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Impact of different within-canopy wind attenuation formulations on modelling sensible heat flux using TSEB

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Abstract

The unique vertical canopy structure and clumped plant distribution/row structure of vineyards and orchards creates an environment that is likely to cause the wind profile inside the canopy air space to deviate from how it is typically modelled for most crops. This in turn affects the efficiency of turbulent flux exchange and energy transport as well as their partitioning between the plant canopy and soil/substrate layers. The objective of this study was to evaluate a new wind profile formulation in the canopy air space that explicitly considers the unique vertical variation in plant biomass of vineyards. The validity of the new wind profile formulation was compared to a simpler wind attenuation profile that assumes attenuation through a homogeneous canopy. We evaluated both attenuation models using measurements of wind speed in a vineyard interrow, as well as turbulent flux estimates retrieved from a two-source energy balance model, which uses land surface temperature as the key boundary condition for flux estimation. This is relevant in developing a robust remote sensing-based energy balance modelling system for accurately monitoring vineyard water use or evapotranspiration that can be applied using satellite and airborne imagery for field-to-regional scale applications. These tools are needed in intensive agricultural production regions with arid climates such as the Central Valley of California, which experiences water shortages during extended drought periods requiring an effective water management policy based on robust water use estimates for allocating water resources. Results showed that the new wind profile model improved sensible heat flux estimates (RMSE reduction from 42 to 35 W m^{-2}) when the vine canopy is in early growth stage resulting in a strongly clumped canopy.

Introduction

As water resources become more limited, there is a greater need for precision agricultural management at the field/ subfield-scale and hence remote sensing is becoming a powerful tool for managing irrigation, particularly for highvalued crops (Bellvert et al. 2016). Thermal remote sensing

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allows to detect plant stress and hence, when applied within an energy balance model, allows the estimation of evapotranspiration (ET) without intensive in situ measurements related to the water balance that are usually required in energy combination equations (Ortega-Farias et al. 2007; Teixeira et al. 2007; Zhang et al. 2008). There have been numerous surface temperature-based energy balance models developed for estimating surface fluxes and ET (Kalma et al. 2008). However, many of these models used moderate resolution data that are too coarse to inform variable rate application of water or nutrients within a field (Zipper and Loheide II 2014). Furthermore, there is a growing interest in precision agriculture for partitioning evapotranspiration into crop transpiration and soil evaporation, as the latter is considered non-productive water loss from an agronomic perspective (Kool et al. 2014).

Although several remote sensing ET models have already been applied for estimating ET on vineyards, such as SEBAL (Bastiaanssen et al. 1998) or SEBS (van der Kwast et al. 2009), few of them have the capability to partition fluxes from the vegetated canopy and the underlying soil/substrate layer. One such modelling approach is the Two Source Energy Balance-TSEB land surface scheme (Norman et al. 1995), which contains a level of complexity that has allowed successful application to many different landscapes (Kustas and Anderson 2009). As any other dual source energy balance model, TSEB requires the estimation of turbulent transport efficiency coefficients, usually related to a resistance or their reciprocal conductance (Shuttleworth and Wallace 1985; Choudhury et al. 1987; Shuttleworth and Gurney 1990; McNaughton and Van Den Hurk 1995; McInnes et al. 1996). In TSEB, R_s is defined as the resistance to heat transport in the boundary layer immediately above the soil surface (s m^{-1}) and hence controls the evaporation process. Conversely, R_r is the boundary layer resistance of the canopy of leaves (s m⁻¹) and controls heat and mass interchanges between the canopy and the air-canopy interspace (i.e., transpiration process). Norman et al. (1995) and Kustas and Norman (1999), based on previous studies (McNaughton and Van Den Hurk 1995; Sauer et al. 1995; Kondo and Ishida 1997), derived semi-empirical formulas for these two resistances to heat transport, which depend on the wind speed (u_s) at the height above the soil surface where the effect of the soil roughness is minimal $(z_{0,\text{soil}} \approx 0.01 - 0.05 \text{ m})$, and the wind speed at the bulk heat source/sink $d_0 + z_{0M}$ (i.e., $u_{d_0+z_{0M}}$), respectively, for estimating R_s and R_x . Since wind speed is attenuated when flowing through porous roughness elements such a plant canopy, adequately modelling the vertical wind profile within the canopy is needed for an accurate estimation of the resistances to heat transport, and hence for estimating evapotranspiration and its partitioning.

The TSEB modelling approach for u_s and $u_{d_0+z_{0M}}$ described in Norman et al. (1995) and Kustas and Norman (1999) is based on an exponential wind attenuation proposed by Goudriaan (1977). However, this attenuation profile model was particularly designed for homogeneous and dense canopies (Goudriaan 1977). Other wind attenuation formulations are based on hyperbolic cosine mathematical relationships with the aim of simulating sparse canopies (Massman 1987) or canopies with a vertical discontinuity (Lalic et al. 2003). A previous study (Cammalleri et al. 2010) applied Goudriaan (1977), Massman (1987) and Lalic et al. (2003) profile models in TSEB over an olive orchard. From the three models tested, Cammalleri et al. (2010) found that Lalic et al. (2003) gave poor performance when comparing the estimated TSEB sensible heat flux with in situ measured fluxes, with Massman (1987) and Goudriaan (1977) yielding similar satisfactory estimates.

More recently, Massman et al. (2017) developed a new physically based wind attenuation profile that eliminates the assumptions of uniform vertical canopy structure in modelling wind attenuation throughout the canopy. Therefore this new model provides a more physically realistic method for calculating wind speed attenuation for canopies of vertically non-uniform foliage distribution and leaf area, such as orchards and vineyards.

The objective of this study is to evaluate and compare the Massman et al. (2017) and Goudriaan (1977) wind attenuation profiles to estimate the wind speed below the canopy and the turbulent fluxes derived with TSEB in a clumped and vertically heterogeneous canopy such as a vineyard. Both Massman et al. (2017) and Goudriaan (1977) models were evaluated using in situ continuous input measurements from flux towers in two adjacent vineyards over a three year period, where different canopy vertical foliage distributions were modelled depending on phenological/management stage. In the next section we describe the implementation and inputs required for the Massman et al. (2017) wind attenuation profile model. In "Materials and methods" we describe the experimental setup while in "Results and discussion" we discuss the results. A detailed mathematical formulation in TSEB is described in the Appendix.

Massman et al. (2017) wind profile

Compared to previously used canopy wind profiles such as Goudriaan (1977) or Massman (1987), the additional key input required in Massman et al. (2017) wind attenuation model is the relative canopy foliage distribution $ha(\xi)$, computed as in Eq. 1

$$ha(\xi) = PAI \frac{f_a(\xi)}{\int_0^1 f_a(\xi') d\xi'}$$
(1)

where $\frac{f_a(\xi)}{\int_0^1 f_a(\xi')d\xi'}$ is the relative canopy shape (i.e., $\sum \frac{f_a(\xi)}{\int_0^1 f_a(\xi')d\xi'} = 1$, and $\xi = z/h_c$) and PAI is the plant (leaves + stems) area index. Massman et al. (2017) modelled the shape of the plant surface distribution $f_a(\xi)$ as a combination of asymmetric Gaussian curves, but $f_a(\xi)$ can also be estimated as a continuous curve obtained from canopy structure measurements or three dimensional cloud points, such as in Nieto et al. (2018).

The canopy wind speed profile is then the product of two terms: a logarithmic profile (U_b) that is dominant near the ground, and a hyperbolic cosine profile (U_t) that dominates near the top of the canopy, where the canopy foliage distribution plays a major role. Ancillary input in U_t is the drag coefficient of the individual foliage elements (C_d) , which is usually considered equal to 0.2 (Goudriaan 1977; Massman et al. 2017). Also, the Massman et al. (2017) model has the ability to consider variations of the drag coefficient due to either wind sheltering between foliage elements, or vertical variations independent of wind blocking. This effect can usually be disregarded in most canopies (Massman et al. 2017) so was it in this study.

Wind speed above the canopy

Most of canopy wind attenuation profiles known (Goudriaan 1977; Massman 1987; Lalic et al. 2003; Massman et al. 2017) require an estimate of the wind speed directly above the top of the canopy height (u_c). Assuming that wind profile above the canopy is logarithmic (Brutsaert 2005), and ignoring corrections associated to the roughness sub-layer (Raupach 1994; Massman et al. 2017), u_c is estimated as (Eq. 2):

$$u_{\rm c} = \frac{u_*}{\kappa'} \left[\ln\left(\frac{h_{\rm c} - d_0}{z_{\rm 0M}}\right) - \Psi_{\rm m}\left(\frac{h_{\rm c} - d_0}{L}\right) + \Psi_{\rm m}\left(\frac{z_{\rm 0M}}{L}\right) \right]$$
(2)

where u_* is the friction velocity (m s⁻¹), $\kappa' = 0.4$ is the von Kàrman constant, h_c is the canopy height (m), d_0 and z_{0M} (m) are, respectively, the zero-plane displacement height and aerodynamic roughness length for momentum transport, and $\Psi_m\left(\frac{h_c-d_0}{L}\right) + \Psi_m\left(\frac{z_{0M}}{L}\right)$ are stability correction functions for momentum transport (Brutsaert 2005).

Materials and methods

Study site

Two adjacent vineyards, labeled North and South, which were planted in 2008 and 2011, respectively, at the Borden ranch near Lodi, CA (38.29°N 121.12°W), are used as part of the GRAPEX project (Kustas et al. 2018b). The management of the two vineyards, which includes the timing and amount of irrigation, pruning activities, cover crop management, and application of agrochemicals also differed from season-to-season and between the blocks due to variation in weather and climate conditions.

In both fields, the configuration of the trellising system and interrow is the same (Fig. 1). The vine trellises are 3.35 m apart and run east–west. There is an individual vine planted every 1.52 m, with the two main vine stems attached to the first cordon at a height of 1.45 m above ground level (agl). There is a second cordon at 1.9 m agl where vine shoots are managed. Typically, the vines reach a maximum height of between 2.0 m and 2.5 m agl during the growing season with the vine biomass concentrated in the upper half of the total canopy height. The typical vine canopy width is nominally 1 m mid-season. Pruning of the vines is mainly performed to remove shoots growing significantly into the interrow. Due to irrigation management practices, a grass layer in the interrow is kept in the early stages of the growing



Fig. 1 Dimensions of trellis system in both North and South vineyards

season, which is then mowed several times in spring time and allowed to go into senescence in summer.

Eddy covariance/energy balance (EC) systems were located approximately 20 m inside each vineyard at the east edge to have an adequate fetch for the prevailing winds from the west. A detailed description of the measurements and their post-processing is described by Alfieri et al. (2018b). Briefly the tower at each site is instrumented with an infrared gas analyzer (EC150, Campbell Scientific,¹ Logan, Utah) and a sonic anemometer (CSAT3, Campbell Scientific) co-located at 5 m agl to measure the concentrations of water and carbon dioxide and wind velocity, respectively. The full radiation budget was measured using a four-component net radiometer (CNR-1, Kipp and Zonen, Delft, Netherlands) mounted at 6 m agl. Air temperature and water vapor pressure at 5 m agl was measured using a Gill-shielded temperature and humidity probe (HMP45C, Vaisala, Helsinki, Finland). Subsurface measurements include the soil heat flux measured via a cross-row transect of five plates (HFT-3, Radiation Energy Balance Systems, Bellevue, Washington) buried at a depth of 8 cm. The soil heat flux was corrected for heat storage in the overlying soil layer following Oke and Cleugh (1987). Processing of turbulent data included despiking of high-frequency data (Goring and Nikora 2002), 2-D coordinate rotation of wind components (Tanner and Thurtell 1969), and Massman (2000) frequency response correction. The initial estimates of latent heat flux were corrected

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<u>a:</u> ,	IOD	<u> </u>			
Site	IOP	Start date	End date		
N	2	1 June 2015	3 June 2015		
	4	10 August 2015	13 August 2015		
S	2	31 May 2015	3 June 2015		
	3	10 July 2015	13 July 2015		
	4	10 August 2015	13 August 2015		

 Table 1
 Available dates of wind speed below the vine canopy (1.45 m agl) for each site

IOP intensive observation period

for density effects following Webb et al. (1980), whereas sensible heat flux estimates were corrected for buoyancy effects (Foken 2008).

With the purpose of estimating fluxes from the soil/grass layer system, and to evaluate the turbulence intermittency between the above and below vine canopy, one additional eddy covariance system was placed in each vineyard in the interrow space at a height of 1.45 m during Intensive Observation Periods in 2015. Table 1 shows the dates for each site when wind speed below the canopy is available. A more detailed description of all experiments and measurements taken during the GRAPEX experiment is described in Kustas et al. (2018b).

Model evaluation

Both Massman et al. (2017) and Goudriaan (1977) wind attenuation profiles were evaluated to assess their performance in estimating below-canopy wind attenuation speed in the interrow space at 1.45 m (namely $u_{z,ref}$), using input data from atmospheric measurements above the crop together with estimates of canopy structure, and validated using the wind speed from the deployed EC in the interrow during IOPs in 2015. Also, we evaluated the capability of both attenuation profiles to estimate above-canopy bulk sensible heat flux H in TSEB. Both variables were evaluated in terms of percentage of variance explained by the model (R^2) , as well as error measurement metrics such as mean bias, Mean Absolute Error MAE, Root Mean Square Error RMSE, and its decomposition between systematic and unsystematic RMSE (Willmott 1981). Significant differences in errors between both models were tested using Student's t-test, establishing the null hypothesis that the mean error, mean absolute error, or mean squared error are equal between Massman et al. (2017) and Goudriaan (1977) models.

To run both attenuation profile models as well as TSEB, several ancillary canopy properties (i.e., Leaf Area Index, canopy height, foliage distribution density) were estimated on a daily basis using combined information from Landsat and MODIS satellites.

Estimation of daily canopy properties

Estimates of bulk LAI (i.e., leaf area of grapevines and grass) were obtained by fusing MODIS LAI (MCD15A3H) product and Landsat surface reflectance using the reference-based approach (Gao et al. 2012, 2014). The homogeneous and high-quality LAI retrievals from the MODIS LAI product were extracted to train Landsat surface reflectance aggregated at the MODIS spatial resolution. The trained regression trees were then applied to original 30 m Landsat surface reflectance to produce Landsat LAI. Since the study sites are located in an area that is overlapped by two Landsat paths and are normally cloud free, more than 60 clear Landsat observations were acquired for each year. Daily LAI at 30 m Landsat resolution were generated using the Savitzky-Golay moving window filter approach which smooths and fills the temporal gaps (Sun et al. 2017).

Canopy width w_c , canopy height h_c , the height of the bottom of the canopy h_b and the green fraction f_g were estimated from the daily LAI using empirical curves fit with measured in situ values during four Intensive Observation Periods in 2015 (Fig. 2). The empirical fits were constrained by the following boundary conditions based on Fig. 1:

• canopy height should tend to the height of the vine trellis when LAI tends to zero, as this is where the branches with sprouts are located:

$$\lim_{\text{LAI}\to 0} h_{\text{c}} = 1.45 \,\text{m}$$

• canopy width should tend to the width of the vine trellis when LAI tends to zero, as the branches with sprouts follows a "T" pattern:

 $\lim_{\mathrm{LAI}\to 0} w_{\mathrm{c}} = 0.60 \,\mathrm{m}$

• the height of the bottom of the canopy tends to h_c when LAI tends to zero. In other words, the ratio of bottom-to-top of the canopy h_b/h_c tends to 1 when LAI tends to zero.

$$\lim_{\text{LAI}\to 0} \frac{h_{\text{b}}}{h_{\text{c}}} = 1$$

• the green fraction is held constant to 1 during the growing season until observed senescence from daily phenocam photos near flux towers (typically mid September), afterwards f_g linearly decreases with LAI, tending to 0 when LAI is zero.

$$\lim_{\mathbf{L} \to \mathbf{I} \to 0} f_{\mathbf{g}} = 0; \quad \text{when DOY} > 250.$$

= 1.45 + 0.42 LAI

3.0

2.5

2.0

(u) 1.5

1.0

0.5

0.0

0.0

0.5

1 0

1.5

LAI

(a) canopy height

2.0



(b) canopy width



(c) height of bottom of the canopy

Fig. 2 Empirical models relating canopy height h_c , canopy width w_c and the bottom of the canopy h_b with the fused STARFM LAI. Solid dots represent in situ measured values

Figure 3 shows the timeseries of LAI and green fraction f_g in both vineyards spanning the whole study period (2014–2016). Since the Landsat LAI product represents 30 m effective LAI values, the decreases in LAI in springtime are due to grass mowing management. Neither LAI or f_g reach to zero since at the time of grapevine senescence and leaf-off in autumn, there is a regrowth of the grass layer in the interrow.

The relative foliage density profiles required in Massman et al. (2017) wind attenuation profile are derived after visual inspection of daily phenocam photos (Fig. 4). At our study site, there is a canopy overstory comprised of vertically non homogeneous biomass/leaf area, as grapevines are usually clumped due to the trellis system and pruning, and an understory at ground level having a dense layer of cover crop, which eventually is mowed and finally becomes stubble later during the growing season (early June). Therefore, we assumed our canopy foliage distribution changes with seasons/phenological stages. Before grapevine budbreak the only photosynthetic element is the grass layer in the interrow, but the trellis system and grapevine branches are still present and hence they provide additional roughness and wind attenuation. After bud-break (usually around mid March) there is a rapid increase of foliage biomass at the grapevine overstory and hence we assume the vineyard foliage distribution is represented as a bimodal asymmetric Gaussian function, with a higher relative foliage distribution at the grapevine canopy, until grass is mowed (typically in the beginning of May). Later on, when no standing grass is present, only the grapevine foliage contributes to the aboveground biomass, which due to the weight of fully developed branches and fruits the height at maximum foliage density tends to get closer to the ground. Finally, after leaf-off (at the end of November) there is still some attenuation due to the leafless vine shoots, and the regrowth of the cover crop.



Fig. 3 Timeseries of daily estimates for LAI and green fraction at North (left) and South (right) vineyard

TSEB evaluation with in situ surface temperature

To evaluate the effects of the modifications in TSEB model mentioned in the previous section, we used in situ data measured at the two EC towers installed over the study area. We used the 2014–2016 year periods using 15 min averaged values during daytime (i.e., solar irradiance $S^{\downarrow} > 100 \text{ W m}^{-2}$). Surface composite temperate T_{rad} was estimated from the 4-component net radiometer, Eq. 3:

$$T_{\rm rad} = \left(\frac{L^{\uparrow} - (1 - \epsilon_{\rm surf})L^{\downarrow}}{\sigma \epsilon_{\rm surf}}\right)^{1/4}$$
(3)

where L^{\uparrow} and L^{\downarrow} are the upwelling and downwelling measured longwave radiance, σ is the Stefan–Boltzmann constant, and $\epsilon_{surf} = 0.99f_{C} + 0.94(1 - f_{C})$ is the surface emissivity, assuming leaf and bare soil emissivity values of 0.99 and 0.94, respectively (Sobrino et al. 2005).

Additional inputs from the EC system were downwelling shortwave S^{\downarrow} irradiance, wind speed and direction, air temperature and humidity, and atmospheric pressure, all of them measured at 5 m above the ground. Furthermore, to reduce the uncertainties in modelling the flux partitioning associated to errors in the estimation of soil heat flux, we forced TSEB to use the estimated *G* by the EC system instead of making an estimate based on $R_{n,S}$ (Choudhury et al. 1987; Santanello Jr and Friedl 2003). Details on TSEB modelling are addressed in Appendix, and in Norman et al. (1995), Kustas and Norman (1999) and Kustas et al. (2016). A version of the TSEB model is available online at https://githu b.com/hectornieto/pyTSEB.

Aerodynamic resistances parameterization Kustas et al. (2016) showed that in case of sparse and heavily clumped vegetation and/or when the soil surface is very rough, the values for the *C'*, *b* and *c* parameters in the Kustas and Norman (1999) soil (R_s , Eq. 7b) and canopy boundary layer (R_x , Eq. 7c) resistances for heat transport might deviate from the default values proposed in Kustas and Norman (1999) and Norman et al. (1995). In our case we follow this rationale assuming that the soil is rougher than usual due to the presence of a grass stubble layer. Therefore, we used in the estimation R_s the value $c = 0.0038 \text{ m s}^{-1} \text{ K}^{-1/3}$ for a rough soil surface suggested in Kondo and Ishida (1997) and used successfully in Kustas et al. (2016). The estimation of aerodynamic roughness length and zero-plane displacement height considered the effects of wind direction relative to row orientation, as observed and modelled by Alfieri et al. (2018a), with larger roughness values at the across-row than the down-row winds.

Net radiation partitioning for row crops We developed a simplified method to derive the clumping index in row crops such as vineyards (Parry et al. 2018). The new clumping index is based on the ideas of the geometric model by Colaizzi et al. (2012), but instead of considering the crops as elliptical hedge-rows, we assumed a rectangular canopy shape, which simplifies the trigonometric calculations. The clumping index is defined as the factor that modifies the LAI of a real canopy (F) in a fictitious homogeneous canopy with LAI_{eff} = ΩF such as its gap fraction is the same as the gap fraction of the actual canopy ($G(\theta, \phi)$). This effective LAI is then used as input in the Campbell and Norman (1998) canopy radiative transfer model to estimate soil and canopy net radiation.

Results and discussion

Wind attenuation profile evaluation

Figure 5 is a the scatterplot between measured and modelled wind speed at 1.45 m ($u_{z,ref}$) using both profiles compared to

0.8

1.0

Fig. 4 Representative phenocam snapshots (left panels) and modelled relative foliage distribution function (right panels) for the different seasons/ stages considered in this study: bud-break, spring, summer and leaf-off



GALL -PN

(a) Bud-break

1DAY

FEB.11,15 09:00 AM



(e) Summer

(1 TAS -BROC DEC.14,15 03:00 PM 1DAY

(g) Leaf-off



 $f_a(z/h)$

0.4

0.6



(f) Summer

1.0

0.8

0.6 u/z0.4

0.2

0.8

0.2

(d) Spring

 $f_a(z/h)$









Fig. 5 Scatterplot of modelled (x axis) vs. measured wind from the eddy covariance 3D sonic anemometer (y axis) at 1.45 m in the interrow space for **a** Goudriaan (1977) and **b** Massman et al. (2017). The plotted line represents a 1:1 relationship



(**a**) Goudriaan (1977)



(**b**) Massman et al. (2017)

Table 2 Error assessment of wind speed at 1.45 m ($u_{z,ref}$, m s⁻¹) using Goudriaan (1977) and Massman et al. (2017) wind attenuation profiles

Site	Model	Bias	MAE	RMSE	RMSE _u	RMSE _s	R^2
N	Goudriaan (1977)	0.01	0.08	0.11	0.10	0.03	0.86
	Massman et al. (2017)	0.05**	0.10*	0.12	0.11	0.05	0.86
S	Goudriaan (1977)	0.05	0.12	0.15	0.13	0.07	0.87
	Massman et al. (2017)	0.13**	0.17**	0.21**	0.16	0.13	0.86
Both	Goudriaan (1977)	0.03	0.10	0.13	0.12	0.05	0.87
	Massman et al. (2017)	0.10**	0.14**	0.17**	0.15	0.10	0.85

Error metrics significantly different between Massman et al. (2017) and Goudriaan (1977) are flagged with an asterisk (*) when Student's *t* test showed that averages were significantly different at 95% confidence, and with a double asterisk (**) at 99% confidence

the in situ horizontal wind speed from the sonic anemometer placed at 1.45 m agl. The scatterplot shows that $u_{z,ref}$ modelled with Goudriaan (1977) fits closer to the 1:1 line compared to Massman et al. (2017). This surprising result is numerically shown in Table 2, which lists the error statistics for IOPs in 2015 when the below-canopy EC system was operating. Goudriaan (1977) has a higher coefficient of determination (i.e., higher R^2), it yields significantly lower errors, with bias closer to 0 than Massman et al. (2017) and lower Mean Absolute Error and Root Mean Square Error.

Table 2 indicates a slight-to-moderate better performance with the original Goudriaan (1977) wind speed at 1.45 m agl, a height at which the attenuation due to the grapevine is significant. In fact, a comparison of the wind attenuation profiles using Massman et al. (2017) and Goudriaan (1977) is shown in Figs. 6 and 7 illustrate the wind attenuation profiles of Goudriaan and Massman for a canopy with total LAI = 2 and a canopy height of 2 m. Figure 6 represents the four different attenuation profiles corresponding to the foliage densities used in this study and previously illustrated in Fig. 4. Comparison between the two figures demonstrates more clearly the effect of non-uniform vertical profile, particularly near the soil surface. Furthermore, Massman et al. (2017) attenuation profiles also significantly differ between growth stages, with very little attenuation at the vine canopy/ trellis system before bud-break and after leaf-off. Since in the summer stage the grapevine canopy is well developed, spreading towards both the interrow and the ground (see Fig. 4e, f), its attenuation becomes more uniform compared to earlier in the growing season (Fig. 6b vs. Fig. 6c). Finally, it is worth noting that Goudriaan (1977) attenuation profile (Fig. 7) seems to provide unrealistic values near the soil, as it has been observed that wind speed near the soil should tend to zero (Heilman et al. 1994, Fig. 5).

It is worth noting that the effect of wind direction on wind attenuation, which was already observed in vineyards by Heilman et al. (1994), is implicitly considered on the roughness dependence on the wind direction relative to the row orientation (Alfieri et al. 2018a). Figure 8 shows a typical wind attenuation profile when wind direction is parallel to the rows (i.e., down-row wind, dashed red line) and perpendicular to the rows (i.e., cross-row wind, dotted blue line). This figure shows a stronger attenuation, both above and below the canopy, when wind blows in the cross-row direction, and is an effect that is in agreement with the observations from Heilman et al. (1994, Fig. 4)

Evaluation in TSEB

The TSEB sensible heat flux estimates (H) using Massman and Goudriaan wind profiles are compared to measured 15 min flux data for both sites between years 2014 and

Fig. 6 Massman et al. (2017) wind profile attenuation $(u(z)/u(h_c))$ for a leaf area index, LAI = 2, and canopy height $h_c = 2$ m, corresponding to the relative foliage distributions shown in Fig. 4. Red dots indicate relevant heights for this study (z_{ref} , $z_{d_0+z_{0M}}$ and $z_{0,soil}$). (Color figure online)

2.0

1.5

Ξ́1.0

0.

0.8

0.2



Fig.7 Goudriaan (1977) wind profile attenuation $(u(z)/u(h_c))$ for a leaf area index, LAI = 2, canopy height $h_c = 2$ m and leaf width $l_{\rm w} = 0.1$ m. Red dots indicate relevant heights for this study ($z_{\rm ref}$, $z_{d_0+z_{0M}}$ and $z_{0,soil}$). (Color figure online)

2016. The model inter-comparison is evaluated for H only since errors in R_n and G will add noise and H is directly computed by TSEB while λE is solved as a residual. Table 3 lists the sensible heat flux H error statistics corresponding to the TSEB runs using either Goudriaan (1977) or Massman et al. (2017) models. Error metrics include the 3 years studied (2014-2016) for the two sites. Despite of the fact that Table 2 showed a better accuracy in wind speed at 1.45 m for Goudriaan (1977) model, comparison between attenuation

8.0 0.5 3.0 1.0 1.5 2.0 2.5 3.5 u(ms)-1)

Fig. 8 Standard wind profiles u estimated for both the down-row direction (dotted red line) and cross-row direction (dashed blue line). Profiles assume neutral conditions, 3.5 m s⁻¹ wind speed at 5 m above ground level, and a standard vineyard canopy with LAI = 2 and other canopy parameters retrieved based on curves of Fig. 2. The horizontal line represents the canopy height, below which the Massman et al. (2017) attenuation profile was applied. (Color figure online)

profiles implemented in TSEB did not show any significant difference, except Goudriaan (1977) attenuation showing a mean bias closer to zero, and Massman et al. (2017) having a larger R^2 , but both models yielding similar RMSE of 42–43 W m⁻² and 41–42 W m⁻² for the north (N) and south Table 3Error statisticsfor estimates of H runningTSEB with Goudriaan (1977)and Massman et al. (2017)attenuation profiles

Error measurements expressed in W m⁻². Error metrics significantly different between Massman et al. (2017) and Goudriaan (1977) are flagged with an asterisk (*) when Student's *t* test showed that averages were significantly different at 95% confidence, and with a double asterisk (**) at 99% confidence

 Table 4
 Error statistics for estimates of H at local noon for the period 2014–2016 running TSEB with Goudriaan (1977) and Massman et al. (2017) attenuation profiles

Model	Bias	MAE	RMSE	RMSE _u	RMSE _s	R^2
Goudriaan (1977)	- 16	41	54	45	31	0.49
Massman et al. (2017)	- 22**	40	54	40	37	0.50

Error measurements expressed in W m⁻². Error metrics significantly different between Massman et al. (2017) and Goudriaan (1977) are flagged with an asterisk (*) when Student's *t* test showed that averages were significantly different at 95% confidence, and with a double asterisk (**) at 99% confidence

(S) sites, respectively. Conversely, TSEB errors seem to be slightly larger for the N site, with larger bias, MAE, RMSE and R^2 than in the S site. Moreover these errors are fairly consistent between the years (results not shown), which indicates some degree of robustness in TSEB modelling.

Results listed in Table 3 give the performance for all in situ observations measured during daytime (i.e., $S_{\rm dn} > 100 \,{\rm W}\,{\rm m}^{-2}$). To allow a more straightforward comparison against model performance from other studies that were using satellite or airborne data, Table 4 shows similar statistics for both wind profiles at local noon (12 PM), time near the acquisition time of most of sun-synchronous satellites (see Kustas et al. (2018a), Nieto et al. (2018) or Knipper et al. (2018) in this issue for detailed discussions on errors in TSEB and comparison with published literature). Again, wind attenuation schemes yield the same error statistics with 41 W m⁻² MAE, 55 W m⁻² RMSE, and a determination coefficient of 0.50. Only mean bias showed significant differences between attenuation profiles, with Goudriaan (1977) model showing lower bias (-16 W m⁻²) compared to Massman et al. (2017) profile (-22 W m^{-2}).

Nevertheless, a more detailed seasonal analysis of error assessment for both attenuation models was performed where the whole timeseries for both Goudriaan (1977) and Massman et al. (2017) TSEB implementations are separated by the different growth stages described in "Estimation of daily canopy properties". Table 5 lists the errors, for what we defined "spring" or bud-break through flowering stage (between 15 March and 1 May). Results for the other stages

are not shown in Table 5 as no significant differences were found between models.

Results in Table 5 indicate that at this stage, when grapevine canopy is more vertically clumped and there is still a photosynthetic grass layer (Fig. 4c, d), most of the error statistics for modelled sensible heat flux are significantly (based on the t test statistic) reduced with Massman et al. (2017) wind profile. This fact is evident in the S site, with a reduction of 84% in bias, 22% in MAE, and 26% in RMSE. These results confirms the observations by Cammalleri et al. (2010), who stated that within-canopy wind profile modelling has a larger impact in TSEB estimated H for sparse and clumped vegetation. Actually, the wind profile modelled for the spring or early vine growth stage in Fig. 6b seems quite distinct compared to Goudriaan (1977) exponential attenuation (Fig. 7), causing significantly different wind speeds at both canopy sink/source height (i.e., at $d_0 + z_{0M}$) and near the soil surface $(z_{0,\text{soil}})$. This issue is confirmed in Fig. 9, where modelled wind speed at these two relevant heights (Fig. 9a, b) and their corresponding estimated resistances to heat transport (Fig. 9c, d) are quite different using Goudriaan (1977) versus Massman et al. (2017).

Modelled wind speed near the soil surface consistently yields ca. two times lower values using Massman et al. (2017) (Fig. 9a), as in this model the wind speed attenuates asymptotically to zero near the soil surface (Fig. 6). This is reflected in the estimation of the resistance to heat transport near the soil layer, with overall larger R_s values in Massman et al. (2017) (Fig. 9c), but those differences are not as strong

Table 5Springtime errorstatistics for estimates of Hrunning TSEB with Goudriaan(1977) and Massman et al.(2017) attenuation profiles

Site	Model	Bias	MAE	RMSE	RMSE _u	RMSE _s	R^2
N	Goudriaan (1977)	1	25	36	36	5	0.77
	Massman et al. (2017)	- 15**	25	36	29	22	0.79
S	Goudriaan (1977)	19	32	47	43	20	0.75
	Massman et al. (2017)	3**	25**	35**	34	6	0.77
Both	Goudriaan (1977)	10	28	42	41	10	0.74
	Massman et al. (2017)	- 6**	25**	35**	33	12	0.76

Error measurements expressed in W m⁻². Error metrics significantly different between Massman et al. (2017) and Goudriaan (1977) are flagged with an asterisk (*) when Student's *t* test showed that averages were significantly different at 95% confidence, and with a double asterisk (**) at 99% confidence



Fig. 9 Scatterplots between modelled wind speed (top) and resistances (bottom) using Massman et al. (2017) and Goudriaan (1977) profile models

as with u_s (Fig. 9c vs. Fig. 9a). This is due to the fact that R_s in TSEB not only depends on wind speed but also on the buoyancy near the soil, expressed as the temperature gradient between the soil surface and the overlying air (see A, Eq. 7b and Kustas and Norman 1999). Besides, small differences were found in modelled u_s between stages, since Massman et al. (2017) models the wind attenuation near the soil surface as a logarithmic function where canopy foliage plays a lesser role (Massman et al. 2017). On the other hand, significant differences are found in the estimation of wind speed at $d_0 + z_{0M}$ (Fig. 9b) and its related resistance to heat transport at the canopy boundary layer R_x . In spring, Massman et al. (2017), whereas in summer similar values

are produced in both models and larger speeds are usually modelled before grapevine bud-break and after leaf-off. This effect is directly affecting the estimation of R_x (Fig. 9d), with significantly different values in the modelled R_x between Goudriaan (1977) and Massman et al. (2017) during spring. Wind attenuation in the interrow was validated only during the IOPs showed in Table 1, which correspond mostly to dates during summer (after mowing of cover crop). Therefore we hypothesize that a larger improvement in the wind attenuation assessment would be observed in Table 2 and Fig. 5 if below-canopy wind speed measurements were available earlier in the season. Likewise, the "spring" stage is a relatively short period spanning from mid-March to early May or 1 1/2 months and hence its contribution to the overall



Fig. 10 Standard aerodynamic soil resistance R_s estimated at different wind directions relative to the row orientation using Massman et al. (2017) wind attenuation model. R_s was computed using Kustas and Norman (1999) equation for neutral conditions, 3.5 m s⁻¹ wind speed at 5 m above ground level, and a standard vineyard canopy with LAI = 2 and other canopy parameters retrieved based on curves of Fig. 2

performance in TSEB is relatively small, as seen in Tables 3 and 4. However this period is when decisions about water status in the root zone and initiation of irrigation is being made, so it is crucial to have an accurate accounting of water use by the vines and cover crop.

Based on the results in Fig. 8, the effect of wind direction on soil aerodynamic resistance is illustrated in Fig. 10. As expected, aerodynamic resistance near the soil surface is lower when wind is blowing parallel to the rows, as lower wind attenuation occurs (Fig. 8). This effect is also observed on the average conductance values (the reciprocal of resistances) measured at the soil surface by McInnes et al. (1996, Fig. 3). Both modelled (this study) and measured (McInnes et al. 1996) showed a sinusoidal increase (decrease) of soil resistance (conductance) when wind direction changes from parallel (0°) to perpendicular (90°) to the rows.

Finally, the fact that significant differences were found in R_s and primarily in R_x during spring are also reflected in latent heat flux partitioning between canopy transpiration and soil evaporation (Fig. 11). Massman et al. (2017) yields slightly lower values in $\lambda E_C / \lambda E$ (Fig. 11). These lower values in spring appear to be consistent with estimates coming from using the correlation-based flux partitioning method with the high-frequency eddy covariance data (Scanlon and Sahu 2008; Scanlon and Kustas 2010, 2012) summarized in Kustas et al. (2018a).

Discussion on irrigation management

Many studies on irrigation have quantified crop water needs using tabulated or empirically retrieved crop coefficient (Girona et al. 2006; Romero et al. 2014; Intrigliolo et al.



Fig. 11 Scatterplots and timeseries between modelled Massman et al. (2017) and Goudriaan (1977) latent heat flux partitioning $\lambda E_C / \lambda E$

2016; Zúñiga et al. 2018). This approach assumes that the water consumed for a given crop and phenological stage is linearly related to a grass or alfalfa reference evapotranspiration (e.g., Allen et al. 1998 FAO-56 or Walter et al. 2000 ASCE). However, the radiative and aerodynamic regime in a heterogeneous row crop is likely to deviate from these simple empirical relationships. Indeed this refined model, which also includes the effect of hedgerow structure in energy partitioning (Parry et al. 2018) as well as aerodynamic roughness variations with wind direction (Alfieri et al. 2018a), can be incorporated into a two-source energy combination model (Shuttleworth and Wallace 1985; Brenner and Incoll 1997) and estimate water use and energy use efficiency separately for the row crop and interrow. This would result in more a robust definition of crop water needs for future irrigation experiments. Moreover, this modelling framework could be further developed using a canopy conductance model to run simulations using different vineyard trellis configurations, vine varieties and management scenarios that would provide optimal solutions for designing row spacing and trellis systems when planting new vineyards in different climate regions.

On the other hand, regulated deficit irrigation (RDI) is a regular strategy in viticulture to submit a moderate stress to the vines thus increasing yield quality. Crop stress has been usually defined from measurements of water potential Ψ (either leaf, stem or pre-dawn, Flexas et al. 2004) and hence several studies have proposed Ψ thresholds when applying RDI (van Leeuwen et al. 2009; Girona et al. 2006; Intrigliolo et al. 2016; Merli et al. 2016). Nevertheless, these Ψ thresholds may vary depending on root distribution, vine vigour, yield, and/or isohydric/anisohydric varieties (van Leeuwen et al. 2009; Romero et al. 2010; Flexas et al. 2004). Therefore, other authors suggested that stomatal conductance g_s is a more precise and sensitive indicator of water stress than Ψ (Romero et al. 2010; Cifre et al. 2005). Measurements of g_s (Zúñiga et al. 2018; Romero et al. 2010; Cifre et al. 2005; Flexas et al. 2004) or sap-flow measurements (Eastham and Gray 1998; Ginestar et al. 1998; Patakas et al. 2005) have therefore been conducted as proxy for canopy transpiration and assimilation in RDI. With a correct ET partitioning in TSEB, robust and spatially distributed estimates of canopy transpiration can be obtained either from in situ (Kustas et al. 2018b), airborne (Nieto et al. 2018) or satellite (Knipper et al. 2018) data, from which it is possible to derive effective values of stomatal conductance from top-down approaches (Baldocchi et al. 1991), similar to the ones proposed in Jones et al. (2002), Leinonen et al. (2006), or Berni et al. (2009). This type of approach using Earth observations has a major advantage from traditional techniques used in vineyard water management in that it has the capability of mapping in a spatially distributed manner water use and stress conditions over large areas.

Conclusions

This study evaluated a new wind attenuation profile that explicitly considers the vertical heterogeneity in foliage distribution in canopies such as row crops. In a first stage, our results indicated that the Massman et al. (2017) profile did not improve the modelled wind speed in the interrow below the canopy in two, respectively, mature and young vineyards. However, when the new proposed wind profile was implemented in the Two Source Energy Balance model (Kustas and Norman 1999; Kustas et al. 2016), an improvement in the estimation of sensible heat flux was found during spring, when there coexist two vegetative layers, an upper horizontally discontinuous canopy with heterogeneous vertical distribution of foliage, and a lower more homogeneous grass layer of little height.

Similar to the findings of Cammalleri et al. (2010), wind profile attenuation modelling has been shown to have an effect on clumped canopies with moderate vegetation density. Before bud-break and after grapevine leaf-off, the canopy extinction effect is fairly small, while during summer, as the canopy in our study sites become well developed with a lower vertical and horizontal discontinuity, the new Massman et al. (2017) attenuation profile resembles more to the Goudriaan (1977) profile. The younger vineyard in the South gave a better performance with Massman et al. (2017) as its canopy is less developed, more clumped and with a larger influence of the cover crop layer in the interrow. Nevertheless, in future research additional sites will be evaluated under the hypothesis that Massman et al. (2017) profile has a larger potential use in more clumped canopies with more significant vertically non-uniform biomass distributions such as Vertical Shoot Position VSP vineyards,

tree wall (i.e., central leader system) orchards, as well as in wooded savannah.

Although the impact on irrigation and possible savings in water is not the focus or topic of this study—as this will depend on irrigation strategies (full irrigation, controlled deficit irrigation, support irrigation), as well as the available technology for irrigation and its efficiency—we believe that the improvement of irrigation systems will require integrating these types of energy balance models that can create evapotranspiration and transpiration maps with soil water balance models. This topic requires, therefore, a separate study and paper. In addition, more reliable ET partitioning using two-source energy balance models with the proposed wind attenuation profile will be necessary to account more accurately, crop water use and requirements.

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Appendix: TSEB model

The basic equation of the energy balance at the surface can be expressed following Eq. 4.

$$R_n \approx H + \lambda E + G \tag{4a}$$

$$R_{n,\rm S} \approx H_{\rm S} + \lambda E_{\rm S} + G \tag{4b}$$

$$R_{n,\mathrm{C}} \approx H_{\mathrm{C}} + \lambda E_{\mathrm{C}} \tag{4c}$$

with R_n being the net radiation, H the sensible heat flux, λE the latent heat flux or evapotranspiration, and G the soil heat flux. "C" and "S" subscripts refer to canopy and soil layers, respectively. The symbol " \approx " appears since there are additional components of the energy balance that are usually neglected, such as heat advection, storage of energy in the canopy layer or energy for the fixation of CO₂ (Hillel 1998).

The key in TSEB models is the partition of sensible heat flux into the canopy and soil layers, which depends on the soil and canopy temperatures ($T_{\rm S}$ and $T_{\rm C}$, respectively). If we assume that there is an interaction between the fluxes of canopy and soil, due to an expected heating of the in-canopy air by heat transport coming from the soil, the resistances network in TSEB can be considered to be in series. In that case *H* can be estimated as in Eq. 5 (Norman et al. 1995, Eqs. A1–A3)

$$H = H_{\rm C} + H_{\rm S} = \rho_{\rm air} C_{\rm p} \frac{T_{\rm AC} - T_{\rm A}}{R_{\rm a}}$$
$$= \rho_{\rm air} C_{\rm p} \left[\frac{T_{\rm C} - T_{\rm AC}}{R_{\rm x}} + \frac{T_{\rm S} - T_{\rm AC}}{R_{\rm s}} \right]$$
(5)

where ρ_{air} is the density of air (kg m⁻³), C_p is the heat capacity of air at constant pressure (J kg⁻¹ K⁻¹), T_{AC} is the air temperature at the canopy interface, equivalent to the aerodynamic temperature T_0 , computed with Eq. 6 (Norman et al. 1995, Eq. 4).

$$T_{\rm AC} = \frac{\frac{T_{\rm A}}{R_{\rm a}} + \frac{T_{\rm C}}{R_{\rm x}} + \frac{T_{\rm S}}{R_{\rm s}}}{\frac{1}{R_{\rm a}} + \frac{1}{R_{\rm x}} + \frac{1}{R_{\rm s}}}.$$
(6)

Here R_a is the aerodynamic resistance to heat transport (s m⁻¹), R_s is the resistance to heat flow in the boundary layer immediately above the soil surface (s m⁻¹), and R_x is the boundary layer resistance of the canopy of leaves (s m⁻¹). The mathematical expressions of these resistances are detailed in Eq. 7 and in Norman et al. (1995) and Kustas and Norman (2000) and discussed in Kustas et al. (2016).

$$R_{\rm a} = \frac{\ln\left(\frac{z_T - d_0}{z_{0H}}\right) - \Psi_h\left(\frac{z_T - d_0}{L}\right) + \Psi_h\left(\frac{z_{0H}}{L}\right)}{\kappa' \, u_*} \tag{7a}$$

$$R_{\rm s} = \frac{1}{c(T_{\rm S} - T_{\rm A})^{1/3} + b\,u_{\rm s}} \tag{7b}$$

$$R_{x} = \frac{C'}{\text{LAI}} \left(\frac{l_{\text{w}}}{U_{d_{0}+z_{0\text{M}}}} \right)^{1/2}$$
(7c)

where u_* is the friction velocity (m s⁻¹) computed as:

$$u_* = \frac{\kappa' u}{\left[\ln\left(\frac{z_u - d_0}{z_{0M}}\right) - \Psi_m\left(\frac{z_u - d_0}{L}\right) + \Psi_m\left(\frac{z_{0M}}{L}\right)\right]}.$$
(8)

In Eq. 8 z_u and z_T are the measurement heights for wind speed u (m s⁻¹) and air temperature T_A (K), respectively. d_0 is the zero-plane displacement height, z_{0M} and z_{0H} are the roughness length for momentum and heat transport, respectively (all those magnitudes expressed in m), with $z_{0H} = z_{0M} \exp(-kB^{-1})$. In the series version of TSEB z_{0H} is assumed equal to z_{0M} since the term R_x already accounts for the different efficiency between heat and momentum transport (Norman et al. 1995), and therefore $kB^{-1} = 0$. The value of $\kappa' = 0.4$ is the von Karman's constant. The $\Psi_m(\zeta)$ terms in Eqs. 7a and 8 are the adiabatic correction factors for momentum. The formulations of these two factors are described in Brutsaert (1999, 2005). These corrections depend on the atmospheric stability, which is expressed using the Monin–Obukhov length L (m):

$$L = \frac{-u_*^3 \rho_{\rm air}}{\log \left[\frac{H}{(T_{\rm A}C_{\rm p})} + 0.61E \right]}$$
(9)

where *H* is the bulk sensible heat flux (W m⁻²), *E* is the rate of surface evaporation (kg s⁻¹), and *g* the acceleration of gravity (m s⁻²).

The coefficients *b* and *c* in Eq. 7b depend on turbulent length scale in the canopy, soil-surface roughness and turbulence intensity in the canopy, which are discussed in Sauer et al. (1995), Kondo and Ishida (1997) and Kustas et al. (2016). *C'* is assumed to be 90 s^{1/2} m⁻¹ and l_w is the average leaf width (m).

Wind speed at the heat source–sink $(z_{0M} + d_0)$ and near the soil surface was originally estimated using Goudriaan (1977) wind attenuation model (Eq. 10)

$$U(z) = U_{\rm C} \exp\left[-a_G \left(1 - z/h_{\rm c}\right)\right] \tag{10}$$

$$a_G = 0.28 \text{LAI}^{2/3} h_c^{1/3} l_w^{-1/3}.$$
 (11)

Since Eqs. 5–9 are interrelated, an iterative scheme is performed until the convergence of *L* and u_* is reached. The iterative process is as follows: neutral conditions are firstly assumed $(L \to \infty, \Psi_M(\zeta) = 0$ and $\Psi_H(\zeta) = 0)$ and an initial estimate of *H* is calculated using Eqs. 8 to 5, and *E* with Eq. 4. An initial value of *L* is then obtained from Eq. 9 and the stability functions are then calculated, which gives a new friction velocity (Eq. 8) and resistance set (Eq. 7) and new estimates of *H* and *E* (Eqs. 6, 5 and 4). *L* is recalculated again and the process continues (Eqs. 9–5) until the change in *L* and u_* between two successive iterations is lower than a certain threshold.

When only a single observation of $T_{\rm rad}$ is available (i.e., measurement at a single angle), partitioning of $T_{\rm rad}$ requires some assumptions to help to define $T_{\rm C}$ or $T_{\rm S}$. One approach developed for TSEB (Norman et al. 1995) starts with an initial estimate that assumes plants are transpiring at a potential rate, as defined by the Priestley and Taylor (1972) relationship, applied to the canopy divergence of net radiation ($R_{n,{\rm C}}$)

$$\lambda E_{\rm C} = \alpha_{\rm PT} f_{\rm g} \frac{\Delta}{\Delta + \gamma} R_{n,\rm C} \tag{12}$$

where $\alpha_{\rm PT}$ is the Priestley–Taylor coefficient, initially set to 1.26, $f_{\rm g}$ is the fraction of vegetation that is green and hence capable of transpiring, Δ is the slope of the saturation vapor pressure versus temperature curve, and γ is the psychrometric constant. This allows the canopy-sensible heat flux to be calculated using the energy-balance at the canopy layer ($H_{\rm c} = R_{n,\rm C} - \lambda E_{\rm C}$) and hence an estimate of $T_{\rm C}$ to be obtained by inverting Eq. 5 (Norman et al. 1995, Eqs. A7, A11 and A12). Then $T_{\rm S}$ is the derived from Eq. 13 having both $T_{\rm rad}$ and $T_{\rm C}$ and an estimate of $f_{\rm c}(\theta)$ the fraction of vegetation observed by the sensor view zenith angle θ .

$$T_{\rm rad}^4(\theta) = f_{\rm c}(\theta)T_{\rm C}^4 + [1 - f_{\rm c}(\theta)]T_{\rm S}^4.$$
 (13)

The value of $f_c(\theta)$ is typically estimated as an exponential function of the leaf area index, which includes a clumping factor or index Ω for row crops and canopies where the LAI is concentrated for plants sparsely distributed or are organized such as row crops (Kustas and Norman 1999; Anderson et al. 2005) and has the following form.

$$f_{\rm c}(\theta) = 1 - \exp\left(\frac{-0.5\Omega LAI}{\cos\theta}\right). \tag{14}$$

If the initial $T_{\rm C}$ implied by this approximation is unusually low in comparison with the observed $T_{\rm rad}$, $T_{\rm S}$ will likely be overestimated and therefore produce unrealistic estimates of soil latent heat flux (negative values during daytime). In this case, the $\alpha_{\rm PT}$ coefficient is iteratively reduced assuming the canopy is stressed and transpiring at sub-potential levels until soil latent heat flux becomes zero or positive.

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