#### **ORIGINAL PAPER**



# **Preparation and focculation properties of biodegradable konjac glucomannan‑grafted poly(trimethyl allyl ammonium chloride)**

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# **Abstract**

Preparation of konjac glucomannan-grafted poly(trimethyl allyl ammonium chloride) (KGM-*g*-PTMAAC) was carried out using KGM as polysaccharide matrix and TMAAC as cationic comonomer to develop biodegradable focculants. The structure of KGM-*g*-PTMAAC was characterized by FTIR, 13C solid-state NMR, elemental analysis (EA) and SEM. Thermal properties of KGM-*g*-PTMAAC were studied by thermal gravimetric (TG) analysis. In addition, focculation properties of KGM-*g*-PTMAAC were investigated in a kaolin suspension. The results of the FTIR, NMR, and EA showed that the cationic moiety containing quaternary ammonium has been introduced in the backbone of KGM. SEM images indicated that the surface of KGM-*g*-PTMAAC was rougher than that of KGM. TG results indicated that the thermal stability of KGM-*g*-PTMAAC was diferent to that of KGM. The obtained products had a good biodegradable performance. Moreover, the results of the focculation test showed that KGM-*g*-PTMAAC could be potentially used as a good focculating agent.

**Keywords** Graft copolymerization · Konjac glucomannan · Flocculant · Biodegradable · Trimethyl allyl ammonium chloride

# **Introduction**

With the continuous advancement of industrialization, water resources problems in various countries around the world have become increasingly serious, mainly due to the scarcity and the increasing pollution situation of water resources. In particular,

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industrial sewage and domestic sewage become the main source of water pollution. Seeking low-cost and high-efficiency water pollution treatment is one of the problems that we urgently need to solve, and also an inevitable requirement for sustainable development. At present, there are various water treatment methods [\[1](#page-20-0)], such as flocculation [\[2](#page-20-1)], biochemical treatment [\[3](#page-20-2)], ion exchange [\[4](#page-20-3)], adsorption [\[5](#page-20-4)], chemical oxidation [[6\]](#page-20-5), microbial method [[7\]](#page-20-6) and so on. However, the lowest cost and most widely used treatment method is still focculation method. The focculation method is as follows: adding specifc chemical substances (i.e., focculants) to the wastewater to be treated, and under the action of chemistry, physics and physical chemistry, the fine substances in the original wastewater which are difficult to be settled and fltered are aggregated to form large focs, and settled down, and then can be simply separated from water.

The commonly used focculants can be divided into three categories: inorganic focculants, synthetic polymer focculants, and natural polymer focculants. Among them, inorganic focculants are mainly represented by aluminum salts, iron salts and magnesium salts, which are widely used for printing and dyeing wastewater treatment. However, the defect of inorganic focculants is that the dosage is high, and the residual amount in the water is high, which inevitably causes secondary pollution of water. Although synthetic polymer focculants such as polyacrylamide and polyacrylic acid have good focculating performance, their applications are limited because they are difficult to be degraded and have certain toxicity due to the use of synthetic monomers.

With the enhancement of people's awareness of environmental protection and sustainable development, focculants based on natural polymers have been attracting more attention due to the properties of pollution-free, biodegradability, low cost, non-toxicity, and abundance. Recently, a large number of natural focculants have been developed using natural polymers such as starch [[8\]](#page-20-7), cellulose [\[9](#page-20-8)], chitosan [\[10](#page-20-9)], guar gum [\[11](#page-20-10)] and so on. Moreover, cationic focculants have attracted more and more attention because the surface of pollutant particles in modern industrial and domestic drainage is usually negatively charged [\[12](#page-20-11), [13\]](#page-20-12). Therefore, a large number of cationic natural polymer flocculants have been developed [\[11](#page-20-10), [14–](#page-20-13)[16\]](#page-20-14). Relatively, there are not many researches on the cationic KGM-based focculant.

Konjac Glucomannan (KGM) is a kind of natural polysaccharide extracted from *Konjac* tuber, which is composed of p-glucose and p-mannose linked by  $\beta$ -1,4glycosidic bond in a molar ratio of about 1:1.6 [[17\]](#page-20-15). Because of its hydrophilic, edible, gelatinous and degradable properties, KGM has been widely used in food, medicine, chemical industry, agriculture, bioengineering and other felds [[18–](#page-20-16)[20\]](#page-20-17). Cationization of KGM is one of the important means of chemical medication for KGM. Lei et al. [[21\]](#page-20-18) reported the preparation and antimicrobial activity of KGM modifed with a quaternary ammonium compound. Yu et al. [[22\]](#page-20-19) used KGM to react with 3-chloro-2-hydroxypropyltrimethylammonium chloride (CHPTAC) in the presence of sodium hydroxide to prepare a quaternary ammonium derivative of KGM and studied its antimicrobial activity. Recently, Gao et al. [\[23](#page-20-20)] reported a homogenous method of synthesized cationic KGM in NaOH/urea by reacting KGM with 3-chloro-2-hydroxypropyltrimethylammonium chloride (CHPTAC). Using 2, 3-epoxypropyl trimethyl ammonium chloride (EPTMAC) as cationization reagent,

our group [[24\]](#page-20-21) recently synthesized quaternary ammonium cationic KGM by the dry method and found the obtained product was a kind of focculants. Recently, Zhang et al. [[25\]](#page-20-22) prepared a cationic polymer by grafting KGM with poly-(2-methacryloyloxyethyl)trimethyl ammonium (PDMC) and evaluated their focculation properties; however, they did not investigate the biodegradability of the products. In general, most of cationic focculants based on KGM mentioned above are realized on the etherifcation. Etherifcation may inevitably involve more or less side reactions and/ or use a lot of organic solvents. Obviously, grafting copolymerization can efectively avoid these drawbacks. Nevertheless, there are not many reports on the preparation of cationic focculants by grafting modifcation of KGM.

Although the closed vessel method for grafting copolymerization is a conventional method, it has many advantages such as relatively simple operation and no special equipment, so it is still used by many researchers [[26–](#page-20-23)[28\]](#page-21-0). In addition, according to the literature  $[26, 29]$  $[26, 29]$  $[26, 29]$  $[26, 29]$  $[26, 29]$ , if ceric (IV) ammonium nitrate is applied as an initiator in the grafting modifcation of polysaccharides, the absence of free radical initiators in the reactive medium can limit the formation of homopolymer, and at the same time, the reaction can be easily carried out at lower temperature in aqueous medium. As far as the cost and the beneft are concerned, the closed vessel method is also used to prepare the grafting copolymer of KGM.

Therefore, in this work, a novel cationic focculant of biodegradable KGM grafted poly(trimethyl allyl ammonium chloride) was prepared in aqueous solution using trimethyl allyl ammonium chloride (TMAAC) as cationic comonomer and cerium ammonium nitrate (CAN) as initiator. And focculation properties of KGM-*g*-PT-MAAC were evaluated in kaolin suspensions. Moreover, the biodegradable behavior of the resultant focculant was also investigated.

# **Materials and methods**

#### **Materials**

Konjac glucomannan (KGM), supplied by Hubei Enshi Hongye Konjac Co., Ltd., was refned with ethanol before use and dried *in vacuum* to constant weight. Trimethyl allyl ammonium chloride (TMAAC) was purchased from Jintan Southwest Chemical Research Institute. Other reagents were analytically pure without any treatment before use.

#### **Synthesis of KGM‑***g***‑TMAAC**

The synthesis process was presented in line with Scheme [1](#page-3-0) [\[21,](#page-20-18) [30\]](#page-21-2). Namely, a proper amount of deionized water (200 mL) was added to a tri-necked bottle with a constant pressure titration funnel, and a certain amount of KGM and CAN were added in the stirring state. A certain amount of TMAAC was dissolved in deionized water to form a 25% solution (4–36 mL) and then was put into a constant pressure titration funnel. The temperature of the reaction system was raised to a certain temperature under the



<span id="page-3-0"></span>**Scheme 1** Possible reaction of KGM with TMA AC

protection of nitrogen, and TMAAC solution was added after 10 min to carry out the grafting copolymerization.

Moreover, the purifcation of the products could be described as follows [\[15](#page-20-24), [31\]](#page-21-3). After the reaction was completed, the products were precipitated using an excess of anhydrous ethanol, washed with anhydrous ethanol 5 times, separated by fltration, and then extracted using ethanol/water  $(4/1, v/v)$  as solvent in a Soxhlet apparatus for 24 h to remove all unreacted monomer and homopolymer [\[30](#page-21-2), [32](#page-21-4), [33\]](#page-21-5). Afterward, the purifed products were dried *in vacuum* at 35 °C. At the end, they were crushed and weighed in turn.

The grafting yield (GY) was calculated from the following formula [\[31,](#page-21-3) [34](#page-21-6)].

$$
GY(\%) = \frac{W_1 - W_0}{W_0} \times 100
$$
 (1)

where GY,  $W_1$  and  $W_0$  represented the grafting yield of graft copolymers, the weight of obtained products (KGM-*g*-PTMAAC) and the weight of KGM, respectively.

Moreover, using initiator amount, reaction temperature, reaction time and monomer amount as experimental factors, respectively, an orthogonal experiment with four factors and three levels, i.e.,  $L9(3^4)$  matrix was carried out to clarify the interaction between the parameters. The design of orthogonal experiment is listed in Table [1](#page-4-0).

### **FTIR**

FTIR spectra of graft polymers were carried out using a KBr pellet method with Avatar 370 Fourier transform infrared spectrometer of Thermoelectric Co., LTD, USA.

<span id="page-4-0"></span>

# **13C CP/MAS NMR**

 $13$ C CP/MAS NMR experiment was performed on Bruker AVANCE III 600 spectrometer at a resonance frequency of 150.9 MHz. <sup>13</sup>C CP/MAS experiments were performed on a 4 mm probe with a contact time of 3 ms, a recycle delay of 4 s, and a sample spinning rate of 12 kHz. The chemical shifts of  $^{13}$ C were externally referenced to TMS.

# **Elemental analysis**

The elemental analysis of samples was taken by PerkinElmer 2400 Series II elemental analyzer. The contents of C, H and N were determined.

# **Zeta potential**

A sample solution (4 mg/L) was thoroughly stirred, and then the Zeta potential was measured using a Nano-ZS Zetasizer (Malvern Instruments, UK). The pH values were adjusted by 0.01 mol/L HCl or 0.01 mol/L NaOH aqueous solution.

# **TG analysis**

The thermal stability of graft polymers was analyzed after fully dried and accurately weighed. Under  $N_2$ , TG analysis was carried out with TG/DTA6300 made by Japanese Seiko, with heating rate of 20  $\degree$ C/min and scanning temperature range of  $30-600$  °C.

### **SEM**

The morphology of samples dried *in vacuum* was observed using the JSM-6510LV scanning electron microscope manufactured by the Japan Electronics Corporation.

### **Flocculation experiment**

The focculation performance of KGM-*g*-PTMAAC was carried out using standard Jar Test method [[35](#page-21-7), [36\]](#page-21-8). Firstly, 200 mL of 1.0 wt% kaolin suspension was used to simulate waste water. Then, a certain amount of graft copolymers was added to the kaolin suspension and was stirred at 25 rpm for 2 min. The turbidity of the supernatant was measured by WGZ-200 photoelectric turbidity meter (Shanghai Precision Instrument Company, China). The turbidity removal rate (Tr, %) was calculated as follows [\[35,](#page-21-7) [36](#page-21-8)].

$$
Tr(\%) = \frac{T_0 - T_1}{T_0} \times 100
$$
 (2)

where  $T_0$  and  $T_1$  represents the turbidity of kaolin suspension before treatment (nephelometric turbidity units, NTU) and the turbidity of kaolin suspension after treatment (NTU), respectively.

#### **Biodegradation studies**

The biodegradation performance of KGM-g-PTMAAC was tested using soil extract [[37\]](#page-21-9). 100 g of fresh soils was added into 200 mL of deionized water and vigorously stirred using a stirrer for 20 min, and then centrifuged with a highspeed centrifuge at 6000 r/min for 15 min. Then fne particles and impurities in the soil supernatant were removed by fltration, and the fltrate was diluted to 200 mL with deionized water for biodegradation experiment.

0.2 g of KGM-g-PTMAAC was added to the above 200 ml of the soil extract and was incubated at 37  $\degree$ C in an incubator. After having been degraded for every interval, these samples were taken out and washed with 100 mL absolute ethanol to remove the impurities on the surface, then dried and weighed, respectively.

The degradation ratio (DR) could be determined by measuring the weight loss of sample, which was calculated by the following formula  $[38]$  $[38]$ :

$$
DR(\%) = \frac{W_0 - W_i}{W_0} \times 100
$$

where DR is the degradation rate of the sample,  $W_i$  is the residual weight of the sample after  $i$  d, and  $W_0$  is the weight of the original sample.

### **Results and discussion**

### **Synthesis of the graft copolymer**

### **Efect of time on graft copolymerization**

In this grafting copolymerization,  $Ce^{4+}$  was selected as initiator, which has some following advantages [[30\]](#page-21-2). For example, there were few free initiators in the reactive medium, limiting the formation of homopolymers, and moreover, the reaction was easy to carry out in aqueous solution. Nevertheless, some homopolymers would inevitably be formed during graft copolymerization. However, both these homopolymers and unreacted monomers could be removed by Soxhlet extraction method [[25,](#page-20-22) [33](#page-21-5)]. When the weight ratio of TMAAC/KGM was 5:1, the weight ratio of CAN/  $(KGM+TMAAC)$  was 0.7%, and the reaction temperature was 70 °C; the influence of reaction time on the grafting yield is shown in Fig. [1.](#page-6-0) As shown in Fig. [1,](#page-6-0) the grafting yield increased with the extension of reaction time and reached a maximum value at 4 h, and then the values decreased after 4 h. This could be explained that there were a large number of active sites on KGM backbone in the early stage of reaction, and the grafting yield increased due to the rapid graft reaction. However, with the reaction proceeding, the grafting yield decreased. Many researchers reported similar results, and most of them believed that the reduction of the grafting yield with time might be interpreted as follows [[39,](#page-21-11) [40\]](#page-21-12). On the one hand, the increased viscosity of the system retarded the difusion of the monomers to reach the active sites on the KGM. On the other hand, the number of site available for grafting reduced due to the consumption of initiators. Moreover, another possible explanation was the fragmentation of KGM chain in the presence of  $Ce<sup>4+</sup>$ . The obtained



<span id="page-6-0"></span>**Fig. 1** Efect of reaction time on graft copolymerization (5:1 TMAAC/KGM, 0.7% CAM/  $(KGM+TMAAC)$ , 70 °C)

low molecular KGM chains were not all precipitated in the ethanol–water mixture, which also results in a decrease in the measured grafting yield. The optimal reaction time was selected as 4 h.

### **Efect of weight ratio of TMAAC to KGM on graft copolymerization**

Figure [2](#page-7-0) shows the infuence of weight ratio of TMAAC to KGM on the graft yield. It can be seen from Fig. [2](#page-7-0) that when the weight ratio was less than 5:1, the grafting yield increased with the increase in the TMAAC/KGM ratio, and when the weight ratio was higher than 5:1, the grafting yield did not increase any more.

When the weight ratio was low, the probability of collision between TMAAC and KGM in the system was low, and TMAAC and KGM did not fully react. With the increase in TMAAC dosage, the probability of contacting between KGM active sites and TMAAC increased, then the graft yield increased. However, when too much TMAAC was added into the system, the homopolymerization of TMAAC was easy to occur, and the resulting homopolymers could not graft with KGM, thus reducing the grafting yield. Therefore, 5:1 of TMAAC to KGM was chosen as the appropriate dosage.

#### **Efect of amount of initiator on graft copolymerization**

Figure [3](#page-8-0) shows the effect of amount of  $Ce^{4+}$  on the grafting yield in the case of other reaction parameters being fxed. When the weight ratio of CAM/(KGM+TMAAC) was lower than 0.7%, the grafting yield increased with the increase in the  $Ce^{4+}$ amount; however, when the weight ratio was higher than 0.7%, the grafting yield decreased. Because Ce<sup>4+</sup> reacted with KGM to produce free radicals, and the



<span id="page-7-0"></span>**Fig. 2** Efect of weight ration of TMAAC to KGM on graft copolymerization (0.7% CAM/  $(KGM+TMAAC)$ , 70 °C, 4 h)



<span id="page-8-0"></span>Fig. 3 Effect of amount of initiator on graft copolymerization (5:1 TMAAC/KGM, 70 °C, 4 h)

number of free radicals increased as the increase in the  $Ce<sup>4+</sup>$  concentration, resulting in the increase in the grafting yield. However, when the  $Ce<sup>4+</sup>$  concentration was high enough, free radicals probably transfer to initiators, that is, induced decomposition occurs, thus reducing the grafting yield.

#### **Efect of temperature on graft copolymerization**

Figure [4](#page-9-0) shows the temperature on the graft copolymerization when other reaction parameters were fxed. It can be seen from Fig. [4](#page-9-0) that the grafting yield increased with the increase in temperature when the temperature was lower than 70 °C, and then decreased with the increase in temperature when the temperature was higher than  $70^{\circ}$ C.

When the reaction temperature was too low, the generation rate of the primary radicals was slow, and the probability of TMAAC contacting with the radical was relatively low, then the grafting reaction could not be fully carried out. As the reaction temperature increased, CAM could react with KGM to form more active sites, resulting in increased grafting yield. However, when the reaction temperature was higher than 70 °C, the reaction occurred too fast, causing some side reactions such as chain transfer and/or fracture of molecular chains, then the grafting yield decreased. In this system, the best reaction temperature was 70 °C.

#### **Analysis of orthogonal experiments**

In order to study the infuence of multiple factors on the graft copolymerization of KGM with TMAAC, a four-factor and three-level orthogonal experiment, i.e.,  $L9(3<sup>4</sup>)$  matrix was carried out using initiator amount (A), reaction temperature (B), reaction time (C) and monomer amount (D) as experimental factors, respectively.



<span id="page-9-0"></span>**Fig. 4** Efect of temperature on the graft copolymerization (5:1 TMAAC/KGM, 0.7% CAM/  $(KGM+TMAAC)$ , 4 h)

The design of orthogonal experiments is shown in Table [1](#page-4-0). The orthogonal experiment of  $L9(3^4)$  matrix was conducted according to Table [1,](#page-4-0) and the result of orthogonal experiments was obtained, as shown in Table [2.](#page-9-1)

In Table [2,](#page-9-1)  $k_1$ ,  $k_2$  and  $k_3$  represents the average grafting yield of the graft copolymer at each level of each factor, respectively. And Ri is the extreme diference of the average grafting yield at all levels under the same factor. Generally, the average value refects the infuence of diferent levels under the same factor on the experimental

<span id="page-9-1"></span>

results, and it determines the optimal level under that factor. The extreme diference refects the magnitude of the infuence of the level change of each factor on the experimental results. The high value of extreme diference indicates that the level change of this factor has strong impact on the experimental results. On the contrary, it has a weak impact on the experimental results.

Therefore, as shown in Table [2,](#page-9-1) the optimal combination of various factors was  $A_3B_2C_1D_3$ , namely the optimal process condition was 0.7% of initiator amount, 70 °C of reaction temperature, 4 h of reaction time and 5:1 of  $m_{TMAAC}/m_{KGM}$ , respectively, which was consistent with the previous experimental results. Moreover, according to the magnitude of extreme diference, the infuencing order of each factor followed as  $A > B > C > D$ . In particular, it should be pointed out that in this work, the samples used for further structural characterization and performance testing were prepared under the optimal condition.

#### **Characterization of the samples**

#### **FTIR of the graft copolymers**

The infrared spectra of KGM (a) and KGM-*g*-PTMAAC (b) are shown in Fig. [5.](#page-10-0) As shown in Fig. [5a](#page-10-0), the broad peak at 3390 cm<sup>-1</sup> was attributed to the stretching vibration absorption of O–H in KGM, and the peak at 1644 cm−1 was caused by the frst overtone of O–H bending vibration. The peak at 1727 cm−1 was attributed to the C=O stretching vibration absorption of acetyl groups in KGM, and two peaks at 1065 and 1025  $cm^{-1}$ were due to the C–O–C stretching vibration absorption. Comparing the infrared spectra of KGM and that of KGM-*g*-PTMAAC, it could be found from Fig. [5](#page-10-0)b that besides the characteristic absorption peaks of KGM, there were the bending vibration absorption peak of methylene bonded with  $N^+$  at 1430 cm<sup>-1</sup>, the in-plane asymmetric bending



<span id="page-10-0"></span>**Fig. 5** FTIR spectra of KGM (a) and KGM-*g*-PTMAAC (b)

vibration absorption peak of methyl bonded with  $N^+$  appeared at 1415 cm<sup>-1</sup>, and the C–C stretching vibration absorption peak of ammonium salt at 1058 cm−1. Moreover, the peak at 2922 cm<sup>-1</sup> was attributed to C–H stretching of methane in the TMAAC. All above indicated that TMAAC were successfully grafted onto the main chain of KGM.

# **13C solid‑state NMR spectroscopy**

The 13C solid-state NMR spectra of KGM (a) and KGM-*g*-PTMAAC (b) are shown in Fig. [6.](#page-12-0) The assignment of  ${}^{13}C$  NMR peaks of KGM was suggested on the basis of previous solid-state NMR work on KGM [[17,](#page-20-15) [41](#page-21-13)[–43\]](#page-21-14). The peak at 102.42 ppm was the characteristic anomeric signal due to C-1 resonance of sugar ring and that at 61.60 ppm was attributed to the resonance of pendant methylene carbon of C-6. The peaks from 81.30 to 68.45 ppm overlapped to some extent due to the complex nature of the spectra of polysaccharides; however, they corresponded to the remaining carbon atoms in the KGM backbone, which could be assigned as C-4 (81.30 ppm), C-5 (75.26 ppm), C-3 (73.10 ppm), and C-2 (68.45 ppm), respectively. Comparing the  $^{13}$ C NMR spectra of KGM and that of KGM-*g*-PTMAAC, it could be found from Fig. [6](#page-12-0)b that besides the characteristic peaks of KGM, there appeared some new peaks in the latter. The sharp new peak at 53.62 ppm was due to the resonance of *N*-methyl carbon of quaternary ammonium salt  $[22, 44]$  $[22, 44]$  $[22, 44]$ . The peak at 70.00 ppm was attributed to the resonance of propyl carbon directly connected to  $N^+$ . Furthermore, the two peaks appearing around 130 ppm were the resonance of two carbonyl carbons at the sugar ring. In all, the  $^{13}C$ solid-state NMR spectroscopy also confrmed the structure of the graft copolymer.

### **Elemental analysis and Zeta potential of sample**

The results of elemental analysis of KGM and KGM-*g*-PTMAAC (typical sample) are listed in Table [3](#page-12-1). As shown in Table [3](#page-12-1), the amount of N in KGM was very low, which might be related to the presence of trace quantities of proteins in the commercial polysaccharides. However, the content of N in the graft copolymer was significantly higher, which indicated that the presence of graft chain of PTMAAC. According to the count of N, the weight ratio of PTMAAC to KGM was determined as 0.57:1, which was consistent with the grafting yield of the KGM-g-PTMAAC.

In addition, Fig. [7](#page-13-0) presents the infuence of pH on the Zeta potential of the KGM*g*-PTMAAC solution. As shown in Fig. [7](#page-13-0), the solution of the graft copolymer had a positive Zeta potential at all measured pH range from 2.0 to 12.0. This phenomenon was attributed to the introduction of cationic quaternary ammonium salt groups on the KGM. Of course, both the elemental analysis results and the Zeta potential results further supported the success of the graft copolymerization.

### **Morphology of samples**

Figure [8](#page-13-1) shows an SEM image of KGM and that of KGM-*g*-PTMAAC, respectively. Macroscopically, KGM and KGM-g-PTMAAC were spherical particles. However, on the micro-level, they were irregular-shaped with diferent morphologies. The



<span id="page-12-0"></span>**Fig. 6** 13C solid-state NMR spectra of KGM (**a**) and KGM-*g*-PTMAAC (**b**)

<span id="page-12-1"></span>

SEM image of KGM indicated that it had a relatively smooth surface, and that of KGM-*g*-PTMAAC implied that the graft copolymer had a spike-like surface. This was due to the introduction of the quaternary ammonium salt groups on the main



<span id="page-13-0"></span>**Fig. 7** pH dependence of zeta potential of the KGM-*g*-PTMAAC solution



**Fig. 8** SEM images of KGM (**a**) and KGM-*g*-PTMAAC (**b**)

<span id="page-13-1"></span>chain of KGM resulted in signifcant change of the surface morphology, which further proved that TMAAC was successfully grafted onto KGM.

# **TG curves of samples**

Figure [9](#page-14-0) shows TG (A) and DTG (B) curves of KGM (a) and KGM-*g*-PTMAAC (b). As it is shown from TG curves, in a relatively low temperature (for example, under 320 °C), the stability of KGM-*g*-PTMAAC was poorer than that of KGM. However, in a relatively high temperature (for example, more than 320 °C), the stability of KGM-*g*-PTMAAC was better than that of KGM. And these phenomena could also be found from DTG curves. Namely, the frst DTG peak of KGM-g-PTMAAC appeared in relatively lower temperature than that of KGM while the second DTG peak shifted (weak) to higher temperature than that of KGM (strong). This can



<span id="page-14-0"></span>**Fig. 9** TG (**A**) and DTG (**B**) curves of KGM (a) and KGM-*g*-PTMAAC (b)

probably be explained as follows: On the one hand, as the quaternary ammonium salt groups introduced onto the KGM probably undergo decomposition at a lower temperature, resulting in a lower stability of the graft copolymer. On the other hand, according to the report  $[45, 46]$  $[45, 46]$  $[45, 46]$  $[45, 46]$ , the decomposition mechanism of polysaccharides was generally involved in the dehydration reaction between molecules and the formation of polynuclear aromatic and graphitic carbon structure at high temperature. And since hydroxyl on KGM molecules was replaced by graft monomers, which prevented the elimination reaction to some extent, the thermal stability of the graft copolymer was better than that of KGM at high temperature.

# **Flocculation**

#### **Efect of focculant dosage on turbidity removal rate**

Figure [10](#page-15-0) shows the infuence of focculant dosage on the turbidity removal rate. As shown in Fig. [10](#page-15-0), when the dosage was lower than 4 mg/L, the turbidity removal rate increased with the increase in the dosage; however, when the dosage was higher than 4 mg/L, the turbidity removal rate decreased with the increase in the focculant dosage. The coagulation–focculation mechanism of most cationic focculants can be explained by the synergistic efect of charge neutralization and bridging mechanism [\[47](#page-21-18)].

On the one hand, as it is known, the surface of kaolin particles showed negative zeta potentials in the solution [\[9](#page-20-8), [25](#page-20-22)]. On the other hand, as it was mentioned above (Fig. [7](#page-13-0)), the focculant solution presented positive zeta potentials in a wide pH range from 2.0 to 12.0. This meant that when cationic focculant was added to kaolin suspension, the focculants with positive charge were adsorbed on the kaolin fakes and neutralized the negative charge on their surfaces, causing the destabilization of kaolin particles and the efficient flocculation of suspensions. However, the overdosing of focculant might lead to charge reversal and the re-stabilization of kaolin particles, which exhibited inefficient flocculation of suspensions.

On the other hand, focculant polymers adsorbed on kaolin particles still had other free active sites for adsorbing more kaolin particles. Therefore, a so-called



<span id="page-15-0"></span>Fig. 10 Effect of flocculant dosage on turbidity removal rate

bridging efect was formed in the three-dimensional space, and the coagulation of kaolin particles occurred due to the function of gravity. When the dosage was low, the bridging efect was not obvious, and the settlement of suspended particles was not evident, i.e., Tr was relatively low. However, when the dosage of focculant was high enough, the charge reversal occurred, thus re-stabilizing the suspended particles. Namely, the charge neutralization efect restrained the bridge efect. In addition, due to the steric hindrance of the macromolecules, the aggregation between suspended particles became difficult, which also led to the decline of Tr. Then, the best focculant dosage was 4 mg/L in this system. However, it should be noted that although graft copolymers are likely to show self-caused turbidity in the solution, our experiments determined that the turbidity was very low (all below 1 NTU) within the whole concentration range we measured, which was similar to the fndings of other searchers [\[20](#page-20-17), [48](#page-21-19)]. This could be explained by the fact that both KGM and its graft copolymers had high water-solubility, leading to the low self-caused turbidity of the graft copolymers in relatively low concentration solution. Therefore, the infuence of the self-caused turbidity of the focculants on the value of Tr was not considered in this study.

### **Efect of pH of kaolin suspension on the turbidity removal rate**

Figure [11](#page-16-0) shows the infuence of pH of kaolin suspension on the turbidity removal rate. It can be seen from Fig. [11](#page-16-0) that, when pH value was lower than 5, the turbidity removal rate increased with the increased pH. However, when pH was higher than 5, Tr decreased as pH increasing. For cationic focculants, their focculation performance is evidently afected by the strength and availability of positive charges, which is relied on the cationicity and the conformation of focculants in the aqueous solution. Of course, the pH in the solution can infuence the cationicity and the



<span id="page-16-0"></span>Fig. 11 Effect of pH of kaolin suspension on the turbidity removal rate

conformation of focculants in the solution. This theory has been supported by some studies [\[47](#page-21-18), [49](#page-21-20)]. Under lower pH, a large number of cations in the system resulted in the declining fexibility of polymer chains, which could not freely adjust to the appropriate conformation to form bridging efect, leading to a declined turbidity removal rate. However, under alkaline environment, both the charge neutralization and bridging efect were reduced due to the shielding efect of anionic ions on the cationic focculants, which also reduced the turbidity removal rate. In addition, as shown in Fig. [7](#page-13-0), the lower pH was, the higher zeta potential of a cationic focculant solution was, which implied stronger charge neutralization with kaolin particles. This explained why the optimal pH value appeared in acidic environments (around 5 of pH).

### **Efect of settling time on the turbidity removal rate**

Figure [12](#page-17-0) shows the infuence of focculation time on the turbidity removal rate in the case of KGM-*g*-PTMAAC added to 1.0 wt% of kaolin suspension. The amount of KGM-*g*-PTMAAC used was 4 mg/L; the pH was 5. As it is shown in Fig. [12,](#page-17-0) when the settling time is shorter than 20 min, the turbidity removal rate of KGM*g*-PTMAAC frequently increased with the increase in settling time. When the settling time ranged from 20 to 50 min, the turbidity removal rate increased slowly with settling time. The turbidity removal rate decreased with the settling time longer than 50 min. At the beginning, focculants and colloidal particles could not fully contact, which was not conductive to the capture of colloidal particles by the flocculants, and the efficiency of flocculants could not be fully realized. However, after a long time of focculation, due to the instability of bridging action, the adsorbed colloidal particles were re-dispersed into the solution, resulting in a decrease in the turbidity removal rate.



<span id="page-17-0"></span>**Fig. 12** Effect of settling time (*t*) on the turbidity removal rate

### **Efect of temperature on the turbidity removal rate**

Figure [13](#page-18-0) shows the infuence of temperature on focculation. It could be seen that, as the temperature increased, the turbidity removal rate increased at frst and then decreased. When the temperature was 35 °C, the turbidity removal rate reached a maximum value. This can probably be explained as follows: When the temperature was low, the Brownian motion of colloidal particles in water was relatively slow, and the probability of collision between colloidal particles and focculant molecules was relatively low, which did not favor the formation of focks, and the turbidity removal rate was low. As the temperature increased, the Brownian motion of the colloidal particles was accelerated, and it could easily collide with the focculant agents to form focs, then the turbidity removal rate increased. However, when the temperature was too high, the rapid Brownian motion of the colloidal particles led to relatively small focs, and the settlement of focs was not easy to occur. Furthermore, high temperature probably also accelerated the decomposition of focs, which was not conducive to the bridging efect, resulting in the decline of Tr.

# **Biodegradation properties of focculants**

Although polysaccharides have complete biodegradability, their properties cannot meet the requirements of practical application. Therefore, chemical modifcation must be carried out to improve their performance for practical applications. However, the premise of modifcation is that it does not essentially afect their degradation performance. In this work, graft modifcation of KGM was carried out to endow it with good focculating properties. Figure [14](#page-18-1) shows the biodegradation ratio of focculants in the soil extract at diferent time intervals. For KGM, the degradation



<span id="page-18-0"></span>Fig. 13 Effect of temperature on the turbidity removal rate

rate was fast, which could be completely degraded in about 20 d. However, for the graft copolymer, the degradation rate was relatively slow. As shown in Fig. [14](#page-18-1), the biodegradation ratio of focculants achieved more than 40% within 5d and then exceeded 50% after 20 d. Subsequently, the biodegradation ratio gradually increased and attained approximately 80% after 90 d.

This probably was explained as follows: KGM was an easily biodegradable polysaccharide, while the graft copolymer contained some synthesized graft chains besides KGM as a matrix. In other words, KGM-*g*-PTMAAC had a comb-like



<span id="page-18-1"></span>**Fig. 14** Biodegradation properties of focculants (Square, KGM; circle, KGM-*g*-PTMAAC)

structure where PTMAAC was dangled from the backbone of KGM. The secretions of the microbes from soil extracts were involved in the degradation of polysaccharides, resulting in the cleavage of chemical bonds. For KGM-*g*-PTMAAC, the degradation process started with the polymer backbone. At the beginning, there were many polysaccharides in the sample, and the microbial activity in the degradation solution was high, so the degradation rate was fast at the initial stage. However, as the polysaccharides of KGM degraded gradually, the grafted chains of PTMAAC were released. As mentioned above, KGM-*g*-PTMAAC had a comb-like structure where PTMAAC was dangled from the backbone of KGM. Obviously, microbes could split PTMAAC from the backbone of polysaccharide. Due to the slow degradation of releasing grafted chains in microorganism, the degradation ratio was no longer evidently increased when the degradation time exceeded 60 d. Therefore, in this sense, the graft copolymer could be considered as partially biodegradable, which might be mainly attributed to the grafted chains of PTMAAC. Trippathy et al. [\[34](#page-21-6)] in the report on the amylopectin grafted poly(acrylamide-co-*N*-methylacryamide) obtained similar results.

# **Conclusions**

In this work, we systematically studied the preparation process, characterization and related properties of cationic focculants based on biodegradable KGM. The graft copolymer (KGM-*g*-PTMAAC) of TMAAC with KGM was prepared using KGM as graft matrix, TMAAC as cationic monomer and CAN as initiator, respectively. The results showed that when the reaction time was 4 h, the weight ratio of TMAAC to KGM was 5:1, the amount of initiator was 0.7%, and the reaction temperature was 70 °C; the grafting yield of the product was the highest. And the interaction between the process parameters was clarifed by the orthogonal experiments. Both FTIR and NMR confrmed the incorporation of quaternary ammonium cationic groups on the backbone of KGM. The SEM image showed that the morphology of the modifed product was evidently diferent from that of unmodifed KGM. The result of TG indicated that the thermal stability of KGM-*g*-PTMAAC was lower than that of KGM at relatively low temperatures, while the opposite was true at relatively high temperature. The biodegradable studied showed that the graft copolymer was partially biodegradable. Moreover, the focculation performance test demonstrated that modifed products had good focculation for on kaolin suspension. When the dosage of KGM-*g*-PTMAAC was 4 mg/L, the pH of the medium was 5, and settling time was 30 min; the focculation performance was the best. The obtained graft copolymer might potentially be used as a novel biodegradable focculant in wastewater treatment.

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