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Cuckoo optimization algorithm for unit production cost in multi-pass turning operations

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Abstract The multi-pass turning process is one of the most used machining methods in manufacturing industry. The minimization of the unit production cost is considered the key objective of this operation. In this work, the cutting parameters are carried out using a recently developed advanced bioinspired optimization algorithm, called the cuckoo optimization algorithm (COA). The obtained results are compared with previously published results available in the literature. It has been proven that the COA competes robustly with a wide range of optimization algorithms.

Keywords Multi-pass turning operations \cdot Cutting parameters \cdot Unit production cost \cdot Cuckoo optimization algorithm

Nomenclature

UC	Unit production cost, excluding material cost
	(\$/piece)
$C_{\rm M}$	Cutting cost by actual time in cutting (\$/piece)
$C_{\rm I}$	Machine idle cost due to loading and unloading
	operations and tool idle motion time (\$/piece)
$C_{\rm R}$	Tool replacement cost (\$/piece)

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C_{T}	Tool cost (\$/piece)
$V_{\rm p}, V_{\rm s}$	Cutting speeds in rough and finish machining,
	respectively (m/min)
$V_{\rm rL}, V_{\rm rU}$	Lower and upper bounds of cutting speed
	in rough machining, respectively (m/min)
$V_{\rm sL}, V_{\rm sU}$	Lower and upper bounds of cutting speed
	in finish machining, respectively (m/min)
f_r, f_s	Feed rates in rough and finish machining,
0.700	respectively (mm /rev)
$f_{\rm rL}, f_{\rm rU}$	Lower and upper bounds of feed rate in rough
	machining, respectively (mm/rev)
$f_{\rm sL}, f_{\rm sU}$	Lower and upper bounds of feed rate in finish
	machining, respectively (mm/rev)
$d_{\rm r}, d_{\rm s}$	Depths of cut for each pass of rough and finish
	machining, respectively (mm)
$d_{\rm rL}, d_{\rm rU}$	Lower and upper bounds of depth of roughing
	cut, respectively (mm)
$d_{\rm sL}, d_{\rm sU}$	Lower and upper bounds of depth of finishing
	cut, respectively (mm)
n	Number of rough cuts (rough passes)
$d_{\rm t}$	Total depth of metal to be removed (mm)
D, L	Diameter and length of work piece,
	respectively (mm)
k_0	Direct labor cost, including overheads (\$/min)
k _t	Cutting edge cost (\$/edge)
$t_{\rm mr}, t_{\rm ms}, t_{\rm m}$	Rough machining time, finish machining time,
	and actual machining time, respectively (min)
$t_{\rm c}, t_{\rm e}, t_{\rm i}$	Constant term of machine idling time, tool
	exchange time, and total machine idle time,
	respectively (min)
h_1, h_2	Constants pertaining to tool travel and
	approach/depart time, respectively (min)
$T_{\rm r}, T_{\rm s}$	Expected tool life for rough and finish
	machining, respectively (min)
$T_{\rm P}$	Tool life of weighted combination
	of T_r and T_s (min)

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θ	Weight for $T_{\rm p}$
$T_{\rm L}, T_{\rm U}$	Lower and upper bounds for tool life,
	respectively (min)
α, β, γ, C	Constants of the tool life equation
p, q, r, C_0	$p=1/\alpha, q=\beta/\alpha, r=\gamma/\alpha, \text{ and } C_0=C^{1/\alpha}$
SR	Maximum allowable surface roughness (mm)
SC	Limit of stable cutting region
R	Nose radius of the cutting tool (mm)
$F_{\rm r}, F_{\rm s}$	Cutting forces during rough and finish
	machining, respectively (kgf)
$F_{\rm U}$	Maximum allowable cutting force (kgf)
k_1, u, v	Constants of the cutting force equation
$P_{\rm r}, P_{\rm s}$	Cutting powers during rough and finish
	machining, respectively (kW)
$P_{\rm U}$	Maximum allowable cutting power (kW)
η	Power efficiency
λ, υ	Constants related to expression of the stable
	cutting region
$Q_{\rm r}, Q_{\rm s}$	Limit of stable cutting region constraint
	chip-tool interface temperatures during
	rough and finish machining, respectively (°C)
$Q_{ m U}$	Maximum allowable chip-tool interface
	temperature (°C)
k_2, τ, ϕ, δ	Constants related to the equation of chip-tool
	interface temperature
k_3, k_4, k_5	Constants for roughing and finishing
	parameter relations
Х	$\{x_1, x_2,, x_{NCOA}\}$ Set of cutting parameters,
	i.e. design variables

1 Introduction

The process of metal removal using multi-pass turning operations involves two separated stages, the rough machining stage and the finish machining stage. Several variables should be considered to achieve products that meet the specifications. These can be categorized as input variables, such as cutting speed, feed rate, depth of cut, number of passes, work material and its properties, tool material and tool geometry, and cutting fluid properties and characteristics and output variables, such as production cost, production time, tool life, dimensional accuracy, surface roughness, cutting forces, cutting temperature, and power consumption [1–3].

The present work focuses on the well-known multi-pass turning optimization problem which consists of selecting the optimal cutting parameters, i.e., cutting speeds, feed rates, depths of cut, and number of passes, for minimizing a production cost-based objective function [3–9]. The first application of a prevailing metaheuristic called the cuckoo optimization algorithm (COA) to the optimization of turning operations in the literature is addressed for this purpose. The reminder of the paper is organized as follows. A brief overview of the literature on the multi-pass turning operations is presented in the next section. Section 3 presents the optimization problem of unit production cost in multi-pass turning operations. Section 4 describes the basic idea behind the cuckoo optimization algorithm and presents pseudocode summarizing its fundamental steps. Section 5 is devoted to the results obtained by the implemented COA and the discussion. Section 6 concludes this work.

2 Literature review

The overview of the literature shows that several researchers from different backgrounds have investigated the optimization of cutting parameters in turning operations. Generally, the authors used traditional mathematical programming techniques, probabilistic or heuristic/metaheuristic methods, and hybrid approaches to optimize the machining conditions. It should be noted that evolutionary algorithms were the most powerful approach, and this constitutes their advantages: an efficient way to produce acceptable solutions by trial-anderror in reasonably practical time, diversified solutions, and the possibility of handling the constraints.

After the pioneer works developed in [10–14], Shin and Joo [4] proposed a comprehensive mathematical model solved by a dynamic programming approach. Later, several researchers have relied on the data of this model to improve the results using different resolution methods.

Chen and Tsai [5] solved the optimization problem by combining the simulated annealing algorithm and a Hook-Jeeves pattern search technique (SA-PS), whereas Chen and Su [15] solely used a simulated annealing. Gupta et al. [16] proposed an approach based on linear programming. Onwubolu and Kumalo [6] investigated the use of the genetic algorithm (GA) to optimize the parameters of multi-pass turning operations. However, M. Chen and K. Chen [17] applied a float-encoding genetic algorithm (FEGA) and revealed that Onwubolu and Kumalo [6] incorrectly manipulated the machining model presented by Chen and Tsai [5]. Similarly, the results found by Aryanfar and Solimanpur [18] using GA exceed the bound of some constraints.

Vijayakumar et al. [19] proposed an approach based on ant colony optimization (ACO). In the technical note [20], Wang revealed that Vijayakumar et al. [19] did not provide the optimal values they found for the depth of the rough cuts and the finishing cut and the constraint related to the number of passes.

A hybrid approach by combining genetic algorithm and artificial immune system (GA-AIS) has been implemented by Zheng and Ponnambalam [21] without considering the bounds on the number of passes. In [22], a comparison of six non-traditional methods, the genetic algorithm (GA), simulated annealing algorithm (SA), Tabu search algorithm (TS), ant colony optimization (ACO), memetic algorithm (MA), and particle swarm optimization (PSO), has been performed to determine the optimal machining parameters for turning cylindrical stocks into various continuous finished profiles and different data. It has been shown that the results were outperformed by the PSO.

Yildiz implemented several optimization techniques for solving the multi-pass turning operations problem, such as differential evolution algorithm and receptor editing (DERE), artificial bee algorithm (ABC), differential evolution algorithm (DE) [23], hybrid artificial bee colony algorithm [8], hybrid robust differential evolution algorithm (HRDE), artificial immune algorithm (AIA) [24], and hybrid robust teaching-learning-based optimization algorithm (HRTLBO) [25]. It should be noted that the minimum production cost was provided without any information about the optimal values of the machining parameters. Hence, the constraint violations cannot be fully investigated from these works.

Venkata Rao and Kalyankar [3] applied the teachinglearning-based optimization algorithm (TLBO). The authors showed that the TLBO requires a lower number of iterations for convergence to the optimal solution.

Belloufi et al. [26] used a firefly algorithm (FA) and a hybrid genetic algorithm-sequential quadratic programming (GA-SQP) [27]. The obtained numerical value of the cost was better than that of other optimization techniques. However, the constraints have been incorrectly handled.

In [7], Srinivas et al. used the particle swarm optimization (PSO) with a carefully detailed comparison of the constraint violations found in ACO [19], GA [6], and SA-PS [5]. Later, Costa et al. [9] improved the results of Srinivas et al. [7] by applying a hybrid particle swarm optimization technique (HPSO) which combines the PSO and SA.

The next section presents the comprehensive mathematical model for minimizing the unit production cost in multi-pass turning operations.

3 Optimization model of multi-pass turning operations

In this paper, the detailed mathematical model presented in [3, 7–9] is adopted. The numerical data are reported in Table 1.

3.1 Objective function: Unit production cost

The aim considered here is to minimize the unit production cost (UC) in multi-pass turning operations. The UC is divided into four basic cost elements:

(1) Cutting cost by actual time, $C_{\rm M}$;

- (2) Machine idle cost due to loading and unloading operations and idling tool motion, C_{I} ;
- (3) Tool replacement cost, $C_{\rm R}$;
- (4) Tool cost $C_{\rm T}$.

Thus, the objective function is defined as follows:

$$F(X) = \operatorname{Min}(\operatorname{UC}) = \operatorname{Min}(C_{\mathrm{M}} + C_{\mathrm{I}} + C_{\mathrm{R}} + C_{\mathrm{T}})$$
(1)

The expression of each cost element is given below.

3.1.1 Machining cost

The machining cost involves the multi-pass roughing and a single-pass finishing, respectively:

$$C_{\rm M} = k_0 \left[\frac{\pi DL}{1,000V_{\rm r}f_{\rm r}} n + \frac{\pi DL}{1,000V_{\rm s}f_{\rm s}} \right]$$

= $k_0 \left[\frac{\pi DL}{1,000V_{\rm r}f_{\rm r}} \left(\frac{d_{\rm t} - d_{\rm s}}{d_{\rm r}} \right) + \frac{\pi DL}{1,000V_{\rm s}f_{\rm s}} \right]$ (2)
= $k_0 (t_{\rm mr} + t_{\rm ms})$

Finally,

$$C_{\rm M} = k_0 t_{\rm m} \tag{3}$$

where $t_{\rm m}$ is the actual machining time.

3.1.2 Machine idling cost

The machine idling cost is defined by the sum of a constant term related to the loading/unloading operations and a variable term representing the idle tool motion:

$$C_{1} = k_{0}[t_{c} + (h_{1}L + h_{2})(n+1)]$$

$$= k_{0}\left[t_{c} + (h_{1}L + h_{2})\left(\frac{d_{t}-d_{s}}{d_{r}} + 1\right)\right]$$
(4)

Finally,

$$C_{\rm I} = k_0 t_{\rm i} \tag{5}$$

where t_i is total machine idle time.

3.1.3 Tool replacement cost

From Taylor's tool-life equation, the life of a tool is given by:

$$T = \frac{C^{1/\alpha}}{V^{1/\alpha} f^{\beta/\alpha} d^{\gamma/\alpha}} = \frac{C_0}{V^p f^q d^r}$$
(6)

Table 1 Machining model data

Parameter	Value	Parameter	Value	Parameter	Value
D	500 mm	L	300 mm	d_{t}	6 mm
V _{rU}	500 m/min	$V_{\rm rL}$	50 m/min	$f_{\rm rU}$	0.9 mm/rev
f _{rL}	0.1 mm/rev	$d_{ m rU}$	3 mm	$d_{ m rL}$	1 mm
$V_{\rm sU}$	500 m/min	$V_{\rm sL}$	50 m/min	$f_{\rm sU}$	0.9 mm/rev
f _{sL}	0.1 mm/rev	$d_{ m sU}$	3 mm	$d_{ m sL}$	1 mm
p	5	q	1.75	r	0.75
и	0.75	v	0.95	η	0.85
λ	2	v	-1	au	0.4
ϕ	0.2	δ	0.105	R	1.3 mm
C_0	6×10^{11}	h_1	7×10^{-4}	h_2	0.3
$T_{\rm L}$	25 min	t _c	0.75 min/piece	te	1.5 min/edge
$P_{\rm U}$	5 kW	$T_{\rm U}$	45 min	$F_{\rm U}$	200 kgf
SC	140	$SR_{\rm U}$	10 µm	$Q_{ m U}$	1,000 °C
k_0	\$0.5 per minute	k_1	108	k_2	132
k ₃	1	k_4	2.5	k_5	1
k _t	\$2.5 per edge	θ	0.8		

It has been considered that the same tool is used for the entire machining operation process of both roughing and finishing. Furthermore, the wear rate of tools differs between the operations. Thus, the tool life can be expressed as:

$$T_{\rm p} = \theta T_{\rm r} + (1 - \theta) T_{\rm s}, \quad \theta \in [0, 1]$$

$$\tag{7}$$

where:

$$T_{\rm r} = \frac{C_0}{V_{\rm r}^p f_{\rm r}^q d_{\rm r}^r}, \quad T_{\rm r} = \frac{C_0}{V_{\rm s}^p f_{\rm s}^q d_{\rm s}^r} \tag{8}$$

It should be noted that the majority of authors simplify T_{p} (Eq. (7)) by ignoring the weight θ :

$$T_{\rm p} = T_{\rm r} + T_{\rm s} \tag{9}$$

The tool replacement time depends on the tool life (T_p) , time required to exchange a tool (t_e), and machining time (t_m):

$$C_{\rm R} = \frac{t_{\rm e}}{T_{\rm p}} \left[\frac{\pi DL}{1,000V_{\rm r}f_{\rm r}} \left(\frac{d_{\rm t} - d_{\rm s}}{d_{\rm r}} \right) + \frac{\pi DL}{1,000V_{\rm s}f_{\rm s}} \right]$$
$$= t_{\rm e} \frac{t_{\rm m}}{T_{\rm p}}$$
(10)

The tool replacement cost $C_{\rm R}$ is given by:

$$C_{\rm R} = k_0 t_{\rm e} \frac{t_{\rm m}}{T_{\rm p}} \tag{11}$$

3.1.4 Tool cost

The tool cost $C_{\rm T}$ is given by:

$$C_{\rm T} = k_{\rm f} \frac{t_{\rm m}}{T_{\rm p}} \tag{12}$$

3.2 Machining constraints

The unit production cost (UC) defined by Eq. (1) is subject to several constraints during the roughing and finishing operations. These constrains can be classified as follows:

- (1) Parameter bounds;
- Tool-life constraint; (2)
- (3) Operating constraints consisting of surface finish constraint (only for finish machining), cutting force constraint, and power constraint;
- (4) Stable cutting region constraint;
- (5) Chip-tool interface temperature constraint;
- Roughing and finishing parameter relations; (6)
- (7) Bounds on the number of rough passes.

3.2.1 Rough machining

(a) Parameter bounds:

The range of cutting speeds is:

$$V_{\rm rL} \le V_{\rm r} \le V_{\rm rU} \tag{13}$$

The feed rate is restricted as:

$$f_{\rm rL} \le f_{\rm r} \le f_{\rm rU} \tag{14}$$

Bounds on the depth of cut are:

$$d_{\rm rL} \le d_{\rm r} \le d_{\rm rU} \tag{15}$$

(b) Tool-life constraint:

 $T_{\rm L} \le T_{\rm r} \le T_{\rm U} \tag{16}$

(c) Operating constraints:

(i) Cutting force constraint: The cutting force constraint is given in terms of maximum force $F_{\rm U}$ according to:

$$F_{\rm r} = k_1 (f_{\rm r})^u (d_{\rm r})^v \le F_{\rm U} \tag{17}$$

(ii) Power constraint:

The power required during the cutting operation should not exceed the available power $P_{\rm U}$ of the machine tool:

$$P_{\rm r} = \frac{F_{\rm r} V_{\rm r}}{6,120\eta} = \frac{k_1 (f_{\rm r})^u (d_{\rm r})^v V_{\rm r}}{6,120\eta} \le P_{\rm U}$$
(18)

(iii) Stable cutting region constraint:

The constraint on the stable cutting region in turning is expressed as:

$$(V_{\rm r})^{\lambda}(f_{\rm r})(d_{\rm r})^{\nu} \ge SC \tag{19}$$

(iv) Chip-tool interface temperature constraint: The temperature generated at the chip-tool interface should not exceed the permissible limit:

$$Q_{\rm r} = k_2 (V_{\rm r})^{\tau} (f_{\rm r})^{\phi} (d_{\rm r})^{\delta} \leq Q_{\rm U}$$

$$\tag{20}$$

3.2.2 Finish machining

For all the constraints defined in Eqs. (13)–(20), the suffix *r* is replaced by *s* for the finish machining constraints:

$$V_{\rm sL} \le V_{\rm s} \le V_{\rm sU} \tag{21}$$

 $f_{sL} \le f_s \le f_{sU} \tag{22}$

 $d_{\rm sL} \le d_{\rm s} \le d_{\rm sU} \tag{23}$

$$T_{\rm L} \le T_{\rm s} \le T_{\rm U} \tag{24}$$

$$F_{\rm s} \le F_{\rm U}$$
 (25)

$$P_{\rm s} \le P_{\rm U} \tag{26}$$

$$Q_{\rm s} \le Q_{\rm U} \tag{27}$$

$$(V_s)^{\lambda} (f_s) (d_s)^{\nu} \ge SC \tag{28}$$

The surface finish constraint is given by:

$$\frac{f_s^2}{8R} \le (SR)_{\rm U} \tag{29}$$

The cutting parameter relation constraints are:

$$V_{\rm s} \ge k_3 V_{\rm r} \tag{30}$$

$$f_{\rm r} \ge k_4 f_{\rm s} \tag{31}$$

$$d_{\rm r} \ge k_5 d_{\rm s} \tag{32}$$

The number of rough passes $(n = \frac{d_t - d_s}{d_t})$ should be an integer and is restricted as follows:

$$\frac{d_{\rm t}-d_{\rm sL}}{d_{\rm rL}} \leq \frac{d_{\rm t}-d_{\rm s}}{d_{\rm r}} \leq \frac{d_{\rm t}-d_{\rm sU}}{d_{\rm rU}} \tag{33}$$

4 Cuckoo optimization algorithm

The cuckoo optimization algorithm (COA) is a bio-inspired and a population-based stochastic optimization technique recently proposed by Ramin Rajabioun [28]. COA can deal with several otherwise intractable problems, such as multivariable controller design [28], replacement of obsolete components in industrial plants [29, 30], job scheduling [31], statistical process control [32], fractional-order hyperchaotic system [33], analyzing the electrochemical machining process [34], unconventional machining processes [35], and determination of the warranty period [36].

The COA uses the biological inspiration of the social behavior of a bird species called cuckoos. The cuckoos have the ability to lay eggs in the nest of another species and the cuckoo chicks will be fed by the host birds. As some of the eggs are dissimilar to the host bird's eggs, they are detected and destroyed by the host birds (Fig. 1).





Fig. 2 Migration of the cuckoos toward goal habitat

$$\lambda \sim U(0,1)$$

$$\varphi \sim U\left(-\frac{\pi}{6}, \frac{\pi}{6}\right)$$
(37)

Fig. 1 Egg laying of cuckoos

First, a given population of mature cuckoos starts to lay eggs in their habitat:

Habitat =
$$[x_1, x_2, ..., x_{N_{CO4}}] = [V_r, f_r, d_r, V_s, f_s, d_s]$$
 (34)

where $(x_1, x_2, ..., x_{N_{COA}})$ represent the design variables.

The value of the cost function is obtained by evaluating the profit of a habitat:

$$Profit = -f_{COA}(Habitat) = -f_{COA}(V_r, f_r, d_r, V_s, f_s, d_s)(35)$$

where the sign (–) is attributed to generate a cost minimization because the cuckoos try to maximize the number of surviving cuckoo eggs. Therefore, a candidate habitat matrix $N_{pop} \times N_{COA}$ is randomly generated.

The eggs will be laid within a distance ELR (egg laying radius):

$$ELR = \alpha \times \frac{\text{Number of current cuckoos' eggs}}{\text{Total number of eggs}} \times (\text{var}_{hi} - \text{var}_{low})$$
(36)

where α is an integer imposed to accommodate the value of ELR, var_{hi} and var_{low} are the upper limit and the lower limit for variables, respectively.

When the eggs hatch, the cuckoo chicks will eat most of the food of the host birds and the food is insufficient for all the chicks. Thus, some chick cuckoos will starve. Once the cuckoos mature and the reproduction period approaches, they migrate toward best habitat. To recognize which cuckoo belongs to which group, the algorithm uses K-clustering method.

Figure 2 shows an illustrative outline of the cuckoo's migration. Each cuckoo flies only λ % of all way toward goal with a deviation φ (rad):

where λ is a random number uniformly distributed between 0 and 1.

After the migration step, a new egg-laying process restarts. Thus, the cuckoo optimization algorithm is summarized as follows [28]:

- Step 1: Initialize the habitats with some random points on the profit function;
- Step 2: Dedicate some eggs to each cuckoo;
- Step 3: Define ELR for each cuckoo;
- Step 4: Let cuckoos lay eggs inside their corresponding ELR;
- Step 5: Destroy those eggs that are recognized by host birds;
- Step 6: Let eggs hatch and chicks grow;
- Step 7: Evaluate the habitat of each newly grown cuckoo;
- Step 8: Limit cuckoos' maximum number in environment and kill those who live in worst habitats;
- Step 9: Cluster cuckoos, find best group and select goal habitat;
- Step 10: Let new cuckoo population migrate toward goal habitat;
- Step 11: If stop condition is satisfied, stop; otherwise, go to Step 2.

Figure 3 shows the flowchart of the cuckoo optimization algorithm (COA). The pseudocode of the proposed approach is as follows:

%Parameters Habitat size = N Number of initial cuckoos = InitCuck Maximum number of eggs for each initial cuckoo = MaxEggs



Fig. 3 Flowchart of COA [28]

Minimum number of eggs for each initial cuckoo = MinEggs Maximum cuckoos may live at the same time = MaxCuck Maximum iterations = CuckIter **Begin** %Initialization Generate some random points; %Loop until the termination condition For Iter = CuckIter Do Dedicate some eggs to each cuckoo; Calculate the ELR for each cuckoo according to Eq. (36); Laying eggs inside the calculated ELR; End

Table 2 COA property and value

COA property	Value
Dimension of the problem to optimize (number of cutting parameters)	6
Number of initial population of cuckoos	5
Minimum number of eggs for each initial cuckoo	2
Maximum number of eggs for each initial cuckoo	9
Maximum number of cuckoos that can live at the same time	50
Maximum iterations of the algorithm	70



Fig. 4 Convergence of unit production cost (case $T_p = T_r + T_s$)

Destroy some eggs; Let eggs hatch and chicks grow; Evaluate the fitness function according to Eq. (1) and implemented by Eq. (35); Constraint handling with violation terms by considering Eqs. (13)–(33);

Limit the number of cuckoos;

Table 3 Results obtained by COA (case $T_p = T_r + T_s$)

	Variable	Range/Limit	COA result
Cutting parameters	$V_{\rm r}$	50-500	123.1462 (m/min)
	$f_{\rm r}$	0.1-0.9	0.5655 (mm/rev)
	d_{r}	1.0-3.0	3.0 (mm)
	$V_{\rm s}$	50-500	169.9876 (m/min)
	$f_{\rm s}$	0.1-0.9	0.2262 (mm/rev)
	$d_{\rm s}$	1.0-3.0	3.0 (mm)
Constraints for rough cut	$T_{\rm r}$	25-45	25.2028 (min)
	$F_{\rm r}$	≤200	199.9924 (kgf)
	$P_{\rm r}$	≤5	4.7344 (kW)
	SC	≥140	2.8586e+003
	$Q_{\rm r}$	≤1,000	906.4140 (°C)
Constraints for finish cut	$T_{\rm s}$	25-45	25 (min)
	$F_{\rm s}$	≤200	100.5908 (kgf)
	$P_{\rm s}$	≤5	3.2870 (kW)
	SC	≥140	2.1787e+003
	$Q_{\rm s}$	≤1,000	858.4936 (°C)
	$(SR)_{\rm U}$	10	0.0053 (µm)
Constraint on variable	$\geq k_3$	1.0	1.38
relations	$\geq k_4$	2.5	2.5
	$\geq k_5$	1.0	1.0
Unit production cost			1.959 (\$/piece)

Method	Cutting speed (m/min)		Feed rate (mm/rev)		Depth of cut (mm)		UC (\$/piece)	Constraint violation	
	V _r	Vs	fr	$f_{\rm s}$	$\overline{d_{\mathrm{r}}}$	ds			
COA (present study)	123.1462	169.9876	0.5655	0.2262	3	3	1.959	0	
GA [6]	114.22	164.369	0.7	0.2978	2.9745	2.9863	1.8450	(16), (17), (18), (24) (31), (32)	
PSO [7]	106.69	155.89	0.897	0.28	2	2	2.272	0	
ACO [19]	103.05	162.02	0.9	0.24	—	—	1.626	(33): not considered	
HPSO [9]	123.3424	169.9783	0.5655	0.2262	3	3	1.959	0	
SA-PS [5]	_	—	_	_	—	—	2.313	-	
TLBO [3]	110	170	0.565	0.225	3	3	1.973	0	
HRDE [24]	—	—	_	—	_	—	2.046	-	
AIA [24]	—	—	_	—	_	—	2.12	-	
DERE [23]	—	—	_	—	_	—	2.046	-	
ABC [23]	_	_	_	_	_	_	2.118	-	
DE [23]	—	—	_	—	—	—	2.136	-	
HABC [8]	—	—	_	—	—	—	2.046	-	
HRTLBO [25]	—	—	_	—	—	—	2.046	-	
GA-SQP [27]	94.464	162.289	0.866	0.258	3	3	1.814	(16), (17)	
FA [26]	98.4102	162.2882	0.820	0.2582	3	3	1.824	(17)	

Table 4 Comparison of different optimization methods (case $T_p = T_r + T_s$)

Apply K-means clustering, find best group, and select goal habitat by considering Eq. (37);

Migrate toward goal habitat;

End For

Generate the optimal cutting parameters Generate the minimum unit production cost

Fig. 5 Convergence of unit production cost (case $T_p = \theta T_r + (1 - \theta)T_s$)

5 Results and discussion

The goal is to minimize the unit production cost (UC) in multipass turning operations using the cuckoo optimization algorithm. The problem is defined by the object function (Eq. (1)) and subject to the constraints (Eqs. (13)–(33)). Table 2 contains



Table 5 Results obtained by COA (case $T_p = \theta T_r + (1 - \theta)T_s$)

	Variable	Range/Limit	COA result
Cutting parameters	$V_{\rm r}$	50-500	117.9322 (m/min)
	$f_{\rm r}$	0.1–0.9	0.5655 (mm/rev)
	$d_{ m r}$	1.0-3.0	3.0 (mm)
	$V_{\rm s}$	50-500	123.1993 (m/min)
	$f_{\rm s}$	0.1-0.9	0.2262 (mm/rev)
	$d_{\rm s}$	1.0-3.0	3.0 (mm)
Constraints for rough cut	$T_{\rm r}$	25–45	25.031 (min)
	$F_{\rm r}$	≤200	199.992 (kgf)
	$P_{\rm r}$	≤5	4.533 (kW)
	SC	≥140	2.6217e+003
	$Q_{\rm r}$	≤1,000	890.863 (°C)
Constraints for finish cut	$T_{\rm s}$	25–45	25 (min)
	$F_{\rm s}$	≤200	100.590 (kgf)
	$P_{\rm s}$	≤5	2.382 (kW)
	SC	≥140	1.1444e+003
	$Q_{\rm s}$	≤1,000	754.768 (°C)
	$(SR)_{\rm U}$	10	0.005 (µm)
Constraint on variable	$\geq k_3$	1.0	1.044
relations	$\geq k_4$	2.5	2.5
	$\geq k_5$	1.0	1.0
Unit production cost			2.239 (\$/piece)

the rules and parameters for the COA implemented to solve this optimization problem. These values were chosen by trial-anderror and based on experience. The algorithm has been run on Intel Pentium Processor G620 (3Mo Cache, 2.60GHz, Sandy Bridge) PC with 4 GB memory (Windows 7, 64 bits).

The optimization process of the COA is shown in Fig. 4, whereas the results are reported in Table 3. The algorithm used 3,500 function evaluations and the execution time was 22.58 s of CPU time.

From Table 3, it can be observed that the minimum unit production cost value is 1.959 (\$/piece). It should be noted that the results were obtained at the 37th iteration of the COA.

From the comparison of the results given in Table 4, it is seen that the minimum of the UC in multi-pass turning operations is achieved by the COA with feasible solutions compared to the published works. The results which should be considered as competitive from the literature are the particle swarm optimization (PSO) of Srinivas et al. [7], teachinglearning-based optimization algorithm (TLBO) of Venkata Rao and Kalyankar [3], and hybrid particle swarm optimization (HPSO) of Costa et al. [9]. It can be seen also that the HPSO provided the same UC with COA (1.959 \$/piece). However, the COA has outperformed the HPSO since the COA required 3,500 function evaluations and the convergence iteration was 37, whereas the HPSO required 62,500 function evaluations and the convergence iteration was 202.

As mentioned in Section 3, some authors consider $T_p = \theta T_r + (1-\theta)T_s$. The COA has been implemented to consider this case using the same number of function evaluations fixed in Table 2, where the execution time here was 24.74 s of CPU time. Figure 5 shows the optimization process of the COA, whereas the optimal results are given in Table 5.

From Table 5, it can be observed that the minimum unit production cost value is 2.239 (\$/piece). The results were obtained at the 24th iteration. Table 6 reveals that the COA has outperformed the results obtained by the HPSO [9].

6 Conclusions and future research

In this paper, the prevailing cuckoo optimization algorithm (COA) has been implemented for the optimization of cutting parameters in the multi-pass turning operations. The goal was to minimize the unit production cost (UC). Several authors tried to solve this problem using other optimization techniques without overlooking on the constraint violations. Furthermore, it has been observed that the optimal parameters were not reported in many works; only the UC value was provided.

The results showed that the COA is highly competitive to other published optimization techniques available in the literature. The COA required a lower number of function evaluations, improved the convergence rate, and showed its ability to handle different constraint forms.

For future work, another optimization technique may be applied to perhaps provide better results. Another point to explore is to propose a hybrid and/or multi-objective COA.

Table 6 Comparison of different optimization methods (case $T_p = \theta T_r + (1 - \theta)T_s$)

Method	Cutting speed (m/min)		Feed rate (mm/rev)		Depth of cut (mm)		UC (\$/piece)	Constraint violation
	$V_{\rm r}$	Vs	$f_{\rm r}$	$f_{\rm s}$	$d_{ m r}$	$d_{\rm s}$		
COA (present study)	117.9322	123.1993	0.5655	0.2262	3	3	2.239	0
HPSO [9]	109.663	169.97	0.5655	0.226	3	3	2.035	(24)

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