# Terahertz metasurfaces to demonstrate an extremely wide range of refractive indices in the 0.3-THz band

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#### Abstract

Metasurfaces suitable for the terahertz gap are alternatives to naturally occurring materials and could accelerate the development of terahertz flat optics integrated with terahertz continuous-wave sources. However, metasurfaces have yet to be commonly adopted in terahertz devices that require a number of specific material properties because of the many choices in meta-atom design. In this paper, we demonstrate that simple dimension control of a single kind of meta-atom enables the design of a wide range of refractive indices from large positive to negative values in the 0.3-THz band. Measurements by terahertz time-domain spectroscopy verify three kinds of metasurfaces with (1) an extremely high refractive index of 12.3 + j0.88 and reflectance of 5.1% at 0.31 THz, (2) a zero refractive index of -0.44 + j0.12 and reflectance of 2.6% at 0.34 THz, and (3) a negative refractive index of -5.4 + j0.32 and reflectance of 22.7% at 0.31 THz. The 0.3-THz band is a frequency band for candidates to 6G wireless communications. Our results offer an accessible material platform for terahertz flat optics such as metalenses, antennas, and phase plates. Terahertz flat optics based on our presented metasurfaces would be a welcome contribution to the development of terahertz industries, including 6G wireless communications.

Keywords Metasurface · Metamaterial · High refractive index · Zero refractive index · Negative refractive index

# 1 Introduction

Manipulating terahertz waves is a key to developing emerging terahertz industrial applications such as 6G wireless communications [1–4], imaging [5–7], and security [8]. Devices in terahertz industrial applications could contain continuous-wave (CW) sources radiating terahertz waves. Terahertz CW sources have developed rapidly to include resonant tunneling diodes (RTD) [9], quantum cascade

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lasers (QCL) [10], and Gunn diodes [11], to fulfill the commonly called terahertz gap. Terahertz waves radiated from terahertz CW sources pass through optical components to produce wavefronts including collimating [12, 13], focusing [14-16], circularly polarized waves [17], and optical vortices [18–20]. Many optical components manipulating terahertz waves are frequently made of naturally occurring materials such as cyclo-olefin polymer (COP) with a refractive index of 1.54 [21], magnesium oxide (MgO) 3.1 [22], and silicon (Si) 3.4 [23] in the terahertz waveband. However, three-dimensional bulky optical components made of naturally occurring materials are designed based on materials offering limited choices of refractive indices. Further, naturally occurring materials in the terahertz waveband commonly have the relative permeability fixed at 1.0 and are subject to high Fresnel reflections.

Metasurfaces enable the design of a wide range of refractive indices due to the simultaneous control of both relative permittivity and relative permeability. Flat optics based on metasurfaces makes it possible to replace frequently used three-dimensional bulky optical components with two-dimensional planar optical components [24–28]. The design of refractive indices, distribution, and polarization



properties of the metasurfaces enables the development of two-dimensional planar optical components such as collimating [29, 30], focusing [31–33], optical vortices [34], polarization conversion [35, 36], beam steering [37], and beam splitter [38, 39]. Our previous work in [29] has experimentally demonstrated a gradient-refractive-index collimating metalens made with our original metasurface with an extremely high refractive index and low reflectance [40]. The two-dimensional planar collimating metalens has a sharp gradient of refractive indices distributed from the center to the periphery. The collimating metalens converts terahertz waves radiated from an RTD to plane waves with high directivity. Further, a metalens is mounted on an RTD with the short focal distance of 1 mm  $(1 \lambda)$  [30]. Simulations have verified a focusing metalens [33] made with a negative refractive index [41]. Metasurfaces with high [40, 42–46]; zero [47, 48]; and negative refractive indices [41, 49-56] have been reported with different meta-atoms, frequency bands, and fabrication methods all helping to accelerate the development of terahertz flat optics [29-39]. Metasurfaces with a wide range of refractive indices consisting of rectangular meta-atoms at the same frequency would be a welcome contribution to enable an accessible platform for terahertz flat optics.

This paper aims to develop materials with on-demand optical constants to accelerate the growth of terahertz industrial applications. In this paper, we show that rectangular meta-atoms with different dimensions make it possible to design low-reflection metasurfaces with an extremely high refractive index above 10, a zero refractive index, and a negative index below 0 [57]. The material properties are produced by the control of the relative permeability as well as the permittivity. This is in contrast to the permeability of naturally occurring materials which cannot commonly be controlled in the terahertz waveband. The metasurfaces consist of cut metal wires symmetrically aligned on the front and back of a dielectric substrate. The operating frequency is the 0.3-THz band, a candidate frequency band for 6G wireless communications. Measurements by terahertz time-domain spectroscopy (THz-TDS) verify the three kinds of metasurfaces with an extremely high refractive index of 12.3 + j0.88and low reflectance of 5.1% at 0.31 THz, a zero refractive index of -0.44 + i0.12 and low reflectance of 2.6% at 0.34 THz, and a negative refractive index of -5.4 + j0.32 and low reflectance of 22.7% at 0.31 THz. These metasurfaces with a wide range of refractive indices would provide an accessible platform for terahertz flat optics. Terahertz flat optics based on the metasurfaces would offer attractive components such as high numerical aperture metalenses, high directivity antennas, and optical vortex phase plates.

## 2 Metasurfaces with an extremely wide range of refractive indices in the 0.3-THz band

Figure 1(a)-(c) illustrate metasurfaces with extremely high, zero, and negative refractive indices at 0.3-THz, respectively. Figure 1(d) shows an enlarged view of the metasurface with an extremely high refractive index. The metasurfaces consist of symmetrically aligned paired cut metal wires on the front and back of a dielectric substrate. The meta-atoms of the cut metal wires allow more design freedom than those of the square metal patches [58]. The length of the cut metal wires, the gap along the y-axis, the thickness of the dielectric substrate, the distance between the cut metal wires along the x-axis, the width of the cut metal wires, and the thickness of the cut metal wires are g, l, d, s, w, and t, respectively. The meta-atoms of the cut metal wires have the six parameters of g, l, d, s, w, and t. The meta-atoms of the square metal patches have the four parameters of l, d, s, and t. The design freedom of the cut metal wires would offer a wide range of refractive indices, maintaining low reflectance.

The double-sided cut metal wires on the front and back of a dielectric substrate control the relative permittivity  $\varepsilon_r$  and permeability  $\mu_r$  of the metasurfaces. The refractive index and relative impedance of the metasurfaces are expressed as  $n = \sqrt{\epsilon_{\rm r} \mu_{\rm r}}$  and  $Z_r = \sqrt{\mu_{\rm r}}/\epsilon_{\rm r}$ , respectively. The metasurface with an extremely high refractive index and low reflectance in Fig. 1(a) has the relative permittivity  $\varepsilon_r$  and permeability  $\mu_{\rm r}$  with high values. The metasurface with a zero refractive index and low reflectance in Fig. 1 (b) has the relative permittivity  $\varepsilon_r$  and permeability  $\mu_r$  with zero values. The metasurface with a negative refractive index and low reflectance in Fig. 1(c) has the relative permittivity  $\varepsilon_r$  and permeability  $\mu_r$  with negative values. The simultaneous control of the relative permittivity and permeability with high, zero, and negative values at the same frequency make it possible to design extremely high, zero, and negative refractive indices, respectively. The control of the relative permittivity  $\varepsilon_r$  and permeability  $\mu_r$  with similar values at the same frequency can also produce low reflection characteristics because the Fresnel reflections is reduced due to impedance matching as in circuit theory.

Tables 1, 2, and 3 give an overview of the reported high, zero, and negative refractive index metasurfaces, respectively. To the best of our knowledge, this is the only work that has demonstrated, by measurements, that simple dimensional control of a single kind of meta-atoms enables the design of a wide range of refractive indices from extremely high to negative values in the 0.3-THz band.



#### Table 1 Measured and simulated material characteristics of high refractive index metasurfaces

Year	f (THz)	Structure of	п	R (%)	T (%)	
		meta-atoms				
2011	0.522	I-shaped metal patches	24.34	-	-	[42]
2013	0.48	I-shaped metal patches	18.4	-	<10	[43]
2015	0.315	Z-shaped metal patches	14.36	>90*	<10	[44]
2017	0.309	Double-sided paired cut metal wires	6.66	1.16	91.8	[40]
2017	0.827	Double-sided window-type metal wires	6.8*	5*	42*	[45]
2021	2.97	Double-sided paired cut metal wires	5.88	1.3	35.7	[46]
2024	0.31	Double-sided paired cut metal wires	12.3	5.1	73.1	This work

#### Table 2 Measured and simulated material characteristics of zero refractive index metasurfaces

Year	f (THz)	Structure of	n	R (%)	T (%)	
		meta-atoms				
2014	0.522	Double-sided metal fishnets	-0.307*	-	-	[47]
2020	0.5	Double-sided paired cut metal wires	0.16	0.7	97.3	[48]
2024	0.34	Double-sided paired cut metal wires	-0.44	0.7	97.3	This work

Table 3 Measured and simulated material characteristics of negative refractive index metasurfaces

Year	f (THz)	Structure of	n	R (%)	T (%)	
		meta-atoms				
2008	0.458	I-shaped metal patches	-2.74	-	-	[49]
2008	1.02	Cross shaped metal patches	-1.81*	-	-	[50]
2008	2.64*	Double-sided rectangular metal patches	-11.7*	14.7*	88.3*	[52]
2008	2.22	S-shaped gold strings	-	-	-	[53]
2009	1.3	I-shaped metal patches	-1.7*	-	-	[51]
2009	0.69	Double-sided window-type metal wires	-2.8	75.8*	-	[54]
2013	0.373	Dielectric cube array	-4.37	68.3*	4.0*	[55]
2013	0.55	Double-sided metal fishnets	-15	98.8	23.1	[56]
2014	0.31	Metal fish net	-4.47	94.4*	4.68*	[47]
2018	0.42	Double-sided paired cut metal wires	-4.2	4.3	81.5	[41]
2024	0.31	Double-sided paired cut metal wires	-5.4	22.7	56.4	This work

The n, R, and T represent the refractive index, reflectance, and transmittance, respectively

\*Asterisks denote values obtained through simulations

#### 3 Design of the metasurfaces

Figure 2(a) and (b) illustrate equivalent circuits that explain the operating principle of the metasurfaces. Equivalent circuit theory approximately explains the dielectric and magnetic properties of the metasurfaces. The control of the length l and the gap g of the cut metal wires determines the dielectric and magnetic properties. The dielectric property arises from the electric field of the incident terahertz waves. The electric field of the incident terahertz waves generates currents on the cut metal wires of the front and back of the dielectric substrate in the same direction, resulting in the formation of serial resonance circuits. The resonance frequency of the dielectric property is determined by the inductance components L<sub>E</sub> of the cut metal wires and the capacitance components CE of the gaps between the cut metal wires along the y-axis. The magnetic property arises from the magnetic field of the incident terahertz waves. The magnetic field of the incident terahertz waves generates a current on the cut metal wires of the front and back of the dielectric substrate in the opposite direction, resulting in parallel resonance circuits. The resonance frequency of the magnetic property is determined by the inductance components L<sub>H</sub> of the cut metal wires and the capacitance components C<sub>H</sub> of the gaps between cut metal wires on the front and back of the dielectric substrate.

Figures 3, 4, and 5 show contour maps of the real part of the refractive indices, reflectance, transmittance relative permittivity, relative permeability, and relative impedance for the metasurfaces with extremely high, zero, and negative refractive indices, respectively. Table 4 shows the parameters



Fig. 2 Equivalent circuits of symmetrically aligned paired cut metal wires on the front and back of a dielectric substrate with (a) dielectric and (b) magnetic properties

g, l, d, s, w, and t of the fabricated metasurfaces with (a) extremely high, (b) zero, and (c) negative refractive indices, respectively. The contour maps in Figs. 3, 4, and 5 show the optical constants with varying gaps g between the cut metal wires along the y-axis from 50 to 150 µm and lengths l from 250 to 350 µm, respectively. The other parameters of distance s between the cut metal wires along the x-axis, width w of the cut metal wires along the x-axis, and the thickness t of the cut metal wires are fixed in Table 4. When the length *l* of the cut metal wire is changed, the adjacent cut metal wires are moved along the +y or -y direction. The gap g is kept constant when changing the length *l*. The black dots in Figs. 3, 4, and 5 show the parameters of the fabricated metasurfaces described in Table 4. The optical constants of the metasurfaces are derived from scattering matrices S<sub>11</sub> and S<sub>21</sub> calculated by a finite element method simulator ANSYS HFSS [59]. The dielectric substrate is cyclo-olefin polymer (COP) with low loss properties and a refractive index of 1.53 + i0.001 [60] measured in the terahertz waveband. The metal of the cut metal wires is copper with a conductivity of  $5.8 \times 10^7$  S/m. Copper can be used for metasurfaces [40, 41, 48, 57, 58] and antennas [29, 30] in the terahertz waveband. The complex conductivity of copper with the Drude model is  $5.8 \times 10^7 + 2.7 \times 10^6$  S/m [46], and the real part of the conductivity is larger than the imaginary part.

Figure 3 shows the parameters of a metasurface with an extremely high refractive index  $n_{\rm eff}$  of 12.2 + j1.5, a low reflectance of 70%, and transmittance of 65.1% for cut metal wires with  $l=313 \mu m$  and  $g=94 \mu m$ . The material property with a high refractive index of 12.2 is produced by the simultaneous control of the relative permittivity and relative permeability with high values. The relative permittivity  $\varepsilon_r$  and permeability  $\mu_r$  are 13.0-*j*1.5 and 10.8+*j*4.1, respectively, at 0.31 THz. The relative impedance  $Z_r$  is 0.91 + j0.22. Figure 4 shows the parameters of a metasurface with a nearzero refractive index  $n_{\rm eff}$  of 0.43 + j0.009, low reflectance of 2.0%, and high transmittance of 97.4% for cut metal wires with  $l=318 \ \mu m$  and  $g=60 \ \mu m$ . The material property with a near-zero refractive index of 0.43 is produced by the simultaneous control of the relative permittivity and relative permeability from 0 to 1.0. The relative permittivity and permeability are 0.87 + j0.009 and 0.21 + j0.007, respectively, at 0.31 THz. The relative impedance  $Z_r$  is 0.49 + j0.006. Figure 5 shows the parameters of a metasurface with a negative refractive index  $n_{\rm eff}$  of -4.6+j0.16, reflectance of 53.7%, and transmittance of 37.6% for cut metal wires with of  $l=307 \ \mu m$  and  $g=136 \ \mu m$ . The material property with a negative refractive index of -4.6 is produced by the simultaneous control of the relative permittivity and relative permeability below 0. The relative permittivity and permeability are -12.9 - j0.10 and -1.6 + j0.12, respectively, at 0.34 THz. The relative impedance  $Z_r$  is 0.35 - j0.01.

**Fig. 3** Contour maps for (**a**) the real part of the refractive indices  $n_{\text{eff}}$ , (**b**) reflectance, (**c**) transmittance, (**d**) the real part of the relative permittivity  $\varepsilon_{rr}$  (**e**) the real part of the relative permeability  $\mu_{rr}$  and (**f**) the relative impedance  $Z_{rr}$ Dots on the contour maps show the parameters of the fabricated metasurface with an extremely high refractive index of 12.2 + j1.5 at 0.31 THz



# 4 Fabrication and measurement of the metasurfaces

Figure 6 (a) shows a photograph of a fabricated metasurface with an extremely high refractive index. Figures 6 (b)–(d) show microscope images of fabricated meta-atoms composing the metasurfaces with extremely high, zero, and negative refractive indices, respectively. The dimensions of the metasurfaces are  $40 \times 40$  mm<sup>2</sup>. The metasurfaces with extremely high, zero, and negative refractive indices consist of 27,420, 5,349, and 5,088 pairs of double-sided cut metal wires. Cyclo-olefin polymer films coated with copper layers on the front and back are etched to fabricate the metasurfaces. The copper layers are coated without adhesive layers to reduce conductor losses in the metasurfaces.

Figure 7 (a) and (b) are photographs of the optical system for the measurements of transmittance and reflectance of the fabricated metasurfaces. Measurements by terahertz time-domain spectroscopy (THz-TDS) with TOPTICA Photonics TeraFlash verify the transmittance and reflectance of the fabricated metasurfaces and reference. The references of the transmittance and reflectance measurements are dry air and a silver mirror, respectively. The ratio of frequency characteristics of a metasurface to those of a reference in transmittance and reflectance measurements derives scattering matrices and calculates optical constants of the





metasurfaces such as refractive indices, relative permittivity, and permeability [59].

The main points of the measurement procedure are as follows. Pulsed terahertz waves are focused at the metasurfaces and silver mirror in transmittance and reflectance measurements. The calculated spot diameter and focal depth in the transmittance measurements are 3.5 and 19.6 mm, respectively. The calculated spot diameter and focal depth in the reflectance measurements are 7.1 and 78.5 mm. The optical lengths from the transmitted to the received photoconductive antennas are 419 and 698 mm in the transmittance and reflectance measurements, respectively. The fabricated metasurfaces are often deflected during the fabrication process. The deflection causes a difference in the position of the metasurfaces and the reference mirror in the reflectance measurements. The differences in optical lengths result in experimental errors. The metasurfaces have to be put in the same position as the reference mirror in the reflectance measurements to obtain accurate optical constants. The measured phases of the reflectance are compensated on the condition that the frequency characteristics of the measured phases are the same as those of the simulated phases. The compensation predicts that the metasurfaces with extremely high, zero, and negative refractive indices are concave with depths of 30, 7.5, and 45 µm along the incident terahertz waves, respectively.

Figure 8 (a)–(e), 9 (a)–(e), and 10 (a)–(e) show measurements of the material properties of the metasurfaces with an



the refractive indices  $n_{\text{eff}}$ , (b) reflectance, (c) transmittance, (d) the real part of the relative permittivity  $\varepsilon_r$ , (e) the real part of the relative permeability  $\mu_r$ , and (f) the relative impedance  $Z_r$ . Dots on the contour maps show the parameters of the fabricated metasurface with a negative refractive index of -4.6 + j0.16 at 0.31 THz

Table 4 Parameters of the designed metasurfaces with (a) an extremely high refractive index at 0.31 THz, (b) a zero refractive index at 0.34 THz, and a negative refractive index at 0.31 THz

	g (mm)	l (mm)	d (mm)	s (mm)	w (mm)	t (mm)
(a)	94	313	23	86	54	0.5
(b)	60	318	50	597	208	6
<u>(c)</u>	136	307	50	557	149	6

extremely high refractive index, a zero refractive index, and a negative refractive index, respectively. The dots and solid lines in Figs. 8, 9, and 10 show measurements and simulations, respectively. Figure 8 (a)–(c) show that measurements verify that the fabricated metasurface with an extremely high refractive index has a refractive index of 12.3 + j0.88, low reflectance of 5.1%, and high transmittance of 73.1% at 0.31

THz. The relative permittivity, permeability, and impedance are 15.5 - j1.4, 9.6 + j2.3, and 0.79 + j0.13, respectively, at 0.31 THz. Figure 9 (a)-(c) show that the measurements verify that a fabricated metasurface with a zero refractive index has a refractive index of -0.44 + i0.12, low reflectance of 2.6%, and high transmittance of 94.6% at 0.34 THz. The relative permittivity, permeability, and impedance are



Fig. 6 (a) Photographs of the fabricated metasurfaces with an extremely high refractive index. Laser microscopic image of the fabricated metasurfaces with (b) extremely high, (c) near-zero, and (d) negative refractive indices

-0.19+j0.12, -0.93-j0.05, and 1.9-j0.63, respectively, at 0.34 THz. Figure 10 (a)–(c) show that measurements verify that a fabricated metasurface with a negative refractive index has a refractive index of -5.4+j0.32, low reflectance of 22.7%, and high transmittance of 56.4% at 0.31 THz. The relative permittivity, permeability, and impedance are -9.7-j2.9, -2.6+j1.1, and 0.5-j0.18, respectively, at 0.31 THz.

# 5 Discussion of the metasurfaces

Figures 11, 12, and 13 show the measured dielectric energy loss, magnetic energy loss, and the sum of the dielectric energy and magnetic energy losses in the metasurfaces with extremely high, zero, and negative refractive indices, respectively. The energy loss in the metasurfaces is derived by the following equation

$$Q = \frac{\omega \epsilon_0 |E|^2}{2 |\mu_{\rm r}|} [|\mu_{\rm r}| \operatorname{Im} (\epsilon_{\rm r}) + |\epsilon_{\rm r}| \operatorname{Im} (\mu_{\rm r})]$$
(1)  
[61].

Here  $\omega$  is the angular frequency, E is the electric field, and  $\varepsilon_0$  is the permittivity in vacuum. The terms of the dielectric energy and magnetic energy losses are  $|\mu_r| \operatorname{Im}(\epsilon_r)$  and  $|\epsilon_r| \operatorname{Im}(\mu_r)$ , respectively. The energy is absorbed in the metasurfaces when the sum of the dielectric energy and magnetic energy losses is positive also when the dielectric energy loss or magnetic energy loss is negative. Figures 11, 12, and 13 show that the measurements are very similar to the simulations, while the sum of the dielectric energy





Fig. 7 Optical system of the (a) transmittance and (b) reflectance measurements for the fabricated metasurfaces

loss and magnetic energy loss is negative at a few frequencies. The regions highlighted with gray in Figs. 11, 12, and 13 show the frequency bands where the conservation of energy in the measurements is not satisfied due to measurement errors. The sum of the dielectric energy and magnetic energy losses calculated from the simulations are always positive from 0.25 to 0.35 THz. The simulations show that the energy is not amplified in the metasurfaces. The errors between the measurements and simulations would be caused by experimental errors.



Fig. 8 Frequency characteristics of (a) refractive index, (b) reflectance and transmittance, (c) relative permittivity, (d) relative permeability, and (e) relative impedance for metasurfaces with an extremely high refractive index

### 6 Conclusions

Metasurfaces consisting of double-sided paired cut metal wires make it possible to design a wide range of refractive indices including high, zero, and negative refractive indices. The simultaneous control of the relative permittivity and relative permeability with high, zero, and negative values at the same frequencies allow the design of extremely high, zero, and negative refractive indices. The control of the relative permittivity and permittivity with similar values reduces the Fresnel reflections. Measurements by THz-TDS verified the metasurfaces with an extremely high refractive index of 12.3 and low reflectance of 5.1%; a zero refractive index of -0.44 and low reflectance of 2.6%; and a negative index of 5.4 and reflectance of 22.7% in the 0.3-THz band. The measurements presented here show that the parameter design of the cut metal wires enables a wide range of refractive indices: extremely high, zero, and negative. The



Fig. 9 Frequency characteristics of (a) refractive index, (b) reflectance and transmittance, (c) relative permittivity, (d) relative permeability, and (e) relative impedance for metasurfaces with a near-zero refractive index

metasurfaces enabling a wide range of refractive indices consisting of meta-atoms with the same structures may be applied to material platforms for terahertz flat optics, such as collimating lenses, focusing lenses, and refractive plates. The proposed metasurfaces would be a welcome contribution in the development of terahertz industries such as 6G wireless communications.



Fig. 10 Frequency characteristics of (a) refractive index, (b) reflectance and transmittance, (c) relative permittivity, (d) relative permeability, and (e) relative impedance for metasurfaces with a negative refractive index



Fig. 11 Frequency characteristics of (a) power loss, (b) dielectric energy and magnetic energy losses, and (c) the sum of the dielectric energy and magnetic energy losses for the metasurface with an extremely high refractive index



Fig. 12 Frequency characteristics of (a) power loss, (b) dielectric energy and magnetic energy losses, and (c) the sum of the dielectric energy and magnetic energy losses for the metasurface with a near-zero refractive index



Fig. 13 Frequency characteristics of (a) power loss, (b) dielectric energy and magnetic energy losses, and (c) the sum of the dielectric energy and magnetic energy losses for the metasurface with a negative refractive index

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Data availability Data is available upon reasonable request.

#### Declarations

Conflict of interest The authors have no conflicts of interest to declare.

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