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# Salt crystallization in pores: quantification and estimation of damage

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**Abstract** The objective of this study is to understand and predict the alteration of porous rock by crystallization of salts. Samples of different rocks have been tested according to the EN 12370 standard test. Two parameters are proposed to evaluate the alteration of a rock during these tests. The alteration index AI represents the cycle in which the first damages occur. The alteration velocity AV represents the alteration rate at the end of the experiment, when the decay has become regular. These parameters can be estimated with the help of a microstructural study of the rocks. The most relevant intrinsic parameters of the stones for this estimation are capillary coefficient, evaporation coefficient, tensile strength and P-waves velocity. An evaluation of the alteration pattern is also proposed depending on the eventual heterogeneities and anisotropies of the rocks. The influence of the dimension and shape of the samples is also discussed.

**Keywords** Salt crystallization · Alteration · Quantification · Estimation · Evaporation · Durability

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## Introduction

Salts, and particularly sodium sulphate, are known to be among the most destructive agents in porous stones, concrete or brick weathering. Their study is thus very important to fully understand their crystallization process in porous networks and, in the future, to find a way to prevent or limit their damage to porous materials. Recent studies attribute the decay to the salt crystallization pressure of mirabilite (Na<sub>2</sub>SO<sub>4</sub>·10H<sub>2</sub>O), rather than thenardite (Na<sub>2</sub>SO<sub>4</sub>) (Rodriguez-Navarro and Doehne 1999; Scherer 1999; Flatt 2002; Benavente et al. 2004a; Steiger 2005). This damage depends on the quantity of salt in the stone as well as the characteristics of the porous network (a review can be found in Steiger 2005).

This study aims to evaluate building stone behaviour during accelerated ageing, and to understand how the porous network is affected. Then weathering will be quantified by few intrinsic parameters and evaluated thanks to a microstructural study. A review about estimation of damage can be found in Benavente et al. (2004b). Most of the existing estimators evaluate weathering with only one parameter. This study proposes two parameters, the alteration index (AI) and the alteration velocity (AV), to quantify weathering, and a method to preview how these damages will be organised in the stone. The influence of the shape and dimensions of the samples is also discussed.

### Materials and methods

## Materials

Nine stones from different lithologies have been used in this study: four limestones and five sandstones. The

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four limestones come from the Parisian Basin. Three of them are of lutetian age: the "roche fine" (FL), the "roche franche" (RL) and the "liais" (LL). These three limestones have high porosity compared to the other stones in this study (respectively 37.2, 18.5 and 14.4%). FL is a detritic limestone made of calcite (90%) and quartz (10%). Its tensile strength is very low (1.5 MPa). RL and LL are two boundstones composed by more than 90% of calcite, with traces of iron oxides. They also contain some macrofossils (bivalves, gasteropods) responsible of an heterogeneous aspect. The other limestone is of bartonian age: the "Pierre de Souppes" (SL), a variety of the "Calcaire de Chateau-Landon". It is just made of calcite. Its porosity is low (4.2%) and its tensile strength high (5.2 MPa).

Two sandstones are Fontainebleau sandstones (Oligocene). These two varieties are called hard (HF) and soft (SF). They are composed of more than 99% of quartz. Their porosity is low (respectively 4.1 and 5.5%). The main difference between the two is their tensile strength: very high for HF (5.2 MPa) and very low for SF (1.5 MPa). The three others sandstones are three layered sandstones: one from China, the white sandstone (CS); and two from India: the green sandstone (VS) and the brown sandstone (MS). The white sandstone is composed of more than 99% of quartz. The two others are also composed mostly of quartz, but contain some clay which give the general colour of the rock. All three sandstones present a very high tensile strength (6.1, 15.0 and 16.0 MPa) and low porosity (2.6, 4.5 and 4.7%). Complete hydromechanic properties of these nine sedimentary rocks are given in Table 1.

The capillary coefficient *C* is the sorptivity expressed in  $g/m^2/s^{1/2}$ . The evaporation coefficient *E* is also expressed in  $g/m^2/s^{1/2}$ , and corresponds to the slope of the curve representing the weight loss as a function of the square root of time. This parameter is related to the

**Table 1** Hydromechanic properties of the nine stones

diffusive part of evaporation (second stage), during which the external conditions (temperature, relative humidity, wind) have no influence (Hammecker 1993).

## Methods

Two experiments have been performed according to the EN 12370 (1999) standard about stone resistance to crystallization of salts in pores. They differ in the size and shape of the samples and in the number of cycles. They are composed of cycles which last 24 h:

- 2 h of immersion in a saturated solution with respect to sodium sulfate (14%);
- 15 h of drying at 105°C in order to prevent mirabilite crystallization during drying of the samples (Fig. 1);
- 7 h of cooling at room temperature (20–25°C, 30– 40% relative humidity RH). The samples were weighed after 2 h during this stage.

The first test concerns  $4 \times 4 \times 4$  cm<sup>3</sup> cubes with two samples per type of stone (18 cubes in total). The test has been run for 30 cycles. In the second test, cylinders of 2.5 cm diameter and 4.5 cm height were used. Two samples of each stone were used for all stones except FL (five samples), SF (four samples) and WS (one sample), i.e. 22 cylinders. Most of the samples suffered 15 cycles except one sample of FL and one of RL (11 cycles).

## Results

Quantification of alteration

## Representation of results

For each sample, results are plotted in diagrams showing normalized weight versus number of cycles.

		()	(%)	density (g/cm <sup>3</sup> )	coef. $(g/m^2/s^{1/2})$	coef. $(g/m^2/s^{1/2})$	radius (µm)	velocity (m/s)	strength (Mpa)
Limestones I	Liais (St Maximin), LL	14.4	58.2	2.3	26.7	32.25	0.444	4879	4.2
F	Roche franche (St Maximin), RL	18.5	59.7	2.2	40.7	37.55	4.710	4645	3.0
F	Roche fine (St Maximin), FL	37.2	75.9	1.7	66.9	1106.1	12.004	2898	1.5
P	Pierre de Souppes, SL	4.2	55.0	2.57	8.0	1.47	0.082	6249	5.2
Sandstones F	Hard Fontainebleau, HF	4.1	29.0	2.54	15.4	6.39	2.866	3903	5.2
S	Soft Fontainebleau, SF	5.5	48.2	2.5	12.6	40.12	3.761	1514	1.5
V	White, CS	2.6	94.2	2.6	6.4	5.45	0.310	3329	6.1
(	Green, VS	4.5	88.3	2.54	12.3	5.81	0.047	4598	15.0
E	Brown, MS	4.7	81.5	2.53	10.5	3.86	0.034	5115	16.0



Fig. 1 Phase diagram of mirabilite (after Flatt 2002, data from Kracek 1928)

Three representative examples of those graphs are presented on Fig. 2a, b and c. All the samples show the same evolution as a function of time. It can be described in two or three stages that are:

- stage I: weight increase due to salt supply;
- stage II (sometimes inexistent, starts after the first visual damage): weight variation depending on a competition between salt supply and stone damage. It can be either a weight increase or decrease;
- stage III: weight decrease because salt uptake becomes negligible compared to stone damage.

## The alteration index

The alteration index (AI; Angeli et al. 2006) is defined as the number of the cycle during which the first visible damage occurs (Table 2). This damage, which is firstly esthetical, may imply a change of physical properties, and happens for the first time when the crystallization pressure is high enough to alter the stone. AI depends only on water circulation possibility, and on mechanical strength (the tensile strength, which evaluates the cohesion between the grains). According to AI, it is possible to classify the nine studied rocks into three categories:

- high AI (19 and more in experiment 1, 10 and more in experiment 2): SL, HF, MS;
- medium AI (10–18 in experiment 1, 5–9 in experiment 2): LL, RL, CS, VS;
- low AI (up to 8 in experiment 1, up to 5 in experiment 2): FL, SF.

AI does not represent exactly the stone resistance to salt crystallization, since some stone can present visual damage rapidly and alter slowly afterwards (e.g. VS



**Fig. 2 a** Normalized weight evolution during the 30 cycles (first test) of a sample of VS. **b** Normalized weight evolution during the 30 cycles (first test) of a sample of SF. **c** Normalized weight evolution during the 30 cycles (first test) of a sample of FL

with relatively low AI compared to its actual durability). On the opposite, some stones can seem rather resistant at first, have no visual damage during few cycles, and then totally break down in three or four cycles (e.g. CS with relatively high AI compared to its durability). This observation leads to the introduction of the concept of alteration velocity (AV).

## The alteration velocity

The alteration velocity (AV) is introduced to evaluate the process of weathering in longer term than AI. **Table 2**Alteration indexand alteration velocity for thetested samples

	Experience 1 (cubes)			Experience 2 (cylinders)			
		Alteration index	Alteration velocity		Alteration index	Alteration velocity	
Liais, LL	L7	19	1.33	L3	8	0.19	
	L8	13	1.93	L4	9	0.25	
Roche franche, RL	<b>R</b> 7	17	3.78	R3	7	4.32	
	<b>R</b> 8	11	3.62	R4	7	2.80	
Roche fine, FL	F7	3	1.81	F1	3	8.25	
	F8	3	2.40	F3	3	9.52	
				F4	3	8.58	
				F5	4	8.14	
				F6	3	9.18	
Pierre de Souppes, SL	<b>S</b> 1	19	0.07	S2	13	0.10	
	S2	20	0.13	<b>S</b> 3	12	0.05	
Hard Fontainebleau, HF	D1	19	0.06	D2	12	0.46	
	D2	19	0.10	D3	10	0.12	
Soft Fontainebleau, SF	T1	6	4.02	T1	2	43.90	
	T2	5	10.93	T4	2	29.71	
				T5	2	32.77	
				T6	3	31.63	
White sandstone, CS	C1	15	5.94	C3	9	5.81	
,	C2	13	8.10				
Green sandstone, VS	V1	16	0.30	V2	9	0.68	
,	V2	17	0.34	V3	9	0.59	
Brown sandstone, MS	M1	23	0.16	M1	12	0.17	
, -	M2	23	0.16	M3	11	0.30	

Mostly, in usual characterization of weathering, only the dry weight loss of samples at a certain stage is used (EN 12370). But the results can be very different if the experiment is stopped after 10 or 20 cycles. AV is used to evaluate the long-term behaviour of the stone independently of the number of cycles. It is the final value of the derivative of the function representing the normalized weight as a function of the number of cycles (Table 2). The nine stones can also be classified by their AV:

- low AV (up to 1% weight/cycle for both experiments): SL, HF, VS, MS;
- medium AV (1-5 in experiment 1, 1-10 in experiment 2): LL, RL, FL;
- high AV (5 and more in experiment 1, 10 and more in experiment 2): SF, CS.

It is important to notice that the classification is different for AI and AV indicating that these two parameters are independent of each other. It suggests that these two parameters must be used together in order to evaluate more accurately the ageing of the stone.

# Alteration pattern

A careful observation of samples through weathering cycles allows to distinguish two different categories of alteration patterns.

# Homo/heterogeneity

It is possible to evaluate the regularity of the weathering of a set of samples from the same type of stone. Some stones present a regular weathering, starting with the progressive smoothing of corners and edges. This type of weathering is regarded as homogeneous, which means it is regular for one sample and approximately the same from a sample to another. Figure 3a gives a good example of this alteration for the FL. The stones which present a homogeneous behaviour are FL, SL and HF.

On the other hand, some stones present various alteration behaviours from one sample to another from the same type of rock, even from one zone to another in a single sample. This is due to pre-existent heterogeneities in the rock. These heterogeneities act as local weaknesses, and thus differential weathering can occur. These weaknesses can be obvious (e.g. fossils in RL or LL) or hidden (e.g. very competent zone in SF, Fig. 3b). They can either consolidate or weaken the sample. For instance, a fossil creates a weak zone and when this zone breaks, the entire fossil can fall at once, even if the fossil itself is not altered. The stone with a heterogeneous decay are LL, RL and SF.

Anisotropy The second type of alteration pattern concerns anisotropy. It means that alteration has a favourite direction for a stone (Fig. 3c). Anisotropy is

Fig. 3 a Sample of FL after 15 cycles: homogeneous behaviour. b Sample of SF after 15 cycles: heterogeneous behaviour. c Sample of VS after 15 cycles: anisotropic behaviour



an intrinsic property of the material and if it exists, it controls the anisotropy of decay. Four different origins can be identified: the grains (mineral composition due to sedimentation, shapes and orientation), the pores (shape, orientation), the joints and the fractures. This predisposition will influence the decay in several ways: for example, layers that contain hygroscopic clays can cause damage during imbibition, less competent layers can be damaged easier by salt crystallization pressure, cracks can act as a localisation of crystallization and thus of damage... The stones from this study which present anisotropy in the decay are CS, VS and MS.

# Discussion

# The stages of accelerated ageing

The duration and importance of the three stages of accelerated ageing (I, II, III) depend on the microstructure of the stone. During stage I, weight increase depends mainly on the characteristics of the porous network (porosity, pore size distribution...). The process of crystallization in pores starts during evaporation. At first, all the pores that can be reached by capillary rise are filled with the brine. During the first stage of evaporation, the capillary phase, the solution and the ions it contains are driven out of the porous



Fig. 4 Stages in the wetting of a porous system (Beck et al. 2003, after Rose 1963)

network. This means that all the salt here only crystallizes as efflorescences on the surface of the samples. The most important stage of evaporation starts at this moment: when the continuity of water is broken in the sample, the diffusion stage of evaporation starts (Fig. 4). The water starts to circulate as vapour in the porous network, thus allowing salts to crystallize in pores. Stage I stops as soon as enough salt has crystallized in pores to allow further supersaturation and cause damage to the sample (Flatt 2002).

Then there are two possibilities: the first visual damage is either before the loss of weight or after. When the first visual damage occurs before the loss of weight, there is still room in the sample for salt to crystallize, and the loss of material is inferior to its salt uptake. The weight variation is then a competition of these two processes, and there is a stage II. When the loss of weight occurs first, it means that most of the room where salt can crystallize has been filled up. The damage starts when the stresses created by the crystallization pressure and transmitted through the supersatured solution is higher than the stone's tensile strength, and in this case there is no stage II.

Phase III starts when the relationship between normalized weight and the number of cycles starts to become approximately linear (Fig. 2a, c), i.e. when the salt uptake starts to be negligible compared to material loss. More precisely, it is linear for homogeneous stones. For the heterogeneous stones, the curve shows several steps, which are each approximately linear, but separated by sudden drops (Fig. 2b). For instance, for RL or LL, these drops can be caused by the loss of an entire fossil.

# Estimators

## Alteration index

In order to estimate the alteration index, a decomposition of the process of accelerated salt weathering has been proposed. This decomposition is based on the existing works about the phase diagram of sodium sulphate (Flatt 2002) and on the drying kinetics presented in Fig. 7:

- imbibition of saline solution: pores are invaded by the brine;
- as relative humidity (RH) grows, thenardite hydrates into mirabilite by dissolution and reprecipitation (Rodriguez-Navarro et al. 2000) if temperature is below 32.5°C;
- with even higher RH, mirabilite is dissolved in the brine. Here stops the imbibition phase;

- evaporation starts with capillary evaporation and development of efflorescences;
- diffusive evaporation and crystallization of thenardite in the pores;

The crucial phase of this scheme is the crystallization of mirabilite in the pores after the dissolution of thenardite, when the temperature is below 32.5°C (Rodriguez-Navarro and Doehne 1999): this is the part of the cycle when the damages occur. The first damage will anyway appear on the weakest part of the sample. The only characteristics that matter are the hydric properties [capillary *C* and evaporation *E* coefficients both in g/m<sup>2</sup>/s<sup>1/2</sup>] and the mechanical strength of the weakest part of the rock (tensile strength  $\sigma_{\rm T}$  in MPa). This also corresponds to the parameters used in the estimation of the crystallization pressure for most models (Benavente et al. 2004b, Scherer 2004).

It is also important to recall that this study is only about sodium sulphate, and thus the estimator is only valid for damages induced by sodium sulphate crystallization. Figure 5a and b represent the estimator of AI (1) as a function of AI for the two experiments,

$$AI_{estim} = \ln \left(\frac{100C}{E\sqrt{\sigma_{T}}}\right).$$
(1)



Fig. 5 a Estimation of the AI for the first experiment. b Estimation of the AI for the second experiment

#### Alteration velocity

During stage III, the pores are considered to be always filled with salt and the supersaturation with respect to mirabilite reached at every cycle. The salts will crystallize and cause damages in the cracks and pores. Thus the more pre-existing cracks and pores in the rock, the more damage. And also the more cracks and pores in a rock, the lower the P-waves velocity ( $V_p$ ).

On the other hand, these damages will be more important if the joints between the grains are weak, since in this case the cohesion of the stone is lower. When the grains are weakly bonded, the loss of energy at the interfaces is higher and thus  $V_p$  decreases.

These two features have the same influence on  $V_{\rm p}$ . This means that  $V_{\rm p}$  can estimate the long term behaviour of a rock. Since this long term behaviour is given by AV,  $V_{\rm p}$  can be considered as a good trend for AV. However, the low values of the coefficient of determination of the linear regression ( $R^2$ ) given in Fig. 6a and b show that it can not still be considered as a good estimator.

A part of this error comes from the fact that the velocity of the P-waves is slightly different in quartz (6050 m/s) and calcite (6600 m/s). Another part also comes from the fact that one of the two cubes of SF turned out to be much more competent than the oth-



Fig. 6 a Estimation of the AV for the first experiment. b Estimation of the AV for the second experiment

ers, as competent as HF. If this value is withdrawn from the experimental values,  $R^2$  rises up to 0.61 (instead of 0.45). The presence of clays can also be very damaging to a stone while not having a strong influence on the estimator, and by this could make this estimation incorrect.

Nevertheless, this estimation can be useful because the P-wave velocity is non-destructive and easy to measure on-field, and a mineral analysis can help us to determine if this estimation is relevant or not.

Dimension effect

The resistance of a sample to salt decay has been estimated for both experiments. Now the importance of the dimension of the sample will be discussed.



Fig. 7 Simplified evaporation kinetics of two samples of the same volume but different dimensions. The same thickness of water evaporates in the two samples between two instants. The part of the sample which is wet is in *black*, the dry part is in *white* 

## Alteration index

As shown in the estimators part, evaporation is a very important phenomenon when it comes to salt crystallization in porous networks (Rodriguez-Navarro and Doehne 1999). When evaporation is impossible through a face of a sample, this face is not altered and the weathering of the whole sample is slowed down (Angeli et al. 2006). The easier the sample can be dried, the easier sodium sulphate can crystallize in the porous network.

For the same volume, the core of a sample will be dried faster if there is a dimension which is significantly smaller than the others. Figure 7 explains this fact in a very simple way. Hence, the smallest dimension of a sample will affect its resistance to salt weathering. It can be considered in multiplying the slope of the linear regression by the smallest dimension of a sample (4 cm for the first experiment, 2.5 cm for the second) for each experiment. It gives two values of 0.99 and 1.20 cm, which differ from 18% (the difference between the two slopes is 50%).

It is important to notice that this estimation is only relevant for the middle term behaviour. For the very short term, other parameters are to be taken into account: for instance, the cubes will alter faster than cylinders since there are more edges and corners.

# Alteration velocity

For a given sample, AV will depend on the total surface exposed to evaporation. The samples seem to lose a small thickness of grain on every side that was exposed to evaporation. During stage III, the samples seem to lose a small thickness of material during each cycle. By using the same approximation technique as in last paragraph, this fact can be estimated by dividing (not multiplying because a resistant stone has a low AV) the slope of the linear regression by the total surface of the sample (the samples are immersed in our experiments). It gives two values of 4.33 and 4.54 cm<sup>-2</sup>, which differ by 4.5% (the difference between the two slopes was 66%).

Nevertheless, those two evaluations need more data to be confirmed, with more shapes tested. In addition to that, the linear regressions in both cases are very approximate. Anyways, it is clear that the shape and size of a sample has an influence on its alteration. For a given volume, the most resistant shape is the one that minimizes the exposed surface and maximizes the smallest dimension, the sphere.

## Conclusion

A new way for evaluating accelerated ageing through crystallization of salt is proposed. It is composed of two parameters: alteration index (AI) and alteration velocity (AV). It is then possible to classify the different stones according to these two indicators: the results show that the stones that are the most resistant at first (high AI) are not necessarily the most resistant at the end (low AV). It allows to characterize the alteration during the whole test and not just at the end of it.

Another classification of alteration is also proposed. It takes into account the alteration patterns: homogeneous, heterogeneous or anisotropic. This can be estimated by a microstructural study of the stone.

The accelerated ageing can be decomposed into three stages. Stage I corresponds to the weight gain due to salt crystallization in the pores. Stage II, when it exists, is an intermediate stage during which there is a competition between salt supply and material loss. Stage III corresponds to the long term alteration, when the weight loss is approximately linear.

Two estimators have been given for respectively AI and AV. Those estimators underline the fact that it is crucial to perform a microstructural study of the stone to predict its weathering. The main result is that the Pwave velocity in the stone gives a good idea of the long term behaviour of the stone: the higher the P-wave velocity, the more resistant the stone.

The shape of a sample has also an important influence on its weathering through crystallization of salts because it directs the evaporation kinetics. A sample that has a significantly smaller dimension with respect to the two others will alter faster as more regular, the most resistant shape being the sphere.

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