

Input–Output Finite-Time Stability of Fractional-Order Positive Switched Systems

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Abstract

Input–output finite-time stability (IO-FTS) of fractional-order positive switched systems (FOPSS) is investigated in this paper. First of all, the concept of IO-FTS is extended to FOPSS. Then, by using co-positive Lyapunov functional method together with average dwell time approach, some sufficient conditions of input–output finitetime stability for the considered system are derived. Furthermore, the state feedback controller and the static output feedback controller are designed, and sufficient conditions are presented to ensure that the corresponding closed-loop system is input–output finite-time stable. These conditions can be easily obtained by linear programming. Finally, three numerical examples are given to show the effectiveness of the theoretical results.

Keywords Fractional-order systems · Positive switched systems · Input–output finite-time stability

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1 Introduction

The concept of fractional calculus and its application have been widely studied during the past three decades. Many people have made outstanding contributions for the development of fractional-order theory [6,7,11,13,23,25]. Among them, Hilfer puts forward fractional-order models which are applied in viscoelastic systems, dielectric polarization and electromagnetic [7], and Podlubny involves in fractional-order control such as $PI^{\lambda}D^{\mu}$ controller [23]. References [6,11,13,25] mainly introduce basic theory of fractional-order integrals and derivations. In some practical applications, fractional calculus is more available than integer calculus for the behavior of systems, such as fractional-order biological systems, fractional-order Chua's circuit, fractional electrical networks, robotics and other areas. At the same time, there have been lots of interesting results for fractional-order systems (see [14,17,18,22,26,34] and the reference therein). These results mentioned above refer to stability [26,34] and robust control [14,22]. In [17,18], new admissibility conditions of fractional-order systems have, respectively, addressed with order $0 < \alpha < 1$ and $1 < \alpha < 2$.

As we all know, switched systems are composed of a family of subsystems and a logical rule. Positive systems are dynamical systems whose state and output variables remain non-negative for future time interval whenever their initial conditions and inputs are non-negative. Therefore, some researchers have investigated the fractional-order positive systems [3,19] and fractional-order positive switched systems [8,32]. For example, stabilization of continuous-time fractional positive systems is addressed by using a Lyapunov function in [3], and positive fractional variable-order discrete-time systems are presented in [19]. However, stability of fractional-order switching systems is solved in frequency domain [8]. State-dependent switching control is discussed for switched positive fractional-order systems by using the sliding sector method in [32]. For normal systems, Lyapunov function and average dwell time (ADT) approach are always used to solve switched systems (see [5,29,34] and the reference cited in). But there are very few articles to solve the control problems of fractional-order positive switched systems by using Lyapunov functional method and ADT approach.

It is worth noting that the above results are focused on asymptotic stability and exponential stability, which reflect the behavior of the system in an infinite-time interval. However, in many practical applications, the systems happen in finite-time interval. Peter has firstly proposed the concept of finite-time stability [24], which requires that the state does not exceed a certain threshold over a appointed time interval. It should be put forward that sometimes only the output, not the state needs to be restrained within a bound. So, the concept of input–output finite-time stability (IO-FTS) is introduced in [1]. It is necessary to study the problem of IO-FTS [2,4,9,15,16,20,28,30,33]. These results are involved in singular systems [30], impulsive jump systems [2] and Markovian systems [28]. In addition, the IO-FTS of positive switched systems with time-varying and distributed delay is proposed in [15], and discrete-time impulsive switched linear systems with state delays are solved in [9].

The concept of input–output finite-time stability is also extended to fractional-order systems in [20]. Recently, considerable attention is focused on fractional-order positive switched systems, which are discussed with order between 0 and 1 based on ADT. The guaranteed cost finite-time control of fractional-order positive switched systems is

considered in [16]. Finite-time stability and stabilization of fractional-order positive switched system is reported in [33]. Global exponential stability and stabilization of fractional-order positive switched system is given in [4]. Since the systems are inevitably affected by external factors, it is necessary to consider the systems with disturbance. However, to our best knowledge, the result on the control problem of IO-FTS for fractional-order positive switched systems (FOPSS) with disturbance has not been investigated yet, which motivates our present paper.

From the above, this paper focuses on the IO-FTS for fractional-order positive switched system with order between 0 and 1 based on ADT. The challenges we face are how to establish Lyapunov function, how to deal with the disturbance and how to design the average dwell time switching signal. The main advantages of this paper are as follows: (i) The definition of IO-FTS is firstly extended to fractional-order positive switched systems; (ii) by using ADT approach and multiple co-positive Lyapunov functional method, two kinds of feedback controllers (state feedback controller and static output feedback controller) are designed. The rest of this paper is organized as follows: In Sect. 2, problem statements and preliminaries are introduced. Some sufficient conditions guaranteeing the IO-FTS of the considered systems are given in Sect. 3. Three numerical examples are provided to illustrate the effectiveness of obtained results in Sect. 4. In Sect. 5, conclusion is drawn.

Notations: Throughout this paper, \mathbb{R}^n is the *n*-dimensional Euclidean space. $\mathbb{R}^{n \times s}$ is the set of all $(n \times s)$ dimensional real matrices. \mathbb{R}^n_+ is the set of n-dimensional real nonnegative vectors. $A \succ 0$ $(A \succeq 0)$ means that all the elements of A are positive (non-negative). $A \succ B$ $(A \succeq B)$ means that $A - B \succ 0$ $(A - B \succeq 0)$. In a similar way, we can define $A \prec 0$ $(A \preceq 0)$, $A \prec B$ $(A \preceq B)$. A^T denotes the transpose of matrix A. $\Gamma(\cdot)$ denotes the Gamma function. Let $x \in \mathbb{R}^n$, $L_{\infty,[0,T]}$ denote the space of the uniformly bounded vector-valued functions on the interval [0, T]; that is, $s(t) \in L_{\infty,[0,T]}$ if $\max_{t \in [0,T]} \parallel w(t) \parallel < \infty$ holds. Matrices have compatible dimensions if there are no special statements.

2 Problem Statements and Preliminaries

Fractional-order calculus is the generalization of integer-order calculus. There are some different definitions of the fractional-order derivative. The commonly used definitions are Grunwald–Letnikov, Riemann–Liouville and Caputo definitions. We mainly use Caputo and Riemann–Liouville fractional-order derivative in this paper.

Definition 1 [20] The uniform formula of a fractional integral with $\alpha \in (0, 1)$ is defined as

$$_{t_0}I_t^{\alpha}f(t) = \frac{1}{\Gamma(\alpha)}\int_{t_0}^t \frac{f(\tau)}{(t-\tau)^{1-\alpha}}\mathrm{d}\tau,\tag{1}$$

where f(t) is an arbitrary integrate function, $t_0 I_t^{\alpha}$ is the fractional integral of order α on $[t_0, t]$ and $\Gamma(\cdot)$ is Gamma function, $\Gamma(s) = \int_0^\infty t^{s-1} e^{-t} dt$.

Definition 2 [20] Caputo (C) definition of fractional derivative with $\alpha \in (0, 1)$ is given as

$${}_{t_0}^C D_t^{\alpha} f(t) = \frac{1}{\Gamma(1-\alpha)} \int_{t_0}^t \frac{f'(\tau)}{(t-\tau)^{\alpha}} \mathrm{d}\tau,$$
(2)

 ${}_{t_0}^C D_t^{\alpha}$ represents Caputo (C) fractional derivatives of order α of f(t) on $[t_0, t]$.

Definition 3 [16] Riemann–Liouville (RL) definition of fractional derivation with $\alpha \in (0, 1)$ is given as

$${}^{RL}_{t_0} D^{\alpha}_t f(t) = \frac{1}{\Gamma(1-\alpha)} \frac{\mathrm{d}}{\mathrm{d}t} \int_{t_0}^t \frac{f(\tau)}{(t-\tau)^{\alpha}} \mathrm{d}\tau, \tag{3}$$

 $_{t_0}^{RL} D_t^{\alpha}$ represents Riemann–Liouville (RL) fractional derivatives of order α of f(t) on $[t_0, t]$.

From the above two definitions, we can obtain the following relations between them:

$${}^{RL}_{t_0} D^{\alpha}_t f(t) = {}^{C}_{t_0} D^{\alpha}_t f(t) + \frac{t^{-\alpha}}{\Gamma(1-\alpha)} f(t_0).$$
(4)

Lemma 1 [16] Let $\alpha \in (0, 1)$; if $f(0) \ge 0$, then ${}_{t_0}^C D_t^{\alpha} f(t) \le {}_{t_0}^{RL} D_t^{\alpha} f(t)$.

Consider the following FOPSS :

$$C_{t_0} D_t^{\alpha} x(t) = A_{\sigma(t)} x(t) + B_{\sigma(t)} u(t) + E_{\sigma(t)} w(t),$$

$$y(t) = C_{\sigma(t)} x(t),$$
(5)

where $x(t) \in \mathbb{R}^n$, $u(t) \in \mathbb{R}^m$ and $y(t) \in \mathbb{R}^z$ represent the system state, the control input and the measure output, respectively. $\sigma(t) : [0, \infty) \longrightarrow N = \{1, 2, ..., n\}$ is switching signal of the system, where N is the number of the subsystems; $\forall p \in N$, A_p , B_p , E_p and C_p are constant matrices with appropriate dimensions. p denotes the pth systems, and t_q denotes the qth switching instant. $w(t) \in \mathbb{R}^l$ is the exogenous disturbance and defined as

$$W_1 = \{ w(\cdot) \in L_{\infty, [0, T]} : \max \parallel w(t) \parallel \le d \},$$
(6)

with a known scalar d > 0.

Assumption 1 For the system (5), A_p ($\forall p \in N$) are Metzler matrices, $B_p \geq 0$, $E_p \geq 0$ and $C_p \geq 0$.

Definition 4 [15] System (5) is said to be positive if for any switching signals $\sigma(t)$, initial condition $x(t_0) \geq 0$, and disturbance input $w(t) \geq 0$, the corresponding trajectory satisfies $x(t) \geq 0$ and $y(t) \geq 0$ for all $t \geq 0$.

Lemma 2 [16] A matrix is a Metzler matrix if and only if there exists a positive constant ς such that $A + \varsigma I_n \ge 0$.

Definition 5 [4] For any switching signals $\sigma(t)$ and $T_2 \ge T_1 \ge 0$, let $N_{\sigma(t)}(T_1, T_2)$ denote the switching numbers of $\sigma(t)$ over the interval $[T_1, T_2]$. If there exist $N_0 \ge 0$ and $T_{\alpha} \ge 0$ such that

$$N_{\sigma(t)}(T_1, T_2) \le N_0 + \frac{T_2 - T_1}{\tau_{\alpha}},$$
(7)

then τ_{α} are called average dwell time (ADT), and N_0 are called chattering bound. Generally speaking, we choose $N_0 = 0$ in the paper.

Lemma 3 [33] *System* (5) *is positive if and only if* A_p ($\forall p \in N$) *are Metzler matrices and* $\forall p \in N$, $B_p \succeq 0$, $E_p \succeq 0$, and $C_p \succeq 0$.

Definition 6 (IO-FTS) (Consider zero initial condition x(0) = 0) For a given time constant T_f , disturbances signals W_1 defined by (6), and a vector $\varepsilon > 0$; System (5) is said to be input–output finite-time stable (IO-FTS) with respect to (ε , T_f , d, $\sigma(t)$), if

$$w(t) \in W_1 \Longrightarrow y^T(t)\varepsilon \le 1, \forall t \in [0, T_f].$$
 (8)

Lemma 4 [27] (Gronwall–Bellman inequality) Let f(t) and g(t) be continuous realvalued functions and non-negative in $a \le t \le b$. If k is a nonnegative constant and f(t) satisfies the integral inequality

$$f(t) \le k + \int_{a}^{t} f(s)g(s)\mathrm{d}s, t \in [a, b],$$
(9)

then

$$f(t) \le k \exp\left(\int_{a}^{t} g(s) \mathrm{d}s\right), t \in [a, b].$$
(10)

Lemma 5 [21] From the definition of fractional integrals and Caputo derivatives, $k - 1 < \alpha < k$, we have

$$I^{\alpha}(D^{\alpha}x(t)) = x(t) - \sum_{i=0}^{k-1} \frac{x^{i}(t_{0})}{i!} t^{i}, \qquad (11)$$

in particular, when $0 < \alpha < 1$ *,*

$$I^{\alpha}(D^{\alpha}x(t)) = x(t) - x(t_0), \qquad (12)$$

where I^{α} represents $_{t_0}I^{\alpha}_t$, and D^{α} represents $_{t_0}^C D^{\alpha}_t$.

Lemma 6 [4] (C_p inequality) For 0 < a < 1 and any positive real numbers $x_1, x_2, ..., x_k$

$$\sum_{k=1}^{n} x_k^a \le n^{1-a} \left(\sum_{k=1}^{n} x_k \right)^a.$$
(13)

Lemma 7 [33] (Young's inequality) For any positive real numbers a, b and any real number x, y, it holds that

$$|x|^{a}|y|^{b} \le \frac{a}{a+b}|x|^{a+b} + \frac{b}{a+b}|y|^{a+b}.$$
(14)

3 Main Results

The purpose of this paper is to design the state feedback controller $u(t) = K_{1\sigma(t)}x(t)$, the static output feedback controller $u(t) = K_{2\sigma(t)}y(t)$ and a class of switching signals $\sigma(t)$ for FOPSS (5) such that the corresponding closed-loop system is input–output finite-time stable.

3.1 Input–Output Finite-Time Stability Analysis

In this subsection, we will focus on the problem of IO-FTS for FOPSS (5) with $u(t) \equiv 0$.

Theorem 1 Consider the system (5). Given positive constants T_f , $\lambda(\lambda > 1)$, $\mu \ge 1$ and vector $\varepsilon > 0$, if there exist positive vectors v_p and $\forall p \in N$, such that the following inequalities hold:

$$A_p^T v_p - \mu v_p \le 0, \tag{3.1a}$$

$$E_p^T v_p \prec r, \tag{3.1b}$$

$$v_p \prec \lambda v_q,$$
 (3.1c)

$$C_p^T \varepsilon \prec v_p,$$
 (3.1d)

and the average dwell time of the switching signal $\sigma(t)$ satisfies

$$\tau_{\alpha} > \tau_{\alpha}^{*} = \frac{\delta}{\ln \Gamma(\alpha) - \ln(T_{f}^{\alpha - 1}rd) - \eta},$$
(15)

then the FOPSS (5) is input-output finite-time stable, where

$$\delta = T_f \ln \lambda + \frac{(1-\alpha)\mu T_f}{\Gamma(\alpha+1)}, \quad \eta = N_0 \ln \lambda + \frac{((1-\alpha)(N_0+1) + \alpha T_f)\mu}{\Gamma(1+\alpha)}.$$

Proof According to Lemma 3 and Assumption 1, each subsystem of the switched system (5) is positive. Construct the multiple linear co-positive Lyapunov function for the system (5) as follows:

$$V_{\sigma(t)} = V_{\sigma(t)}(t, x(t)) = x^T(x)v_{\sigma(t)},$$
(16)

where $v_p \in \mathbb{R}^n_+$. Denote $t_0, t_1, t_2, ..., t_k$ (we choose $t_0 = 0$) as the switching instants over the interval $[0, T_f]$. Along the trajectory of the system (5), we have

$${}_{t_0}^C D_t^{\alpha} V_{\sigma(t)}(t, x(t)) = x^T(t) A_{\sigma(t)}^T v_{\sigma(t)} + w^T(t) E_{\sigma(t)}^T v_{\sigma(t)}.$$
(17)

From (3.1a) and (3.1b), which implies that

$${}_{t_0}^C D_t^{\alpha} V_{\sigma(t)}(t, x(t)) \le \mu V_{\sigma(t)}(t, x(t)) + r w^T(t).$$
(18)

Taking the fractional integral $_{t_0}I_t^{\alpha}$ to both sides of (18) yields for $t \in [t_m, t_{m+1}]$

$$V(t, x(t)) \leq V_{\sigma(t_m)}(t_m, x(t_m)) + \frac{\mu}{\Gamma(\alpha)} \int_{t_m}^t (t - \tau)^{\alpha - 1} V_{\sigma(t)}(\tau, x(\tau)) d\tau + \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t - \tau)^{\alpha - 1} w^T(\tau) d\tau.$$
(19)

By Lemma 4, we know

$$V(t, x(t)) \leq V_{\sigma(t_m)}(t_m, x(t_m)) \exp\left\{\frac{\mu}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} d\tau\right\} + \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} w^T(\tau) d\tau = V_{\sigma(t_m)}(t_m, x(t_m)) \exp\left\{\frac{\mu}{\Gamma(\alpha+1)} (t-t_m)^{\alpha}\right\} + \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} w^T(\tau) d\tau.$$
(20)

From (3.1c), we get the following inequality

$$V_{\sigma(t_m)}(t_m, x(t_m)) \le \lambda V_{\sigma(t_m^-)}(t_m^-, x(t_m^-)).$$
(21)

By a similar method, together with $\exp\{\frac{\mu}{\Gamma(\alpha+1)}(t-t_m)^{\alpha}\} \ge 0$, we obtain

$$V(t, x(t)) \leq \lambda V_{\sigma(t_m^-)}(t_m^-, x(t_m^-)) \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(t-t_m)^{\alpha}\right\} + \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} w^T(\tau) d\tau$$
$$\leq \lambda V_{\sigma(t_{m-1})}(t_{m-1}, x(t_{m-1})) \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((t-t_m)^{\alpha} + (t_m - t_{m-1})^{\alpha})\right\}$$
$$+ \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(t-t_m)^{\alpha}\right\} \frac{\lambda r}{\Gamma(\alpha)} \int_{t_{m-1}}^{t_m} (t-\tau)^{\alpha-1} w^T(\tau) d\tau$$
$$+ \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} w^T(\tau) d\tau$$

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$$\leq \lambda^{2} V_{\sigma(t_{m-1}^{-})}(t_{m-1}^{-}, x(t_{m-1}^{-})) \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((t-t_{m})^{\alpha} + (t_{m}-t_{m-1})^{\alpha})\right\}$$

$$+ \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(t-t_{m})^{\alpha}\right\} \frac{\lambda r}{\Gamma(\alpha)} \int_{t_{m-1}}^{t_{m}} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau$$

$$+ \frac{r}{\Gamma(\alpha)} \int_{t_{m}}^{t} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau$$

$$\leq \cdots$$

$$\leq \lambda^{N_{\sigma}(t_{0},t)} V_{\sigma(t_{0})}(t_{0}, x(t_{0})) \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((t-t_{m})^{\alpha} + \cdots + (t_{1}-t_{0})^{\alpha})\right\}$$

$$+ \lambda^{N_{\sigma}(t_{0},t)} \frac{r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((t-t_{m})^{\alpha} + \cdots + (t_{2}-t_{1})^{\alpha})\right\}$$

$$\int_{t_{0}}^{t_{1}} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau$$

$$+ \frac{\lambda^{2}r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((t-t_{m})^{\alpha} + (t_{m}-t_{m-1})^{\alpha})\right\}$$

$$\int_{t_{m-2}}^{t_{m-1}} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau$$

$$+ \frac{\lambda r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(t-t_{m})^{\alpha}\right\} \int_{t_{m-1}}^{t_{m}} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau$$

$$+ \frac{r}{\Gamma(\alpha)} \int_{t_{m}}^{t} (t-\tau)^{\alpha-1} w^{T}(\tau) d\tau.$$
(22)

According to Lemmas 6 and 7

$$\begin{split} V(t, x(t)) \\ &\leq V_{\sigma(t_0)}(t_0, x(t_0)) \exp\left\{N_{\sigma}(t_0, t)\ln\lambda + \frac{\mu}{\Gamma(\alpha+1)}((1-\alpha)(N_{\sigma}(t_0, t)+1) \right. \\ &+ \alpha(t-t_0))\right\} + \frac{r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(N_{\sigma}(t_0, t)(1-\alpha) + (t-t_1)\alpha) \right. \\ &+ N_{\sigma}(t_0, t)\ln\lambda\right\} \int_{t_0}^{t_1} (t-\tau)^{\alpha-1} w^T(\tau) \mathrm{d}\tau + \cdots \\ &+ \frac{r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}(2(1-\alpha) + (t-t_{m-1})\alpha) + 2\ln\lambda\right\} \\ &\int_{t_{m-2}}^{t_{m-1}} (t-\tau)^{\alpha-1} w^T(\tau) \mathrm{d}\tau \end{split}$$

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$$+ \frac{r}{\Gamma(\alpha)} \exp\left\{\frac{\mu}{\Gamma(\alpha+1)}((1-\alpha)+(t-t_m)\alpha)+\ln\lambda\right\}$$

$$\int_{t_{m-1}}^{t_m} (t-\tau)^{\alpha-1} w^T(\tau) d\tau + \frac{r}{\Gamma(\alpha)} \int_{t_m}^t (t-\tau)^{\alpha-1} w^T(\tau) d\tau$$

$$\leq V_{\sigma(t_0)}(t_0, x(t_0))$$

$$\times \exp\left\{N_{\sigma}(t_0, t)\ln\lambda + \frac{\mu}{\Gamma(\alpha+1)}((1-\alpha)(N_{\sigma}(t_0, t)+1)+\alpha(t-t_0))\right\}$$

$$+ \frac{rd}{\Gamma(\alpha)}$$

$$\times \exp\left\{\frac{t-t_0}{\tau_{\alpha}}\ln\lambda + \frac{\mu}{\Gamma(\alpha+1)}((1-\alpha)(N_{\sigma}(t_0, t)+1)+\alpha(t-t_0))\right\}t^{\alpha-1}$$

$$\leq \exp\left\{\frac{t-t_0}{\tau_{\alpha}}\ln\lambda + \frac{\mu}{\Gamma(\alpha+1)}((1-\alpha)(N_{\sigma}(t_0, t)+1)+\alpha(t-t_0))\right\}t^{\alpha-1}$$

$$+\alpha(t-t_0))\right\}\left\{V_{\sigma(t_0)}(t_0, x(t_0)) + \frac{rd}{\Gamma(\alpha)}t^{\alpha-1}\right\},$$
(23)

due to $t - t_0 \leq T_f$ $(t \leq T_f)$. Let x(0) = 0, then $\tau_{\alpha} \geq \frac{\delta}{\ln \Gamma(\alpha) - \ln(T_f^{\alpha - 1}rd) - \eta}$,

$$y^{T}(t)\varepsilon = x^{T}(t)C_{\sigma(t)}^{T}\varepsilon < x^{T}(t)v_{\sigma(t)} \le V_{\sigma(t)}(t, x(t))$$
$$\le \exp\left\{\frac{\delta}{\tau_{\alpha}} + \eta\right\}\frac{rd}{\Gamma(\alpha)}T_{f}^{\alpha-1} \le 1.$$

From Definition 6, we can obtain that the system (5) is IO-FTS with $(\varepsilon, T_f, d, \sigma(t))$. Thus, this completes the proof.

Remark 1 It is noted that the conditions (3.1a) and (3.1c) are the same as those in [10,15,33]. No matter normal positive switched systems or fractional-order positive switched systems, conditions (3.1a) and (3.1c) are indispensable. Especially, when $\alpha = 1$, it is proved that Theorem 1 is consistent with the results of input–output finite-time control of positive switched without time-varying and distributed delays in [15]. Therefore, it is easy to see that IO-FTS of FOPSS is the generalization of IO-FTS on integer-order positive switched systems. However, there are many differences between FOPSS and normal positive switched systems. We can know the former is more complex and challenge from references [33] and the proof of Theorem 1.

Remark 2 In reference [10,15], there are two kinds of definitions for exogenous disturbance input w(t), respectively. L_p space and L_∞ space are adopted in discrete positive switched systems (non-fractional-order systems) [10], and L_1 space and L_∞ space are used in continuous positive switched systems (non-fractional-order systems) [15]. Owing to the special definition of fractional-order integral, L_p space and L_1 space can not specifically defined up to now. So, we require the exogenous disturbance input belonging to L_∞ space in this paper. That is, condition (6) is employed. In previous works [5,9,10,15,30], the stability problems of switched systems with delays (non-fractional-order systems) are addressed based on Lyapunov functions approach. However, for fractional-order switched systems with delays, two problems have not been solved. The first problem is how to express Lyapunov functions; the second one is how to calculate variable limit integral item. Therefore, the problems of fractionalorder switched systems with delays remain open. In the future work, it may be a interesting topic.

Remark 3 In the proof of Theorem 1, equality $I^{\alpha}(D^{\alpha}x(t)) = x(t) - x(t_0)$ is used. By Lemma 4, we can know the papers is investigated for Caputo derivative with order $0 < \alpha < 1$. However, from the relationship between Caputo and Riemann–Liouville fractional derivatives in Lemma 1, Riemann–Liouville derivatives can also be applied to Theorem 1. So, the following conclusion holds.

Corollary 1 Replace $_{t_0}^C D_t^{\alpha}$ by $_{t_0}^{RL} D_t^{\alpha}$ in Theorem 1. If the conditions (3.1a)–(3.1d) and (15) hold, then the system (5) is IO-FTS with $(\varepsilon, T_f, d, \sigma(t))$.

Proof By Lemma 1, we know

The other part of the proof is similar to that in Theorem 1 and omitted here. \Box

In the following subsection, we will design two kinds of controllers. Consider the fractional-order switched systems as follows:

$$C_{t_0} D_t^{\alpha} x(t) = A_{\sigma(t)} x(t) + B_{\sigma(t)} u(t) + E_{\sigma(t)} w(t)$$

$$y(t) = C_{\sigma(t)} x(t)$$
(24)

3.2 State Feedback Controller Design

For the system (24), designing the state feedback controller $u(t) = K_{1\sigma(t)}x(t)$, such that the corresponding closed-loop system is

$$C_{t_0} D_t^{\alpha} x(t) = A_{c\sigma(t)} x(t) + E_{\sigma(t)} w(t),$$

$$y(t) = C_{\sigma(t)} x(t),$$
(25)

with $A_{c\sigma(t)} = A_{\sigma(t)} + B_{\sigma(t)}K_{1\sigma(t)}$.

Theorem 2 Consider the system (25). Given positive constants T_f , $\lambda(\lambda > 1)$, $\mu \ge 1$ and vector $\varepsilon > 0$, if there exist positive vectors v_p and $p \in N$, such that the following inequalities hold:

$$A_{p}^{T}v_{p} + f_{1p} - \mu v_{p} \le 0, \qquad (3.2a)$$

$$E_n^T v_p \prec r, \tag{3.2b}$$

$$v_p \prec \lambda v_q,$$
 (3.2c)

$$C_p^T \varepsilon \prec v_p,$$
 (3.2d)

where $A_p + B_p K_{1p}$ are Metzler matrices. Then under ADT scheme (15), the FOPSS (25) is input–output finite-time stable, where $f_{1p} = K_{1p}^T B_p^T v_p$.

Proof By Lemma 3 and Assumption 1, we know the system (25) is positive. Replacing A_p in (3.1a) with $A_p + B_p K_{1p}$, letting $f_{1p} = K_{1p}^T B_p^T v_p$, then under the ADT (15), we easily know that the closed-loop system (25) is input–output finite-time stable. This completes the proof.

Corollary 2 Replace $_{t_0}^C D_t^{\alpha}$ by $_{t_0}^{RL} D_t^{\alpha}$ in Theorem 2. If the conditions (3.2a)–(3.2d) and (15) hold, then under the state feedback controller the corresponding closed-loop system (25) is IO-FTS with (ε , T_f , d, $\sigma(t)$).

3.3 Static Output Feedback Controller Design

Consider the system (24), under controller $u(t) = K_{2\sigma(t)}y(t)$, the corresponding closed-loop system is given by

$$C_{t_0} D_t^{\alpha} x(t) = (A_{\sigma(t)} + B_{\sigma(t)} K_{2\sigma(t)} C_{\sigma(t)}) x(t) + E_{\sigma(t)} w(t),$$

$$y(t) = C_{\sigma(t)} x(t).$$
(26)

Theorem 3 Consider the system (26). Given positive constants T_f , $\lambda(\lambda > 1)$, $\mu \ge 1$ and vector $\varepsilon > 0$, if there exist positive vectors v_p and $p \in N$, such that the following inequalities hold:

$$A_{p}^{T}v_{p} + f_{2p} - \mu v_{p} \le 0, \qquad (3.3a)$$

$$E_p^T v_p \prec r, \tag{3.3b}$$

$$v_p \prec \lambda v_a,$$
 (3.3c)

$$C_p^T \varepsilon \prec v_p, \tag{3.3d}$$

where $A_p + B_p K_{2p} C_p$ are Metzler matrices. Then under ADT scheme (15), the FOPSS (26) is input–output finite-time stable, where $f_{2p} = C_p^T K_{2p}^T B_p^T v_p$.

Proof By Lemma 3 and Assumption 1, we know the system (26) is positive. Replacing A_p in (3.1a) with $A_p + B_p K_{2p} C_p$, letting $f_{2p} = C_p^T K_{2p}^T B_p^T v_p$, then under the ADT (15), we easily know that the system (26) is input–output finite-time stable. This completes the proof.

Corollary 3 Replace ${}_{t_0}^C D_t^{\alpha}$ by ${}_{t_0}^{RL} D_t^{\alpha}$ in Theorem 3. If the conditions (3.3a)–(3.3d) and (15) hold, then under the output feedback controller the corresponding closed-loop system (26) is IO-FTS with $(\varepsilon, T_f, d, \sigma(t))$.

Remark 4 From above, two kinds of controllers are designed, and some sufficient conditions of IO-FTS for FOPSS are obtained by linear programming in Theorem 3 and 4. In practical applications, it is not always possible to obtain all state. So, static output feedback controller is better than state feedback controller. In the literature [4,15], output feedback design approach is employed. obviously, it is easy to see that conditions (3.2a) and (3.3a) are not standard linear programming after disposed. But we convert nonlinear inequalities into linear inequalities by using variable substitution method.

Next, we show an algorithm to obtain the feedback gain matrices K_{1p} (or K_{2p}).

Step 1 Giving the parameters λ , μ and solving (3.2a)–(3.2d) (or (3.3a)–(3.3d)) by linear programming, positive vectors v_p and f_{1p} (or f_{2p}) can be obtained.

Step 2 Substituting v_p , f_{1p} (or f_{2p}) into $f_{1p} = K_{1p}^T B_p^T v_p$ (or $f_{2p} = C_p^T K_{2p}^T B_p^T v_p$), K_{1p} (or K_{2p}) can be obtained.

Step 3 The gain K_{1p} (or K_{2p}) is substituted into $A_p + B_{1p}K_p$ (or $A_p + B_pK_{2p}C_p$). If $A_p + B_pK_{1p}$ (or $A_p + B_pK_{2p}C_p$) are Metzler matrices, the K_{1p} (or K_{2p}) are acceptable. Otherwise, go to Step 1, then repeat Steps 2, 3.

4 Numerical Example

In this section, three examples will be given to illustrate the effectiveness of the proposed methods.

Example 1 Consider linear electrical circuits composed of resistors, supercondensators (ultra-capacitors), coils and voltage (current) sources. In practical problem, a circuit is always containing exogenous disturbance signals such as circuit aging, environment and human factors. Using the relations (2.82), (2.83) in [12] and Kirchhoff's laws, a switching-type fractional linear circuits systems could be written by the system (5). Among them, $x_1(t) \in \mathbb{R}^{n_1}$ represents voltages across the supercondensators; $x_2(t) \in \mathbb{R}^{n_2}$ represents currents in coils; $u(t) \in \mathbb{R}^m$ represents the voltages of the circuits. And the parameters are given as follows:

$$A_{1} = \begin{bmatrix} -1.6 & 0 \\ 0 & 1.2 \end{bmatrix}, E_{1} = \begin{bmatrix} 1 \\ 1.2 \end{bmatrix}, C_{1} = \begin{bmatrix} 1.2 & 0.2 \\ 0.2 & 1.2 \end{bmatrix};$$
$$A_{2} = \begin{bmatrix} -1.5 & 0 \\ 0 & -1.3 \end{bmatrix}, E_{2} = \begin{bmatrix} 1.2 \\ 1 \end{bmatrix}, C_{2} = \begin{bmatrix} 1.5 & 0 \\ 0 & 1.5 \end{bmatrix}.$$

Let $\alpha = 0.5$, $\mu = 1$, $\lambda = 2$, $T_f = 10$, r = 3 and d = 0.00001. Solving the inequalities in Theorem 1 by linear programming, we get

$$v_1 = \begin{bmatrix} 0.0208\\ 0.6654 \end{bmatrix}, \ v_2 = \begin{bmatrix} 0.1264\\ 0.4920 \end{bmatrix}.$$

It is easily verified that A_p are Metzler matrices for p = 1, 2. Then according to (15), we can obtain $\tau_{\alpha}^* = 1.7884$. Choose $\tau_{\alpha} = 2 > \tau_{\alpha}^*$. Let $w(t) = e^{-0.5t} \sin t$.



Fig. 1 Switching signal of system (5)



Fig. 2 State trajectories of system (5)

Figures 1, 2, 3 and 4 show the simulation results, where $x(0) = \begin{bmatrix} 0 & 0 \end{bmatrix}^T$. Switching signal of the system (5) with ADT is shown in Figure 1. State trajectories of the system (5) are depicted in Figure 2. Figure 3 plots step responses of the system (5). Figure 4 plots the evolution of $y^T(t)\varepsilon \le 1$. From Figure 4, we know the system (5) is IO-FTS. It follows that the fractional electrical circuits systems (5) are positive and IO-FTS.



Fig. 3 Step responses of system (5)



Fig. 4 Evolution of $y^T(t)\varepsilon$ of system (5)

Example 2 Consider the system (25) under the state feedback controller $u(t) = K_{1\sigma(t)}x(t)$, the parameters are given as follows:

$$A_{1} = \begin{bmatrix} -0.1 & 0 \\ 0 & -0.1 \end{bmatrix}, B_{1} = \begin{bmatrix} 0.1 \\ 0 \end{bmatrix}, E_{1} = \begin{bmatrix} 0.1 \\ 0.2 \end{bmatrix}, C_{1} = \begin{bmatrix} 0.2 & 0.2 \\ 0.2 & 0.3 \end{bmatrix};$$
$$A_{2} = \begin{bmatrix} -0.1 & 0 \\ 0 & -0.1 \end{bmatrix}, B_{2} = \begin{bmatrix} 0.2 \\ 0.1 \end{bmatrix}, E_{2} = \begin{bmatrix} 0.1 \\ 0.2 \end{bmatrix}, C_{2} = \begin{bmatrix} 0.2 & 0.2 \\ 0.3 & 0.2 \end{bmatrix}.$$

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Fig. 5 Switching signal of system (25)

Let $\alpha = 0.5$, $\mu = 1$, $\lambda = 1.5$, $T_f = 10$, r = 4 and d = 0.00001. Solving the inequalities in Theorem 2 by linear programming, we have

$$f_{1} = \begin{bmatrix} -3777.9\\4101.0 \end{bmatrix}, v_{1} = \begin{bmatrix} 845.3\\120.36 \end{bmatrix}; f_{2} = \begin{bmatrix} 97.8059\\140.0599 \end{bmatrix}, v_{2} = \begin{bmatrix} 0.7125\\1.2700 \end{bmatrix};$$

$$K_{1} = \begin{bmatrix} -44.6932\\48.5154 \end{bmatrix}, K_{2} = \begin{bmatrix} 0.3629\\0.5197 \end{bmatrix};$$

$$A_{1} + B_{1}K_{1} = \begin{bmatrix} -4.5693 & 4.8515\\0 & -0.1000 \end{bmatrix}, A_{2} + B_{2}K_{2} = \begin{bmatrix} -0.0274 & 0.1039\\0.0363 & -0.0480 \end{bmatrix}$$

It is easily verified that $A_p + B_p K_p$ are Metzler matrices for p = 1, 2. Then according to (15), we can obtain $\tau_{\alpha}^* = 1.7181$. Choosing $\tau_{\alpha} = 2 > \tau_{\alpha}^*$. Let $w(t) = e^{-0.5t} \sin t$. Figures 5, 6, 7 and 8 show the simulation results, where $x(0) = [0 \ 0]^T$. Switching signal of the system (25) with ADT is shown in Fig. 5. State trajectories of the system (25) are depicted in Fig. 6. Figure 7 plots step responses of the system (25). Figure 8 plots the evolution of $y^T(t)\varepsilon \le 1$. From Fig. 8, we know the system (25) is IO-FTS.

Example 3 Consider the system (26) under the output feedback controller $u(t) = K_{2\sigma(t)}y(t)$, the parameters are given as follows:

$$A_{1} = \begin{bmatrix} -0.2 & 0 \\ 0 & -0.2 \end{bmatrix}, B_{1} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, E_{1} = \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}, C_{1} = \begin{bmatrix} 0.2 & 0.1 \\ 0.1 & 0.1 \end{bmatrix};$$
$$A_{2} = \begin{bmatrix} -0.1 & 0 \\ 0 & -0.1 \end{bmatrix}, B_{2} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, E_{2} = \begin{bmatrix} 0.1 \\ 0.2 \end{bmatrix}, C_{2} = \begin{bmatrix} 0.3 & 0.1 \\ 0.1 & 0.2 \end{bmatrix}.$$

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Fig. 6 State trajectories of system (25)



Fig. 7 Step responses of system (25)

Let $\alpha = 0.6$, $\mu = 1.1$, $\lambda = 1.5$, r = 4, $T_f = 10$ and d = 0.00001. Solving the inequalities in Theorem 3 by linear programming, we have

$$f_{1} = \begin{bmatrix} 198.1667\\28.7002 \end{bmatrix}, v_{1} = \begin{bmatrix} 535.5710\\428.909 \end{bmatrix}; f_{2} = \begin{bmatrix} -1.2747\\41.2399 \end{bmatrix}, v_{2} = \begin{bmatrix} 39.3612\\462.559 \end{bmatrix};$$

$$K_{1} = \begin{bmatrix} 3.1642\\-2.6283 \end{bmatrix}, K_{2} = \begin{bmatrix} -2.2250\\6.3511 \end{bmatrix};$$

$$A_{1} + B_{1}K_{1} = \begin{bmatrix} 0.2700 \ 0.0536\\0 \ -0.1000 \end{bmatrix}, A_{2} + B_{2}K_{2} = \begin{bmatrix} -0.1324 \ 1.0477\\0 \ -0.1000 \end{bmatrix}.$$

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Fig. 8 Evolution of $y^T(t)\varepsilon$ of system (25)



Fig. 9 Switching signal of system (26)

It is easily verified that $A_p + B_p K_p C_p$ are Metzler matrices for p = 1, 2. Then according to (15), we can obtain $\tau_{\alpha}^* = 2.5174$. Choosing $\tau_{\alpha} = 2.7 > \tau_{\alpha}^*$. Let $w(t) = e^{-0.6t} \sin t$. Figures 9, 10, 11 and 12 show the simulation results, where $x(0) = [0 \ 0]^T$. Switching signal of the system (26) with ADT is shown in Fig. 9. State trajectories of the system (26) are depicted in Fig. 10. Figure 11 plots step responses of the system (26). Figure 12 plots the evolution of $y^T(t)\varepsilon \le 1$. From Fig. 12, we know the system (26) is IO-FTS.



Fig. 10 State trajectories of system (26)



Fig. 11 Step responses of system (26)

5 Conclusion

In the paper, we have dealt with the problem of IO-FTS for FOPSS with order between 0 and 1. By constructing multiple linear co-positive Lyapunov functions and using ADT approach, two kinds of controllers are designed, and some sufficient conditions in terms of linear programming are obtained to guarantee that the closed-loop system is IO-FTS. Finally, three examples are given to illustrate the effectiveness of the proposed methods.



Fig. 12 Evolution of $y^T(t)\varepsilon$ of system (26)

Our future efforts will focus on input–output finite-time stability of fractional-order positive switched time-delay systems (or singular fractional-order positive switched systems). IO-FTS (or FTS, GES) of FOPSS with order between 1 and 2 may be interesting topics in the future study.

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