rm c}}{2(t - t_0)}} + \frac{\theta^2}{2\left(1 + \frac{t_{\rm c}}{2(t - t_0)}\right)^2} \right]^{-1}.
$$
 (1)

The probe beam phase shift θ is related to thermal power radiation:

$$
\theta = \frac{P_{\text{th}}\left(\frac{\text{d}n}{\text{d}T}\right)}{\lambda_{\text{L}}k},\tag{2}
$$

where λ_L is the excitation laser wavelength. Characteristic time for thermal diffusivity t_c is given by

$$
t_{\rm c} = \omega^2 \left(\frac{\rho C_{\rm p}}{4k} \right). \tag{3}
$$

The thermal diffusivity α is given by

$$
\alpha = \frac{k}{\rho C_{\rm p}}.\tag{4}
$$

Using Eq. (4) (4) (4) , Eq. (3) becomes

$$
t_{\rm c} = \frac{\omega^2}{4\alpha}.\tag{5}
$$

The parameters θ and t_c can be estimated by curve fitting the experimental data to time-dependent intensity (Eq. [1\)](#page-3-3).

Fig. 3 Dual-beam collinear thermal lens experimental set up

The uncertainty in the determination of beam radius can lead to error in the TL technique. To eliminate this uncertainty, experimental setup has been calibrated by measuring the thermal difusivity of deionised water as reported in the literature [[15](#page-6-9)]. The measured TL signal is shown in Fig. [4,](#page-4-0) where the calculated value of difusivity is 1.41×10^{-7} m²/s as compared to the diffusivity value of water 1.43×10^{-7} m²/s. The estimated and theoretical values are thus found to be comparable and all further measurements were made under same experimental conditions. Thermal difusivity of the unknown sample can be determined by the following equation:

$$
\alpha_{\text{sample}} = \alpha_{\text{water}} \frac{t_c^{\text{water}}}{t_c^{\text{sample}}}.
$$
\n(6)

3 Results and discussion

To understand particle size and concentration dependence on thermal difusivity, ZnO nanoparticles with diferent sizes were dispersed in water for concentrations ranging from

Fig. 4 Typical thermal lens signal recorded for water

0.02 to 0.1 mg/ml. The thermal difusivity of these ZnO nanocolloids was measured by ftting theoretical TL signal (Eq. [1\)](#page-3-3) to the experimentally recorded signal. The resulting thermal difusivity values are summarized in Table [1](#page-4-1). It is clear that both particle size and concentration are efectively infuencing the thermal difusivity. All the measurements are triplicated and the uncertainty was found to be in the order of 10^{-4} .

3.1 Nanoparticle size

Figure [5](#page-4-2) shows the variation of thermal difusivity value of water-based ZnO nanofuid as a function of particle size at constant concentration. From the obtained results, it is clear that thermal difusivity increases with the size of nanoparticles. While the thermal difusivity increases slightly for samples A, B and C, there is a considerable increase in the difusivity for sample D compared to other samples at all concentrations. This result indicates that there is an optimum particle size for the enhancement of thermal properties.

Phonon scattering effect and interfacial thermal contact are the main reasons for the enhancement in thermal diffusivity with particle size. When the particle size reaches

Fig. 5 Thermal difusivity of ZnO nanofuid with varying particle size

the order of phonon mean free path, the phonon scattering effect is reduced $[49, 50, 53, 54]$ $[49, 50, 53, 54]$ $[49, 50, 53, 54]$ $[49, 50, 53, 54]$ $[49, 50, 53, 54]$ $[49, 50, 53, 54]$ $[49, 50, 53, 54]$. This increases the thermal difusivity value. The interfacial thermal contact resistance between water and solid surfaces affects the thermal transporting behaviour of the fuid. Interfacial thermal resistance/ Kapitza resistance is dominant for smaller particle sizes. The poor contact between small size nanoparticles and surrounding liquid decreases the thermal conductivity [[54,](#page-8-2) [55](#page-8-3)].

3.2 Concentration

From the concentration dependence of thermal difusivity, shown in Fig. [6,](#page-5-0) it is clear that a rise in the nanoparticle concentration increases thermal difusivity. Sample D shows the largest variation in thermal difusivity compared to the other samples. It can also be noticed that at particular concentration (0.1 mg/ml), the thermal difusivity of ZnO nanofuid is higher than that of the base fuid (water).

According to the dynamical models, increase in thermal conductivity depends on various parameters such as Brownian motion assisted micro-convection, convective heat transfer, lowering of heating resistance, nanoparticle size and shape [[49](#page-7-20), [53,](#page-8-1) [56,](#page-8-4) [57](#page-8-5)]. Since the specifc heat capacity of solids is lower than that of fuids, the nanofuid possesses lower specifc heat capacity than that of the base fuid, as predicted by thermal equilibrium model [[58\]](#page-8-6). Specifc heat capacity also decreases with increase in the nanoparticle concentration. Increase in thermal conductivity and decrease in specifc heat capacity are contributing to the observed enhancement of the thermal diffusivity [[49\]](#page-7-20). Also, the increase in optical absorption with nanoparticle concentration leads to an enhancement in thermal difusivity [[53](#page-8-1), [55](#page-8-3)] .

Figure [7](#page-5-1) depicts the variation of thermal difusivity with the concentration of nanoparticles indicating the role of

Fig. 6 Thermal difusivity of ZnO nanofuid with varying concentration

Fig. 7 Thermal difusivity of ZnO nanofuid with varying concentration of sample D

nanoparticle concentration in the stability of nanofuid. For a particular concentration, the difusivity of nanofuid is higher than that of the base fuid. Above this concentration, difusivity tends to decrease. The stability of the dispersion is a primary prerequisite for the thermal nanofluid $[6, 13, 13]$ $[6, 13, 13]$ $[6, 13, 13]$ $[6, 13, 13]$ [59](#page-8-7)]. Stability of the ZnO nanofuid was determined by measuring the zeta potential (Horiba SZ-100). Table [2](#page-5-2) depicts the zeta potential values of ZnO nanoparticle of size 16.6 nm at diferent concentrations. If the zeta potential value is greater than \pm 60 mV, the nanofluid is said to have excellent stability. Nanofluid with zeta potential value near \pm 45 mV is stable and that with value near to ± 30 mV is moderately stable [[18,](#page-7-22) [33](#page-7-10), [60](#page-8-8)]. From Table [2](#page-5-2), we understand that 0.1 mg/ml is optimum concentration, in which nanofuid possesses good stability.

When the concentration is increased beyond the maximum limit, the stability of the dispersion gets distorted and there is a tendency for the formation of aggregates. The aggregated nanoparticles get precipitated out of the fuids and settle down, which cause the reduction in original

properties (heat transfer enhancement) of the nanofuid. The dispersion behaviour of nanofuids depends on various microscopic forces such as gravitational force, Brownian force, viscous force and inter-particle interaction force [[13,](#page-6-4) [59,](#page-8-7) [61\]](#page-8-9). Inter particle interaction force plays a dominant role in the dispersion behaviour of nanofuids compared to other forces. During the interaction, the attractive van der Waals force tends to aggregate the neighbouring nanoparticles. Inter-particle distance and shape of nanoparticles afects the aggregation rate. At short distances, the attractive force (van der Waals force) dominates over the repulsive force (electrostatic force). To overcome the attractive interaction, mainly two types of the dispersion mechanisms are developed to increase the repulsive inter particle interaction, namely electrostatic stabilization and steric stabilization. In electrostatic stabilization, surface charges are introduced into the colloidal solution, and an equal number of counter ions will surround the charged nanoparticles to maintain over all charge neutrality. In steric stabilization, macromolecules (long chain polymers) are attached on the surface of the nanoparticles which screen the van der Waals interaction. So the dispersion stability of nanofuid is further improved by surface modifications [\[5,](#page-6-6) [6,](#page-6-7) [61\]](#page-8-9).

Thermal conductivity (k) of sample D (0.1 mg/ml) was calculated using Eq. (4) (4) (4) . From the literature [[62](#page-8-10)], fluid density (ρ) is 0.995 g/cm³ and the specific heat capacity is C_p =4.185 J/g K. So the thermal conductivity (*k*) was found to be 0.6108 W/mK. The thermal conductivity of copper nanoparticles as reported by John et al. is 0.512 W/mK [\[62](#page-8-10)]. The present study suggests that ZnO nanoparticles can be used in potential cooling applications.

We have estimated the thermal difusivity of water-based ZnO nanoparticles without any surface treatments. Results show that at a particular size and concentration of nanoparticles, the fuid shows an enhancement in thermal difusivity than that of the base fuid. According to the literature, the morphological aspects and the surfactant treatments can further improve the thermal properties. Works along these lines are under progress in our laboratory.

4 Conclusion

The present study investigates the effect of particle size and concentration on the thermal difusivity of the water-based ZnO nanofuid. Thermal difusivity is found to increase with the particle size and the concentration. This increment is due to the phonon scattering at the interface of liquid, Kapitza resistance and optical absorption. The noticeable result is that the enhanced thermal difusivity is observable at an optimum value of concentration and particle size. This work suggests that by optimizing the dependent factors, the water-based ZnO nanofuids can be used as coolant for thermoelectric devices.

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