Adsorption of Endotoxin from Aqueous Solution Using Bone Char

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Abstract The aim of this study is the removal of endotoxin from aqueous solution using bone char (BC) as an adsorbent material. The BC was prepared from cattle animal bone by pyrolysis in a furnace at 850°C. The morphology and physico-chemical characteristics of the adsorbent were investigated. Kinetic studies revealed that the adsorption of endotoxin is rapid. The adsorption mechanisms in the endotoxin-BC had a significant contribution from film diffusion. The maximum adsorption efficiency achieved is 98% at an adsorbent dose of 40 g L^{-1} with an initial endotoxin concentration of 80 Eu mL $^{-1}$. The results show that the Langmuir isotherm adsorption equation model describe the experimental adsorption isotherm with good accuracy. A survey of the regeneration capabilities showed that the BC could be regenerated and rendered endotoxin free by heating at 350°C for 30 min. The results suggest that BC could be used as effective adsorbent for endotoxin removal.

Keywords Endotoxin \cdot Bone char \cdot Adsorption \cdot Aqueous solution

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S. D. Siyadat Pastteur Institute of Iran, Tehran, Iran Endotoxins, also called pyrogens, are biologically active lipopolysaccharides (LPS) that are found in the outer layer of the cell walls of most gram-negative bacteria and some cyanobacteria (Hanora et al. [2006\)](#page-4-0). The release of endotoxins from bacteria takes place either during either cell lyses or multiplication and has a high stability even at high temperatures (stable at 121° C for 1 h) and pH values due to its amphoteric structure (Anderson et al. [2003\)](#page-4-0). The general symptoms of endotoxin exposure for humans include fever, diarrhea, vomiting, hypotension, shock, intravascular coagulation and death (Tessarolo et al. [2006\)](#page-4-0). Endotoxin is not only injurious by itself, but it also augments other toxic agents so that together they may cause greater and more sustained damage. For example, endotoxin may boost the toxicity of ethanol and a variety of drugs (Anderson et al. [2002](#page-4-0)). Also, it is known that endotoxin may act as a co-allergen, facilitating sensitization to other allergens, or they may increase the severity of allergic disease (Szymanska [2005](#page-4-0)). The potential pathways of water-associated endotoxin exposure in humans include direct introduction in to the blood stream via semi permeable dialysis membranes and inhalation of moisture-saturated air in showers, swimming pools, hot tubs, saunas, and dental offices (Anderson et al. [2007](#page-4-0)). Exposure to endotoxins by drinking water used for preparation or dilution of solutions for intravenous injection or dialysis may be even more serious (Castor et al. [2005\)](#page-4-0). Several other settings for endotoxin exposure include sawmills, paper recycling plants (repulping and deinking), fiberglass manufacturing, animal handling, cotton/textile milling, hemp processing and potato sorting (Sarantila et al. [2001;](#page-4-0) Anderson et al. [2007](#page-4-0)). Although several exposure routes and the adverse effects of this pollutant have been identified, unfortunately there is only limited information available on untreated surface water, ground water, and drinking water endotoxin

concentrations. There are several ways in which endotoxin polluted water can be detoxified. For treat drinking water, the peracetic acid, heat, association of heat and citric acid, oxidation with hydrogen peroxide, or permanganate are most commonly applied. Although these procedures are the most common methods, the energy requirements for heating, control over chemical doses, the safety of operators, storage problems, and the control of their by products are difficult obstacles (Anderson et al. [2002](#page-4-0)). In contrast with these methods, sorption processes are simple to perform, usually inexpensive, and applicable for decentralized water treatment facilities and on-site decontamination (Daus et al. [2004\)](#page-4-0). A wide variety of different materials has been proposed for the sorption of pollutants (Tsai et al. [2002](#page-4-0); Wanngah and Hanafiah [2008](#page-4-0)). It has recently been suggested that poorly crystallized apatite, such as BC apatite, might represent a low-cost and readily available phosphate source that could be used to as an adsorbent (Smiciklas et al. [2008\)](#page-4-0). Every year in many countries, a large number of domestic animals (sheep and cows) are slaughtered for meat and these animals have a large amount of bone waste that can be used as feedstock or a fuel for energy generation. Some countries have large hydrocarbon resources and no need for this alternative fuel source, but safe bone disposal is a problem. Therefore, using these wastes for producing BC and other products provides a safe and useful disposal route (Purevsuren et al. [2004\)](#page-4-0). BC is a mixed compound adsorbent in which carbon is distributed throughout the porous structure of hydroxyapatite $(Ca_{10}(PO_4)_6(OH)_2$ or CaHAP). BC is 76% CaHAP, which is not only a major inorganic constituent of teeth and bones but also phosphate rock (Cheung et al. [2001\)](#page-4-0). The physical and chemical properties of CaHAP have been widely reported; studies show that the removal mechanism provide not only an adsorption effect but also a type of ionexchange reaction between the ions in solution and the calcium ions of the apatites (Danny et al. [2004](#page-4-0)). Although it is not used on a large scale commercially, BC is occasionally used to treat drinking water (Xie et al. [2004\)](#page-5-0). Its potential as a defluoridating agent and to remove heavy metals from solution has also been reported in the literature (Choy and McKay [2005\)](#page-4-0). In the present study, BC was produced from cattle bone, and it is used as an inexpensive adsorbent to investigate the effectiveness of using BC for endotoxin removal from aqueous solution.

Materials and Methods

All of the chemicals used for the solutions were reagent grade and were used without further purification. The water used in solutions was purified with a MQ-UV water device (Millipore). The electrical conductivity (EC) of the

distillated water that was used for the experiments was lower than 3 μ mohs cm⁻¹. The pH was measured using Hach pH meter (Hach Co., USA).

All glassware was rendered pyrogen free by heating at 400° C for at least 30 min. The plastic apparatuses were treated with 33% H₂O₂ then rinsed with pyrogen-free water and dried at 80°C for 8 h. A fresh bottle of pyrogen-free water was used for each experimental run to avoid potential contamination problems. Escherichia coli (ATCC 25922) was obtained from reference laboratory in Tehran, Iran. Endotoxin extraction was performed using the hot phenol– water (Westphal and Jann [1965\)](#page-5-0). The endotoxin concentrations was determined with a limulus amebocyte lysate (LAL) test (Sarantila et al. [1999](#page-4-0)). The calibration curve was plotted with using the standard endotoxin of E. coli O55:B5 (Choa chrom Co., USA).

The bone from cattle and sheep was crushed into pieces of 10–15 cm in length, rinsed three times in deionized water and boiled at least three times in distillated water for 4 h to remove fate and residual protein pieces. The bone was then dried at 110° C over night and cooled in a desiccator. Pyrolises of bone was performed in a rectangular furnace that was externally heated by electric power sources. The pyrolysis was carried out at 850° C for 4 h so that the heating rate was 35 K min⁻¹. The solid yield from the pyrolysis step was transport to a desiccator and cooled to room temperature. The BC was then pulverized using ASTM standard sieves with range of 10–16 mesh (ASTM [2003](#page-4-0)); deionized water was used for washing. The solid structures were analyzed using X-ray diffraction (Philips) and scanning electronic microscopy (XL30 Philips model) techniques. The BC was characterized by pH_{zpc} , BET and iodine adsorption from solution. The pH_{zpc} of the BC was determined using the batch equilibrium technique with 1:1000 and 1:80 solid to liquid ratios in 0.1 (M) $KNO₃$ solution. Potassium nitrate was employed as an inert electrolyte. The initial pH value of the $KNO₃$ solution was adjusted range from 2 to 12 by adding 0.1 (M) $HNO₃$ or KOH. The solutions were allowed to equilibrate for 24 h in an isothermal shaker at 25 ± 1 °C. The suspensions were filtered through filter paper, and the pH values were measured again using an ion pH meter. A blank test without BC was also made in order to eliminate the influence of interferences (Smiciklas et al. [2000\)](#page-4-0). To measure the surface area, nitrogen gas was used for the adsorption, and the surface areas were calculated via the BET method using a Micromeritics (ASAP-2000). The iodine number (mg iodine/g carbon) was determined by using a 0.1N standardized iodine solution; the titrant was 0.1N sodium thiosulfate (ASTM D [1999\)](#page-4-0).

Batch adsorption experiments were carried out in room temperature (25 \pm 1°C) with the shaker set at 150 rpm. Starting with 100 mL flasks, containing various amount of

adsorbent $(1, 1.5, 2, 2.5, g)$ and $(20, 20, mL)$ of endotoxin solution of known concentration (80 Eu mL⁻¹) were added. After the flasks were shaken for 24 h to reach equilibrium, the supernatants were analyzed to find their endotoxin concentration. The initial and final concentrations of the solutions were measured by the LAL test. The pH of the solutions was adjusted using NaOH or HCl solutions of different concentrations. From preliminary kinetic tests, it was concluded that 6 h was long enough to achieve equilibrium. The endotoxin removal efficiency and amount of endotoxin adsorbed on the adsorbent were calculated by Eqs. 1 and 2, respectively.

$$
E = \frac{C_0 - C}{C_0} \times 100
$$
 (1)

$$
q = \frac{C_0 - C}{W_{\rm m}} \times V \tag{2}
$$

where E is the removal efficiency, q is the adsorption amount (Eu g^{-1}), C_0 and C are the concentration of endotoxin in the initial solution and in the supernatant after adsorption, respectively, and V is the volume of solution (mL).

Results and Discussion

Some properties of the adsorbent are presented in Table 1. The pH_{zpc} of an adsorbent is a very important characteristic that determines the pH at which the adsorbent surface has net electrical neutrality. At this value, the acidic or basic functional groups no longer contribute to the pH of the solution. Experiments showed that the pH_{zpc} of the BC was about 8.3. It has been reported that at any pH below pH_{zpc} the surface charge is positive whereas at pH level above pH_{zpc} the surface charge is negative (Parida et al. [1996](#page-4-0)). Based on the value found for pH_{zpc} , it can be deduced that the BC surface charge is positive as the solution pH is less than 8.3. The positive charge on the surface of the BC may enhance the removal of endotoxins via adsorption. Specific surface area and pore volume were determined with the

Table 1 Bone char characteristics

Specifications	Range	Unit
$\rm{pH}_{\rm{zpc}}$	8.3	
Apparent density	0.768	$g \text{ cm}^{-3}$
Pore volume	8.8	$\text{cm}^3 \text{ g}^{-1}$
BET-surface area	130.75	m^2 g ⁻¹
Iodine number	15.8	$mg g^{-1}$
Size distribution	$1.18 - 2$	mm
Loss weight in acid $(pH 3.31)$	Nil	$mg L^{-1}$
Loss weight in base $(pH 13.11)$	Nil	$mg L^{-1}$

BET. The specific surface area of BC particles was 130.75 m^2 g⁻¹. The tested BC samples were able to adsorb significant amounts of iodine; The iodine number gives an estimation of the relative surface area of two samples and is usually used to measure porosity for pores greater than 1.0 nm in diameter. Thus the iodine number was measured to evaluate the adsorptive capacity of the BC (Moreno-Castilla et al. [2001\)](#page-4-0). The surface structure of the BC was analyzed using an SEM. The SEM micrographs with $5000\times$ magnifications are shown in Fig. 1. The X-ray diffraction tests reveal that the BC is a mixed adsorbent composed of basic tricalcium phosphate and amorphous carbon (Fig. 2). Structurally, the calcium phosphate is in the hydroxyapatite form. The amorphous carbon fraction is distributed throughout the whole of the entire hydroxyapatite structure but most of the carbon exists as a highly active thin film that covers the porous hydroxyapatite surface.

Fast kinetics is one of the most important aspects of removal processes. Therefore, time domain experiments for endotoxin adsorption were performed (pH 7.0; $T = 25 \pm 1$ °C) for up to 24 h of contact time. The data obtained show that a contact time of 6 h is sufficient for achieving equilibrium. The endotoxin binding was fast and

Fig. 1 Scanning electron micrograph of bone char particles

Fig. 2 X-ray diffraction of bone char particles

the adsorption did not change afterwards. Therefore, 6 h was chosen as the contact time for endotoxin adsorption via BC, considering the analytical speed and removal efficiency. Figure 3 shows the adsorption kinetics of endotoxin on BC at 25 ± 1 °C and at neutral pH. A study of the kinetic curve reveals a rapid adsorption within the first 6 h to achieve the equilibrium conditions. The adsorption kinetics may be expressed as (Lalvani et al. [1998](#page-4-0)).

$$
R = \text{kt} \, \text{tm} \tag{3}
$$

The equation can be expressed in linearized form as

$$
\ln R = \ln kt + m \ln t \tag{4}
$$

where R is the endotoxin removal efficiency $(\%)$, t is the contact time (min) and kt and m are the constants. A plot of In R versus $\ln t$ show that the sorption kinetics can be divided into two linear phases: (1) the first phase, corresponding to a rapid removal phase and (2) the second phase, where removal becomes constant, indicating equilibrium conditions (Fig. 4). Applying Eq. 4 to the first linear phase, since a maximum occurs in this phase, the values of ln kt and m as calculated are calculated to be 2.21 and 0.68, respectively. In order for pore diffusion to be the rate limiting step, the value of *m* should be 0.5, i.e., the rate of adsorption should vary with the square root of time $(t^{0.5})$. However, in the present study, the rate of adsorption varies

Fig. 3 Adsorption kinetics of endotoxin (pH 7, $T = 25 \pm 1$ °C)

Fig. 4 Plot of $\ln R$ versus $\ln t$

as $t^{0.68}$, which implies that pore diffusion is not the rate limiting step. Therefore, the rate limiting step may be film diffusion. Furthermore, as shown in Fig. 4, that the plots do not pass through the origin, further suggesting that pore diffusion is not the rate-limiting step and that the process may be controlled by film diffusion mechanism (Poots et al. [1978\)](#page-4-0).

The adsorption isotherm represents the relationship between the amount adsorbed by a unit weight of solid sorbent and the amount of solute remaining in the solution at equilibrium. To deduce the adsorption capacity, the adsorption isotherm was plotted by measuring the equilibrium adsorption of endotoxin at a concentration of 80 Eu mL^{-1} with various amounts of adsorbent. The measurement was performed at neutral pH as this has been reported as to be the best condition for endotoxin decontamination (Zhang et al. [2007\)](#page-5-0). The data obtained were well fitted to the Langmuir adsorption model. The Langmuir model assumes the presence of a finite number of binding sites, homogeneously distributed over the sorbent surface, presenting the same affinity for sorption of a single layer with no interaction between sorbed species. The well-known Langmuir expression (Yu et al. [2001](#page-5-0)) is given as follows:

$$
q_{\rm e} = \frac{q_{\rm max}bC_{\rm e}}{1 + bC_{\rm e}}\tag{5}
$$

where q_e is the amount of endotoxin bound per gram of biomass at equilibrium, C_e is the residual endotoxin concentration in solution after binding, Q_0 is the maximum amount of endotoxin per unit weight of biomass required to form a complete monolayer on the surface for a high C_{e} , and b is a constant related to the affinity of the binding sites. Q_0 and b can be determined from linear graphs (a plot of C_e/q_e versus C_e). Figure 5 shows the relationship between the adsorption capability (q_e) and equilibrium concentration (C_e) . The adsorption, in this case, is random due to the existence of active sites with different energies. Table [2](#page-4-0) shows the quantities of the constants and

Fig. 5 Relationship between adsorption capability (q_e) and equilibrium concentration (C_e)

Table 2 Langmuir constants for endotoxin removal by BC

Parameter	Quantities	Unit
b	1.1	mL Eu^{-1}
$q_{\rm max}$	28.82	Eu g^{-1}
$R_{\rm L}$ R^2	0.011	
	0.9982	

correlation coefficient (R^2) . The dimensionless equilibrium parameter is defined as $R_{\text{L}} = 1/(1 + bC_0)$, where b is the langmuir constant (mL Eu^{-1}) and C_0 is the initial concentration. It has been shown that parameter R_L indicates the shape of the isotherm. R_L values between 0 and 1 indicate favorable adsorption. The results show that the adsorption capacity of the BC is 29 Eu g^{-1} . These results agree with the results of Zhang et al. [\(2007](#page-5-0)), who studied the adsorption capability of a synthetic adsorbent based on a silica gel for the removal of endotoxin. Our results show that the q_{max} of BC is 29 Eu g^{-1} , which is lower than that reported by Zhang et al. ([2007\)](#page-5-0). The differences between their study and this study may be related to the adsorbent characteristics because they used histidine as a modifier for the adsorbent, while we used. Because histidine may have adverse public health effects, it cannot be used for water treatment.

The recovery of adsorbed material as well as the regeneration of adsorbent is also an important aspect of water and wastewater treatment. Since the recovery of endotoxin is not necessary and logical in practice, for this research regeneration BC was been carried out by thermal process that was regenerated and rendered endotoxin free by heating at 350° C for 30 min.

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