

## Controller Failure Analysis for Systems with Interval Time-Varying Delay: A Switched Method

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**Abstract** This paper studies the problem of controller failure analysis for a class of interval time-varying delay systems with a predesigned state feedback controller. Our objective is to establish conditions concerning controller failure time, under which the systems still keep exponentially stable. For this purpose, the systems with controller failures are first formulated as a class of switched delay systems. Next, based on a piecewise Lyapunov functional method, the exponential stability of such systems is guaranteed by restricting the unavailable rate and failure frequency of the controller. All the results are presented in terms of linear matrix inequalities. Two examples are provided to demonstrate the effectiveness of the proposed technique.

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## 1 Introduction

Controller failures are frequently encountered in practical control systems due to various factors [21–24]. One reason is that the data is not transmitted smoothly over the unreliable links, such as in packet dropout in networked control systems [25]. Failure can also occur when we suspend the controller purposefully in a positive way. In [21], exponential stability of feedback control systems with occasional controller failures is guaranteed by using a piecewise Lyapunov functional method. The corresponding result was extended to linear time-invariant discrete-time systems [22]. The corresponding method was also used to deal with  $L_2$  gain analysis [23] and dynamical output feedback [24]. However, in all the above results, time delay is not taken into account, and it is often a source of instability and performance deterioration [1, 4–7, 10, 11, 18–20]. In particular, systems with interval time-varying delay are important, where the lower bound of the time-varying delay can vary in a time interval [6, 7, 16, 17]. The interval time-varying delay contains a time-invariant delay and a time-varying delay, where the lower bound of the time-varying delay is restricted to be zero. Nevertheless, controller failure problems for systems with interval time-varying delay are obviously more challenging and important issues, because unstable subsystems occur in engineering applications and in practical systems; there are many systems with interval time-varying delay such as networked control systems [20]. For example, a controller is designed to stabilize a networked control system with interval time-varying delay, which is an open-loop unstable system. Due to certain factors, the controller fails for some time such that the system is open loop and unstable until the controller resumes working. A system with such a process can be looked upon as a switched system, consisting of a stable subsystem (the closed-loop system with stabilizing controller) and an unstable subsystem (the open-loop system without the stabilizing controller). To date, controller failure problems for systems with interval time-varying delay have not been fully investigated yet due to some difficulties. In this paper, we overcome two main difficulties in dealing with controller failure problems for systems with interval time-varying delay. One is the system model description. It is assumed that the designed controller can stabilize the system and that the complete breakdown of the controller causes the system to be unstable in a time interval. Using the idea of switched control, the systems with control failures are modeled as one kind of switched system (see, for example, the survey papers [3, 8, 13], recent books [9, 14] and the references [12, 15, 26]). Then, the stability problems of the considered systems can be reduced to the corresponding problems for switched systems, for which many results are available in the literature. The other difficulty is stability analysis for the proposed new model. Two lemmas are first given to reflect the change property of Lyapunov functionals. Then, based on a piecewise Lyapunov functional method, exponential stability criteria for switched delay systems are developed under certain conditions of unavailability rate and failure frequency of the controller.

The paper is organized as follows. In Sect. 2, the model description and preliminaries are given. Section 3 presents two lemmas and the main results in this paper. Two

examples are provided in Sect. 4 to show the effectiveness of the proposed methods. The conclusions are drawn in Sect. 5.

*Notation* The notation used in this paper is fairly standard.  $P < 0$ ,  $\lambda_{\max}(P)$  ( $\lambda_{\min}(P)$ ) and  $*$  denote a negative definite matrix  $P$ , the maximum (minimum) eigenvalues of  $P$  and the symmetric terms in symmetric matrices, respectively.

## 2 Model Description and Preliminaries

Consider the following delay system:

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Ex(t - d_1(t)) + Fu(t), \\ x(\theta) &= \phi(\theta), \quad \theta \in [-h_2, 0],\end{aligned}\tag{1}$$

where  $A$ ,  $E$  and  $F$  are constant matrices with the appropriate dimensions.  $x(t) \in R^n$  is the system state and  $d_1(t)$  denotes an interval time-varying delay satisfying

$$h_1 \leq d_1(t) \leq h_2, \quad \dot{d}_1(t) \leq d_1,\tag{2}$$

where  $h_2 > h_1 \geq 0$  are scalars representing the upper and the lower bounds of the time delay, respectively.  $\phi(\theta)$  is the initial vector function, which is continuous on the segment  $[-h_2, 0]$ .

For system (1), the following assumptions are made throughout the paper:

- (A1) When  $u(t) = 0$ , system (1) is unstable.  
 (A2) A state feedback controller  $u(t) = Kx(t - d_2(t))$  has been designed to stabilize system (1), where  $d_2(t)$  denotes the interval time-varying delay satisfying

$$h_3 \leq d_2(t) \leq h_4, \quad \dot{d}_2(t) \leq d_2\tag{3}$$

where  $h_4 > h_3 \geq 0$  are scalars representing the upper and the lower bounds of the time delay, respectively. Then, the resulting closed-loop system is

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Ex(t - d_1(t)) + Bx(t - d_2(t)), \\ x(\theta) &= \phi(\theta), \quad \theta \in [-\tau, 0],\end{aligned}\tag{4}$$

where  $B = FK$  and  $\tau = \max\{h_2, h_4\}$ .

- (A3) Let  $t_0 < t_1 < \dots < t_{2k}$ ,  $k = 0, 1, \dots$  denote the switching points during  $[0, t)$ . The designed controller  $u(t)$  is available during  $[t_{2k}, t_{2k+1})$ ,  $k = 0, 1, 2, \dots$ , while it fails during  $[t_{2k+1}, t_{2k+2})$ . Moreover, it finally resumes working when  $t \in [t_{2k+2}, \infty)$ .

*Remark 1* Assumption (A1) shows that the unforced system (1) is unstable. Assumption (A2) means that system (1) can be stabilized by state feedback controllers. In Assumption (A3), it is shown that the controller may fail over some time interval until it resumes working. For example, in networked control systems over Internet-type or wireless networks, the controller is prone to failure due to unreliable communication links, that is  $u(t) = 0$ .

Using the above assumptions, we formulate system (1) with controller failures as a class of switched delay system described by

$$\begin{aligned} \dot{x}(t) &= Ax(t) + Ex(t - d_1(t)) + B_{\sigma(t)}x(t - d_2(t)), \\ x(\theta) &= \phi(\theta), \quad \theta \in [-\tau, 0], \end{aligned} \tag{5}$$

where  $\sigma(t) : [0, \infty) \rightarrow N = \{1, 2\}$  is the switching law which is a piecewise constant function; subsystem 1 denotes system (1) with the controller available while subsystem 2 denotes it without the controller, that is,  $B_1 = FK$ ,  $B_2 = 0$ . Then, such switched delay systems are composed of a stable subsystem and an unstable one.

**Definition 1** [15] The equilibrium point  $x^* = 0$  of switched delay system (5) is exponentially stable if there exist  $\gamma \geq 1$  and  $\lambda > 0$  such that the solution  $x(t)$  of system (5) satisfies

$$\|x(t)\| \leq \gamma \|x(t_0)\|_{\theta} e^{-\lambda(t-t_0)}, \quad \forall t \geq t_0, \tag{6}$$

where  $\|\bullet\|$  denotes the Euclidean norm and  $\|x(t)\|_{\theta} = \max_{-\tau \leq \theta \leq 0} \{\|x(t + \theta)\|, \|\dot{x}(t + \theta)\|\}$ .

**Definition 2** Let  $N_c(t_0, t)$  and  $T_c(t_0, t)$  denote the number and the total time interval of controller failure during  $[t_0, t)$  while  $f_N(t_0, t) = N_c(t_0, t)/(t - t_0)$  and  $f_T = T_c(t_0, t)/(t - t_0)$  are referred to as the failure frequency and the unavailable rate of the controller.

The objective of this paper is to find conditions concerning  $f_N$  and  $f_T$ , under which system (1) with occasional controller breakdown ( $u = 0$ ) is still exponentially stable in the sense of (6).

### 3 Stability Analysis

In this section, the exponential stability criterion of system (5) is presented. First, based on the Lyapunov functional method, we address exponential estimations of the Lyapunov functional of subsystems 1 and 2, respectively. Then, delay-dependent exponential stability of the entire system is guaranteed by using the piecewise Lyapunov functional method.

For subsystem 1 of system (5), which is also denoted by (4), we select the Lyapunov functional candidate as

$$\begin{aligned} V_1(t) &= x^T(t)P_1x(t) + \sum_{i=1}^4 \int_{t-h_i}^t x^T(s)e^{\alpha(s-t)} Q_{1i}x(s) ds \\ &+ \int_{-h_2}^0 \int_{t+\theta}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{11}\dot{x}(s) ds d\theta \\ &+ \int_{-h_2}^{-h_1} \int_{t+\theta}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{12}\dot{x}(s) ds d\theta \end{aligned}$$

$$\begin{aligned}
 &+ \int_{-h_4}^0 \int_{t+\theta}^t \dot{x}^T(s) e^{\alpha(s-t)} Z_{13} \dot{x}(s) \, ds \, d\theta \\
 &+ \int_{-h_4}^{-h_3} \int_{t+\theta}^t \dot{x}^T(s) e^{\alpha(s-t)} Z_{14} \dot{x}(s) \, ds \, d\theta \\
 &+ \int_{t-d_1(t)}^t x^T(s) e^{\alpha(s-t)} Q_{15} x(s) \, ds \\
 &+ \int_{t-d_2(t)}^t x^T(s) e^{\alpha(s-t)} Q_{16} x(s) \, ds, \tag{7}
 \end{aligned}$$

where  $P_1 > 0$ ,  $Z_{1k} > 0$ ,  $Q_{1j} > 0$ ,  $j = 1, 2, \dots, 6$ ,  $k = 1, 2, 3, 4$  are symmetric matrices.

**Lemma 1** Under (2) and (3), for some positive scalars  $\alpha$ ,  $h_k$ ,  $d_1$  and  $d_2$ , system (4) is exponentially stable if there exist symmetric matrices  $P_1 > 0$ ,  $Z_{1k} > 0$ ,  $Q_{1j} > 0$ ,  $j = 1, 2, \dots, 6$  and matrices  $Y_{1k}$ ,  $T_{1k}$ ,  $L_{1k}$ ,  $k = 1, 2, 3, 4$  such that

$$\begin{bmatrix} \Omega_1 & R_1 \\ * & -S_1 \end{bmatrix} < 0. \tag{8}$$

Then, we have

$$V_1(t) \leq e^{-\alpha(t-t_0)} V_1(t_0), \tag{9}$$

where

$$\begin{aligned}
 \Omega_1 &= \begin{bmatrix} \varphi_{11} & \varphi_{12} & \varphi_{13} \\ * & \varphi_{14} & 0 \\ * & * & \varphi_{15} \end{bmatrix}, \\
 R_1 &= \begin{bmatrix} L_{11} & -T_{11} & L_{13} & -T_{13} & Y_{11} & T_{11} & L_{11} & Y_{13} & T_{13} & L_{13} & A^T U_1 \\ L_{12} & -T_{12} & 0 & 0 & Y_{12} & T_{12} & L_{12} & 0 & 0 & 0 & E^T U_1 \\ 0 & 0 & L_{14} & -T_{14} & 0 & 0 & 0 & Y_{14} & T_{14} & L_{14} & B^T U_1 \end{bmatrix}, \\
 S_1 &= \text{diag}\{e^{-\alpha h_1} Q_{11}, e^{-\alpha h_2} Q_{12}, e^{-\alpha h_3} Q_{13}, e^{-\alpha h_4} Q_{14}, H_{10a}^{-1} Z_{11}, \\
 &\quad H_{11a}^{-1} Z_3, H_{11a}^{-1} Z_{12}, H_{10b}^{-1} Z_{13}, H_{11b}^{-1} Z_4, H_{11b}^{-1} Z_{14}, U_1\}, \\
 H_{11a} &= \frac{e^{\alpha h_2} - e^{\alpha h_1}}{\alpha}, \quad H_{10a} = \frac{e^{\alpha h_2} - 1}{\alpha}, \\
 H_{10b} &= \frac{e^{\alpha h_4} - 1}{\alpha}, \quad H_{11b} = \frac{e^{\alpha h_4} - e^{\alpha h_3}}{\alpha}, \\
 U_1 &= h_2 Z_{11} + (h_2 - h_1) Z_{12} + h_4 Z_{13} + (h_4 - h_3) Z_{14}, \\
 Z_3 &= Z_{11} + Z_{12}, \quad Z_4 = Z_{13} + Z_{14}, \\
 \varphi_{11} &= P_1 A + A^T P_1 + \sum_{i=1}^6 Q_{1i} + Y_{11} + Y_{11}^T + Y_{13} + Y_{13}^T + \alpha P_1,
 \end{aligned}$$

$$\begin{aligned} \varphi_{12} &= P_1 E - Y_{11} + Y_{12}^T + T_{11} - L_{11}, & \varphi_{13} &= P_1 B - Y_{13} + Y_{14}^T + T_{13} - L_{13}, \\ \varphi_{14} &= (d_1 - 1)e^{-\alpha h_1} Q_{15} - Y_{12} - Y_{12}^T + T_{12} + T_{12}^T - L_{12} - L_{12}^T, \\ \varphi_{15} &= (d_2 - 1)e^{-\alpha h_3} Q_{16} - Y_{14} - Y_{14}^T + T_{14} + T_{14}^T - L_{14} - L_{14}^T. \end{aligned}$$

*Proof* Along the trajectory of system (4), taking the derivative of (7), we have

$$\begin{aligned} \dot{V}_1(t) &= 2x^T(t)P_1\dot{x}(t) + x^T(t)\alpha P_1x(t) - \alpha V_1(t) \\ &+ x^T(t)Q_{11}x(t) - x^T(t-h_1)e^{-\alpha h_1}Q_{11}x(t-h_1) \\ &+ x^T(t)Q_{12}x(t) - x^T(t-h_2)e^{-\alpha h_2}Q_{12}x(t-h_2) \\ &+ x^T(t)Q_{13}x(t) - x^T(t-h_3)e^{-\alpha h_3}Q_{13}x(t-h_3) \\ &+ x^T(t)Q_{14}x(t) - x^T(t-h_4)e^{-\alpha h_4}Q_{14}x(t-h_4) \\ &+ x^T(t)Q_{15}x(t) - (1-\dot{d}_1(t))x^T(t-d_1(t))e^{-\alpha d_1(t)}Q_{15}x(t-d_1(t)) \\ &+ x^T(t)Q_{16}x(t) - (1-\dot{d}_2(t))x^T(t-d_2(t))e^{-\alpha d_2(t)}Q_{16}x(t-d_2(t)) \\ &+ h_2\dot{x}^T(t)Z_{11}\dot{x}(t) - \int_{t-h_2}^t \dot{x}^T(s)e^{\alpha(s-t)}Z_{11}\dot{x}(s)ds \\ &+ (h_2-h_1)\dot{x}^T(t)Z_{12}\dot{x}(t) - \int_{t-h_2}^{t-h_1} \dot{x}^T(s)e^{\alpha(s-t)}Z_{12}\dot{x}(s)ds \\ &+ h_4\dot{x}^T(t)Z_{13}\dot{x}(t) - \int_{t-h_4}^t \dot{x}^T(s)e^{\alpha(s-t)}Z_{13}\dot{x}(s)ds \\ &+ (h_4-h_3)\dot{x}^T(t)Z_{14}\dot{x}(t) - \int_{t-h_4}^{t-h_3} \dot{x}^T(s)e^{\alpha(s-t)}Z_{14}\dot{x}(s)ds. \end{aligned} \tag{10}$$

The following Leibniz–Newton formula is introduced:

$$\begin{aligned} &[x^T(t)Y_{11} + x^T(t-d_1(t))Y_{12}] \\ &\times \left[ x(t) - x(t-d_1(t)) - \int_{t-d_1(t)}^t \dot{x}(s)ds \right] = 0, \end{aligned} \tag{11}$$

$$\begin{aligned} &[x^T(t)T_{11} + x^T(t-d_1(t))T_{12}] \\ &\times \left[ x(t-d_1(t)) - x(t-h_2) - \int_{t-h_2}^{t-d_1(t)} \dot{x}(s)ds \right] = 0, \end{aligned} \tag{12}$$

$$\begin{aligned} &[x^T(t)L_{11} + x^T(t-d_1(t))L_{12}] \\ &\times \left[ x(t-h_1) - x(t-d_1(t)) - \int_{t-d_1(t)}^{t-h_1} \dot{x}(s)ds \right] = 0, \end{aligned} \tag{13}$$

$$\begin{aligned}
 & [x^T(t)Y_{13} + x^T(t - d_2(t))Y_{14}] \\
 & \times \left[ x(t) - x(t - d_2(t)) - \int_{t-d_2(t)}^t \dot{x}(s) ds \right] = 0, \tag{14}
 \end{aligned}$$

$$\begin{aligned}
 & [x^T(t)T_{13} + x^T(t - d_2(t))T_{14}] \\
 & \times \left[ x(t - d_2(t)) - x(t - h_4) - \int_{t-h_4}^{t-d_2(t)} \dot{x}(s) ds \right] = 0, \tag{15}
 \end{aligned}$$

$$\begin{aligned}
 & [x^T(t)L_{13} + x^T(t - d_2(t))L_{14}] \\
 & \times \left[ x(t - h_3) - x(t - d_2(t)) - \int_{t-d_2(t)}^{t-h_3} \dot{x}(s) ds \right] = 0, \tag{16}
 \end{aligned}$$

where  $Y_{1k}, T_{1k}, L_{1k}, k = 1, 2, 3, 4$  are matrices with appropriate dimensions, called the free weighting matrices [19]. They are used to express the relationship between the terms in the Leibniz-Newton formula and can be determined by solving the corresponding linear matrix inequalities (LMIs).

For the integral terms of (10) and (11), we get

$$\begin{aligned}
 & 2[x^T(t)Y_{11} + x^T(t - d_1(t))Y_{12}] \int_{t-d_1(t)}^t \dot{x}(s) ds + \int_{t-d_1(t)}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{11} \dot{x}(s) ds \\
 & = \int_{t-d_1(t)}^t Y^T(e^{\alpha(s-t)} Z_{11})^{-1} Y ds - \int_{t-d_1(t)}^t \xi_1^T(t) Y_1 (e^{\alpha(s-t)} Z_{11})^{-1} Y_1^T \xi_1(t) ds \\
 & \geq -H_{10a} \xi_1^T(t) Y_1 Z_{11}^{-1} Y_1^T \xi_1(t), \tag{17}
 \end{aligned}$$

where

$$\begin{aligned}
 \xi_1^T(t) &= [x^T(t) \quad x^T(t - d_1(t))], \quad Y_1^T = [Y_{11}^T \quad Y_{12}^T], \\
 Y^T &= \xi_1^T(t) Y_1 + \dot{x}^T(s) e^{\alpha(s-t)} Z_{11}.
 \end{aligned}$$

By using similar methods to those above, from (10), (12)–(16), we get

$$\begin{aligned}
 & \int_{t-h_2}^{t-d_1(t)} \dot{x}^T(s) e^{\alpha(s-t)} Z_{11} \dot{x}(s) ds + \int_{t-h_2}^{t-d_1(t)} \dot{x}^T(s) e^{\alpha(s-t)} Z_{12} \dot{x}(s) ds \\
 & + 2[x^T(t)T_{11} + x^T(t - d_1(t))T_{12}] \times \int_{t-h_2}^{t-d_1(t)} \dot{x}(s) ds \\
 & \geq -H_{11a} \xi_1^T(t) T_1 (Z_{11} + Z_{12})^{-1} T_1^T \xi_1(t), \tag{18}
 \end{aligned}$$

$$\begin{aligned}
 & 2[x^T(t)L_{11} + x^T(t - d_1(t))L_{12}] \int_{t-d_1(t)}^{t-h_1} \dot{x}(s) ds + \int_{t-d_1(t)}^{t-h_1} \dot{x}^T(s) e^{\alpha(s-t)} Z_{12} \dot{x}(s) ds \\
 & \geq -H_{11a} \xi_1^T(t) L_1 Z_{12}^{-1} L_1^T \xi_1(t), \tag{19}
 \end{aligned}$$

$$\begin{aligned}
 &2[x^T(t)Y_{13} + x^T(t - d_2(t))Y_{14}] \int_{t-d_2(t)}^t \dot{x}(s) ds + \int_{t-d_2(t)}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{13}\dot{x}(s) ds \\
 &\geq -H_{10b}\xi_2^T(t)Y_2Z_{13}^{-1}Y_2^T\xi_2(t), \tag{20}
 \end{aligned}$$

$$\begin{aligned}
 &\int_{t-h_4}^{t-d_2(t)} \dot{x}^T(s)e^{\alpha(s-t)} Z_{13}\dot{x}(s) ds + \int_{t-h_4}^{t-d_2(t)} \dot{x}^T(s)e^{\alpha(s-t)} Z_{14}\dot{x}(s) ds \\
 &+ 2[x^T(t)T_{13} + x^T(t - d_2(t))T_{14}] \times \int_{t-h_4}^{t-d_2(t)} \dot{x}(s) ds \\
 &\geq -H_{11b}\xi_2^T(t)T_2(Z_{13} + Z_{14})^{-1}T_2^T\xi_2(t), \tag{21}
 \end{aligned}$$

$$\begin{aligned}
 &2[x^T(t)L_{13} + x^T(t - d_2(t))L_{14}] \int_{t-d_2(t)}^{t-h_3} \dot{x}(s) ds + \int_{t-d_2(t)}^{t-h_3} \dot{x}^T(s)e^{\alpha(s-t)} Z_{14}\dot{x}(s) ds \\
 &\geq -H_{11b}\xi_2^T(t)L_2Z_{14}^{-1}L_2^T\xi_2(t), \tag{22}
 \end{aligned}$$

where

$$\begin{aligned}
 T_1^T &= [T_{11}^T \quad T_{12}^T], & L_1^T &= [L_{11}^T \quad L_{12}^T], & \xi_2^T(t) &= [x^T(t) \quad x^T(t - d_2(t))], \\
 Y_2^T &= [Y_{13}^T \quad Y_{14}^T], & T_2^T &= [T_{13}^T \quad T_{14}^T], & L_2^T &= [L_{13}^T \quad L_{14}^T].
 \end{aligned}$$

Substituting (11)–(16) into (10) and using (17)–(22), we have

$$\dot{V}_1(t) + \alpha V_1(t) \leq \zeta^T(t)\Theta_1\zeta(t), \tag{23}$$

where

$$\begin{aligned}
 \Theta_1 &= \tilde{\Omega}_1 + \bar{A}^T U_1 \bar{A} + H_{20a} Y_{1a} Z_{11}^{-1} Y_{1a}^T + H_{21a} T_{1a} Z_3^{-1} T_{1a}^T + H_{21a} L_{1a} Z_{12}^{-1} L_{1a}^T \\
 &+ H_{20b} Y_{1b} Z_{13}^{-1} Y_{1b}^T + H_{21b} T_{1b} Z_4^{-1} T_{1b}^T + H_{21b} L_{1b} Z_{14}^{-1} L_{1b}^T,
 \end{aligned}$$

$$\tilde{\Omega}_1 = \begin{bmatrix} \varphi_{11} & \varphi_{12} & \varphi_{13} & L_{11} & -T_{11} & L_{13} & -T_{13} \\ * & \varphi_{14} & 0 & L_{12} & -T_{12} & 0 & 0 \\ * & * & \varphi_{15} & 0 & 0 & L_{14} & -T_{14} \\ * & * & * & -e^{-\alpha h_1} Q_{11} & 0 & 0 & 0 \\ * & * & * & * & -e^{-\alpha h_2} Q_{12} & 0 & 0 \\ * & * & * & * & * & -e^{-\alpha h_3} Q_{13} & 0 \\ * & * & * & * & * & * & -e^{-\alpha h_4} Q_{14} \end{bmatrix},$$

$$\zeta(t) = \begin{bmatrix} x(t) \\ x(t - d_1(t)) \\ x(t - d_2(t)) \\ x(t - h_1) \\ x(t - h_2) \\ x(t - h_3) \\ x(t - h_4) \end{bmatrix},$$

$$Y_{1a}^T = [Y_{11}^T \quad Y_{12}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0],$$



$$\begin{aligned}
 T_{1a}^T &= [T_{11}^T \quad T_{12}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], \\
 L_{1a}^T &= [L_{11}^T \quad L_{12}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], \\
 Y_{1b}^T &= [Y_{13}^T \quad Y_{14}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], \\
 T_{1b}^T &= [T_{13}^T \quad T_{14}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], \\
 L_{1b}^T &= [L_{13}^T \quad L_{14}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], \\
 \bar{A} &= [A \quad E \quad B \quad 0 \quad 0 \quad 0 \quad 0].
 \end{aligned}$$

Thus, it follows from Schur complements [2] that  $\Theta_1 < 0$  is equivalent to (8). Then, it is obvious that

$$\dot{V}_1(t) + \alpha V_1(t) \leq 0. \tag{24}$$

Furthermore, by integration, the inequality (9) is obtained, which completes the proof.  $\square$

*Remark 2* It is clear to see that Lemma 1 implies exponential stability of the normal time delay systems. According to (7), it is true that

$$a_1 \|x(t)\|^2 \leq V_1(t), \quad V_1(t_0) \leq b_1 \|x(t_0)\|_\theta^2, \tag{25}$$

where

$$\begin{aligned}
 a_1 &= \lambda_{\min}(P_1), \\
 b_1 &= \lambda_{\max}(P_1) + (1 - e^{-\alpha h_1})\lambda_{\max}(Q_{11})/\alpha \\
 &\quad + (1 - e^{-\alpha h_2})(\lambda_{\max}(Q_{12}) + \lambda_{\max}(Q_{15}))/\alpha \\
 &\quad + (e^{-\alpha h_2} + \alpha h_2 - 1)\lambda_{\max}(Z_{11})/\alpha^2 \\
 &\quad + (e^{-\alpha h_2} + \alpha h_2 - e^{-\alpha h_1} - \alpha h_1)\lambda_{\max}(Z_{12})/\alpha^2 \\
 &\quad + (1 - e^{-\alpha h_3})\lambda_{\max}(Q_{13})/\alpha \\
 &\quad + (1 - e^{-\alpha h_4})(\lambda_{\max}(Q_{14}) + \lambda_{\max}(Q_{16}))/\alpha \\
 &\quad + (e^{-\alpha h_4} + \alpha h_4 - 1)\lambda_{\max}(Z_{13})/\alpha^2 \\
 &\quad + (e^{-\alpha h_4} + \alpha h_4 - e^{-\alpha h_3} - \alpha h_3)\lambda_{\max}(Z_{14})/\alpha^2.
 \end{aligned}$$

Combining (9) and (25) yields

$$\|x(t)\| \leq \sqrt{\frac{b_1}{a_1}} e^{-\alpha(t-t_0)/2} \|x(t_0)\|_\theta. \tag{26}$$

Then, system (4) is exponentially stable. Moreover, if  $\alpha = 0$ , which means asymptotical stability, the results obtained by Lemma 1 are found in [6]. Thus, Lemma 1 is also applicable to normal interval time-varying delay systems.

Since  $B_2 = 0$ , subsystem 2 of system (5) can be rewritten as

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Ex(t - d_1(t)), \\ x(\theta) &= \phi(\theta), \quad \theta \in [-h_2, 0]\end{aligned}\quad (27)$$

and the Lyapunov functional candidate is chosen as

$$\begin{aligned}V_2(t) &= x^T(t)P_2x(t) + \sum_{i=1}^4 \int_{t-h_i}^t x^T(s)e^{\beta(t-s)} Q_{2i}x(s) ds \\ &+ \int_{-h_2}^0 \int_{t+\theta}^t \dot{x}^T(s)e^{\beta(t-s)} Z_{21}\dot{x}(s) ds d\theta \\ &+ \int_{-h_2}^{-h_1} \int_{t+\theta}^t \dot{x}^T(s)e^{\beta(t-s)} Z_{22}\dot{x}(s) ds d\theta \\ &+ \int_{-h_4}^0 \int_{t+\theta}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{23}\dot{x}(s) ds d\theta \\ &+ \int_{-h_4}^{-h_3} \int_{t+\theta}^t \dot{x}^T(s)e^{\alpha(s-t)} Z_{24}\dot{x}(s) ds d\theta \\ &+ \int_{t-d_1(t)}^t x^T(s)e^{\beta(t-s)} Q_{25}x(s) ds \\ &+ \int_{t-d_2(t)}^t x^T(s)e^{\alpha(s-t)} Q_{26}x(s) ds,\end{aligned}\quad (28)$$

where  $P_2 > 0$ ,  $Z_{2k} > 0$  and  $Q_{2j} > 0$ ,  $j = 1, 2, \dots, 6$ ,  $k = 1, 2, 3, 4$  are symmetric matrices.

**Lemma 2** For (27) under (2) and given  $\beta > 0$ , if there exist symmetric matrices  $P_2 > 0$ ,  $Z_{2k} > 0$  and  $Q_{2j} > 0$ ,  $j = 1, 2, \dots, 6$  and matrices  $Y_{2k}, T_{2k}, L_{2k}$ ,  $k = 1, 2, 3, 4$  such that

$$\begin{bmatrix} \Omega_2 & R_2 \\ * & -S_2 \end{bmatrix} < 0, \quad (29)$$

then one can have

$$V_2(t) \leq e^{\beta(t-t_0)} V_2(t_0), \quad (30)$$

where

$$\Omega_2 = \begin{bmatrix} \varphi_{21} & \varphi_{22} & \varphi_{23} \\ * & \varphi_{24} & 0 \\ * & * & \varphi_{25} \end{bmatrix},$$

$$R_2 = \begin{bmatrix} L_{21} & -T_{21} & L_{23} & -T_{23} & Y_{21} & T_{21} & L_{21} & Y_{23} & T_{23} & L_{23} & A^T U_2 \\ L_{22} & -T_{22} & 0 & 0 & Y_{22} & T_{22} & L_{22} & 0 & 0 & 0 & E^T U_2 \\ 0 & 0 & L_{24} & -T_{24} & 0 & 0 & 0 & Y_{24} & T_{24} & L_{24} & B^T U_2 \end{bmatrix},$$

$$S_2 = \text{diag}\{e^{-\alpha h_1} Q_{21}, e^{-\alpha h_2} Q_{22}, e^{-\alpha h_3} Q_{23}, e^{-\alpha h_4} Q_{24}, H_{20a}^{-1} Z_{21},$$

$$H_{21a}^{-1} Z_5, H_{21a}^{-1} Z_{22}, H_{20b}^{-1} Z_{23}, H_{21b}^{-1} Z_6, H_{21b}^{-1} Z_{24}, U_2\},$$

$$H_{20a} = \frac{1 - e^{-\beta h_2}}{\beta}, \quad H_{21a} = \frac{e^{-\beta h_1} - e^{-\beta h_2}}{\beta},$$

$$H_{20b} = \frac{1 - e^{-\beta h_4}}{\beta}, \quad H_{21b} = \frac{e^{-\beta h_3} - e^{-\beta h_4}}{\beta},$$

$$U_2 = h_2 Z_{21} + (h_2 - h_1) Z_{22} + h_4 Z_{23} + (h_4 - h_3) Z_{24},$$

$$Z_5 = Z_{21} + Z_{22}, \quad Z_6 = Z_{23} + Z_{24},$$

$$\varphi_{21} = P_2 A + A^T P_2 + \sum_{i=1}^6 Q_{2i} + Y_{21} + Y_{21}^T + Y_{23} + Y_{23}^T - \beta P_2,$$

$$\varphi_{22} = P_2 E - Y_{21} + Y_{22}^T + T_{21} - L_{21}, \quad \varphi_{23} = P_2 B - Y_{23} + Y_{24}^T + T_{23} - L_{23},$$

$$\varphi_{24} = (d_1 - 1)e^{\beta h_2} Q_{25} - Y_{22} - Y_{22}^T + T_{22} + T_{22}^T - L_{22} - L_{22}^T,$$

$$\varphi_{25} = (d_2 - 1)e^{\beta h_4} Q_{26} - Y_{24} - Y_{24}^T + T_{24} + T_{24}^T - L_{24} - L_{24}^T.$$

*Proof* The proof is similar to that of Lemma 1. Thus, it is omitted. □

*Remark 3* Note that Lemmas 1 and 2 present the decay and growth estimations of  $V_1(t)$  and  $V_2(t)$ , respectively. Their sufficient conditions are given in the form of LMIs.

**Theorem 1** Under (2) and (3), given  $\alpha > 0, \beta > 0, h_k > 0, d_k > 0$  and  $\mu \geq 1$ , if there exist symmetric matrices  $P_p > 0, Q_{pi} > 0, Z_{pk} > 0, p \in N$  satisfying

$$P_s \leq \mu P_l, \quad Q_{si} \leq \mu Q_{li}, \quad Z_{sk} \leq \mu Z_{lk}, \quad \forall s, l \in N \tag{31}$$

and matrices  $Y_{pk}, T_{pk}, L_{pk}, k = 1, 2, 3, 4, i = 1, 2, \dots, 6$  such that LMIs (8) and (29) hold, then system (5) is exponentially stable under such conditions, satisfying

$$f_T \leq \frac{\alpha - \alpha^*}{\alpha + \beta}, \quad \alpha^* \in (0, \alpha) \tag{32}$$

and

$$f_N \leq \frac{\alpha_0}{\ln \mu^2 \mu_1}, \quad \alpha_0 \in (0, \alpha^*). \tag{33}$$

Then, the state decay of system (5) can be estimated as

$$\|x(t)\| \leq \sqrt{\frac{b_1}{a_1}} e^{-\lambda(t-t_0)} \|x(t_0)\|_\theta \tag{34}$$

where  $\lambda = (\alpha^* - \alpha_0)/2$ ,  $\mu_1 = e^{(\alpha+\beta)\max\{h_2, h_4\}}$ .

*Proof* We choose the following piecewise Lyapunov functional candidate:

$$V_{\sigma(t)}(t) = \begin{cases} V_1(t_{2k}), & \text{if } t \in [t_{2k}, t_{2k+1}), \\ V_2(t_{2k+1}), & \text{if } t \in [t_{2k+1}, t_{2k+2}), \end{cases} \tag{35}$$

where  $k = 0, 1, 2, \dots, \infty$ .  $V_1(t)$  and  $V_2(t)$  are defined in (7) and (28), respectively.

From (31), it is obtained on the switching point  $t$  that

$$V_1(t) \leq \mu V_2(t^-), \quad V_2(t) \leq \mu \mu_1 V_1(t^-), \tag{36}$$

where  $t^- = \lim_{\tau \rightarrow t} \tau$ . Noting (A3), based on Lemmas 1 and 2, by induction during  $t \in [t_{2k+2}, \infty)$ , we have

$$\begin{aligned} V_1(t) &\leq e^{-\alpha(t-t_{2k+2})} V_1(t_{2k+2}) \leq e^{-\alpha(t-t_{2k+2})} \mu V_2(t_{2k+2}^-) \\ &\leq e^{-\alpha(t-t_{2k+2})} \mu e^{\beta(t_{2k+2}-t_{2k+1})} V_2(t_{2k+1}) \\ &\leq e^{-\alpha(t-t_{2k+2})} \mu^2 \mu_1 e^{\beta(t_{2k+2}-t_{2k+1})} V_1(t_{2k+1}^-) \\ &\leq e^{-\alpha(t-t_{2k+2})} \mu^2 \mu_1 e^{\beta(t_{2k+2}-t_{2k+1})} e^{-\alpha(t_{2k+1}-t_{2k})} V_1(t_{2k+1}^-) \\ &\leq \dots \leq \mu^{2k+2} \mu_1^{k+1} e^{-\alpha(t-t_0-T_c(t))} e^{\beta T_c(t)} V_1(t_0). \end{aligned} \tag{37}$$

From (32), it holds that

$$-\alpha(t - t_0 - T_c(t_0, t)) + \beta T_c(t_0, t) \leq -\alpha^*(t - t_0). \tag{38}$$

Notice Definition 2,  $N_c(t_0, t) = k + 1$  for  $t \in [t_{2k+2}, \infty)$ ; then from (33), it is obtained that

$$\mu^{2(k+1)} \mu_1^{k+1} = \mu^{2N_c(t_0, t)} \mu_1^{N_c(t_0, t)} \leq e^{\alpha_0(t-t_0)}. \tag{39}$$

Combining (37), (38) and (39) yields

$$V_1(t) \leq e^{-(\alpha^* - \alpha_0)(t-t_0)} V_1(t_0). \tag{40}$$

Combining (25) and (40) leads to (34). The proof is completed. □

*Remark 4* Note that to obtain  $\mu$  with respect to the failure frequency of the controller  $f_N$ , we first solve LMIs (8) and (29), then find  $\mu$  according to (31). This method may lead to a larger  $\mu$ . Another method is that we first select a known constant  $\mu$ , and then solve (8), (29) and (31) simultaneously. If these LMIs have no solutions, a larger  $\mu$  will be selected to yield a solution. On the contrary, if a solution is found, a smaller  $\mu$  will be chosen. So, a proper  $\mu$  could be obtained.

*Remark 5* Note that Theorem 1 considers the case where the derivative of the interval time-varying delay is bounded by (2) and (3). As for the delay-derivative-free case, however,

$$0 \leq h_1 \leq d_1(t) \leq h_2, \quad 0 \leq h_3 \leq d_2(t) \leq h_4. \quad (41)$$

Theorem 1 is still applicable, provided that the terms containing  $Q_{15}$ ,  $Q_{16}$  in (8) and  $Q_{25}$ ,  $Q_{26}$  in (29) are removed. On the other hand, Theorem 1 assumes that the delay in state and control input are different. Nevertheless, when they are the same, that is, when  $h_1 = h_3$  and  $h_2 = h_4$ , similar results can be obtained if the terms concerning  $d_2(t)$  are removed.

## 4 Numerical Examples

In this section, two examples are given to show the effectiveness of the proposed methods. Example 1 is for the case of (2) and (3) and Example 2 is for the case of (41).

*Example 1* Consider system (1) under (2) and (3) with

$$A = \begin{bmatrix} 0.2 & 0 \\ 0 & 1.1 \end{bmatrix}, \quad E = \begin{bmatrix} -1 & 0 \\ -1 & -1 \end{bmatrix}, \quad F = \begin{bmatrix} 0 \\ 1 \end{bmatrix},$$

$$h_1 = 0.1, \quad h_2 = 0.5, \quad d_1 = 2.0.$$

System (1) is assumed to be controlled through a network by a feedback controller  $u(t) = Kx(t - d_2(t))$ , where  $K = [0.4 \ -0.3]$  and  $h_3 = 0.3$ ,  $h_4 = 0.9$ ,  $d_2 = 3.0$ . Under initial state  $\phi(\theta) = [10 \ 5]^T$ ,  $\theta \in [-0.9, 0]$ , the state trajectories of system (1) with and without the controller are shown in Figs. 1 and 2, respectively. Figure 1 shows that the designed controller can stabilize the resulting closed-loop system, which implies that Assumption (A2) is satisfied. Figure 2 depicts the state response of the system when  $u(t) = 0$ . It is easy to see that the open-loop system is unstable, that is, assumption (A1) is satisfied. Therefore, system (1) can be transformed to (5). Under this mode, applying Theorem 1 with  $\alpha = 0.22$  and  $\beta = 0.39$ , the corresponding matrices are obtained as

$$P_1 = \begin{bmatrix} 4.0469 & -0.3935 \\ -0.3935 & 0.5530 \end{bmatrix}, \quad Q_{11} = \begin{bmatrix} 0.5174 & -0.0017 \\ -0.0017 & 0.0012 \end{bmatrix},$$

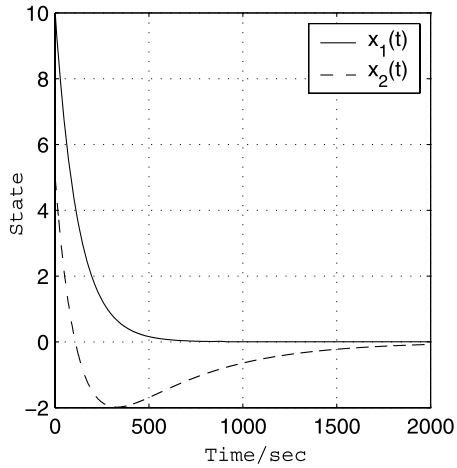
$$Q_{12} = \begin{bmatrix} 0.5767 & -0.0018 \\ -0.0018 & 0.0009 \end{bmatrix}, \quad Q_{13} = \begin{bmatrix} 0.4678 & 0.0001 \\ 0.0001 & 0.0007 \end{bmatrix},$$

$$Q_{14} = \begin{bmatrix} 0.4891 & 0.0001 \\ 0.0001 & 0.0006 \end{bmatrix}, \quad Q_{15} = \begin{bmatrix} 0.2124 & -0.0001 \\ -0.0001 & 0.0001 \end{bmatrix},$$

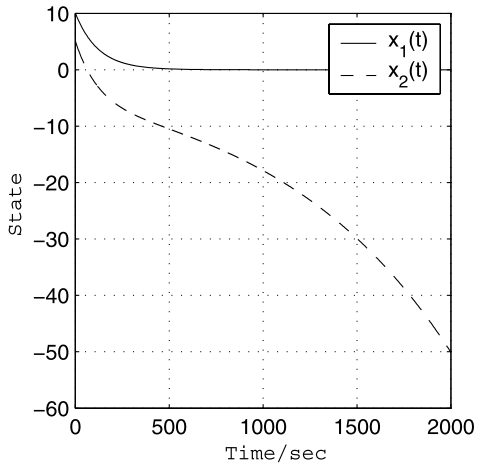
$$Q_{16} = \begin{bmatrix} 0.1730 & -0.0004 \\ -0.0004 & 0.0000 \end{bmatrix}, \quad Z_{11} = \begin{bmatrix} 2.9277 & 0.1562 \\ 0.1562 & 2.8221 \end{bmatrix},$$

$$Z_{12} = \begin{bmatrix} 0.7213 & -0.0227 \\ -0.0227 & 0.0371 \end{bmatrix}, \quad Z_{13} = \begin{bmatrix} 2.0010 & -1.1354 \\ -1.1354 & 0.8734 \end{bmatrix},$$

**Fig. 1** State response of system (1) with the controller (Example 1)

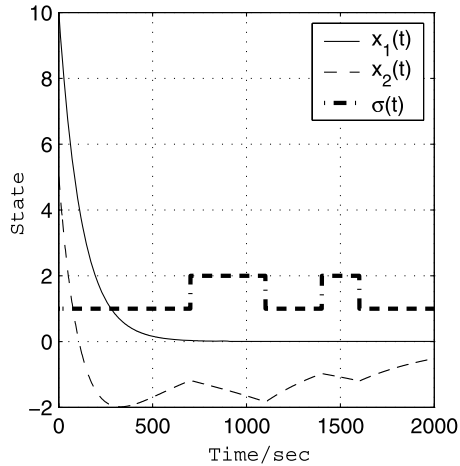


**Fig. 2** State response of system (1) without the controller (Example 1)



$$\begin{aligned}
 Z_{14} &= \begin{bmatrix} 0.6272 & -0.0108 \\ -0.0108 & 0.0246 \end{bmatrix}, & P_2 &= \begin{bmatrix} 2.5627 & -0.1994 \\ -0.1994 & 0.4401 \end{bmatrix}, \\
 Q_{21} &= \begin{bmatrix} 0.6266 & -0.0020 \\ -0.0020 & 0.0024 \end{bmatrix}, & Q_{22} &= \begin{bmatrix} 0.6846 & -0.0021 \\ -0.0021 & 0.0019 \end{bmatrix}, \\
 Q_{23} &= \begin{bmatrix} 0.5770 & 0.0001 \\ 0.0001 & 0.0014 \end{bmatrix}, & Q_{24} &= \begin{bmatrix} 0.5904 & 0.0002 \\ 0.0002 & 0.0011 \end{bmatrix}, \\
 Q_{25} &= \begin{bmatrix} 0.2626 & -0.0002 \\ -0.0002 & 0.0001 \end{bmatrix}, & Q_{26} &= \begin{bmatrix} 0.2059 & -0.0004 \\ -0.0004 & 0.0001 \end{bmatrix}, \\
 Z_{21} &= \begin{bmatrix} 1.9893 & -0.0269 \\ -0.0269 & 1.2602 \end{bmatrix}, & Z_{22} &= \begin{bmatrix} 0.7829 & -0.0381 \\ -0.0381 & 0.0732 \end{bmatrix},
 \end{aligned}$$

**Fig. 3** State response of system (1) with controller failures (Example 1)



$$Z_{23} = \begin{bmatrix} 1.1185 & -0.5023 \\ -0.5023 & 0.5062 \end{bmatrix}, \quad Z_{24} = \begin{bmatrix} 0.6985 & -0.0204 \\ -0.0204 & 0.0491 \end{bmatrix}.$$

Furthermore, it is obtained from (31) that  $\mu = 2.7$ . From (32), selecting  $\alpha^* = 0.02$  yields  $f_T \leq 1/3$ , which means that the controller failure time is not more than 1/3 of the total time. Given  $\alpha_0 = 0.01$ , it holds from (33) that  $f_N \leq 0.0039$ , which implies that the controller failure frequency is permitted to be 0.0039. Thus, if the two conditions are satisfied, then system (1) is exponentially stable with the state delay

$$\|x(t)\| \leq 3.6754e^{-0.01t} \|x(0)\|_{\theta}.$$

Choose the following switching signal:

$$\sigma(t) = \begin{cases} 1, & t \in \Pi = [0, 700] \cup [1000, 1300] \cup [1600, 2000], \\ 2, & t \in [0, 2000] \setminus \Pi, \end{cases}$$

which satisfies the restriction conditions. In this switching signal, the total time and the number of controller failures are 600 seconds and 2 times, respectively. Figure 3 gives the state trajectories of system (1) under  $\sigma(t)$  in 2000 seconds. Comparing the state responses in Figs. 1 and 3, it can be observed that the states of system (1) are not seriously affected for a less unavailable rate and failure frequency of the controller.

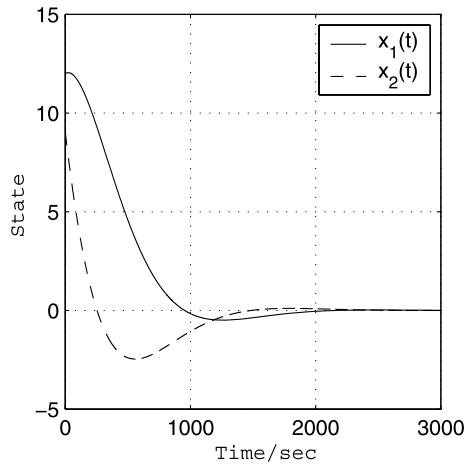
*Example 2* Consider system (1) under (41) with

$$A = \begin{bmatrix} 0.5 & 0.1 \\ 0 & 0.8 \end{bmatrix}, \quad E = \begin{bmatrix} -0.3 & 0 \\ -0.2 & -1.1 \end{bmatrix}, \quad F = \begin{bmatrix} 1 \\ 0 \end{bmatrix},$$

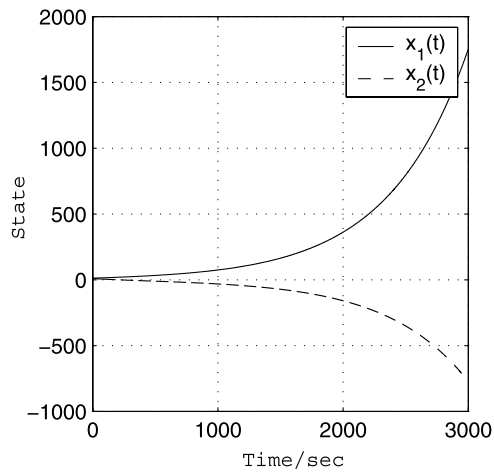
$$h_1 = 0.1, \quad h_2 = 0.8.$$

A state feedback controller  $u(t) = Kx(t - d_2(t))$  has been designed, where  $K = [-0.4 \ 0.2]$  and  $h_3 = 0.3, h_4 = 1.0$ . The controller stabilizes system (1) over an unreliable path. Under initial state  $\phi(\theta) = [12 \ 9]^T, \theta \in [-1.0, 0]$ , the state trajectories of

**Fig. 4** State response of system (1) with the controller (Example 2)



**Fig. 5** State response of system (1) without the controller (Example 2)

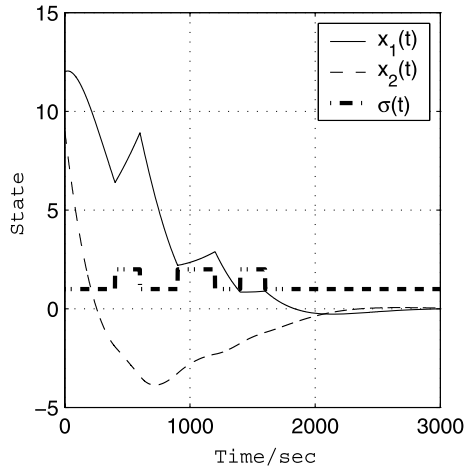


system (1) with and without the controller are shown in Figs. 4 and 5, respectively. Figure 4 shows that the designed controller can stabilize the system. This implies that the resulting closed-loop system is stable. Figure 5 depicts the state response of the system when  $u(t) = 0$ . It can be clearly seen that the open-loop system is unstable. Then Assumptions (A2) and (A1) are satisfied. Therefore, system (1) can be formulated as (5). By applying the methods mentioned in Remark 5 with  $\alpha = 0.15$ ,  $\beta = 0.41$  and  $\mu = 4.35$  to solve this problem, the obtained results are

$$\begin{aligned}
 P_1 &= \begin{bmatrix} 0.1054 & 0.0204 \\ 0.0204 & 0.1755 \end{bmatrix}, & Q_{11} &= \begin{bmatrix} 0.0021 & 0.0002 \\ 0.0002 & 0.0028 \end{bmatrix}, \\
 Q_{12} &= \begin{bmatrix} 0.0024 & 0.0002 \\ 0.0002 & 0.0032 \end{bmatrix}, & Q_{13} &= \begin{bmatrix} 0.0018 & 0.0001 \\ 0.0001 & 0.0035 \end{bmatrix},
 \end{aligned}$$



**Fig. 6** State response of system (1) with controller failures (Example 2)



$$\begin{aligned}
 Q_{14} &= \begin{bmatrix} 0.0020 & -0.0001 \\ -0.0001 & 0.0038 \end{bmatrix}, & Z_{11} &= \begin{bmatrix} 0.1176 & 0.0818 \\ 0.0818 & 0.5119 \end{bmatrix}, \\
 Z_{12} &= \begin{bmatrix} 0.0130 & 0.0004 \\ 0.0004 & 0.0156 \end{bmatrix}, & Z_{13} &= \begin{bmatrix} 0.1268 & -0.0475 \\ -0.0475 & 0.0354 \end{bmatrix}, \\
 Z_{14} &= \begin{bmatrix} 0.0110 & 0.0008 \\ 0.0008 & 0.0169 \end{bmatrix}, & P_2 &= \begin{bmatrix} 0.0637 & 0.0021 \\ 0.0021 & 0.0708 \end{bmatrix}, \\
 Q_{21} &= \begin{bmatrix} 0.0067 & 0.0006 \\ 0.0006 & 0.0086 \end{bmatrix}, & Q_{22} &= \begin{bmatrix} 0.0074 & 0.0007 \\ 0.0007 & 0.0098 \end{bmatrix}, \\
 Q_{23} &= \begin{bmatrix} 0.0057 & 0.0002 \\ 0.0002 & 0.0105 \end{bmatrix}, & Q_{24} &= \begin{bmatrix} 0.0064 & -0.0002 \\ -0.0002 & 0.0115 \end{bmatrix}, \\
 Z_{21} &= \begin{bmatrix} 0.0703 & 0.0145 \\ 0.0145 & 0.1427 \end{bmatrix}, & Z_{22} &= \begin{bmatrix} 0.0328 & -0.0001 \\ -0.0001 & 0.0329 \end{bmatrix}, \\
 Z_{23} &= \begin{bmatrix} 0.0687 & -0.0123 \\ -0.0123 & 0.0362 \end{bmatrix}, & Z_{24} &= \begin{bmatrix} 0.0289 & 0.0009 \\ 0.0009 & 0.0353 \end{bmatrix}.
 \end{aligned}$$

Furthermore, according to (32), selecting  $\alpha^* = 0.02$  leads to  $f_T \leq 0.23$ . Given  $\alpha_0 = 0.01$ , it holds from (33) that  $f_N \leq 0.029$ . Thus, system (1) is exponentially stable with

$$\|x(t)\| \leq 1.7055e^{-0.005t} \|x(0)\|_{\theta},$$

if the conditions  $f_T \leq 0.23$  and  $f_N \leq 0.029$  are satisfied with the following switching signal:

$$\sigma(t) = \begin{cases} 1, & t \in \Pi = [0, 400] \cup [600, 900] \cup [1200, 1400] \cup [1600, 3000], \\ 2, & t \in [0, 3000] / \Pi, \end{cases}$$

which means that the total time and the number of controller failures are 700 seconds and 3 times, respectively. Figure 6 gives the state trajectories of system (1) under

$\sigma(t)$  in 3000 seconds. It can be seen from the comparison of the state responses in Figs. 4 and 6 that the state responses of system (1) do not degenerate seriously for a less unavailable rate and failure frequency of the controller. It follows from the preceding two examples that the systems with controller failure still remain stable under a certain failure frequency and an unavailable rate of the controller. We also find that Theorem 1 is applicable to both cases, where the derivative of the time delay is either known or unknown.

## 5 Conclusions

This paper has studied the problem of controller failure for systems with interval time-varying delay, which are controlled by a predesigned state feedback controller. Using the idea of switched control, this problem is first converted into a stability analysis problem for a class of switched delay systems composed of both stable and unstable subsystems. Then, two lemmas have been developed to reflect the change property of the Lyapunov functional for each subsystem. Finally, based on the piecewise Lyapunov functional method, a class of switching laws has been proposed to guarantee exponential stability of the switched delay system. We have also extended the results to the case where there is no restriction on the derivative of the interval time-varying delay, which allows a fast time-varying delay. Simulation results have been provided to illustrate the effectiveness of the proposed methods.

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