RESEARCH PAPER



Reliability and global sensitivity analysis based on importance directional sampling and adaptive Kriging model

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Received: 21 September 2022 / Revised: 24 April 2023 / Accepted: 1 May 2023 / Published online: 5 June 2023 © The Author(s), under exclusive licence to Springer-Verlag GmbH Germany, part of Springer Nature 2023

Abstract

This paper adopts importance directional sampling (IDS) and adaptive Kriging model for reliability and global sensitivity analysis. IDS is the combination of importance sampling (IS) and directional sampling (DS) by establishing directional vector in the importance region, which has the advantages of both IS and DS. A novel stopping criterion which tries to minimize the difference between the real failure region and fitted failure region is proposed based on the idea of auxiliary region to increase the efficiency of active learning. An improved active learning strategy is proposed based on the combination of optimization and learning function to synchronize the calculation process of design point and Kriging model updating, so as to ensure the accuracy of both Kriging model and importance directional density function. Different learning functions are adopted to select the most suitable active learning function of IDS. The global sensitivity index is calculated through failure probability and Bayes theorem based on Gaussian mixture model (GMM). The results show that: Through the proposed auxiliary region-based stopping criterion, the efficiency of active learning in IDS can be improved. The proposed active learning strategy can obtain high accuracy importance directional density function and failure probability with lower required function calls. Considering the accuracy and robustness of failure probability and global sensitivity index, U and EFF functions should be adopted on IDS.

Keywords Reliability analysis · Global sensitivity analysis · Importance directional sampling · Adaptive Kriging model · Auxiliary region · Improved active learning strategy

1 Introduction

Reliability and global sensitivity analysis theory is a very important research content, which has been widely used in many engineering problems (Rachedi et al. 2021; Hwang et al. 2021; Pan et al. 2021; Su et al. 2020; Mansour et al. 2020). Presently, reliability methods mainly include numerical simulation methods and moment estimation methods. Numerical simulation methods usually require a large number of random samples, and the efficiency is quite low. Moment estimation methods use the Taylor expansion of the limit state function, and the accuracy will be low for high nonlinearity problems. Global sensitivity analysis methods

Responsible Editor: Byeng D. Youn

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mainly include variance-based method (Zhang et al. 2017), moment independent-based method (Liu and Homma 2010) and failure probability-based method (Lu et al. 2008). The global sensitivity based on failure probability can more comprehensively measure the average impact of the input variables on the failure probability when the input variables are changed in the entire distribution region (Lemaitre et al. 2015). Through the global sensitivity analysis, the uncertain factors which significantly affect the failure probability can be obtained. Specially, by introducing Bayes theorem into failure probability-based global sensitivity analysis, the computational cost can be significantly reduced (Wang et al. 2019). Since the Bayes method requires the conditional probability density function of input variable in the failure region, it is usually combined with numerical simulation methods for global sensitivity analysis (Guo et al. 2021).

In order to increase the efficiency of numerical simulation methods, most researchers use surrogate model to reduce the required function calls. The most widely used surrogate model is adaptive Kriging model (Zhang et al. 2020; Wang

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et al. 2021; Xiao et al. 2020a, b; Cadini et al. 2020), as it can provide the variance information of the predicted values and select the most informative samples through learning function. Notably, AK-MCS (Echard et al. 2011) is a milestone in the development of Kriging-based methods, as AK-MCS combines the U learning function and Monte Carlo (MC) method. Based on the idea of AK-MCS, different learning functions (Bichon et al. 2008; Zhang et al. 2019; Yang 2015; Lv et al. 2015; Shi et al. 2020; Meng et al. 2020; Zhou and Li 2023) and stopping criterions (Wang and Shafieezadeh 2019a, b) are also proposed. Researchers also used MC-based failure probability for global sensitivity analysis (Guo et al. 2021). However, a large population of candidate samples are required for MC-based active learning. At least 10^{M+2} , $M = 1, 2, \cdots$ samples are required for the failure probability with 10^{-M} (Lelièvre et al. 2018), where M is the order of magnitude of failure probability. For small failure probability problems, MC cannot obtain failure samples effectively, which may completely fill the computer memory and lead to computing crash.

In order to solve the shortcomings of MC, researchers often combine other numerical methods with Kriging model, such as importance sampling (IS) (Zhao et al. 2015; Wang et al. 2022; Zhou et al. 2015), subset simulation (SS) (Chen et al. 2021; Tian et al. 2021), line sampling (LS) (Song et al. 2021; Papaioannou and Straub 2021), and directional sampling (DS) (Grooteman 2011). This paper mainly focus on IS and DS methods. Presently, IS might be the most widely used method to improve efficiency. Reference (Echard et al. 2013) proposed the famous AK-IS method, in which sampling center was transplanted to the design point and Kriging model was built through U learning function. Reference (Dubourg et al. 2013) proposed a metamodel-based IS method to approximate the optimal IS density function. Reference (Zhu et al. 2020) proposed a Meta-IS-AK method combining AK-IS and Meta-IS. Reference (Xiao et al. 2020a, b) proposed combined meta-model and stratified IS for reliability analysis. Reference (Zhang et al. 2020) proposed an improved IS method with multiple sampling centers defined by the U learning function. Reference (Yun et al. 2020) proposed a radial-based IS method to increase the efficiency of AK-MCS, and the U learning function was adopted. Reference (Chen et al. 2022) proposed a parallel active learning strategy based on K-medoids clustering and IS.

Compared with IS, DS can reduce the dimension of variable space. Sample points are generated based on the directional vector, and the required candidate samples can be significantly reduced. Reference (Zhang et al. 2021) proposed the AK-DS method, which combined DS and adaptive Kriging through U function. The results show that the required computational cost and computer memory of DS are much lower than those of IS. Specially,

importance directional sampling (IDS) is the combination of DS and IS by establishing the directional vector in the importance region. Based on DS, IDS can obtain the failure samples more effectively, and the computational efficiency could be highly improved (Zhang et al. 2022). Reference (Guo et al. 2020) used the design point-based IDS and adaptive Kriging model for reliability analysis. However, in previous studies, U learning function is often adopted for IS- and DS-based Kriging methods. Recent study (Yun et al. 2021) has shown that the stopping criterion of U function is too conservative, which may lead to many redundant training samples. Moreover, in the design point-based IDS method, in addition to the number of IDS samples, the main factor that affects the accuracy is whether the importance directional density function can represent the location of failure region accurately. The accuracy of design point will inevitably affect the accuracy of the method. Reference (Guo et al. 2020) used the approximate design point to establish importance directional density function. However, the approximate degree is not specified, and the calculation of design point is before the establishment of Kriging model through learning function. The model accuracy is quite low at this time, and the precision of the fitted limit state boundary may be poor. This may lead to low accuracy of approximate design point, which may lead to improper importance directional density function. Some researchers suggest that to ensure the accuracy of design point, the condition $\left\|\mathbf{y}_{i}^{*}-\mathbf{y}_{i-1}^{*}\right\| / \left\|\mathbf{y}_{i-1}^{*}\right\| < \delta$, where \mathbf{y}_{i}^{*} is the design point in the *i*-th iteration and δ is a small positive constant in standard normal space, should be met (Jia and Wu 2022). As IDS method also needs to update Kriging model in the sample space defined by importance direction density function, using this strategy will inevitably generate many redundant training samples around the real design point, thus significantly increasing the required function calls.

This paper proposes a novel active learning strategy for IDS and adaptive Kriging model for reliability and failure probability-based global sensitivity analysis to solve the above problems, which is called Adaptive Kriging-Importance Directional Sampling-Reliability and Global Sensitivity (AK-IDS-RGS) method. First, an improved stopping criterion is proposed based on the idea of auxiliary region (Katafygiotis et al. 2007) to solve the problem that the stopping criterion of U function is too conservative. Then, an improved active learning strategy is proposed through the combination of optimization calculation and learning function, which realizes the synchronous updating of importance directional density function and Kriging model for the design point-based IDS, so as to ensure the accuracy of both Kriging model and importance directional density function with higher efficiency and avoid the

problem of only using approximate design point. Finally, the failure probability and failure samples obtained by IDS are adopted for variable global sensitivity analysis.

2 Importance directional sampling

DS is a uniform sampling strategy in the whole sample space. If the directional vector is only established in the importance region, DS will change into IDS. When the input random variables are converted to standard normal variables $\mathbf{Y} = (Y_1, Y_2, \dots, Y_n)$, the failure probability is calculated by:

$$p_f = \int_{\mathbf{B}} \frac{\left[1 - F_{\chi^2}\left(r_b^2\right)\right] f_{\mathbf{A}}(\mathbf{b})}{p_{\mathbf{B}}(\mathbf{b})} p_{\mathbf{B}}(\mathbf{b}) d\mathbf{b}$$
(1)

where **B** is the importance direction of **Y**. $p_{\mathbf{B}}(\mathbf{b})$ is the importance directional density function. $F_{\chi^2}(\cdot)$ is the cumulative distribution function of Chi-square distribution. r_b is the module of IDS sample point $\mathbf{b}.f_{\mathbf{A}}(\mathbf{b})$ is the uniform directional density function, which is expressed as:

$$f_{\mathbf{A}}(\mathbf{b}) = \Gamma(n/2) / \left(2\pi^{n/2}\right)$$
⁽²⁾

The IDS point $\mathbf{b}_i (i = 1, 2, \dots, N_{IDS})$ can be generated through $p_{\mathbf{B}}(\mathbf{b})$. Then Eq. (1) is estimated by:

$$\hat{p}_{f} = \frac{1}{N_{IDS}} \sum_{i=1}^{N_{IDS}} I(-r_{\mathbf{b}i}) \left[1 - F_{\chi^{2}}(r_{\mathbf{b}i}^{2}) \right] \frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}$$
(3)

where $I(\cdot)$ is the indicator function of r_{bi} . If $r_{bi} > 0$, $I(-r_{bi}) = 1$, otherwise $I(-r_{bi}) = 0$. $I(-r_{bi})$ is introduced here considering that there is no intersection at the limit state boundary along the direction of \mathbf{b}_i under the case of $r_{bi} < 0$. The variance of \hat{p}_f can be obtained by calculating the variance at both ends of Eq. (3), which is estimated by: $\mathbf{p}_{\mathbf{r}}(\mathbf{h})$ the following methodology

In order to determine $p_{\mathbf{B}}(\mathbf{b})$, the following methodology based on the design point could be adopted. In standard normal space, the tangent plane Z_L of the limit state boundary $Z = g_{\mathbf{Y}}(\mathbf{Y}) = 0$ at the design point \mathbf{y}^* is expressed as:

$$Z_L = \left\| \nabla g_{\mathbf{Y}}(\mathbf{y}^*) \right\| \left(\boldsymbol{\beta} - R \boldsymbol{\alpha}_{\mathbf{Y}}^{\mathsf{T}} \mathbf{B} \right) = 0$$
(5)

where $\boldsymbol{\alpha}_{\mathbf{Y}}$ is the directional vector at the design point, that is, $\boldsymbol{\alpha}_{\mathbf{Y}} = -\nabla g_{\mathbf{Y}}(\mathbf{y}^*) / \|\nabla g_{\mathbf{Y}}(\mathbf{y}^*)\|$. β is the reliability index. $\|\cdot\|$ is the norm of vector. For Eq. (5), in order to make $Z_L < 0$, $R\boldsymbol{\alpha}_{\mathbf{Y}}^{\mathrm{T}}\mathbf{B} > \beta$ is required. That is, the directional vector which satisfies the condition $\boldsymbol{\alpha}_{\mathbf{Y}}^{\mathrm{T}}\mathbf{B} > 0$ can direct to the importance region. If β is obtained, p_f can be approximately calculated by $p_f \approx \Phi(-\beta)$, where $\Phi(\cdot)$ is the cumulative distribution function of standard normal distribution. If only the importance region with $\boldsymbol{\alpha}_{\mathbf{Y}}^{\mathrm{T}}\mathbf{B} > 0$ is considered, submit $\Phi(-\beta)$ into Eq. (1), the following integral can be obtained based on Eq. (1):

$$\int_{\boldsymbol{\alpha}_{\mathbf{Y}}^{\mathbf{T}}\mathbf{B}>0} \frac{1}{\Phi(-\beta)} \left\{ 1 - F_{\chi^2} \left[\beta^2 / \left(\boldsymbol{\alpha}_{\mathbf{Y}}^{\mathbf{T}}\mathbf{b} \right)^2 \right] \right\} f_{\mathbf{A}}(\mathbf{b}) d\mathbf{b} \approx 1 \qquad (6)$$

Based on Eq. (6), $p_{\mathbf{B}}(\mathbf{b})$ can be selected as:

$$p_{\mathbf{B}}(\mathbf{b}) = \frac{1}{\Phi(-\beta)} \left\{ 1 - F_{\chi^2} \left[\beta^2 / \left(\mathbf{\alpha}_{\mathbf{Y}}^{\mathrm{T}} \mathbf{b} \right)^2 \right] \right\} f_{\mathbf{A}}(\mathbf{b})$$
(7)

When the directional vector meets the condition $\mathbf{\alpha}_{\mathbf{Y}}^{\mathbf{T}}\mathbf{B} > 0$, the generated IDS samples **b** are all located in the region $Z_L < 0$. If the nonlinearity degree of Z is low, Z can be approximated by Z_L around the design point, and Eq. (7) can completely cover the importance region. If the nonlinearity degree of Z at the design point is high, Z cannot be approximated by Z_L . The region Z < 0 is not completely included in $Z_L < 0$, and the direction $\mathbf{\alpha}_{\mathbf{Y}}^{\mathbf{T}}\mathbf{B} < 0$ should also be considered. In order to ensure that the samples fall into the region $Z_L \ge 0 \cap Z < 0$,

$$\begin{aligned} \operatorname{Var}\left(\hat{p}_{f}\right) &= \operatorname{Var}\left[\frac{1}{N_{IDS}}\sum_{i=1}^{N_{IDS}}I(-r_{\mathbf{b}i})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2})\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right] \\ &= \frac{1}{N_{IDS}^{2}}\sum_{i=1}^{N_{IDS}}\operatorname{Var}\left[I(-r_{\mathbf{b}i})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2})\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right] \\ &= \frac{1}{N_{IDS}}\operatorname{Var}\left[I(-r_{\mathbf{b}})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2})\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right] \\ &= \frac{1}{N_{IDS}}\operatorname{Var}\left[I(-r_{\mathbf{b}})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2})\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right] \\ &= \frac{1}{N_{IDS}}\operatorname{Var}\left[I(-r_{\mathbf{b}})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2}\right]\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right] \\ &\approx \frac{1}{N_{IDS}-1}\left\{\frac{1}{N_{IDS}}\sum_{i=1}^{N_{IIS}}\left[I(-r_{\mathbf{b}i})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2}\right]\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right]^{2} - \left[\frac{1}{N_{IDS}}\sum_{i=1}^{N_{IDS}}I(-r_{\mathbf{b}i})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2}\right]\frac{f_{\mathbf{A}}(\mathbf{b}_{i})}{p_{\mathbf{B}}(\mathbf{b}_{i})}\right]^{2}\right\} \\ &= \frac{1}{N_{IDS}-1}\left\{\frac{1}{N_{IDS}}\sum_{i=1}^{N}\left[I(-r_{\mathbf{b}i})\left[1-F_{\chi^{2}}(r_{\mathbf{b}i}^{2}\right]\right]^{2}\frac{f_{\mathbf{A}}(\mathbf{b}_{i})^{2}}{p_{\mathbf{B}}(\mathbf{b}_{i})^{2}}\right] - \hat{p}_{f}^{2}\right\} \end{aligned}$$

The COV of \hat{p}_f can be calculated by $_{\text{Cov}}(\hat{p}_f) = \sqrt{\text{Var}(\hat{p}_f)} / \hat{p}_f$.

a combination coefficient p could be adopted to combine Eqs. (7) and (2), as shown in Eq. (8):

$$p_{\mathbf{B}}(\mathbf{b}) = \left\{ p + \frac{1-p}{\Phi(-\beta)} \left\{ 1 - F_{\chi^2} \left[\beta^2 / \left(\mathbf{\alpha}_{\mathbf{Y}}^{\mathrm{T}} \mathbf{b} \right)^2 \right] \right\} f_{\mathbf{A}}(\mathbf{b}) \right\}$$
(8)

by defining p, the application scope of Eq. (7) can be expanded, which makes it more suitable for the limit state function with high nonlinearity. p is generally a small constant, which is usually assumed in the interval [0, 0.2]. If the nonlinearity degree of limit state function is high, p can be appropriately increased. Specially, if p = 0, all samples are located in the region $Z_L < 0$.

In order to generate samples based on Eq. (8), a following distribution is defined:

$$F_{V}(v) = \begin{cases} p\Phi(v) & v \le \beta\\ p\Phi(v) + (1-p) \left[1 - \frac{\Phi(-v)}{\Phi(-\beta)}\right] & v > \beta \end{cases}$$
(9)

If random samples are generated for variable V, the directional vector $\mathbf{Y} + (V - \boldsymbol{\alpha}_{\mathbf{Y}}^{\mathrm{T}} \mathbf{Y}) \boldsymbol{\alpha}_{\mathbf{Y}}$ is distributed on both sides of $Z_L = 0$. In order to generate random sample v, random samples u could be generated firstly based on standard uniform distribution, and v could be calculated by:

$$v = \begin{cases} \Phi^{-1}(u/p) & u \le p, \Phi^{-1}(u/p) \le \beta \\ -\Phi^{-1} \left[\frac{\Phi(-\beta)(1-u)}{1-p+p\Phi(-\beta)} \right] \text{ else} \end{cases}$$
(10)

Once *v* are obtained, the corresponding IDS sample **b** could be obtained, that is:

$$\mathbf{b} = \left[\mathbf{y} + \left(v - \boldsymbol{\alpha}_{\mathbf{Y}}^{\mathbf{T}} \mathbf{y} \right) \boldsymbol{\alpha}_{\mathbf{Y}} \right] / \left\| \mathbf{y} + \left(v - \boldsymbol{\alpha}_{\mathbf{Y}}^{\mathbf{T}} \mathbf{y} \right) \boldsymbol{\alpha}_{\mathbf{Y}} \right\|$$
(11)

Then the failure probability could be calculated by Eq. (3).

3 Global sensitivity analysis based on failure probability and Bayes theorem

Based on failure probability, the impact of *i*th variable Y_i is measured by:

$$s(y_i) = \left| \hat{p}_f - p_f(F|y_i) \right|$$
(12)

where $p_f(F|y_i)$ is the conditional failure probability, which is defined as:

$$p_f(F|y_i) = P\{g(\mathbf{Y}) \le 0|y_i\}$$
(13)

Based on Bayes theorem, $p_f(F|y_i)$ is rewritten as:

$$p_f(F|y_i) = \left(\hat{p}_f f_{Y_i}(y_i|F)\right) / f_{Y_i}(y_i)$$
(14)

where $f_{Y_i}(y_i|F)$ is conditional probability density function of Y_i in the failure region. Then the global sensitivity index could be calculated by:

$$\eta_i = \frac{1}{2} \int_{Y_i} \left| \hat{p}_f - p_f(F|y_i) \right| f_{Y_i}(y_i) dy_i = \frac{p_f}{2} \int_{Y_i} \left| f_{Y_i}(y_i) - f_{Y_i}(y_i|F) \right| dy_i$$
(15)

where $f_{Y_i}(y_i|F)$ is the conditional probability density function of Y_i . Equation (15) could be calculated by discreting $f_{Y_i}(y_i)$ and $f_{Y_i}(y_i|F)$ in the entire distribution region of Y_i , that is:

$$\eta_{i} = \frac{\hat{p}_{f}}{2} \sum_{j=1}^{N_{dis}} \left| f_{Y_{ij}}(y_{ij}) - f_{Y_{ij}}(y_{ij}|F) \right| \Delta(f)$$
(16)

where $\Delta(f)$ is the width of discrete interval of Y_i . N_{dis} is the number of discrete points. $f_{Y_{ij}}(y_{ij})$ and $f_{Y_{ij}}(y_{ij}|F)$ are the probability density function and the conditional probability density function values of Y_i at the j - th discrete point. In standard normal space, the distribution region of random variables could be defined in the interval of [-5,5] (Zhang et al. 2019). In Refs. (Wang et al. 2019; Guo et al. 2021; Lei et al. 2022), kernel density estimation is adopted to build $f_{Y_i}(y_i|F)$. However, it has some limitations, such as the bandwidth has a great impact on the estimation results, and the fitting of edge data is easy to make mistakes. In this paper, Gaussian mixture model (GMM) (Lu et al. 2017), which has stronger applicability than KDE, is used to fit $f_{Y_i}(y_i|F)$. The expression of GMM is:

$$f(\mathbf{y}_i) = \sum_{k=1}^{M} \pi_k N(\mathbf{y}_i | \mathbf{\mu}_k, \mathbf{\delta}_k)$$
(17)

where $N(\cdot)$ is the probability density function of normal distribution. *M* is the number of Gaussian distributions. π_k is the weight, and $\sum_{k=1}^{M} \pi_k = 1$. μ_k , δ_k are the mean and covariance matrix of the *k*th Gaussian distribution, respectively. In order to estimate μ_k , δ_k and π_k , expectation maximization (EM) method is often adopted, as shown in Eqs. (18)–(21).

$$\tau_{ij}^{k} = \left[\pi_{j} N(\mathbf{y}_{i} | \mathbf{\mu}_{j}, \mathbf{\delta}_{j})\right] / \left[\sum_{k=1}^{M} \left(\mathbf{y}_{i} | \mathbf{\mu}_{k}, \mathbf{\delta}_{k}\right)\right]$$
(18)

$$\pi_i^{k+1} = \frac{1}{n_d} \sum_{j=1}^{n_d} \tau_{ij}^k$$
(19)

$$\mu_i^{k+1} = \left[\sum_{j=1}^{n_d} \left(\tau_{ij}^k \mathbf{y}_j\right)\right] \middle/ \left(\sum_{j=1}^{n_d} \tau_{ij}^k\right)$$
(20)

$$\delta_i^{k+1} = \left\{ \sum_{j=1}^{n_d} \left[\tau_{ij}^k (\mathbf{y}_j - \boldsymbol{\mu}_i^k) (\mathbf{y}_j - \boldsymbol{\mu}_i^k)^T \right] \right\} \middle/ \left(\sum_{j=1}^{n_d} \tau_{ij}^k \right)$$
(21)

where n_d is the number of training samples. Through continuously iterating, the iteration stops when the variation of the likelihood function less than a small constant *eps*. eps = 1e - 12 is adopted to ensure the accuracy. The likelihood function is expressed as:

$$L(\mathbf{x}|\boldsymbol{\delta}) = \sum_{i=1}^{n_d} \ln\left(\sum_{k=1}^K \pi_k N(\mathbf{y}_k|\boldsymbol{\mu}_k, \boldsymbol{\delta}_k)\right)$$
(22)

function calls of IDS. The concept of Kriging model has been described in many previous researches, which will not be discussed in this paper. Learning function is the core of active learning. Presently, U and EFF are the most commonly used learning functions for active learning. Besides, Researchers also provided different learning functions, such as REIF (Zhang et al. 2019), ERF (Yang 2015) and H (Lv et al. 2015) functions. The above learning functions are shown in Eqs. (23)–(27). The adding point criterions of the above learning functions are $\mathbf{x}^* = \arg\min(\mathbf{U}(\mathbf{x})), \mathbf{x}^* = \arg\max(\text{EFF}(\mathbf{x})),$ $\mathbf{x}^* = \arg\max(\text{REIF}(\mathbf{x})), \quad \mathbf{x}^* = \arg\max(\text{ERF}(\mathbf{x}))$ and $\mathbf{x}^* = \arg\max(\text{H}(\mathbf{x}))$ respectively.

$$\mathbf{U}(\mathbf{x}) = \left| \mu_{\widehat{g}}(\mathbf{x}) \right| / \sigma_{\widehat{g}}(\mathbf{x})$$
(23)

$$EFF(\mathbf{x}) = \mu_{\widehat{g}}(\mathbf{x}) \left[2\Phi\left(\frac{-\mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \Phi\left(\frac{-2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \Phi\left(\frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] - \sigma_{\widehat{g}}(\mathbf{x}) \left[2\phi\left(\frac{-\mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \phi\left(\frac{-2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \phi\left(\frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] + 2\sigma_{\widehat{g}}(\mathbf{x}) \left[\Phi\left(\frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \Phi\left(\frac{-2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] \right]$$
(24)

As η is derived from \hat{p}_f and random generated failed sample points, the randomness of η should also be considered. Suggested by Refs. (Wang et al. 2019; Zhang et al. 2021), 20 independent runs of the method could be adopted to estimate the mean and standard deviation of η , which are defined as $\mu(\eta)$ and $\sigma(\eta)$ respectively. Then COV(η) = $\sigma(\eta)/\mu(\eta)$ could be used to measure the randomness.

4 Adaptive Kriging model

4.1 Learning function

This paper adopts the most commonly used adaptive Kriging model as the surrogate model to reduce the required

$$\operatorname{REIF}(\mathbf{x}) = \mu_{\widehat{g}}(\mathbf{x}) \left[1 - 2\Phi\left(\frac{\mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] + \sigma_{\widehat{g}}(\mathbf{x}) \left[2 - \sqrt{\frac{2}{\pi}} \exp\left(-\frac{1}{2}\frac{\mu_{\widehat{g}}(\mathbf{x})^{2}}{\sigma_{\widehat{g}}(\mathbf{x})^{2}}\right) \right]$$
(25)

$$\operatorname{ERF}(\mathbf{x}) = -\operatorname{sign}\left(\mu_{\widehat{g}}(\mathbf{x})\right)\mu_{\widehat{g}}(\mathbf{x})\Phi\left[-\operatorname{sign}\left(\mu_{\widehat{g}}(\mathbf{x})\right)\frac{\mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right] + \sigma_{\widehat{g}}(\mathbf{x})\varphi\left(\frac{\mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right)$$

$$(26)$$

$$H(\mathbf{x}) = \begin{vmatrix} \ln\left(\sqrt{2\pi}\sigma_{\widehat{g}}(\mathbf{x}) + 0.5\right) \left[\Phi\left(\frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) - \Phi\left(\frac{-2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] \\ - \frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{2} \phi\left(\frac{2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) + \frac{2\sigma_{\widehat{g}}(\mathbf{x}) + \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})} \phi\left(\frac{-2\sigma_{\widehat{g}}(\mathbf{x}) - \mu_{\widehat{g}}(\mathbf{x})}{\sigma_{\widehat{g}}(\mathbf{x})}\right) \right] \end{aligned}$$
(27)

4.2 Stopping criterion of learning function

In Ref. (Guo et al. 2020), the stopping criterion for U function is used for IDS. However, this criterion is too conservative and will introduce many redundant training samples. Presently, the error-based stopping criterion has been widely used to solve the problems. The size of samples \hat{S}_s which are failed predicted by Kriging model but actually reliable is subjected to a normal distribution, that is:

$$\widehat{S}_{s} \sim N\left(\mu_{\widehat{S}_{s}}, \sigma_{\widehat{S}_{s}}\right), \ \mu_{\widehat{S}_{s}} = \sum_{i=1}^{\widehat{N}_{s}} \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right), \\
\sigma_{\widehat{S}_{s}} = \sqrt{\sum_{i=1}^{\widehat{N}_{s}} \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right)\left[1 - \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right)\right]} \quad (28)$$

where N_s is the size of reliable samples predicted by Kriging model. In addition, the size of samples S_f which are reliable predicted by Kriging model but actually failed can be approximately represented by normal distribution with mean and standard deviation μ_s and σ_s respectively:

$$\widehat{S}_{f} \sim N\left(\mu_{\widehat{S}_{f}}, \sigma_{\widehat{S}_{f}}\right), \mu_{\widehat{S}_{f}} = \sum_{i=1}^{\widehat{N}_{f}} \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right),$$

$$\sigma_{\widehat{S}_{f}} = \sqrt{\sum_{i=1}^{\widehat{N}_{f}} \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right)\left[1 - \Phi\left(-\left|\frac{\mu_{\widehat{g}}\left(\mathbf{b}_{i}\right)}{\sigma_{\widehat{g}}\left(\mathbf{b}_{i}\right)}\right|\right)\right]}$$
(29)

where N_f is the size of failed samples predicted by Kriging model.

In order to ensure the fitting accuracy of Kriging model, the difference between \hat{N}_f and N_f should be small enough, where N_f is the size of samples which are actually failed. The maximum relative error κ between \hat{N}_f and N_f could be calculated by:



Fig. 1 Auxiliary region

$$\kappa = \left| \frac{\widehat{N}_f}{N_f} - 1 \right| \le \max\left(\left| \frac{\widehat{N}_f}{\widehat{N}_f - \widehat{S}_f^u} \right| - 1, \left| \frac{\widehat{N}_f}{\widehat{N}_f + \widehat{S}_s^u} \right| - 1 \right) = \kappa_{thr}$$

$$(30)$$

where S_f and S_s are the upper bounds of S_f and S_s respectively. When κ_{thr} small enough, the Kriging model is sufficient accuracy.

The error-based stopping criterion has been widely used in MC-based Kriging reliability methods. However, there are still some limitations. First, researchers have demonstrated that some additional samples with low contribution to the Kriging model will be introduced (Wang et al. 2022). Second, this criterion requires the distributions of both \hat{S}_f and \hat{S}_f . For IDS method, as most of the generated importance directional samples are distributed in the failure region, establishing the distributions of both \hat{S}_f and \hat{S}_f considering the number of reliable samples is unnecessary. This paper will propose a more concise stopping criterion, which is established based on the idea of auxiliary region. As shown in Fig. 1, the auxiliary region Ω_A is defined as the failure region fitted by Kriging model, and the real failure region is defined as Ω_R . Based on Bayes conditional probability formula, the real failure probability $p_f(\Omega_R)$ is defined as:

$$p_f(\Omega_R) = \frac{p_f(\Omega_A)p_f(\Omega_R|\Omega_A)}{p_f(\Omega_A|\Omega_R)}$$
(31)

where $p_f(\Omega_A)$ is the failure probability in Ω_A . The conditional failure probabilities $p_f(\Omega_R | \Omega_A)$ and $p_f(\Omega_A | \Omega_R)$ depend on the overlapping degree of Ω_A and Ω_R . Actually, the ratio of $\frac{p_f(\Omega_R | \Omega_A)}{p_f(\Omega_A | \Omega_R)}$ acts as a correction factor of $p_f(\Omega_A)$ to decrease the difference between $p_f(\Omega_R)$ and $p_f(\Omega_A)$. The closer $\frac{p_f(\Omega_R | \Omega_A)}{p_f(\Omega_A | \Omega_R)}$ to 1 means the lower difference and the higher fitting degree of Ω_R and Ω_A . Then, $\frac{p_f(\Omega_R | \Omega_A)}{p_f(\Omega_A | \Omega_R)}$ could be adopted to define a stopping criterion for Kriging.

Since the introduction of Eq. (31) is to determine whether the failure region can be accurately fitted by Kriging model, it is sufficient to ensure that the symbol of IDS samples can be judged correctly without real failure probability in this step. In regard of this, an estimation method based on the number of failure samples located in the corresponding region and the prediction uncertainty of Kriging model is proposed to estimate $p_f(\Omega_R | \Omega_A)$ and $p_f(\Omega_A | \Omega_R)$. According to Ref. (Yang et al. 2018), the predicted failure region in which the sign of performance function remains uncertain and the region with large probability to be negative are defined as S_f^u and S_f^l respectively:

$$S_{f}^{\mu} = \left\{ \mu | -\delta\sigma_{\widehat{g}}(\mathbf{b}) < \mu_{\widehat{g}}(\mathbf{b}) < 0 \right\}, S_{f}^{l} = \left\{ \mu | \mu_{\widehat{g}}(\mathbf{b}) \le -\delta\sigma_{\widehat{g}}(\mathbf{b}) \right\}$$
(32)

the predicted reliable region in which the sign of performance function remains uncertain and the region with large probability to be positive are defined as S_r^u and S_r^l respectively:

$$S_{r}^{u} = \left\{ \mu | 0 < \mu_{\widehat{g}}(\mathbf{b}) < \delta \sigma_{\widehat{g}}(\mathbf{b}) \right\}, S_{r}^{l} = \left\{ \mu | \mu_{\widehat{g}}(\mathbf{b}) \ge \delta \sigma_{\widehat{g}}(\mathbf{b}) \right\}$$
(33)

 δ = 1.96 could be adopted in Eqs. (32) and (33) to select the samples with large probability (larger than 95%) to be negative or positive. Therefore, the predicted failure samples distributed in S_f^l could be regarded as the real failure samples. Then $p_f(\Omega_R | \Omega_A)$ can be approximately calculated by the ratio of the number of samples falling in the corresponding region to the total number of samples, that is:

$$p_f(\Omega_R | \Omega_A) = N_{S_f} / N_{IDS}$$
(34)

where $N_{S_f^l}$ is the number of samples falling in the region S_f^l . For $p_f(\Omega_A | \Omega_R)$, as the number of real failure samples is unknown, based on the prediction uncertainty of Kriging model, the upper bound of the ratio of the number of samples in the real failure region to the total number of IDS samples can be adopted to define $p_f(\Omega_A | \Omega_R)$, that is:

$$p_f(\Omega_A | \Omega_R) \le \left(N_{S_f^u} + N_{S_f^l} + N_{S_r^u} \right) / N_{IDS}$$
(35)

where $N_{S_f^u}$ and $N_{S_r^u}$ are the numbers of samples falling in the regions S_f^u and S_r^u respectively. The purpose of introducing $N_{S_r^u}$ is to treat all samples which the sign of performance function is uncertain as failure samples, so as to increase the sample size in the auxiliary region, and the upper bound of $p_f(\Omega_A | \Omega_R)$ could be obtained. Then the auxiliary region-based stopping criterion is defined as:

$$\frac{p_f(\Omega_R | \Omega_A)}{p_f(\Omega_A | \Omega_R)} \ge \left(\frac{N_{S_f^l}}{N_{IDS}}\right) \middle/ \left(\frac{N_{S_f^u} + N_{S_f^l} + N_{S_r^u}}{N_{IDS}}\right)$$

$$= \frac{N_{S_f^l}}{N_{S_f^u} + N_{S_f^l} + N_{S_r^u}} \ge \kappa_{af}$$
(36)

 κ_{af} is a positive constant with the maximum value of 1. The larger κ_{af} means the higher coincidence degree of Ω_A and Ω_R . The purpose of Eq. (36) is to minimize the proportion of samples which the sign of performance function has large uncertainty in the total failure samples, so as to minimize the difference between Ω_A and Ω_R . If $N_{S_f^i} / \left(N_{S_f^u} + N_{S_f^i} + N_{S_r^u} \right) = 1$, it means that $N_{S_f^u}$ and $N_{S_r^u}$ are both 0, and Ω_R and Ω_A complete overlap.

4.3 The proposed active learning strategy for IDS

As mentioned in Introduction, the approximate design pointbased importance directional density function may be not accurate enough. This paper proposes an improved active learning strategy. Its main idea is to synchronize the calculation process of design points and Kriging model updating, rather than calculating separately.

Suggested by Ref. (Jia and Wu 2022), the essence of calculating design point in standard normal space is to solve the following optimization problems:

$$\mathbf{y}^* = \arg \max f(\mathbf{y})$$

s.t. $\hat{g}(\mathbf{y}) = 0$ (37)

where $\hat{g}(\mathbf{y}) = 0$ is the current limit state boundary. $f(\mathbf{y})$ is the joint probability density function of input variables. Equation (37) could be solved by gradient-based algorithms or other evolutionary algorithms. Based on Eqs. (11) and (37), the proposed active learning strategy is summarized as follows: First, calculate the design point through Eq. (37), and the obtained design point should be added into the current training set of Kriging model. Then, based on this design point, establish the importance directional sampling function through Eq. (8), and the importance directional samples are generated through Eq. (37). Next, take these important directional samples as current candidate sample set, and Kriging model is updated through learning function in the current sample space. The updating process stops when the stopping criterion defined by Eq. (36) is satisfied, and the failure probability could be obtained through Eq. (7). Finally, use Eq. (37) to solve the new design point based on the updated Kriging model. Re-build the importance directional density function and re-generate importance directional candidate sample set. Repeat the above steps and stop calculating when the final stopping criterion is satisfied. The final stopping criterion is defined as:

$$\left| \hat{p}_{f}^{i} - \hat{p}_{f}^{i-1} \right| / \hat{p}_{f}^{i-1} < \delta \cap \left| \hat{p}_{f}^{i-1} - \hat{p}_{f}^{i-2} \right| / \hat{p}_{f}^{i-2}$$

$$< \delta \cap \left| \hat{p}_{f}^{i} - \hat{p}_{f}^{i-2} \right| / \hat{p}_{f}^{i-2} < \delta$$

$$(38)$$

where \hat{p}_{f} is the obtained *i*-th failure probability. The meaning of Eq. (38) is: when the relative error of failure probability for three consecutive times is less than δ , the accuracy is considered to be sufficient, so as to output the final result.

Compared with Ref. (Guo et al. 2020), the major advantage of the proposed active learning strategy is that it realizes the synchronization of Kriging model updating and importance directional density function establishment, rather than only establishing the importance directional density function through the approximate design point, and it will also not put too much computation cost in the process of calculating design point. Since the design point has the largest contribution to failure probability on limit state boundary, adding the obtained design point into the training set is very helpful for the fitting of limit state boundary of Kriging model. Also, the candidate samples generated by the importance directional density function can be used to update Kriging model in the current sample space through learning function, which can not only improve the fitting accuracy of limit state boundary, but also improve the accuracy of design point, thus the update of importance directional density function in the next iteration is achieved. In this way, after satisfying the final stopping criterion, more accurate importance directional density function and failure probability could be obtained at the same time.

5 Summarized of the proposed method

Based on previous sections, the steps of the proposed AK-IDS-RGS method for reliability and global sensitivity analysis are summarized as follows:

- **Step 1** Transform the random variables into standard normal space, and establish the initial Kriging model. Suggested by Ref. (Zhang et al. 2019), the samples with the population $N = \max(12, n)$ are generated by Sobol sequence as the initial training set in the interval [-5,5]. Calculate the real values of limit state function of these samples. Through the initial training set, the initial Kriging model is established.
- **Step 2** Calculate design point y^* and direction vector α_Y through the current Kriging model based on Eq. (37).
- **Step 3** Generate random samples \mathbf{y}_i , $i = 1, 2, \dots, N_{ids}$ and u_i , $i = 1, 2, \dots, N_{ids}$ through standard normal distribution and standard uniform distribution in the interval [0, 1], respectively.
- **Step 4** Calculate IDS samples \mathbf{b}_i , $i = 1, 2, \dots, N_{ids}$ based on Eq. (11). The sample set containing all IDS samples is defined as the candidate sample set for active learning.
- **Step 5** Calculate the value of learning function of all candidate samples. According to the learning function of adaptive Kriging model, the optimal sample point is selected and added to the training set. Calculate the real value of performance

function of the optimal point, and update the Kriging model.

- **Step 6** Judge the stopping criterion of Kriging model in the current sample space. If the stopping criterion defined by Eq. (36) is satisfied, stop the active learning process and turn to Step 7. Otherwise, return to Step 6 and update the Kriging model. In order to ensure the accuracy, $\kappa_{af} = 0.98$ is adopted.
- **Step 7** Calculate \hat{p}_f and $Var(\hat{p}_f)$ through Eqs. (3) and (4) respectively through the Kriging model.
- **Step 8** Return to Step 2 and re-calculate \mathbf{y}^* and $\boldsymbol{\alpha}_{\mathbf{Y}}$ through the current Kriging model based on Eq. (37). Repeat Step 2-Step 7 until the final stopping criterion defined by Eq. (38) is satisfied. This paper adopts $\delta = 0.05$. If the final stopping criterion is satisfied, output \hat{p}_f and $\operatorname{Var}(\hat{p}_f)$ in the last iteration as the final result. Otherwise, return to Step 2 and obtain new \mathbf{y}^* and $\boldsymbol{\alpha}_{\mathbf{Y}}$.
- **Step 9** Judge whether the $Cov(\hat{p}_f)$ meets the accuracy requirement. This paper selects 5% as the threshold. If $Cov(\hat{p}_f) < 5\%$, output \hat{p}_f and $Cov(\hat{p}_f)$ as the final results. Otherwise, return to Step 3 to expand the candidate sample set.
- **Step 10** Select all failure samples. Calculate global sensitivity index η_i for each input variable through Eq. (15) based on GMM. Based on Eq. (32), the failure samples are distributed in the region S_{t}^l .

The proposed AK-IDS-RGS is the further development of AK-IDS (Guo et al. 2020). The following major improvements are made: (1) A novel auxiliary region-based stopping criterion is introduced based on the size of failure samples, which can reduce the number of training samples and improve the efficiency of active learning. (2) An improved active learning strategy is proposed based on optimization and active learning function, which realizes the synchronous updating of importance directional density function and Kriging model, instead of only establishing importance directional density function through the approximate design point. The flow chart of the proposed AK-IDS-RGS is presented in Fig. 2.



(a) AK-MCS

Fig. 3 Sample distribution of different methods

6 Numerical examples

In this section, five numerical examples are used to illustrate the proposed method. MC method is used as the benchmark, and the relative error is calculated by $\left|\hat{p}_{f} - pf_{mc}\right| / pf_{mc}$, where pf_{mc} is the failure probability calculated by crude MC. Several existing methods are used for comparative calculation, including AK-MCS, AK-IS, AK-DIS, AK-MCS-ESC-U, AK-MCS-ESC-EFF and AK-IS-ESC. Each method is independently calculated for 20 times, and the mean values are taken as the final results. In addition, in order to select the optimal active learning strategy, the learning functions in Eqs. (23)–(27) are adopted on the proposed AK-IDS-RGS respectively, and performance of different learning functions will be studied.

6.1 A simple performance function with two random variables

This section studies a bi-dimensional performance function (Zhou et al. 2015), as shown in Eq. (39), where x_1 and x_2 are both standard normal variables.

$$g_1 = \exp\left(0.2x_1 + 1.4\right) - x_2 \tag{39}$$

U function is adopted on AK-IDS-RGS firstly. Figure 3 shows the distribution characteristics of candidate samples and the fitting accuracy of limit state boundary of AK-MCS, AK-IS and AK-IDS-RGS. The fitting accuracy of limit state boundary by Kriging models of the three methods are all relatively high. However, a large number of candidate samples are required in AK-MCS. Also, a large number of samples fall outside the failure region, which are very far from the

Method	$p_f(10^{-4})$	Function calls	Relative error (%)	COV (%)	Candidate sample size
MC	3.5635	8e6	/	1.87	8e6
AK-MCS	3.5296	22.2	0.95	1.91	8e6
AK-IS	3.6036	21.5	1.13	1.57	2e4
AK-DIS	3.6014	23.5	0.95	1.54	2e3
AK-MC-ESC-U	3.5473	17.8	0.45	1.89	8e6
AK-MC-ESC-EFF	3.5903	22.4	0.75	1.89	8e6
AK-IS-ESC	3.6153	19.6	1.45	1.92	2e4
AK-IDS-RGS	3.5533	21.2	0.29	1.13	2e3

Table 2	Results of AK-IDS-
RGS un	der different learning
functior	is in Example 1

Table 1Results of differentmethods in Example 1

Method	$p_f(10^{-4})$	Function calls	Relative error (%)	COV (%)	Candidate sample size
AK-IDS-RGS-EFF	3.6009	20.4	1.05	1.16	2e3
AK-IDS-RGS-REIF	3.5745	22.3	0.31	1.17	2e3
AK-IDS-RGS-ERF	3.5706	22.9	0.20	1.14	2e3
AK-IDS-RGS-H	3.6039	19.5	1.13	1.15	2e3

Fig. 4 Results of global sensitivity analysis in Example 1







Fig. 5 Aero-engine turbine disk

limit state boundary. AK-IS method significantly reduces the number of candidate samples, but there are still about 50% of the points falling outside the failure region. Compared with AK-MCS and AK-IS, the required candidate samples in AK-IDS-RGS-U are much smaller, and most of these samples are located in the failure region. Although a few training points are distributed far from the limit state boundary, the fitting degree of Kriging model is still high, and the total number of training points is less than MC and IS methods. Therefore, AK-IDS-RGS can effectively obtain the failure samples for reliability and sensitivity analysis. The results of different methods are listed in Table 1. It can be seen that the accuracy of these methods is relatively high, as the relative error and COV are all less than 2%. However, the required computer memory has great differences. The candidate sample size of AK-IDS-RGS is only 2e3, while the required candidate samples of MC- and ISbased Kriging methods are 8e6 and 2e4 respectively. Therefore, the required computation cost of the proposed method is significantly lower than MC and IS.

The results of AK-IDS-RGS under different learning functions are shown in Table 2, where "-EFF" means that the EFF learning function is adopted. It can be seen that the relative errors of the four learning functions are all lower that 1.2%, and the required function calls also have little difference. Therefore, all learning functions can obtain high accuracy failure probability based on the proposed AK-IDS-RGS method in this example.

The global sensitivity index is calculated based on failure probability and Bayes theorem through GMM. This paper only discusses the results based on AK-IDS-RGS under different learning functions, and the index based on MC method is used as benchmark. The results are shown in Fig. 4. From Fig. 4a, it can be seen shown that x_2 is more influential than x_1 on the failure probability. In AK-IDS-RGS, all learning functions can judge the relative importance of the two variables, and the values of $\mu(\eta)$

Table 3Random variables inExample 2		σ_s	ρ	С		Α	H_J	w
Ĩ	Mean	2e9	8240	5.6	57	6.2e-3	1.22e-4	200
	COV (%)	10	20	20		10	10	10
Table 4Results of differentmethods in Example 2	Method	p	$p_f(10^{-4})$	Function ca	lls	Relative error (%)	COV (%)	Candidate sample size
	MC	2	.1320	1e7		/	2.17	1e7
	AK-MCS	2	.0473	109.4		3.97	2.22	1e7
	AK-IS	2	.2018	88.9		3.27	2.18	1e4
	AK-DIS	2	.1702	81.3		1.79	2.32	2e3
	AK-MC-ESC-U	2	.0835	76.5		2.27	2.26	1e7
	AK-MC-ESC-EFF	2	.2284	69.2		4.52	2.31	1e7
	AK-IS-ESC	2	.1085	78.4		1.10	2.36	1e4
	AK-IDS-RGS	2	.1212	63.7		0.51	1.58	2e3
Table 5 Results of AK-IDS-	Method		(10^{-4})		alle	Palativa arror	COV (%)	Candidate
RGS under different learning functions in Example 2	Method		$p_f(10)$	T unction c.	ans	(%)		sample size
	AK-IDS-RGS-EFF		2.1655	59.3		1.57	1.62	2e3
	AK-IDS-RGS-REIF	7	2.1715	77.4		1.85	1.54	2e3
	AK-IDS-RGS-ERF		2.1949	62.1		2.95	1.49	2e3
	AK-IDS-RGS-H		2.2123	63.9		3.77	1.53	2e3

calculated by different learning functions also have little difference. Therefore, AK-IDS-RGS can effectively obtain the failed samples with less candidate samples and computer memory, which is very suitable for failure probability-based global sensitivity analysis. From Fig. 4b, it can be seen that the $COV(\eta)$ of all learning functions are lower than 3%, which illustrates that the proposed method can obtain high robustness global sensitivity index.

6.2 An aero-engine turbine disk

The aero-engine turbine disk is studied in this section, as shown in Fig. 5 (Yun et al. 2020). The performance function is defined as:

$$g_2 = \sigma_s A - \frac{C(2\pi w)^2}{2\pi} + 2\rho(2\pi w)^2 H_J$$
(40)

where $\sigma_s, \rho, C, A, H_J$ and w are the ultimate strength, mass density, coefficient, cross-sectional area, cross section moment of inertia and rotational frequency, respectively. The information of random variables is listed in Table 3, and all variables are independent normal variables. The failure probabilities are listed in Table 4. Comparing AK-IDS-RGS with AK-MCS and AK-IS methods, the number of candidate samples of AK-IDS-RGS is only 2e3, and the number of required function calls is only 63.7. These illustrate that the proposed method has high efficiency with lower computer memory. The required function calls of AK-DIS is 81.3, the efficiency is much lower than the proposed AK-IDS-RGS. The results show that the proposed method can increase the efficiency of active learning of IDS.

The results of AK-IDS-RGS under different learning functions are listed in Table 5. The number of required function calls of EFF is 59.3, which the lowest in the five learning functions. The relative error of H is 3.77%, the accuracy is lower than other functions. The relative errors of REIF



(a) U performance function value





(b) EFF performance function value



(d) EFF failure probability

Fig. 6 Iteration curves of performance function values of training points and failure probability in Example 2





Fig. 8 Conical structure

Table 6 Random variable parameters in Example 3

Random variable	Meaning	Mean	Standard deviation	
E(Pa)	Young's modulus	7e10	3.5e9	
<i>t</i> (m)	Thickness	0.0025	0.000125	
α (rad)	Slope angle	0.524	0.01048	
<i>r</i> ₁ (m)	Internal radius	0.9	0.0225	
$M(N \cdot m)$	Bending moment	90,000	8000	
$P(\mathbf{N})$	Axial load	20,000	1000	
μ	Poisson's ratio	0.3	0.05	
γ	Experimental coef- ficient	0.33	0.033	
λ	Experimental coef- ficient	0.41	0.041	

and ERF functions are 1.85% and 2.95% respectively, which means that the accuracy of the two functions is also slightly lower than EFF and U functions. The iteration curves of the performance function values of training points and failure probability based on U and EFF learning functions by one calculation are shown in Fig. 6. It can be seen that when the number of added samples is larger than 20, the performance function values of added samples are very close to 0, which means that the proposed active learning strategy can effectively obtain the samples around the limit state boundary. In addition, the numbers of failure probability calculations for the U and EFF functions are 13 and 12 respectively, which means that the number of added design point are 13 and 12 respectively. Therefore, after the design point calculation is completed, the number of samples added based on the current Kriging model is approximately 4–5, and the number of training points based on solving design point is significantly less than the number of training points based on learning function.

The global sensitivity indexes calculated by AK-IDS-RGS are shown in Fig. 7 The most influential variable is *w*, while the variable with the least impact is *C*. The learning functions of which the variable sensitivity index order is consistent with MC are U, EFF and H functions, and the $COV(\hat{\eta})$ of all variables are all lower than 5%. This illustrates that the proposed AK-IDS-RGS can obtain sensitivity indexes with high robustness. Therefore, combining sensitivity index and failure probability, the suitable learning functions for AK-IDS-RGS should be U, EFF and H functions in this example.

6.3 A conical structure

A conical structure (Huang et al. 2021) is used in this section, as shown in Fig. 8.

The performance function of this example is defined as:

$$g_3 = 1 - \frac{\sqrt{3(1-\mu^2)}}{\pi E t^2 \cos^2 \alpha} \left(\frac{P}{2\gamma} + \frac{M}{\lambda r_1}\right)$$
(41)

the random variables are listed in Table 6. All of them are independent normal variables, and the results are shown in Table 7. The required candidate samples of AK-IDS-RGS are 2e3, which are much lower than MC- and IS-based **Table 7** Results of differentmethods in Example 3

Method	$p_f(10^{-5})$	Function calls	Relative error (%)	COV (%)	Candidate sample size
MC	7.7150	2e7	/	2.55	2e7
AK-MCS	8.1330	621.6	5.42	2.51	2e7
AK-IS	7.8751	643.8	2.08	2.33	1e4
AK-DIS	7.9231	441.9	2.70	2.16	2e3
AK-MC-ESC-U	7.9118	337.2	2.55	2.42	2e7
AK-MC-ESC-EFF	7.9284	251.7	2.77	2.38	2e7
AK-IS-ESC	7.5927	273.5	1.59	2.47	1e4
AK-IDS-RGS	7.8127	155.7	1.27	1.98	2e3
Method	$p_f(10^{-5})$	Function calls	Relative error (%)	COV (%)	Candidate sample size
AK-IDS-RGS-EFF	7.6804	161.8	0.42	2.04	2e3
AK-IDS-RGS-REIF	8.2140	151.6	6.42	2.07	2e3
AK-IDS-RGS-ERF	7.8933	155.3	2.31	1.86	2e3
AK-IDS-RGS-H	7 6241	160.2	1.18	1 95	2e3

Table 8Results of AK-IDS-RGS under different learningfunctions in Example 3

methods. Therefore, IDS can significantly reduce the candidate sample size in active learning. For MC- and IS-based methods, the required function calls are all larger than 200. In addition, the required function calls of AK-IDS-RGS are only 155.7, which is the lowest in the methods listed in Table 7. The relative error of AK-IDS-RGS is 1.27%, which means that the proposed method also has high accuracy. The required function calls of AK-DIS is 441.9, which is much higher than AK-IDS-RGS. The results show that the proposed active learning strategy is more suitable for IDS.

The results of AK-IDS-RGS under different learning functions are shown in Table 8. The relative error of REIF is 6.42%, the accuracy is lower than other learning functions. The required function calls of AK-IDS-RGS under REIF is 151.6, which is the lowest in the five learning functions, but the relative error is 6.42%, the accuracy is the lowest. The relative error of ERF is 2.31%, which is slightly larger than U and EFF. The learning function with the highest accuracy is EFF, as the relative error is only 0.42%. Therefore, U, EFF, H and ERF could be adopted on AK-IDS-RGS in this example. The iteration curves of the performance function values of training points and failure probability based on U and EFF learning functions by one calculation are shown in Fig. 9. The numbers of failure probability calculations are 8 and 9, respectively, which are is significantly less than the total number of training samples. The results show that the active learning method proposed in this paper does not require too much computation cost in design point calculation.

The results of global sensitivity index are shown in Fig. 10. λ and *t* have the most significant impact on the failure probability, while *P* and γ have little impact. The sensitivity indexes obtained by U, EFF and H functions are slightly different from those of MC method, while the sensitivity indexes obtained by REIF and ERF functions have big difference comparing with MC. From the $COV(\hat{\eta})$, it can be seen that the $COV(\hat{\eta})$ of all variables under U, EFF, and H functions are all lower than 5%. Under other learning functions, the $COV(\hat{\eta})$ of some variables are larger than 10% or even 15%. Therefore, combining the results of failure probability and global sensitivity index, U, EFF, and H functions are suitable for AK-IDS-RGS in this example.

6.4 Automobile front axle beam

The reliability of the automobile front axle beam is studied in this section, as shown in Fig. 11. The performance function is written as:

$$g_{4} = \sigma_{s} - \sqrt{\sigma^{2} + 3\tau^{2}}$$

$$\sigma = M / W_{x}, \tau = T / W_{\rho}$$

$$W_{x} = \frac{a(h-2t)^{3}}{6h} + \frac{b}{6h} [h^{3} - (h-2t)^{3}]$$

$$W_{\rho} = 0.8bt^{2} + 0.4 [a^{3}(h-2t)/t]$$
(42)



Fig. 9 Iteration curves of performance function values of training points and failure probability in Example 3





(a) Front axle



(b) Dangerous cross section

Table 9Random variablesparameters in Example 4		$\sigma_s(\mathbf{N} \cdot \mathbf{m})$	m) <i>a</i> (mm)	<i>b</i> (mm)	t(mm)) <i>h</i> (mm)	$M(N \cdot mm)$	$T(N \cdot mm)$
	Mean	580	12	65	14	85	3.5e6	3.1e6
	Standard derivation	40	0.06	0.325	0.07	0.425	1.75e6	1.55e5
Table 10 Results of different methods in Example 4	Method		$p_f(10^{-4})$	Function ca	lls	Relative error	COV (%)	Candidate
						(70)		
	MC		1.5430	1e7		/	2.55	1e7
	AK-MCS		1.4830	77.1		3.89	2.62	1e7
	AK-IS		1.4938	71.5		3.19	2.14	1e5
	AK-DIS		1.5625	65.8		1.26	2.72	2e3
	AK-MC-ESO	C-U	1.6140	51.2		4.60	2.53	1e7
	AK-MC-ESO	C-EFF	1.5150	48.5		1.81	2.49	1e7
	AK-IS-ESC		1.4048	39.4		8.89	1.83	1e5
	AK-IDS-RG	S	1.5587	37.3		1.02	1.55	2e3
Table 11 Results of AK-IDS-	Method		$p_f(10^{-4})$	Function c	alls	Relative error	COV (%)	Candidate
functions in Example 4			1)())			(%)		sample size
1	AK-IDS-RG	S-EFF	1.5261	38.5		1.10	1.45	2e3
	AK-IDS-RG	S-REIF	1.6055	44.8		4.05	1.49	2e3
	AK-IDS-RG	S-ERF	1.4703	42.7		4.71	1.58	2e3
	AK-IDS-RG	с-н	1 4688	47.2		4.81	1.51	203

The information of random variables is listed in Table 9. All variables are independent normal random variables. The results of failure probability are shown in Table 10. The required candidate sample size of AK-IDS-RGS is 2e3, and the required function calls and relative error are 37.3 and 1.02% respectively. The number of required function calls of AK-IDS-RGS is the lowest compared with other techniques, and the candidate sample size of IDS is much smaller than MC and IS. The results show that the efficiency of AK-IDS-RGS is much higher than MC- and IS-based Kriging method. Compared with AK-IDS-RGS, the number of required function calls of AK-DIS is 65.8. Once again, the results show that the proposed active learning strategy can effectively reduce the number of training samples in IDS.

Initial samples

30

40

Added samples

0



(c) U failure probability



20



(d) EFF failure probability





Fig. 13 Results of global sensitivity analysis in Example 4

Fig. 12 Iteration curves of

ability in Example 4

Fig. 14 Latch lock mechanism of hatch



Table 12 Random variable parameters in Example 5

	$\alpha_1(^\circ)$	r(mm)	$L_1(\text{mm})$	<i>L</i> ₂ (mm)	e(mm)
Mean	0.7844	44.4162	114	144	41
COV (%)	2	2	2	2	2

The results of AK-IDS-RGS under different learning functions are shown in Table 11. The relative error of AK-IDS-RGS under EFF is 1.10%, while the relative errors under REIF, ERF and H functions are both larger than 4%. The required function calls of U and EFF also have little difference, which are all lower than 40, while the required function calls of other three functions are all larger than 40. Therefore, in terms of failure probability, U and EFF functions could be adopted on the proposed method in this example. The iteration curves of the performance function values of training points and failure probability based on U and EFF learning functions by one calculation are shown in Fig. 12.

The global sensitivity indexes are shown in Fig. 13. It can be seen that T and M have the most significant impact on the failure probability, while t and h have little impact. The orders of sensitivity indexes under U, EFF, and H functions are same as those of MC. While in other functions, the orders of some variables are miscalculating. For instances, in REIF, the order of σ_s and a is opposite. In addition, the COV(η) of all variables under U and EFF functions are all lower than 5%. However, the COV(η) of some variables under other learning functions are higher than 10%, even 15%. Therefore, comprehensively considering failure probability and global sensitivity index, the suitable functions should be U and EFF in this example.

6.5 Latch lock mechanism of hatch

A latch lock mechanism of hatch is studied, as shown in Fig. 14 (Ling and Lu 2021). Table 12 illustrates the information of input variables, which are all independent normal variables.

The limit state function of this example is defined as:

$$g_5 = r\cos(\alpha_1) + \sqrt{L_1^2 - (e - r\sin(\alpha_1))^2} + L_2 - L_3 \quad (43)$$

where $L_3 = 270$ mm. The results of failure probability are shown in Table 13. It can be seen that the failure probability of this example is very small, which reaches the level of 10^{-7} . 5e9 candidate samples are required in MC to obtain a robust failure probability. The efficiency is very low, and the required computer memory is very large. Therefore, the MC-based Kriging methods are not used for comparison in this example. The relative errors of AK-IS and AK-IS-ESC are 11.14% and 10.50% respectively, the accuracy of these two methods is quite low. Also, the required function calls of IS-based method are all larger than 300, the efficiency is quite low. For the proposed AK-IDS-RGS, the required function calls of AK-IDS-RGS and AK-DIS are 46.6 and 253.2 respectively, and the relative errors are 1.92% and 3.13% respectively. Compared with AK-DIS, AK-IDS-RGS can significantly reduce the number of required function calls without losing accuracy. Therefore, the proposed active learning strategy can effectively reduce the required function calls.

The results of AK-IDS-RGS under different learning functions are shown in Table 14. The required function calls of the five learning functions have little difference. However, the relative errors under REIF and ERF functions are 11.20% and

Table 13Results of differentmethods in Example 5	Method	$p_f(10^{-7})$	Function calls	Relative error (%)	COV (%)	Candidate sample size
	MC	2.1880	5e9	/	3.20	5e9
	AK-IS	2.4317	439.6	11.14	3.41	4e7
	AK-DIS	2.1195	253.2	3.13	2.68	5e9
	AK-IS-ESC	2.4178	399.5	10.50	3.67	4e7
	AK-IDS-RGS	2.2300	46.6	1.92	1.85	4e3
Table 14 Results of AK-IDS- RGS under different learning functions in Example 5	Method	$p_f (10^{-7})$) Function calls	Relative error (%)	COV (%)	Candidate sample size
	AK-IDS-RGS-EFF	2.2171	55.7	1.33	1.65	4e3
	AK-IDS-RGS-REI	F 2.4331	62.5	11.20	1.46	4e3
	AK-IDS-RGS-ERF	2.0972	47.8	4.15	1.53	4e3
	AK-IDS-RGS-H	2.2261	44.1	1.74	1.48	4e3



Fig. 15 Iteration curves of performance function values of training points and failure probability in Example 4



4.15% respectively, the accuracy of the two functions is quite low. If U, EFF and H functions are used, the accuracy of AK-IDS-RGS will be very high, as the relative errors are all lower than 3%. The results show that AK-IDS-RGS is also suitable for the reliability problem with small failure probability. The iteration curves of the performance function values of training points and failure probability based on U and EFF learning functions by one calculation are shown in Fig. 15.

 Table 15
 Results of AK-IDS-RGS under error-based stopping criterion

Examples	<i>P</i> _f	Function calls	Relative error (%)	COV (%)	Candidate sample size
Example 2	2.2332e-4	67.5	2.07	1.45	2e3
Example 3	7.6917e-5	259.5	0.30	1.68	2e3
Example 4	1.5003e-4	57.4	2.77	1.39	2e3
Example 5	2.2239e-7	138.7	1.64	1.26	4e3

The global sensitivity indexes of AK-IDS-RGS are shown in Fig. 16. The orders of sensitivity indexes under different learning functions are all the same as those of MC. The results show that the combination of IDS and failure probability-based global sensitivity analysis can effectively evaluate the relative importance of random variables. The $COV(\hat{\eta})$ of all variables under U and EFF functions are all lower than 5%. Therefore, the proposed AK-IDS-RGS can effectively and accurately evaluate the global sensitivity index under U and EFF learning functions.

6.6 Discussion about the proposed method

6.6.1 The derived variance formula of IDS-based failure probability

The variance of failure probability calculated by the design point-based IDS method is derived in this paper, and it is adopted on the proposed AK-IDS-RGS to calculate COV. In Ref. (Guo et al. 2020), the MC-based COV formula is directly used for AK-DIS. This section will verify the effectiveness of the derived variance formula. Since the formula of failure probability variance is only related to the calculation method, this section will not use Kriging model. The failure probability is directly calculated through the performance function and the design point is calculated by Eq. (37). Based on the candidate sample size defined by the derived variance formula, each performance function is independently calculated by IDS for 20 times, and the COV of failure probability is obtained through statistical analysis. The results of the five examples are 1.49%, 1.85%, 2.43%, 2.48% and 2.58% respectively. It can be seen that the difference between the results of statistical analysis and derived formula is small. In addition, if the MC-based COV formula is adopted for IDS, the candidate sample size should be same as MC, and the results of COV are 1.85%, 2.21%, 2.51%, 2.62% and 2.39% respectively, the difference between the

Table 16 Results of AK-IDS-RGS under segmented learning strategy

Examples	p_f	Function calls	Relative error (%)	COV (%)	Candidate sample size
Example 2	2.1586e-4	66.7	1.34	1.56	2e3
Example 3	7.9251e-5	162.8	2.72	1.44	2e3
Example 4	1.5716e-4	55.0	1.85	1.62	2e3
Example 5	2.2158e-7	60.3	1.27	1.38	4e3

MC-based formula and the derived formula is also quite small. The results show the effectiveness of the derived variance formula of IDS. Therefore, if MC-based COV formula is directly used, it will cause many unnecessary samples.

6.6.2 The auxiliary region-based stopping criterion

This section will compare the performance between the proposed auxiliary region-based and the existed error-based stopping criterions through the optimal U learning function. As the difference between different methods in Example 1 is guite small, only Examples 2–5 are used in this section. Suggested by Refs. (Yun et al. 2021), the maximum relative error is defined as 0.05, and the error-based stopping criterion is adopted in the proposed active learning strategy, Step 7. Each example is also independently calculated 20 times, and the mean results are taken as the final results, as shown in Table 15. It can be seen that the relative errors of the four examples are all lower than 3%, which means that the error-based stopping criterion can also obtain high accuracy failure probability. However, the number of required function calls is much larger than the proposed auxiliary region-based stopping criterion, since the required function calls of auxiliary region are 63.1, 155.7, 37.3 and 46.6 respectively. Especially in Examples 3 and 5, the number of required function calls has increased by nearly 100 times. This illustrates that the convergence of the proposed auxiliary region-based stopping criterion is significantly higher than the existed error-based stopping criterion in IDS.

6.6.3 The proposed active learning strategy

Besides the auxiliary region-based stopping criterion, the purpose of the proposed active learning strategy is to realize the synchronization of Kriging model updating and importance directional density function establishment. It is noted that if the condition $\|\mathbf{y}_{i}^{*} - \mathbf{y}_{i-1}^{*}\| / \|\mathbf{y}_{i-1}^{*}\| < \delta$ is adopted firstly before using learning function to update Kriging

model, it will also obtain a precise design point, which can also ensure the accuracy of importance directional density function. The method of ensuring the accuracy of design point firstly and then calculating failure probability is called segmented learning strategy in this paper. This section will compare the performance between the two strategies. $\delta = 0.05$ is adopted to ensure the accuracy of design point, and the auxiliary region-based stopping criterion is adopted in Kriging model updating through U function. The results of segmented learning strategy are shown in Table 16. It can be seen that the relative errors are all lower than 3%, which means that both the two active learning strategies have high accuracy. However, in Examples 3-5, the required function calls of segmented learning strategy are 162.8, 55 and 60.3 respectively, which shows that the segmented learning strategy will increase dozens of function calls compared with the synchronized learning strategy. Therefore, the proposed active learning strategy is more suitable for IDS.

7 Conclusions

In this paper, an improved active learning Kriging model is proposed for IDS reliability and failure probability-based global sensitivity analysis, which is called AK-IDS-RGS method. A novel auxiliary region-based stopping criterion based on the size of failure samples is introduced for IDS to accelerate the efficiency of active learning, and an improved active learning strategy based on optimization and learning function, which realizes the synchronization of Kriging model updating and importance directional density function establishment is established. Different learning functions are adopted on AK-IDS-RGS respectively to select the most suitable active learning strategy. The failure probability-based global sensitivity index is calculated through Bayes theorem and GMM. Different numerical examples are adopted to verify the efficiency and accuracy. The conclusions are summarized as follows:

- (1) From numerical examples, it can be seen that only 2e3 candidate samples are required in AK-IDS-RGS to obtain a robust failure probability with COV < 3% in Examples 1–4, and Example 5 requires only 4e3 candidate samples. IDS can significantly reduce the candidate sample size and the required function calls, which is very helpful to improve the efficiency of active learning and reduce the required computer memory. For the reliability problem with small failure probability, AK-IDS-RGS can also obtain high accuracy evaluation results.
- (2) The proposed auxiliary region-based stopping criterion is established based on the proportion of failure samples in total samples and the prediction uncertainty of

Kriging model. Compared with the existed error-based stopping criterion, the auxiliary region-based stopping doesn't require the probability distribution model of the size of failure samples, the form is much simpler. From Sect. 6.6.2, it can also be seen that the required function calls of auxiliary region-based stopping criterion is also smaller than the error-based stopping criterion, which means that the proposed criterion is more suitable for IDS.

- (3) Comparing with AK-DIS, the major advantage of the proposed segmented learning strategy is that it realizes the synchronization of Kriging model updating and importance directional density function establishment, rather than only establishing the importance directional density function through the approximate design point. From the numerical examples, it can be seen that the proposed method can obtain high accuracy failure probability with lower required function calls, the efficiency of the proposed method is higher than AK-DIS. In addition, if an accurate design point is obtained through optimization before using learning function to update Kriging model, it will also ensure the accuracy of importance directional density function. However, the required function calls will be much larger than the proposed segmented learning strategy.
- (4) The relative errors of failure probability of AK-IDS-RGS under U and EFF learning functions in the five numerical examples are all lower than 5%, and the required function calls of these two learning functions are also lower than other functions. From the global sensitivity index, the orders of sensitivity indexes under U and EFF functions are the same as those of MC method, and the COV $(\hat{\eta})$ of all variables under U and EFF functions are also lower than 5%. Therefore, U and EFF learning functions should be adopted on the proposed AK-IDS-RGS method.

Funding This study is supported by the National Natural Science Foundation of China under Grant 51278420.

Declarations

Conflict of interest We declare that we have no financial and personal conflict of interest with other people or organizations.

Replication of results The data and codes are available from the corresponding author through the reasonable request.

Research involving human and/or animal participants This article does not include any studies with human participants or animal performed.

References

- Bichon BJ, Eldred MS, Swiler LP (2008) Efficient global reliability analysis for nonlinear implicit performance functions. AIAA J 46(10):2459–2468
- Cadini F, Lombardo SS, Giglio M (2020) Global reliability sensitivity analysis by Sobol dynamic adaptive Kriging importance sampling. Struct Saf 87:101998
- Chen J, Chen Z, Xu Y, Li H (2021) Efficient reliability analysis combining Kriging and subset simulation with two-stage convergence criterion. Reliab Eng Syst Saf 214:107737
- Chen Z, Li G, He J, Yang Z, Wang J (2022) A new parallel adaptive structural reliability analysis method based on importance sampling and K-medoids clustering. Reliab Eng Syst Saf 218:108124
- Dubourg V, Sudret B, Deheeger F (2013) Metamodel-based importance sampling for structural reliability analysis. Probab Eng Mech 33:47–57
- Echard B, Gayton N, Lemaire M (2011) AK-MCS: an active learning reliability method combining Kriging and Monte Carlo simulation. Struct Saf 33:145–154
- Echard B, Gayton N, Lemaire M (2013) A combined importance sampling and Kriging reliability method for small failure probabilities with time-demanding numerical models. Reliab Eng Syst Saf 111:232–240
- Grooteman F (2011) An adaptive directional importance sampling method for structural reliability. Probab Eng Mech 26:134–141
- Guo Q, Liu Y, Chen B, Zhao Y (2020) An active learning Kriging model combined with directional importance sampling method for efficient reliability analysis. Probab Eng Mech 60:103054
- Guo Q, Liu Y, Chen B, Yao Q (2021) A variable and mode sensitivity analysis method for structural system using a novel active learning model. Reliab Eng Syst Saf 206:107285
- Huang P, Huang HZ, Li YF, Qian HM (2021) An efficient and robust structural reliability analysis method with mixed variables based on hybrid conjugate gradient direction. Int J Numer Methods Eng 122:1990–2004
- Hwang SH, Mangalathu S, Shin J, Jeon JS (2021) Machine learningbased approaches for seismic demand and collapse ductile reinforced concrete building frames. J Build Eng 34:101905
- Jia DW, Wu ZY (2022) A Laplace asymptotic integral-based reliability analysis method combined with artificial neural network. Appl Math Model 105:406–422
- Katafygiotis L, Moan T, Cheung SH (2007) Auxiliary domain method for solving multi-objective dynamic reliability problems for nonlinear structure. Struct Eng Mech 25(3):347–363
- Lei J, Lu Z, Wang L (2022) An efficient method by nesting adaptive Kriging into importance sampling for failure-probabilitybased global sensitivity analysis. Eng Comput Germany 38: 3595–3610
- Lelièvre N, Beaurepaire P, Mattrand C, Gayton N (2018) AK-MCSi: a Kriging-based method to deal with small failure probabilities and time-consuming models. Struct Saf 73:1–11
- Lemaitre P, Sergienko E, Arnaud A, Bousquet N, Gamboa F, Iooss B (2015) Density modification-based reliability sensitivity analysis. J Stat Comput Simul 85:1200–1223
- Ling C, Lu Z (2021) Support vector machine-based importance sampling for rare event estimation. Struct Multidisc Optim 63:1609–1631
- Liu Q, Homma T (2010) A new importance measure for sensitivity analysis. J Nucl Sci Technol 47:53–61
- Lu Z, Song S, Yue Z, Wang J (2008) Reliability and sensitivity method by line sampling. Struct Saf 30:517–532

- Lu K, Zhou R, Zhang J (2017) Approximate Chernoff fusion of Gaussian mixtures for ballistic target tracking in the re-entry phase. Aerosp Sci Technol 61:21–28
- Lv Z, Lu Z, Wang P (2015) A new learning function for Kriging and its applications to solve reliability problems in engineering. Comput Math Appl 33:1182–1197
- Mansour G, Mohsen R, Ameryan A (2020) First order control variates algorithm for reliability analysis of engineering structures. Appl Math Model 77:829–847
- Meng Z, Zhang Z, Li G, Zhang D (2020) An active weight learning method for efficient reliability assessment with small failure probability. Struct Multidisc Optim 61:1157–1170
- Pan QJ, Leung YF, Hsu SC (2021) Stochastic seismic slope stability assessment using polynomial chaos expansions combined with relevance vector machine. Geosci Front 21:405–411
- Papaioannou I, Straub D (2021) Combination line sampling for structural reliability analysis. Struct Saf 88:102025
- Rachedi M, Matallah M, Kotronis P (2021) Seismic behavior & risk assessment of an existing bridge considering soil-structure interaction using artificial neural network. Eng Struct 232:111800
- Shi Y, Lu Z, He R, Zhou Y, Chen S (2020) A novel learning function based on Kriging for reliability analysis. Reliab Eng Syst Saf 198:106857
- Song J, Wei P, Valdebenito M, Michael B (2021) Active learning line sampling for rare event analysis. Mech Syst Signal Process 147:107113
- Su L, Li XL, Jiang YP (2020) Comparison of methodologies for seismic fragility analysis of unreinforced masonry buildings considering epistemic uncertainty. Eng Struct 25:110059
- Tian HM, Li DQ, Cao ZJ, Xu DS, Fu XY (2021) Reliability-based monitoring sensitivity analysis for reinforced slopes using BUS and subset simulation methods. Eng Geol 293:106331
- Wang Z, Shafieezadeh A (2019a) REAK: reliability analysis through error rate-based adaptive Kriging. Reliab Eng Syst Saf 182:33–45
- Wang Z, Shafieezadeh A (2019b) ESC: an efficient error-based stopping criterion for Kriging-based reliability analysis method. Struct Multidisc Optim 59:1621–1637
- Wang Y, Xiao S, Lu Z (2019) An efficient method based on Bayes' theorem to estimate the failure-probability-based sensitivity measure. Mech Syst Signal Process 115:607–620
- Wang J, Sun Z, Cao R (2021) An efficient and robust Kriging-based method for system reliability analysis. Reliab Eng Syst Saf 216:107953
- Wang J, Xu G, Li Y, Kareem A (2022) AKSE: a novel adaptive Kriging method combining sampling region scheme and error-based stopping criterion for structural reliability analysis. Reliab Eng Syst Saf 219:108124
- Xiao NC, Yuan K, Zhou CN (2020a) Adaptive Kriging-based efficient reliability method for structural systems with multiple failure modes and mixed variables. Comput Method Appl Mech 359:112649
- Xiao S, Oladyshkin S, Nowak W (2020b) Reliability analysis with stratified importance sampling based on adaptive Kriging. Reliab Eng Syst Saf 197:106852
- Yang X, Liu Y, Fang X, Mi C (2018) Estimation of low failure probability based on active learning Kriging model with a concentric ring approaching strategy. Struct Multidisc Optim 58:1175–1186
- Yang X, Liu Y, Gao Y, Zhang Y, Gao Z (2015) An active learning kriging model for hybrid reliability analysis with both random and interval variables. Struct Multidisc Optim 51:1003–1016
- Yun W, Lu Z, Jiang X, Zhang L, He P (2020) AK-ARBIS: an improved AK-MCS based on the adaptive radial-based importance sampling for small failure probability. Struct Saf 82:101891
- Yun W, Lu Z, Wang L, Feng K, He P, Dai Y (2021) Error-based stopping criterion for the combined adaptive Kriging and importance

sampling method for reliability analysis. Probab Eng Mech 65:103131

- Zhang K, Lu Z, Wu D, Zhang Y (2017) Analytical variance based global sensitivity analysis for models with correlated variables. Appl Math Model 45:748–767
- Zhang X, Wang L, Sørensen JD (2019) REIF: a novel active-learning function toward adaptive Kriging surrogate models for structural reliability analysis. Reliab Eng Syst Saf 185:440–454
- Zhang X, Wang L, Sørensen JD (2020) AKOIS: an adaptive Kriging oriented importance sampling method for structural system reliability analysis. Struct Saf 82:101876
- Zhang X, Lu Z, Cheng K (2021) AK-DS: an adaptive Kriging-based directional sampling method for reliability analysis. Mech Syst Signal Process 156:107610
- Zhang X, Lu Z, Cheng K (2022) Cross-entropy-based directional importance sampling with von Mises-Fisher mixture model for reliability analysis. Reliab Eng Syst Saf 220:108306
- Zhao H, Yue Z, Liu Y, Zhang Y (2015) An efficient reliability method combining adaptive importance sampling and Kriging metamodel. Appl Math Model 39:1853–1866

- Zhou J, Li J (2023) IE-AK: a novel adaptive sampling strategy based on information entropy for Kriging metamodel-based reliability analysis. Reliab Eng Syst Saf 229:108824
- Zhou C, Lu Z, Zhang F, Yue Z (2015) An adaptive reliability method combining relevance vector machine and importance sampling. Struct Multidisc Optim 52:945–957
- Zhu X, Zhou Z, Yun W (2020) An efficient method for estimating failure probability of the structure with multiple implicit failure domains by combing Meta-IS with IS-AK. Reliab Eng Syst Saf 193:106644

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