## RESEARCH PAPER

# Multi-channel PMMA microfluidic biosensor with integrated IDUAs for electrochemical detection

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Received: 4 March 2013 /Revised: 12 April 2013 /Accepted: 24 April 2013 / Published online: 17 May 2013  $\oslash$  Springer-Verlag Berlin Heidelberg 2013

Abstract A novel multi-channel poly(methyl methacrylate) (PMMA) microfluidic biosensor with interdigitated ultramicroelectrode arrays (IDUAs) for electrochemical detection was developed. The focus of the development was a simple fabrication procedure and the realization of a reliable large IDUA that can provide detection simultaneously to several microchannels. As proof of concept, five microchannels are positioned over a large single IDUA where the channels are parallel with the length of the electrode finger. The IDUAs were fabricated on the PMMA cover piece and bonded to a PMMA substrate containing the microfluidic channels using UV/ozone-assisted thermal bonding. Conditions of device fabrication were optimized realizing a rugged large IDUA within a bonded PMMA device. Gold adhesion to the PMMA, protective coatings, and pressure during bonding were optimized. Its electrochemical performance was studied using amperometric detection of potassium ferri and ferro hexacyanide. Cumulative signals within the same chip showed very good linearity over a range of 0–38  $\mu$ M ( $R^2$ =0.98) and a limit of detection of 3.48  $\mu$ M. The bonding of the device was optimized so that no cross talk between the channels was observed which otherwise would

highly reproducible signals achieved were comparable to those obtained with separate single-channel devices. Subsequently, the multi-channel microfluidic chip was applied to a model bioanalytical detection strategy, i.e., the quantification of specific nucleic acid sequences using a sandwich approach. Here, probe-coated paramagnetic beads and probe-tagged liposomes entrapping ferri/ferro hexacyanide as the redox marker were used to bind to a single-stranded DNA sequence. Flow rates of the non-ionic detergent n-octyl-β-Dglucopyranoside for liposome lysis were optimized, and the detection of the target sequences was carried out coulometrically within 250 s and with a limit of detection of 12.5 μM. The robustness of the design and the reliability of the results obtained in comparison to previously published single-channel designs suggest that the multi-channel device offers an excellent opportunity for bioanalytical applications that require multianalyte detection and high-throughput assays.

have resulted in unreliable electrochemical responses. The

Keywords Microfluidic chip . Multi-channel . Electrochemical biosensor . Ultramicroelectrode . PMMA

Electronic supplementary material The online version of this article (doi:[10.1007/s00216-013-7020-0](http://dx.doi.org/10.1007/s00216-013-7020-0)) contains supplementary material, which is available to authorized users.

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Abbreviations



## Introduction

The Micro-Total Analysis System (μTAS), together with microfluidic technology, has become a highly promising tool for protein and nucleic acid analysis [[1](#page-8-0)–[3\]](#page-8-0). This is due to a number of advantages arising from the detection of biomolecules in a miniaturized system. Those include reducing sample/reagent and power consumption, providing high assay sensitivity with shorter analysis time, increasing repeatability and reliability by system automation, and rendering the integration capability for multiple processes within a single device [[4\]](#page-8-0).

Electrochemical detection is an ideal technique to incorporate into microfluidic devices as it possesses the inherent ability to be miniaturized by existing microfabrication technology and as it offers excellent analytical performance. In addition, the electrochemical response is independent from the optical path length or sample turbidity which is encountered in optical based techniques. Furthermore, low power consumption and cost effectiveness are additional advantages that make miniaturized electrochemical detection systems highly desirable and sustainable [[5](#page-8-0)–[7\]](#page-8-0).

Among the many electrochemical techniques, amperometry coupled with microelectrodes is ideally suited and widely employed in microfluidic chips [[8](#page-8-0)–[14](#page-8-0)]. Microelectrodes are of interest due to their small  $iR$  drop, fast establishment of steady-state mass transfer, and small capacitive charging currents [\[15\]](#page-8-0). In fact, the reduction of the electrode dimensions to micrometer size can greatly enhance their sensitivity, because a highly efficient collection of analyte species can be realized via nonplanar diffusion characteristics at microelectrodes [\[5](#page-8-0)]. This provides in turn an increased signal-to-noise ratio which thus enables lower detection limits and improved sensitivity.

Interdigitated ultramicroelectrode arrays (IDUAs), a pair of microband array electrodes that mesh with each other, is a microelectrode geometry that is particularly well suited for reversible and quasi-reversible redox species determinations [\[15](#page-8-0), [16](#page-8-0)]. A very small gap size between adjacent electrode fingers is considerably favorable for achieving high signal amplification owing to the increase of the diffusion flux of redox species, which consequently leads to an enhanced redox cycling, a decreased equilibrium time, and an increased collection efficiency [[17\]](#page-8-0). Previously, IDUAs have been characterized and studied as a transducer for electrochemical biosensors and have then been applied to a variety of bioanalytical systems in our research group [\[18](#page-8-0)–[22](#page-8-0)].

The development of multi-channel microfluidic chips has received much attention in recent years [\[23](#page-8-0)–[33](#page-9-0)] because it can increase the test throughput and can reduce production costs. Additionally, sample handling and analysis of multiple analytes within the same chip can substantially improve the analytical performance in terms of repeatability and reliability. However, there have been only few investigations toward the

fabrication of multi-channel electrochemical microfluidic chips. For examples, Chen and co-worker developed a multichannel microchip for simultaneously detecting multiparameter of diabetes mellitus [\[24\]](#page-8-0). Moreira and co-worker have developed a poly(dimethyl) siloxane/glass hybrid multi-channel microfluidic device with integrated electrodes for amperometric detection of N-acetyl-p-aminophenol [\[34\]](#page-9-0). However, their design encountered problems of incomplete sealing over the gold surface which led to leaking as soon as positive pressure was applied in the channels. This then considerably influenced the reproducibility of the electrochemical signals. While the authors have proposed a solution, their method is complicated and involves hydrofluoric etching, which is an undesirable fabrication method due to its immense toxicity.

Here, we consequently describe the very robust design and fabrication of multi-channel poly(methyl methacrylate) (PMMA) microfluidic chips with integrated IDUAs. In our design, a single IDUA is shared by five microchannels positioned in parallel with the length of the electrode finger. Five channels were chosen as model number only. Ten or more channels can easily fit across the same IDUA surface. Hot embossing and UV/ozone-assisted thermal bonding were employed for microchannel fabrication and chip assembly, respectively. The fabrication process was optimized with respect to gold adhesion, protective coating, and bonding conditions. The electrochemical performance evaluation of the microfluidic chip was carried out with respect to the cumulative signal response as well as the detection sensitivity. Furthermore, the reproducibility of the multi-channel device was compared to those of individual single-channel devices which were previously designed in our group [\[22\]](#page-8-0). Finally, we also demonstrated the capability of the multi-channel microfluidic chip for nucleic acid detection employing liposomes entrapping potassium ferri/ferro hexacyanide as a redox marker. Here, a well-developed bioanalytical detection strategy for the detection of RNA from Cryptosporidium parvum was chosen as model analyte [\[35](#page-9-0)–[37](#page-9-0)].

#### Experimental

## Materials and reagents

PMMA plates were purchased from Lucite International, Southampton, UK. Copper plates were purchased from McMaster Carr, Princeton, NJ. 2-Propanol, 2-(4-morpholino)-ethane sulfonic acid (MES), 1-ethyl-3-(3-dimethylaminopropyl) carbodiimide (EDC), sodium carbonate, potassium ferrocyanide  $(K_4Fe(CN)_6·3H_2O)$ , and potassium ferricyanide  $(K_3Fe(CN)_6)$ were purchased from Sigma-Aldrich, St. Louis, MO. N-Hydroxysulfosuccinimide (Sulfo-NHS) was purchased from G-Biosciences, St. Louis, MO. Cystamine was purchased from MP Biomedicals, Solon, OH. Silver conductive

epoxy was purchased from MG Chemicals, Burlington, ON. Cyanoacrylate-based adhesive was purchased from Henkel Consumer Adhesives, Avon, OH. Lipids and cholesterol were purchased from Avanti Polar Lipids, Alabaster, AL. n-Octyl-β-D-glucopyranoside (OG) was purchased from Alexis Corporation, Lausen, Switzerland. All oligonucleotides including cholesterol-tagged reporter probes were purchased from Operon, Huntsville, AL. Superparamagnetic beads (Dynabeads MyOne Streptavidin) were purchased from Dynal Biotech Inc., Lake Success, NY. Tygon® tubing and stainless steel blunt needles with Luer polypropylene hub were purchased from Small Parts Inc., Miami Lakes, FL. Syringes were purchased from Hamilton Company, Reno, ND. Magnets were purchased from National Imports LLC, Vienna, VA.

#### Design and fabrication of IDUAs

The pattern of the IDUAs depicted in Fig. [2c](#page-3-0) was designed using L-Edit CAD Software and the 5″ quartz photomask containing the IDUA pattern was fabricated using the 3600F PG Mask Writer. The total length and width of the IDUA pattern are 15 and 7 mm, respectively. The length and width of IDUA fingers are 3.9 mm and 10 μm, respectively, in the  $10 \text{ mm} \times 4 \text{ mm}$  central area of pattern. The gap between IDUA fingers is 5 μm.

The fabrication of IDUAs on PMMA was performed following the procedure described in [[22\]](#page-8-0) with slight modifications. Specifically, the PMMA plate was cut into a 50 mm×30 mm piece and sonicated in 50 % 2-propanol for 10 min to completely remove dust on the PMMA surface. The PMMA pieces were then washed in deionized (DI) water and dried with nitrogen prior to the UV exposure. A UV/ozone stripper (SAMCO International, Inc., Sunnyvale, CA) was used for the oxidation of PMMA to generate carboxylic groups on the surface. The PMMA pieces were immersed in the stripper, treated with UV (10 mW/cm<sup>2</sup> at 254 nm) for 5 min, and then placed in agitated DI water for 30 min for a post-exposure rinse before being dried with nitrogen. For the surface modification, 150  $\mu$ L of a 0.05 M MES pH 6.0 solution containing 300 mM EDC and 300 mM Sulfo-NHS was placed in the middle of two PMMA pieces with the UV-exposed side in contact with the liquid. Capillary action ensured coverage of the entire plates with the solutions. After 25 min, the PMMA pieces were rinsed, and 150 μL of a 0.05 M sodium carbonate buffer pH 9.0 solution containing 300 mM cystamine was placed in the middle of two PMMA pieces for cystamine conjugation. Following a 3-h conjugation period, the surface thiolation was accomplished when the PMMA pieces were rinsed with DI water and dried with nitrogen again. These PMMA substrates were used within 1 or 2 days for gold evaporation.

The thiol-functionalized PMMA pieces were coated with gold using a CHA Mark 50 e-Beam Evaporator (CHA Industries, Freemont, CA). Briefly, the gold was deposited at 1 Å/s for a total thickness of 200 nm. After evaporation, the positive photoresist S1813 (Shipley Co., Marlborough, MA) was spun onto the gold-coated PMMA at 3,000 rpm for 30 s in a manual resist spinner, and the pieces were baked in a 90 °C oven for 20 min to evaporate the remaining solvent on the surface. When the pieces were cooled down at room temperature, the photoresist was exposed under UV light for 12 s through the previously fabricated photomask containing the IDUA pattern using an ABM high-resolution mask contact aligner. The pieces were then placed back in the 90 °C oven for an additional 5 min. Following the post-exposure bake, the exposed resist was removed and immersed in the developer MF-321 (Shipley Co., Marlborough, MA) for 2 min and then rinsed with DI water before being dried with nitrogen. The IDUAs were formed by submerging the pieces in gold etchant (Transene Co., Danvers, MA) for approximately 3 min. The PMMA and remaining photoresist on IDUAs were exposed to UV for 2 min and immersed in MF-321 for 2 min for complete removal of the photoresist on IDUAs. The PMMA with IDUA pieces were washed with DI water and dried with nitrogen for the bonding process.

Design and fabrication of the multi-channel pattern on PMMA

The multi-channel pattern illustrated in Fig. [1](#page-3-0) and [2a](#page-3-0) (upper piece) was designed using L-Edit CAD Software, and the photomask containing multi-channels was fabricated using the 3600F PG Mask Writer, followed by developing in 300MIF and chrome etching. The length and width of the multi-channel pattern are 50 and 25 mm, respectively. The width and height of channels are 400 and 50 μm, respectively, and five separated channels are in the pattern. Two inlet ports and one outlet port allow for sample and OG solution additions and mixture removal, respectively. The micromixers with sawtooth microstructures incorporated into channels are used to maximize the binding efficiency during the hybridization process.

Copper electrodeposition was utilized to construct the master mold of the multi-channel pattern. A copper plate with a polished mirror (1 mm thickness) was cut into 50 mm×50 mm squares and cleaned with acetone and DI water. A negative resist, KMPR 1050 (MicroChem Corp., Newton, MA), was poured onto the center of the copper square and then was spun for 30 s at 3,000 and 500 rpm/s to obtain a thickness of 50 μm using Karl Suss RC-8 wafer spinner. The plate was then baked on a 95 °C hot plate for 15 min followed by gradual cooling to room temperature. The resist was patterned by exposure to UV light for 60 s in the ABM contact aligner through a 365-nm-long pass filter

<span id="page-3-0"></span>

Fig. 1 Multi-channel microfluidic biosensor principle: 1 A 4-μL sample solution is introduced through the inlet hole separating nonhybridized liposomes from the successful sandwiches at a capture zone. 2 After 8 min of washing with running buffer, detergent is injected in order to lyse the liposomes and release ferri/ferro hexacyanide encapsulant. 3 The

released redox marker is then detected over the IDUA, generating a current signal corresponding to the C. parvum DNA target concentration. 4 Finally, the magnet is removed and channels rinsed with running buffer to prepare for the next assays

to obtain vertical side walls. A post-exposure bake for 3 min at 95 °C was followed by developing for 8 min in a SU-8 developer with mild agitation. Prior to electroplating, the KMPR patterned copper plate was de-scummed using  $60$  s of  $O<sub>2</sub>$  plasma in Glen 1000 Resist Strip for stripping of photoresist and other organics. Electroplating was performed at room temperature using Microfab SC Copper Sulfamate solution (MicroFAB, Bremen, Germany), which at a current density of  $0.21 \text{ mA/mm}^2$  has a deposition rate of 0.105 mm<sup>3</sup>/mA h. Current was applied to the

electroplating bath to produce 50-μm-tall copper structures where KMPR did not cover the copper surface, resulting in the raised microchannel design. After plating, the KMPR was stripped off the copper plate by soaking in Microposit Remover 1165 (Shipley Co., Marlborough, MA) for 1 h at 70 °C. The master was then visually inspected for KMPR stripping and multi-channel pattern on the surface.

Hot embossing PMMA was used to replicate the multichannel PMMA. The blank PMMA pieces were placed in an



Fig. 2 Chip fabrication and assembly. (a) Device configuration consists of IDUAs fabricated on PMMA substrate and microchannel PMMA (400 μm channel wide and 50 μm channel high embedded in 1.5 mm PMMA thick) made by hot embossing, (b) assembled multi-

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80 °C vacuum oven (1 kPa) overnight to remove any volatiles that could result in outgassing during the hot embossing process. The PMMA was then sandwiched between the copper master and a blank copper plate after they were preheated. A force of 5,000 lbf was applied with an embossing temperature of 130 °C for 5 min in a Carver Laminating Hot Press (Fred S. Carver Inc., Summit, NJ). The sandwiched setup was allowed to be hot embossed for another 3 min if there were air bubbles between the PMMA plate and the copper master. After that, the copper master and PMMA were removed from the hot press and cooled down to room temperature. The PMMA with multi-channel pattern was manually removed from the copper master, and the inlet and outlet holes were drilled using steel bits. The PMMA was rinsed with DI water and dried with nitrogen, then put into an 80 °C vacuum oven for several hours to completely dry and evaporate any existing volatiles.

## Multi-channel device assembly

The multi-channel structured PMMA and IDUA-attached PMMA pieces were treated under UV light in a UV/ozone stripper for 8 min for the photochemically induced main chain scission of PMMA to lower the glass transition temperature of the PMMA surface. The two PMMA pieces were aligned with the IDUA side in contact with the multi-channel side and then sandwiched between two blank copper plates after the copper plates were preheated. A force of 5,000 lbf was applied with a bonding temperature of 80 °C for 5 min in a Carver Laminating Hot Press. The sandwiched setup was allowed to be thermal bonded for another 3 min if air bubbles were present between two PMMA pieces. Subsequently, the bonded PMMA device and copper plates were removed from the hot press and cooled down to room temperature.

The inlet and outlet Tygon® tubing were glued in the drilled holes using cyanoacrylate-based adhesive, and the adhesive was solidified overnight. Stainless steel blunt needles with Luer polypropylene hub were inserted into the tubing for connection with syringes containing assay solutions. Metal leads connecting the IDUAwith the potentiostat were adhered to the IDUA contact pads with silver conductive epoxy; the epoxy was allowed to solidify for 2 h.

# Detection assay

Superparamagnetic beads coated with streptavidin were coupled with biotinylated capture probe 5′-biotin-AGA TTC GAA GAA CTC TGC GC-3′ according to the manufacturer's protocol. Briefly, 20 μL of bead stock (10 mg/mL) was washed twice in  $2 \times$  concentrated binding and washing (B&W) buffer (10 mM Tris–HCl, 1 mM EDTA, 2 M sodium chloride, 0.01 % sodium azide, pH 7.5) and resuspended in 19 μL of  $1\times$  concentrated B&W buffer. One microliter of DNA capture probe (600 μM) was added to the beads, and the resultant mixture was placed on a rotator for 15 min at room temperature to allow conjugation. After conjugation, the beads were washed three times with 1× B&W buffer and resuspended in the same buffer to a final volume of 20 μL. The beads with immobilized oligonucleotides could be stored at −20 °C for 1 week. At the same time, the liposomes were prepared following the protocol as described in [\[19](#page-8-0)] to encapsulate potassium ferri/ferrocyanide and coupled to a cholesterol-labeled reporter probe 5′-GTC CAA CTT TAG CTC CAG TT-cholesterol-3′. Briefly, 29.6 mg of DPPC, 15 mg DPPG, and 20 mg cholesterol were dissolved in a mixture of 5 mL chloroform, 3 mL isopropyl ether, and 0.3 mL methanol at 45 °C. The cholesterol-labeled oligonucleotide reporter probe was added to the lipid mixture  $(0.013 \text{ mol } \%$  of total lipids). Four milliliters of 100 mM potassium ferricyanide and 100 mM potassium ferrocyanide in 0.01 M potassium phosphate buffer (PB), pH 7.0, were added to the lipid solution, and the mixture was sonicated for 4 min at 45 °C. The organic solvents were evaporated in a rotary evaporator so that liposomes formed, spontaneously entrapping encapsulant solution. To obtain a uniform particle size, the liposomes were subsequently extruded through  $2$ -μm, then 0.4-μm, filters (each 11 times) using the Avanti miniextruder and polycarbonate filters (Avanti Polar Lipids, Alabaster, AL). Liposomes were purified by gel filtration using a Sephadex G50 column and a 0.05 M PB, 0.15 M NaCl, pH 7.0, containing sucrose to increase the osmolarity to 500 mmol/kg. The liposomes were tagged with a reporter probe capable of hybridizing with the target sequence, a synthetic C. parvum target 5'-AAG GAC CAG CAT CCT TGA GTA CTT TCT CAA CTG GAG CTA AAG TTG CAC GGA AGT AAT CAG CGC AGA GTT CTT CGA ATC TAG CTC TAC TGA TGG CAA CTG A-3′. The sequences were chosen from previous biosensor development for the detection of C. parvum [\[36\]](#page-9-0).

To characterize the IDUAs and the multi-channel structure, various concentrations of potassium ferri/ferrocyanide were injected into the channels at a flow rate of 5 μL/min. Fluid flow through the multi-channel network was established by applying a positive pressure at the inlet using a syringe pump (KD Scientific Inc., Holliston, MA) connecting to a Luer polypropylene hub of stainless steel blunt needles and opening the outlet to atmospheric pressure. A 400-mV potential was applied across the IDUA, and the resulting current was measured on an Epsilon potentiostat (Bioanalytical Systems, Inc., West Lafayette, IN).

For the detection assay,  $1 \mu L$  of synthetic target sequence, 1 μL of superparamagnetic beads coupled with capture probe, 1 μL of 11.65 mM liposomes, and 1 μL of hybridization buffer (20 % formamide, 4× SSC, 0.2 % Ficoll, 0.2 M sucrose, and 0.5 % dextran sulfate) were mixed and incubated for 15 min at room temperature in a

shaker. Following the incubation, the assay protocol was carried out following the scheme illustrated in Fig. [1](#page-3-0). First, the sample solution was pumped into the multi-channel device in a reciprocating motion at a flow rate of 1 μL/min in order to aid in mixing through sample inlets. A rare earth magnet was placed over the channels in order to hold the beads in place while the sample solution was pumped out and replaced with a washing solution (20 % formamide, 4× SSC, 0.2 % Ficoll, 0.2 M sucrose, and 0.8 % dextran sulfate) at 1.5 μL/min. The magnet was about 1 mm removed from the middle of the channels. The first magnet was then removed, and a second rare earth magnet was placed directly over the IDUA. Second, the beads were then washed toward the IDUAs again at 1.5 μL/min for 8 min. The placement of the second magnet captured the majority of beads directly upstream of the IDUA. The washing step was needed to remove any unhybridized liposomes from the sample area. Third, a detergent, 60 mM OG (in 0.01 M PB, 0.15 M sodium chloride, 0.01 % sodium azide, pH 7.0) was injected into the channels at 2 μL/min (unless stated otherwise) in order to lyse the liposomes. Subsequently, released potassium ferri/ferrohexacyanide was detected on the IDUA positioned downstream of the capture zone. The resulting current from the redox reaction was detected amperometrically. The resulting current peak height or peak area under the time was determined to be the assay signal. Finally, by removing the magnet, the channels were rinsed with washing solution to retrieve the background current.

## Results and discussion

Multi-channel microfluidic device fabrication and characterization

A multi-channel microfluidic device for the electrochemical detection of analytes was developed. Figure [2](#page-3-0) illustrates design and necessary components of the multi-channel microfluidic device system. The device is composed of two major parts which are IDUAs fabricating on a PMMA substrate using standard photolithography processes and hot embossed microchannel PMMA. Five microchannels are aligned in parallel with the IDUA fingers as depicted in Fig. [2a](#page-3-0). Strong sealing between the IDUA-bearing PMMA substrate and the channel piece was achieved using the UV/ozone-assisted thermal bonding approach. Special care has to be taken during this procedure to avoid sliding of the IDUA chip over the channel substrate in order to prevent short-circuiting of the delicate IDUA structure.

Also, appropriate bonding conditions need to be verified, examining potential leaking of solution from the channels, as this would create varying surface coverage on the IDUA and result in varying signals between the channels. For this instance, 1 mM sulforhodamine B dye solution was injected through all channels and visualized using a microscope, verifying the appropriate channel dimensions prior to use with an electrochemical setup. In order to achieve wellbonded devices with functional IDUAs, the bonding conditions were optimized with special emphasis of keeping a simple protocol.

First, the adhesion of the gold layer on the PMMA was optimized. It was observed that intense bubble formation during the PMMA thiolation protocol led to nonuniform surface modifications which in turn led to unreliable gold adhesion upon gold evaporation and different gold thicknesses. During the etching process, not all fingers and gaps could be realized. Various PMMA modification strategies have been studied (see Electronic Supplementary Material Table S1) demonstrating that the addition of 0.1 % Tween 20  $(v/v)$  greatly reduces bubble formation, especially though in combination with Sulfo-NHS. As expected, these PMMA substrates enabled highly uniform IDUA fabrication fingers and, more importantly, un-short IDUA circuits after etching.

Secondly, the UV/ozone-assisted thermal bonding procedure needed to be optimized to avoid short-circuiting of the IDUAs. We optimized the applied bonding pressure, altered the UV/ozone treatment time, and most importantly, protected the IDUAs with a layer of photoresist (see Electronic Supplementary Material Table S2). A final remaining factor was to avoid sliding of the electrode-bearing PMMA piece over a surface. This resulted in functioning and reliable large IDUAs bonded securely in microfluidic chips.

To evaluate the electrochemical performance of integrated IDUA in a multi-channel microfluidic chip, we determined the cumulative signal response upon injecting ferri/ferro hexacyanide consecutively into each channel, without removing the analytes from filled channels. Data were taken after steady-state current was reached. Since we utilized an IDUA shared by five microchannels, the total amperometric current is the sum of signals generated at the active area in each channel. In order to separate the signals obtained from the different channels, a redox marker was first applied only to channel a, then channel  $a+b$ , then channels  $a+b+c$ , etc. The remaining channels were filled with buffer. The concentrations injected in channel a, b, c, d, and e was  $1, 2, 5, 10$ , and  $20 \mu M$ , respectively. As shown in Fig. [3](#page-6-0), the current signals of ferri/ferro hexacyanide increase proportionally to the cumulative concentrations that were injected into each channel. An excellent linear relationship was found in the range of  $0-38 \mu M$  with the linear equation of y (nA)=-0.5665×( $\mu$ M)–0.2198 (nA),  $R^2$ =0.983. The calculated detection limit is thus 3.48 μM with a signal-tonoise ratio of 3 (background signal=−0.39 (nA)±0.08 (nA)).

The reproducibility of the multi-channel device was tested for each channel and between channels. In the case of

<span id="page-6-0"></span>

Fig. 3 Cumulative amperometric response example of ferri/ferro hexacyanide in 0.1 M PB, pH 7.0, for five channels. The analyte solution was injected consecutively into the different channels. First, only channel a, then channel  $a+b$ , then channels  $a+b+c$ , etc., contained the redox marker. The concentrations injected in channel a, b, c, d, and e were  $1, 2, 5, 10$ , and  $20 \mu M$ , respectively. All measurements were carried out at 400 mV (stagnant condition). Inset: dose response curve from triplicate measurements

in-channel reproducibility, triplicate measurements of  $5 \mu M$ ferri/ferro hexacyanide were performed in each channel. The result showed that all of the five channels provided highly reproducible signals with relative standard deviations below 5 %. Additionally, the reproducibility of the multi-channel design between different channels was compared to separate single-channel devices. Solutions of 10 and 50 μM ferri/ferro hexacyanide were tested. High reproducibility was obtained in



Fig. 4 Replication testing of multi-channel microfluidic device. Ferri/ ferro hexacyanide in 0.1 M PB, pH 7.0, was detected at 5 μl/min flow rate in each channel for 3 min. Current background was achieved by rinsing the channel with 0.1 M PB, pH 7.0, for 3 min at the same flow rate of analyte measurement

Table 1 Replication testing data of multi-channel device

hexacyanide concentration Channel $(\mu M)$	Ferri/ferro Current signal (nA)								
			Average %RSD						
	a	h.	$\mathbf{c}$	d	e				
10	4.49	4.97 4.46 4.38 4.13				4.49	6.88		
50		21.39 21.28 22.92 20.60 19.60 21.16					5.74		

both cases, which was a powerful proof of the feasibility of different electrochemical detection schemes considering the different size and thus complexity of the two different systems. Specifically, signals obtained for the multi-channel device are shown in Fig. 4 and Table 1; signals obtained for the single IDUAs are summarized in Table 2. In contrast to the multi-channel IDUA, background normalization was required for the single IDUA chips in order to obtain reproducible results.

Finally, the cleaning of the IDUAs packaged inside the microfluidic device in between reactions was investigated. As can be seen in Fig. [5a](#page-7-0), a chip without IDUA cleaning procedures, other than rinsing the channels with DI water or buffer, exhibits declining signals for both 10 and 50 μM ferri/ferro hexacyanide in a consecutive measurement. A drop-in signal was observed in a series of just three measurements which is due to the complexity of buffer solutions used leading to electrode fouling. The signals dropped 21 and 27 % for the 10 μM solution and 36 and 40 % for the 50  $\mu$ M solution. A variety of cleaning procedures amenable for in-device cleaning were investigated including electrochemical stripping of the electrode surface, isopropanol, acetone, and acids and bases. Finally, it was found that a treatment with 0.1 M NaOH at 5 μL/min flow rate for 10 min cleaned the IDUA surfaces sufficiently and enabled highly reproducible signals as shown in Fig. [5b.](#page-7-0) In addition, using this cleaning procedure prior to a first use of the IDUA ensures stripping of any remaining photoresist and leads to significantly higher currents and signal-to-noise ratios.

Table 2 Replication testing data of different single-channel devices

Ferri/ferro hexacyanide concentration $(\mu M)$	Normalized peak area with corresponding background signal								
	Microfluidic chip		Average	$%$ RSD					
	A	B							
10 50		$3.81 \pm 0.38$ $3.44 \pm 0.13$ $3.67 \pm 0.45$ $3.64 \pm 0.15$		$20.53\pm2.10$ $16.57\pm1.47$ $17.71\pm1.19$ $18.27\pm1.66$ 9.09	4.09				

<span id="page-7-0"></span>

Fig. 5 Effect of electrode cleaning in channel on current responses of 10 and 50 μM potassium ferri and ferro hexacyanide in 0.1 M PB, pH 7.0. (a) without cleaning IDUA in channel and

Application to nucleic acid detection

## Detergent flow rate optimization

Single-channel electrochemical microfluidic sensors were used [\[22\]](#page-8-0) to determine the dependency of the nucleic acid detection assay on the detergent flow rate. The ultimate goal is the identification of flow rates that will enable time-dependent detection within the multi-channel system where signals are resolved due to different lengths of the detergent supply channels. Thus, a time-resolved multianalyte detection will be possible. Here, C. parvum DNA was detected using a hybridization assay between capture probe-coupled paramagnetic beads and reporter probe-tagged liposomes [\[19,](#page-8-0) [20](#page-8-0), [22](#page-8-0)]. The hybridization complexes were captured via an external magnet located upstream of the IDUA. Upon lysis of the liposome using the non-ionic detergent n-Octyl-β-D-glucopyranoside (OG), the released potassium ferri/ferrohexacyanide was



Fig. 6 Optimization of detergent flow rate for liposome lysis. Signalto-noise ratio was obtained from the normalized peak area of 300 pmol target by negative control signal in which nuclease-free water was used instead of target



(b) clean IDUA in channel before electrochemical measurement with 0.1 M NaOH at 5  $\mu$ L/min flow rate for 10 min

detected on the IDUA. Detergent flow rates were varied at 1, 2 and 5 μL/min to investigate the dependency of the signal-tonoise ratio (SNR) from a 4 μL sample containing 300 pmol synthetic DNA target (75 μM).

As can be seen from Fig. 6, the flow rate of 2  $\mu$ L/min shows the highest SNR whereas 1 and 5  $\mu$ L/min are comparable to each other. We assume that this is due to a combination of detergent contact time resulting in liposome lysis, diffusion of the redox couple away from the electrode, and length of time spent over the electrode area. Overall, full signal development for quantification ranges from 400 to 120 s depending on the flow rates.

## C. parvum assay in multi-channel devices

Finally, a dose response curve for the detection of the synthetic C. parvum DNA [\[36](#page-9-0)] was obtained using the multi-channel microfluidic chip. Figure 7 displays the electrochemical



Fig. 7 Electrochemical responses from C. parvum assays with analyte concentrations from 0, 1.25, 12.5, and 75  $\mu$ M. All measurements were performed at 2-μL/min flow rate. Error bars show the standard deviation of triplicate data

<span id="page-8-0"></span>responses upon the addition of 0, 1.25, 12.5, and 75 μM target injected into four different channels of the device in which time-dependent signal generations were accomplished after a consecutive injection of OG solution through the channels. The background signal obtained from 0 μM DNA target was found to be  $-2.51(nA) \pm 1.33(nA)$ . Even though the average signal of 1.25 μM target is −24.99 nA, the variation of current signal at this concentration was too high to be reliably distinguished from the background signal. As a result, the detection limit of 12.5 μM target is reported as the lowest concentration demonstrated for our multi-channel microfluidic device.

# **Conclusions**

In summary, we have presented the development of a multichannel PMMA microfluidic chip with integrated IDUAs and its application to electrochemical nucleic acid detection. Our simple fabrication approach enables strong sealing for all channels of the multi-channel microfluidic chip. In addition, the chip shows desirable electrochemical performance with respect to analytical sensitivity, linearity, and reproducibility. The multi-channel design will be especially desirable when more complex fluidics and higher degree multianalysis are to be used that can otherwise not be realized with single small IDUAs.

Acknowledgments The authors acknowledge financial support which enabled the research presented. This publication was developed under the auspices of the Cornell University Center for Life Science Enterprise, a New York State Center for Advanced Technology supported by New York State and industrial partners. Also, this publication was supported by a subcontract with Rheonix, Inc. and 1U01 A1082448-01 from the NIH. Any opinions, findings, and conclusions or recommendations expressed in this publication are those of the authors and do not necessarily reflect the views of Rheonix nor those of the National Institutes of Health. This work was performed in part at the Cornell NanoScale Science and Technology Facility, a member of the National Nanotechnology Infrastructure Network, which is supported by the National Science Foundation (grant ECS-0335765). NW and WS thank the Thailand Research Fund through the Royal Golden Jubilee Ph.D. program (grant no. PHD/0319/2548) for financial support.

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