



A characteristic property of circular cylinders

Thomas Hasanis

Abstract. A translation surface in 3-dimensional Euclidean space is a surface that can be constructed as the sum of two regular curves α and β . Recently, the minimal translation surfaces were characterized in terms of the curvature and the torsion of the generating curves. In this paper, we characterize all translation surfaces with constant and non-zero mean curvature by proving that: The only translation surface in 3-dimensional Euclidean space \mathbb{R}^3 with constant and non-zero mean curvature H is the circular cylinder of radius $\frac{1}{2|H|}$.

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1. Introduction and statement of main result

The surfaces of our study have their origin in G. Darboux' classical text [1], where the so-called “*surfaces définies pour des propriétés cinématiques*” are considered; they are referred to as *Darboux surfaces* in the literature. A Darboux surface is defined kinematically as the movement of a curve by a uniparametric family of rigid motions of \mathbb{R}^3 . Hence, a parameterization of such a surface is $\Psi(s, t) = A(t)\alpha(s) + \beta(t)$, where α and β are two space curves and $A(t)$ is an orthogonal matrix. In this paper we consider the case with $A(t)$ the identity. More precisely, we give the following definition.

Definition 1.1. A surface $S \subset \mathbb{R}^3$ is called *translation surface*, if it can, locally, be constructed as the sum $\Psi(s, t) = \alpha(s) + \beta(t)$ of two space curves $\alpha : I \subset \mathbb{R} \rightarrow \mathbb{R}^3$ and $\beta : J \subset \mathbb{R} \rightarrow \mathbb{R}^3$. If α and β are plane curves lying on orthogonal planes, the surface is called translation surface of plane type.

The curves α and β are called the generating curves of S . The terminology “translation surface” is due to the fact that the surface S is obtained by the translation of α along β (or vice versa because the roles of α and β are interchangeable). In particular, all parametric curves $s = \text{const.}$ are congruent by translations (similarly for parametric curves $t = \text{const.}$).

It is natural to ask for a classification of translation surfaces in \mathbb{R}^3 , beyond translation surfaces of plane type, under some conditions on their curvatures. Recently, in collaboration with R. López [4] we completely classified all translation surfaces with constant Gaussian curvature K , proving that the only ones are cylindrical surfaces, and thus K must be zero. In [11], R. López and O. Perdomo characterized all minimal translation surfaces in \mathbb{R}^3 in terms of the curvature and torsion of the generating curves. Finally, in [5] jointly with R. López we offer an alternative approach to the study and construction of minimal translation surfaces. Consequently, it is natural to ask the following question.

Problem. *Which surfaces in the Euclidean space \mathbb{R}^3 with constant and non-zero mean curvature are sums of two space curves?*

The only known translation surface in \mathbb{R}^3 with constant mean curvature $H \neq 0$, is the circular cylinder of radius $\frac{1}{2|H|}$. A surface $z = f(x) + g(y)$ can be viewed as the sum of the plane curves $x \mapsto (x, 0, f(x))$ and $y \mapsto (0, y, g(y))$. Moreover, every translation surface S of plane type (see Definition 1.1) can be viewed as a surface of the above form. The following result was proved by Liu [7]: *Let S be a translation surface $z = f(x) + g(y)$ with constant mean curvature $H \neq 0$. Then, S is congruent to the following surface or part of it*

$$z = -\frac{\sqrt{1 + \alpha^2}}{2H} \sqrt{1 - 4H^2x^2} - \alpha y, \quad \alpha \in \mathbb{R}.$$

It is obvious that this surface is a circular cylinder of radius $\frac{1}{2|H|}$. In [3] we proved: *Circular cylinders are the only translation surfaces of constant and non-zero mean curvature in \mathbb{R}^3 , with a planar generating curve.*

In the present paper we completely classify all translation surfaces with non-zero and constant mean curvature in \mathbb{R}^3 by proving the following result.

Theorem 1.1. *Circular cylinders are the only translation surfaces of constant and non-zero mean curvature in \mathbb{R}^3 .*

Translation surfaces in ambient spaces besides \mathbb{R}^3 have been studied in [6–10] to mention just a few articles.

The paper is organized as follows: In Sect. 2, we recall some known formulas on the local theory of curves and surfaces of \mathbb{R}^3 . Then, at any point $\Psi(s, t)$ of S we represent the rotation of Frenet trihedrons by Euler’s angles and express the mean curvature of S by these angles. The Proof of Theorem 1.1 is given in Sect. 3 after some lengthy calculations.

2. Preliminaries

A general reference on curves and surfaces is [2]. All curves and surfaces considered will be assumed to be regular and of class C^∞ . Let $x : I = (a, b) \rightarrow \mathbb{R}^3$ be a curve parameterized by arc length s , with curvature $k(s) > 0$, torsion $\tau(s)$, and oriented Frenet trihedron $(t(s), n(s), b(s))$. We shall use the equations, referred to as Frenet formulas,

$$\begin{cases} t' = kn \\ n' = -kt + \tau b \\ b' = -\tau n. \end{cases} \tag{2.1}$$

We have omitted the argument s for convenience; by prime ($'$) we denote differentiation with respect to s .

Let $\alpha : I \subset \mathbb{R} \rightarrow \mathbb{R}^3, s \mapsto \alpha(s)$, and $\beta : J \subset \mathbb{R} \rightarrow \mathbb{R}^3, t \mapsto \beta(t)$, be two curves in \mathbb{R}^3 parameterized by arc length with curvatures $k_\alpha(s), k_\beta(t)$, torsions $\tau_\alpha(s), \tau_\beta(t)$, and oriented Frenet trihedrons $(t_\alpha(s), n_\alpha(s), b_\alpha(s)), (t_\beta(t), n_\beta(t), b_\beta(t))$ for every $s \in I, t \in J$. In order that α and β be the generating curves of a regular translation surface $S \subset \mathbb{R}^3$, we suppose that $\alpha'(s) \times \beta'(t) \neq 0$ for all $(s, t) \in I \times J \subset \mathbb{R}^2$, where \times represents the vector product of \mathbb{R}^3 . By prime ($'$) we denote differentiation with respect to s , and by dot ($\dot{}$) differentiation with respect to t .

Let $S = \{\alpha(s) + \beta(t) : s \in I, t \in J\} \subset \mathbb{R}^3$ be the set obtained by the sum of the curves α and β . Then, S is a regular translation surface, and $\Psi(s, t) = \alpha(s) + \beta(t)$ is a parameterization of S .

We will now proceed to calculate the mean curvature of S . For notational convenience, we omit the dependence of functions on s and t ; it is implicitly understood. The derivatives of order 1 of Ψ are $\Psi_s = \alpha' = t_\alpha, \Psi_t = \beta' = t_\beta$ with $\Psi_s \times \Psi_t \neq 0$. Let $\varphi(s, t), 0 < \varphi(s, t) < \pi$, be the angle between $t_\alpha(s)$ and $t_\beta(t)$ at the point $\Psi(s, t)$, that is

$$\langle t_\alpha(s), t_\beta(t) \rangle = \cos \varphi(s, t), \tag{2.2}$$

where $\langle \cdot, \cdot \rangle$ stands for the usual scalar product on \mathbb{R}^3 . The coefficients of the first fundamental form of S in the basis Ψ_s, Ψ_t are

$$E = 1, \quad F = \cos \varphi, \quad G = 1,$$

and the unit normal vector $N(s, t)$ at $\Psi(s, t)$ is

$$N(s, t) = \frac{t_\alpha(s) \times t_\beta(t)}{\sin \varphi(s, t)}.$$

The derivatives of order 2 of Ψ are

$$\Psi_{ss} = t'_\alpha = k_\alpha n_\alpha, \quad \Psi_{st} = 0, \quad \Psi_{tt} = \dot{t}_\beta = k_\beta n_\beta.$$

Hence, the coefficients of the second fundamental form of S are

$$\ell = \langle \Psi_{ss}, N \rangle = -\frac{k_\alpha \langle b_\alpha, t_\beta \rangle}{\sin \varphi}, \quad m = \langle \Psi_{st}, N \rangle = 0, \quad n = \langle \Psi_{tt}, N \rangle = \frac{k_\beta \langle t_\alpha, b_\beta \rangle}{\sin \varphi}.$$

Thus, from the well-known formula $2H = \frac{\ell G - 2Fm + nE}{EG - F^2}$ for the mean curvature H we have

$$-k_\alpha \langle b_\alpha, t_\beta \rangle + k_\beta \langle t_\alpha, b_\beta \rangle = 2H \sin^3 \varphi. \tag{2.3}$$

The orthogonal matrix

$$\mathcal{O} = \begin{pmatrix} \langle t_\alpha, t_\beta \rangle & \langle n_\alpha, t_\beta \rangle & \langle b_\alpha, t_\beta \rangle \\ \langle t_\alpha, n_\beta \rangle & \langle n_\alpha, n_\beta \rangle & \langle b_\alpha, n_\beta \rangle \\ \langle t_\alpha, b_\beta \rangle & \langle n_\alpha, b_\beta \rangle & \langle b_\alpha, b_\beta \rangle \end{pmatrix}$$

represents a rotation of the Frenet frame $(t_\alpha, n_\alpha, b_\alpha)$ to the frame $(t_\beta, n_\beta, b_\beta)$ at the point $\Psi(s, t)$ of S . As it is well known, any rotation can be described by three angles, the Euler angles. There are many ways to do this. Here, we proceed as follows. At the point $\Psi(s, t)$: (i) we rotate the frame $(t_\alpha, n_\alpha, b_\alpha)$ about t_α by an angle $\vartheta(s, t)$, (ii) we rotate about the new position of b_α by an angle $\varphi(s, t)$, and thus the new position of t_α coincides with t_β , (iii) finally, we rotate about the new position of t_α (that is, about t_β) by an angle $\omega(s, t)$. The final position of $(t_\alpha, n_\alpha, b_\alpha)$ is the frame $(t_\beta, n_\beta, b_\beta)$. Therefore, we have

$$\mathcal{O} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \omega & \sin \omega \\ 0 & -\sin \omega & \cos \omega \end{pmatrix} \begin{pmatrix} \cos \varphi & \sin \varphi & 0 \\ -\sin \varphi & \cos \varphi & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \vartheta & \sin \vartheta \\ 0 & -\sin \vartheta & \cos \vartheta \end{pmatrix}$$

or

$$\begin{aligned} \langle t_\alpha, t_\beta \rangle &= \cos \varphi, & \langle n_\alpha, t_\beta \rangle &= \sin \varphi \cos \vartheta, & \langle b_\alpha, t_\beta \rangle &= \sin \varphi \sin \vartheta, \\ \langle t_\alpha, n_\beta \rangle &= -\sin \varphi \cos \omega, & \langle n_\alpha, n_\beta \rangle &= \cos \varphi \cos \vartheta \cos \omega - \sin \vartheta \sin \omega, \\ \langle b_\alpha, n_\beta \rangle &= \cos \varphi \sin \vartheta \cos \omega + \cos \vartheta \sin \omega, & \langle t_\alpha, b_\beta \rangle &= \sin \varphi \sin \omega, \\ \langle n_\alpha, b_\beta \rangle &= -\cos \varphi \cos \vartheta \sin \omega - \sin \vartheta \cos \omega, & \langle b_\alpha, b_\beta \rangle &= -\cos \varphi \sin \vartheta \sin \omega \\ & & & + \cos \vartheta \cos \omega. \end{aligned} \tag{2.4}$$

Hence, relation (2.3) becomes

$$k_\beta \sin \omega = k_\alpha \sin \vartheta + 2H \sin^2 \varphi. \tag{2.5}$$

For later use, we do some calculations. Differentiating $\langle t_\alpha, t_\beta \rangle = \cos \varphi$ with respect to s and taking into account the Frenet equations for α and (2.4), we have

$$k_\alpha \langle n_\alpha, t_\beta \rangle = -\sin \varphi \cdot \varphi_s$$

or

$$k_\alpha \sin \varphi \cos \vartheta = -\sin \varphi \cdot \varphi_s,$$

where φ_s stands for the partial derivative $\frac{\partial \varphi}{\partial s}$. So, we obtain

$$\varphi_s = -k_\alpha \cos \vartheta. \tag{2.6}$$

Moreover, from $\langle n_\alpha, t_\beta \rangle = \sin \varphi \cos \vartheta$ we have

$$-k_\alpha \langle t_\alpha, t_\beta \rangle + \tau_\alpha \langle b_\alpha, t_\beta \rangle = \cos \varphi \cos \vartheta \cdot \varphi_s - \sin \varphi \sin \vartheta \cdot \vartheta_s$$

or, in view of (2.4) and (2.6),

$$-k_\alpha \cos \varphi + \tau_\alpha \sin \varphi \sin \vartheta = -k_\alpha \cos \varphi \cos^2 \vartheta - \sin \varphi \sin \vartheta \cdot \vartheta_s.$$

In the case where $\sin \vartheta \neq 0$, we have

$$\sin \varphi \cdot \vartheta_s = k_\alpha \cos \varphi \sin \vartheta - \tau_\alpha \sin \varphi. \tag{2.7}$$

Differentiating $\langle t_\alpha, n_\beta \rangle = -\sin \varphi \cos \omega$ with respect to s and using (2.6), we obtain

$$k_\alpha (\cos \varphi \cos \vartheta \cos \omega - \sin \vartheta \sin \omega) = -\cos \varphi \cos \omega (-k_\alpha \cos \vartheta) + \sin \varphi \sin \omega \cdot \omega_s$$

or, in the case where $\sin \omega \neq 0$,

$$\sin \varphi \cdot \omega_s = -k_\alpha \sin \vartheta. \tag{2.8}$$

In a similar way, differentiating with respect to t , we see that

$$\varphi_t = k_\beta \cos \omega, \quad \sin \varphi \cdot \vartheta_t = k_\beta \sin \omega, \quad \sin \varphi \cdot \omega_t = -k_\beta \cos \varphi \sin \omega + \tau_\beta \sin \varphi. \tag{2.9}$$

3. Proof of Theorem 1.1

We, firstly, recall that the parametric curves $t = \text{const.}$ are parallel translations and congruent to α (similarly, the parametric curves $s = \text{const.}$ are congruent to β). In what follows, we suppose that the translation surface S has constant and non-zero mean curvature H .

If the curvature of a generating curve vanishes everywhere, that is, if a generating curve is a line ε , then S is cylindrical. Thus, if its mean curvature is constant $H \neq 0$, the section of S by a plane normal to ε is a circle of radius $\frac{1}{2|H|}$, and S is a circular cylinder.

Moreover, if a generating curve is a plane curve, that is, if its torsion vanishes everywhere, then, as we have proved in [3], S is also a circular cylinder.

Therefore, and since the problem is of local nature, in what follows we assume that

$$k_\alpha(s) > 0 \quad \text{and} \quad \tau_\alpha(s) \neq 0 \tag{3.1}$$

everywhere.

We need the following auxiliary result.

Lemma 3.1. *Under the above assumptions, we have*

- (i) $\sin \vartheta \neq 0$
- (ii) $\sin \omega \neq 0$

almost everywhere in $I \times J$.

Proof. (i) Indeed, if this were not the case, then (2.4) would yield $\langle b_\alpha, t_\beta \rangle = 0$ in an open subset of $I \times J$. Differentiating with respect to s and using the fact that $\tau_\alpha(s) \neq 0$, we obtain $\langle n_\alpha, t_\beta \rangle = 0$. So t_β is parallel to $n_\alpha \times b_\alpha = t_\alpha$, which contradicts $0 < \varphi(s, t) < \pi$.

- (ii) In fact, if this were not the case, then from (2.4) we would have $\langle t_\alpha, b_\beta \rangle = 0$ in an open subset of $I \times J$. Differentiating with respect to s and using (3.1), we have $\langle n_\alpha, b_\beta \rangle = 0$. So $b_\alpha = t_\alpha \times n_\alpha = \pm b_\beta$, from which by differentiating with respect to s , we have $\tau_\alpha = 0$. This contradicts our assumption (3.1). \square

Obviously, given a translation surface $\Psi(s, t) = \alpha(s) + \beta(t)$ with constant non-zero mean curvature H and a non-zero constant $\lambda \in \mathbb{R}$, the surface $Z(s, t) = \lambda\Psi(s, t)$ is also a translation surface. The mean curvature $H_Z(s, t)$ of $Z(s, t)$ is the non-zero constant $H_Z(s, t) = \frac{H}{\lambda}$; for $\lambda = 2H$, we have $H_Z(s, t) = \frac{1}{2}$. So, without loss of generality, we may suppose that $H = \frac{1}{2}$, and this hypothesis will be assumed without further comment. Therefore, from (2.5) we obtain

$$k_\beta \sin \omega = k_\alpha \sin \vartheta + \sin^2 \varphi. \tag{3.2}$$

Differentiating (3.2) with respect to s and taking (2.6), (2.7) and (2.8) into account, we get

$$k_\beta \frac{\cos \omega}{\sin \varphi} (-k_\alpha \sin \vartheta) = k'_\alpha \sin \vartheta + k_\alpha \frac{\cos \vartheta}{\sin \varphi} (k_\alpha \cos \varphi \sin \vartheta - \tau_\alpha \sin \varphi) + 2 \sin \varphi \cos \varphi (-k_\alpha \cos \vartheta) \tag{3.3}$$

or

$$-k_\alpha k_\beta \cos \omega \sin \vartheta = k'_\alpha \sin \vartheta \sin \varphi + k_\alpha^2 \cos \varphi \cos \vartheta \sin \vartheta - k_\alpha \tau_\alpha \cos \vartheta \sin \varphi - 2k_\alpha \cos \varphi \sin^2 \varphi \cos \vartheta. \tag{3.4}$$

Hence, in view of (3.1) and Lemma 3.1, we have

$$k_\beta \cos \omega = -\frac{k'_\alpha}{k_\alpha} \sin \varphi - k_\alpha \cos \varphi \cos \vartheta + \tau_\alpha \frac{\cos \vartheta}{\sin \vartheta} \sin \varphi + 2 \cos \varphi \sin^2 \varphi \frac{\cos \vartheta}{\sin \vartheta}. \tag{3.5}$$

Differentiating (3.5) with respect to s again and taking (3.2) into account, we have

$$k_\alpha^2 \frac{\sin^2 \vartheta}{\sin \varphi} + k_\alpha \sin \vartheta \sin \varphi = -\left(\frac{k'_\alpha}{k_\alpha}\right)' \sin \varphi + k_\alpha^2 \frac{\cos^2 \varphi \sin^2 \vartheta}{\sin \varphi} - k_\alpha \tau_\alpha \cos \varphi \sin \vartheta - k_\alpha^2 \sin \varphi \cos^2 \vartheta + \tau'_\alpha \frac{\cos \vartheta \sin \varphi}{\sin \vartheta} - k_\alpha \tau_\alpha \frac{\cos \varphi}{\sin \vartheta} + \tau_\alpha^2 \frac{\sin \varphi}{\sin^2 \vartheta} - k_\alpha \tau_\alpha \frac{\cos^2 \vartheta \cos \varphi}{\sin \vartheta} + 2k_\alpha \frac{\cos^2 \vartheta \sin^3 \varphi}{\sin \vartheta} - 4k_\alpha \frac{\cos^2 \varphi \cos^2 \vartheta \sin \varphi}{\sin \vartheta} - 2k_\alpha \frac{\cos^2 \varphi \sin \varphi}{\sin \vartheta} + 2\tau_\alpha \frac{\cos \varphi \sin^2 \varphi}{\sin^2 \vartheta}$$

or, multiplying by $\frac{\sin^2 \vartheta}{\tau_\alpha}$ and collecting the terms,

$$\begin{aligned} & \frac{\left(\frac{k'_\alpha}{k_\alpha}\right)' + k_\alpha^2}{\tau_\alpha} \sin \varphi \sin^2 \vartheta - \frac{\tau'_\alpha}{\tau_\alpha} \cos \vartheta \sin \vartheta \sin \varphi - \tau_\alpha \sin \varphi - 2 \cos \varphi \sin^2 \varphi \\ & + \frac{2k_\alpha}{\tau_\alpha} (\tau_\alpha \cos \varphi - \sin^3 \varphi + 3 \cos^2 \varphi \sin \varphi) \sin \vartheta \\ & + \frac{k_\alpha}{\tau_\alpha} (2 \sin^3 \varphi + \sin \varphi - 4 \cos^2 \varphi \sin \varphi) \sin^3 \vartheta = 0. \end{aligned}$$

Dividing by $\sin^3 \varphi$, setting $Z := \frac{\cos \varphi}{\sin \varphi}$, and using the relation $\frac{1}{\sin^2 \varphi} = 1 + Z^2$, we see that

$$\begin{aligned} & \frac{\left(\frac{k'_\alpha}{k_\alpha}\right)' + k_\alpha^2}{\tau_\alpha} \sin^2 \vartheta (1 + Z^2) - \frac{\tau'_\alpha}{\tau_\alpha} \cos \vartheta \sin \vartheta (1 + Z^2) - \tau_\alpha (1 + Z^2) - 2Z \\ & + \frac{2k_\alpha}{\tau_\alpha} (\tau_\alpha Z (1 + Z^2) - 1 + 3Z^2) \sin \vartheta + \frac{3k_\alpha}{\tau_\alpha} (1 - Z^2) \sin^3 \vartheta = 0 \end{aligned}$$

or

$$\begin{aligned} & 2k_\alpha \sin \vartheta Z^3 + \left(\frac{\left(\frac{k'_\alpha}{k_\alpha}\right)' + k_\alpha^2}{\tau_\alpha} \sin^2 \vartheta - \frac{\tau'_\alpha}{\tau_\alpha} \cos \vartheta \sin \vartheta - \tau_\alpha + \frac{6k_\alpha}{\tau_\alpha} \sin \vartheta - \frac{3k_\alpha}{\tau_\alpha} \sin^3 \vartheta \right) Z^2 \\ & + (2k_\alpha \sin \vartheta - 2)Z \\ & + \left(\frac{\left(\frac{k'_\alpha}{k_\alpha}\right)' + k_\alpha^2}{\tau_\alpha} \sin^2 \vartheta - \frac{\tau'_\alpha}{\tau_\alpha} \cos \vartheta \sin \vartheta - \tau_\alpha - \frac{2k_\alpha}{\tau_\alpha} \sin \vartheta + \frac{3k_\alpha}{\tau_\alpha} \sin^3 \vartheta \right) = 0. \end{aligned} \tag{3.6}$$

Henceforth, for notational convenience, we set

$$\begin{aligned} k &:= k_\alpha, \quad \tau := \tau_\alpha, \quad \Sigma := \left(\frac{k'}{k}\right)' + k^2 - \tau^2, \quad B := \frac{2k'}{k} + \frac{\tau'}{\tau} \\ C &:= \frac{\Sigma}{\tau} - \tau, \quad D := \frac{\Sigma}{\tau} + \tau, \quad X := \cos \vartheta, \quad Y := \sin \vartheta. \end{aligned} \tag{3.7}$$

Inserting these notations in (3.6) and using the identity $\sin^3 \vartheta = \sin \vartheta (1 - \cos^2 \vartheta)$, we obtain

$$\begin{aligned} & 2kY Z^3 + \left(\frac{3k}{\tau} X^2 Y + DY^2 - \frac{\tau'}{\tau} XY + \frac{3k}{\tau} Y - \tau \right) Z^2 + (2kY - 2)Z \\ & + \left(-\frac{3k}{\tau} X^2 Y + DY^2 - \frac{\tau'}{\tau} XY + \frac{k}{\tau} Y - \tau \right) = 0. \end{aligned} \tag{3.8}$$

Remark 3.1. We note that $Z \neq 0$ almost everywhere in $I \times J$. Indeed, if this were not the case, then (2.1) would yield $\langle t_\alpha, t_\beta \rangle = 0$. Differentiating this twice with respect to s , and using (3.1) and the Frenet formulas (2.1), we are lead to a contradiction $\langle n_\alpha, t_\beta \rangle = \langle b_\alpha, t_\beta \rangle = 0$.

Before we proceed to some more calculations, we need the following obvious consequence of (2.6) and (2.7).

Lemma 3.2. *For the derivatives of X, Y, Z with respect to s we have*

$$\begin{aligned} X_s &= -kY^2 Z + \tau Y, \\ Y_s &= kXYZ - \tau X, \\ Z_s &= kX(1 + Z^2). \end{aligned}$$

Differentiating (3.8) with respect to s and taking Lemma 3.2 into account, we get

$$\begin{aligned}
 &8k^2XYZ^4 + \left(\frac{15k^2}{\tau}X^3Y - \frac{4k\tau'}{\tau}X^2Y + 4kDXY^2 + \frac{3k^2}{\tau}XY - 4k\tau X + kBY\right)Z^3 \\
 &+ \left(-9kX^3 + 3\left(\frac{k}{\tau}\right)'X^2Y + C'Y^2 + (8k^2 - B')XY + kX + 3\left(\frac{k}{\tau}\right)'Y\right)Z^2 \\
 &+ \left(-\frac{3k^2}{\tau}X^3Y + 4kDXY^2 - \frac{4k\tau'}{\tau}X^2Y + \frac{13k^2}{\tau}XY - 4k\tau X + kBY\right)Z \\
 &+ \left(-3\left(\frac{k}{\tau}\right)'X^2Y - 9kXY^2 + C'Y^2 - B'XY + \left(\frac{k}{\tau}\right)'Y\right) = 0,
 \end{aligned} \tag{3.9}$$

where in some steps we have used the relation $X^2 + Y^2 = 1$, the notation (3.7) and the relation $2k^2 - \left(\frac{\tau'}{\tau}\right)' - 2\tau D = -B'$. Now, multiplying (3.8) by $4kXZ$ and subtracting from (3.9), and dividing the result by Y , which is non-zero by Lemma 3.1, we obtain

$$\begin{aligned}
 &k\left(\frac{3k}{\tau}X^3 - \frac{9k}{\tau}X + B\right)Z^3 + \left(3\left(\frac{k}{\tau}\right)'X^2 + 9kXY + C'Y - B'X + 3\left(\frac{k}{\tau}\right)'\right)Z^2 \\
 &+ k\left(\frac{9k}{\tau}X^3 + \frac{9k}{\tau}X + B\right)Z + \left(-3\left(\frac{k}{\tau}\right)'X^2 - 9kXY + C'Y - B'X + \left(\frac{k}{\tau}\right)'\right) = 0.
 \end{aligned} \tag{3.10}$$

Elimination of Z^3 between equations (3.8) and (3.10) yields an equation of the form

$$b_2Z^2 + b_1Z + b_0 = 0. \tag{3.11}$$

This is a polynomial equation of second degree with respect to Z , with coefficients

$$\begin{aligned}
 b_2 &= \frac{9k^2}{\tau^2}X^5Y + \frac{3kD}{\tau}X^3Y^2 - \frac{3k\tau'}{\tau^2}X^4Y - \frac{18k^2}{\tau^2}X^3Y - 3kX^3 \\
 &+ \frac{18k\tau'}{\tau^2}X^2Y - \left(\frac{9kD}{\tau} + 18k\right)XY^2 + (BD - 2C')Y^2 \\
 &+ \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2}\right)XY + 9kX + \frac{9k\tau'}{\tau^2}Y - \tau B, \\
 b_1 &= -\frac{12k^2}{\tau}X^3Y - \frac{6k}{\tau}X^3 - \frac{36k^2}{\tau}XY + \frac{18k}{\tau}X - 2B, \\
 b_0 &= -\frac{9k^2}{\tau^2}X^5Y + \frac{3kD}{\tau}X^3Y^2 - \frac{3k\tau'}{\tau^2}X^4Y + \frac{30k^2}{\tau^2}X^3Y - 3kX^3 \\
 &- \left(\frac{9kD}{\tau} - 18k\right)XY^2 + (BD - 2C')Y^2 + \left(2B' - \frac{B\tau'}{\tau} - \frac{9k^2}{\tau^2}\right)XY \\
 &+ 9kX + \frac{3k\tau'}{\tau^2}Y - \tau B.
 \end{aligned}$$

Next, we shall eliminate Z^3 between equation (3.8) and $b_2Z^3 + b_1Z^2 + b_0Z = 0$. The resulting polynomial equation is of second degree with respect to Z and has the form

$$c_2Z^2 + c_1Z + c_0 = 0, \tag{3.12}$$

with coefficients

$$\begin{aligned}
c_2 = & \frac{27k^3}{\tau^3} X^7 Y^2 + \frac{18k^2 D}{\tau^2} X^5 Y^3 - \frac{18k^2 \tau'}{\tau^3} X^6 Y^2 + \left(-\frac{27k^3}{\tau^3} + \frac{3k(\tau')^2}{\tau^3} \right) X^5 Y^2 \\
& + \frac{3kD^2}{\tau} X^3 Y^4 - \frac{6k\tau'D}{\tau^2} X^4 Y^3 - \frac{18k^2}{\tau} X^5 Y + \frac{63k^2 \tau'}{\tau^3} X^4 Y^2 - \left(\frac{36k^2 D}{\tau^2} + \frac{54k^2}{\tau} \right) X^3 Y^3 \\
& + \left(\frac{27k\tau'D}{\tau^2} + \frac{3k}{\tau} (BD - 2C') + \frac{18k\tau'}{\tau} \right) X^2 Y^3 + \frac{6k\tau'}{\tau} X^4 Y - D \left(\frac{9kD}{\tau} + 18k \right) XY^4 \\
& + \left(\frac{6kB'}{\tau} - \frac{3k\tau'B}{\tau^2} - 6kD - \frac{135k^3}{\tau^3} + \frac{24k^3}{\tau} - \frac{18k(\tau')^2}{\tau^3} \right) X^3 Y^2 + \frac{48k^2}{\tau} X^3 Y \\
& + D(BD - 2C')Y^4 + \left(\frac{108k^2 \tau'}{\tau^3} - \frac{\tau'}{\tau} (2B' - \frac{B\tau'}{\tau}) \right) X^2 Y^2 \\
& + \left(2DB' - \frac{2\tau'}{\tau} (BD - C') - \frac{54k^2 D}{\tau^2} - \frac{54k^2}{\tau} \right) XY^3 + 3k\tau X^3 - \left(6k' + \frac{30k\tau'}{\tau} \right) X^2 Y \\
& + \left(\frac{12k\tau'D}{\tau^2} + \frac{6k'D}{\tau} - \frac{6kC'}{\tau} \right) Y^3 \\
& + \left(18kD + 18k\tau + \frac{72k^3}{\tau} - \frac{81k^3}{\tau^3} - \frac{9k(\tau')^2}{\tau^3} + \frac{6kB'}{\tau} - \frac{3k\tau'B}{\tau^2} \right) XY^2 \\
& + \left(\frac{27k^2 \tau'}{\tau^3} - 2\tau BD + 2\tau C' \right) Y^2 + \left(\frac{18k^2}{\tau} + 2\tau'B - 2\tau B' \right) XY - 9k\tau X \\
& + \left(2k' - \frac{8k\tau'}{\tau} \right) Y + \tau^2 B, \\
c_1 = & \frac{36k^3}{\tau^2} X^5 Y^2 - \frac{18k^2}{\tau^2} X^5 Y - \left(\frac{96k^3}{\tau^2} + \frac{6kD}{\tau} \right) X^3 Y^2 + \frac{6k\tau'}{\tau^2} X^4 Y + \frac{36k^2 \tau'}{\tau^2} X^2 Y^2 \\
& - 72k^2 XY^3 + \frac{36k^2}{\tau^2} X^3 Y + 6kX^3 - \frac{36k\tau'}{\tau^2} X^2 Y + \left(\frac{18kD}{\tau} + 36k - \frac{36k^3}{\tau^2} \right) XY^2 \\
& + \left(\frac{12k^2 \tau'}{\tau^2} - 2BD + 4C' \right) Y^2 - 2 \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2} \right) XY - 18kX \\
& - \frac{18k\tau'}{\tau^2} Y + 2\tau B, \\
c_0 = & -\frac{27k^3}{\tau^3} X^7 Y^2 + \left(\frac{63k^3}{\tau^3} + \frac{3k(\tau')^2}{\tau^3} \right) X^5 Y^2 + \frac{3kD^2}{\tau} X^3 Y^4 - \frac{6k\tau'D}{\tau^2} X^4 Y^3 \\
& - \frac{39k^2 \tau'}{\tau^3} X^4 Y^2 + \left(\frac{54k^2}{\tau} + \frac{12k^2 D}{\tau^2} \right) X^3 Y^3 + \frac{6k\tau'}{\tau} X^4 Y - D \left(\frac{9kD}{\tau} + 18k \right) XY^4 \\
& + \left(-\frac{3k}{\tau} \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2} \right) - 6kD - \frac{18k(\tau')^2}{\tau^3} - \frac{18k^3}{\tau^3} \right) X^3 Y^2 \\
& + \left(-\frac{3k}{\tau} (BD - 2C') + \frac{27k\tau'D}{\tau^2} + \frac{18k\tau'}{\tau} \right) X^2 Y^3 + D(BD - 2C')Y^4 - \frac{12k^2}{\tau} X^3 Y \\
& + \left(D \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2} \right) - \frac{\tau'}{\tau} (BD - 2C') - \frac{k}{\tau} \left(\frac{9kD}{\tau} + 18k \right) \right) XY^3 \\
& - \left(\frac{9k^2 \tau'}{\tau^3} + \frac{\tau'}{\tau} \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2} \right) \right) X^2 Y^2 + \left(3kB - \frac{27k\tau'}{\tau} \right) X^2 Y + 3k\tau X^3 \\
& + \left(\frac{9k\tau'D}{\tau^2} + \frac{k}{\tau} (BD - 2C') \right) Y^3 + \left(\frac{k}{\tau} \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2} \right) + 18kD + 18k\tau \right. \\
& \left. - \frac{9k(\tau')^2}{\tau^3} \right) XY^2 + \left(\frac{9k^2 \tau'}{\tau^3} - 2\tau(BD - C') \right) Y^2 + \left(\frac{36k^2}{\tau} + 2(\tau'B - \tau B') \right) \\
& \times XY - 9k\tau X - \left(2k' + \frac{10k\tau'}{\tau} \right) Y + \tau^2 B.
\end{aligned}$$

Before proving Theorem 1.1, for completeness, let us comment on the case that at least one of the coefficients b_i, c_i ($i = 0, 1, 2$) is zero.

Proposition 3.1. *If at least one of the coefficients b_i, c_i ($i = 0, 1, 2$) is zero in an open subset of $I \times J$, then the curvature of the generating curve β is zero, that is $k_\beta = 0$.*

Proof. Since the proofs are similar in all cases, we shall only consider the case $b_2 = 0$ in an open subset of $I \times J$. Inserting $Y^2 = 1 - X^2$ in the expression of b_2 we have

$$\begin{aligned} &\left(\frac{9k^2}{\tau^2}X^5 - \frac{3k\tau'}{\tau^2}X^4 - \frac{18k^2}{\tau^2}X^3 + \frac{18k\tau'}{\tau^2}X^2 + \left(2B' - \frac{B\tau'}{\tau} - \frac{27k^2}{\tau^2}\right)X \right. \\ &+ \left.\frac{9k\tau'}{\tau^2}\right)Y + \left(-\frac{3kD}{\tau}X^5 + \left(\frac{12kD}{\tau} + 15k\right)X^3 - (BD - 2C')X^2 \right. \\ &\left. - \left(\frac{9kD}{\tau} + 9k\right)X + BD - 2C' - \tau B\right) = 0. \end{aligned}$$

The last equation is of the form

$$P(X)Y + Q(X) = 0,$$

where P and Q are polynomials of one variable X and their coefficients are functions of s . The leading terms are $\frac{9k^2}{\tau^2}X^5$ and $-\frac{3kD}{\tau}X^5$, respectively. Squaring $P(X)Y = -Q(X)$ and inserting $Y^2 = 1 - X^2$, we obtain

$$P^2(X)(X^2 - 1) + Q^2(X) = 0, \tag{3.13}$$

a polynomial equation in X of degree 12 with leading coefficient $\frac{81k^4}{\tau^4} > 0$, since $k > 0$ and $\tau \neq 0$. Thus, the root $X = \cos \vartheta$ is a function $f(s)$ of s , and hence we have

$$\cos \vartheta = f(s). \tag{3.14}$$

Differentiating (3.14) with respect to t , we see that $\sin \vartheta \cdot \vartheta_t = 0$; consequently, in view of Lemma 3.1, we have $\vartheta_t = 0$. From the second relation of (2.9) we obtain $k_\beta = 0$. □

Now, we are ready to prove Theorem 1.1

Proof of Theorem 1.1. Using the expressions for b_i, c_i ($i = 0, 1, 2$) we calculate

$$\begin{aligned}
 b_2c_0 - b_0c_2 &= \\
 &= \left(\frac{9k^2}{\tau^2} X^5 Y + \frac{3kD}{\tau} X^3 Y^2 - \frac{3k\tau'}{\tau^2} X^4 Y - \frac{18k^2}{\tau^2} X^3 Y + \dots \right) \\
 &\quad \cdot \left(-\frac{27k^3}{\tau^3} X^7 Y^2 + \left(\frac{63k^3}{\tau^3} + \frac{3k(\tau')^2}{\tau^3} \right) X^5 Y^2 + \frac{3kD^2}{\tau} X^3 Y^4 - \frac{6k\tau'D}{\tau^2} X^4 Y^3 + \dots \right) \\
 &\quad - \left(-\frac{9k^2}{\tau^2} X^5 Y + \frac{3kD}{\tau} X^3 Y^2 - \frac{3k\tau'}{\tau^2} X^4 Y + \frac{30k^2}{\tau^2} X^3 Y + \dots \right) \\
 &\quad \cdot \left(\frac{27k^3}{\tau^3} X^7 Y^2 + \frac{18k^2 D}{\tau^2} X^5 Y^3 - \frac{18k^2 \tau'}{\tau^3} X^6 Y^2 + \left(-\frac{27k^3}{\tau^3} + \frac{3k(\tau')^2}{\tau^3} \right) X^5 Y^2 \right. \\
 &\quad \left. + \frac{3kD^2}{\tau} X^3 Y^4 - \frac{6k\tau'D}{\tau^2} X^4 Y^3 + \dots \right) = P_1(X, Y), \\
 b_2c_1 - b_1c_2 &= \\
 &= \left(\frac{9k^2}{\tau^2} X^5 Y + \dots \right) \left(\frac{36k^3}{\tau^2} X^5 Y^2 + \dots \right) - \left(-\frac{12k^2}{\tau} X^3 Y + \dots \right) \left(\frac{27k^3}{\tau^3} X^7 Y^2 + \dots \right) \\
 &= \frac{18 \cdot 36k^5}{\tau^4} X^{10} Y^3 + P_2(X, Y), \\
 b_1c_0 - b_0c_1 &= \\
 &= \left(-\frac{12k^2}{\tau} X^3 Y + \dots \right) \left(-\frac{27k^3}{\tau^3} X^7 Y^2 + \dots \right) \\
 &\quad - \left(-\frac{9k^2}{\tau^2} X^5 Y + \dots \right) \left(\frac{36k^3}{\tau^2} X^5 Y^2 + \dots \right) \\
 &= \frac{18 \cdot 36k^5}{\tau^4} X^{10} Y^3 + P_3(X, Y),
 \end{aligned} \tag{3.15}$$

where $P_i(X, Y)$ ($i = 1, 2, 3$) are polynomials of two variables X, Y and of total degree at most 12. The coefficients of $P_i(X, Y)$ are functions of s .

Consider the system

$$\begin{cases} b_2Z^2 + b_1Z + b_0 = 0 \\ c_2Z^2 + c_1Z + c_0 = 0 \end{cases} \tag{3.16}$$

of two polynomial equations of second degree with respect to Z .

If at least one of the coefficients b_i, c_i ($i = 0, 1, 2$) is zero in an open subset of $I \times J$, then, by Proposition 3.1, we have $k_\beta = 0$ and thus S is a circular cylinder.

In the sequel we assume that the coefficients b_i, c_i ($i = 0, 1, 2$) are non-zero almost everywhere on $I \times J$. System (3.16) possesses at least one solution at any point $(s, t) \in I \times J$. We distinguish two cases.

Case I The system has two solutions and thus the two equations coincide up to a multiplicative factor. Then, we must have

$$b_2c_0 - b_0c_2 = b_2c_1 - b_1c_2 = b_1c_0 - b_0c_1 = 0.$$

In particular, we have

$$b_2c_1 - b_1c_2 = \frac{18 \cdot 36k^5}{\tau^4} X^{10} Y^3 + P_2(X, Y) = 0.$$

Inserting $Y^2 = 1 - X^2$ and proceeding as in the proof of Proposition 3.1, we obtain an equation of the form

$$P(X)Y + Q(X) = 0,$$

where P and Q are polynomials of one variable X . The leading term of P is $-\frac{18 \cdot 36k^5}{\tau^4}X^{12}$ and the degree of Q is at most 12. Squaring $P(X)Y = -Q(X)$ and proceeding as before we conclude that $k_\beta = 0$; hence, S is a circular cylinder.

Case II System (3.16) has exactly one solution. Then, the resultant of the two equations of (3.16) must vanish, that is, we have

$$(b_2c_0 - b_0c_2)^2 - (b_1c_0 - b_0c_1)(b_2c_1 - b_1c_2) = 0. \tag{3.17}$$

Inserting (3.15) in (3.17), we get

$$-18^2 \cdot 36^2 \frac{k^{10}}{\tau^8} X^{20} Y^6 + Q_1(X, Y) = 0, \tag{3.18}$$

where $Q_1(X, Y)$ is a polynomial of two variables X, Y and of total degree at most 25. Inserting $Y^2 = 1 - X^2$ in (3.18), we obtain an equation of the form

$$P(X) + Q(X)Y = 0, \tag{3.19}$$

where P and Q are polynomials of one variable X . The leading term of P is $18^2 \cdot 36^2 \frac{k^{10}}{\tau^8} X^{26}$ and the degree of Q is at most 24. Squaring $P(X) = -Q(X)Y$ and inserting $Y^2 = 1 - X^2$ we obtain

$$P^2(X) + (X^2 - 1)Q^2(X) = 0, \tag{3.20}$$

a polynomial equation in X of degree 52, with leading coefficient $18^4 \cdot 36^4 \frac{k^{20}}{\tau^{16}} > 0$, since $k > 0$ and $\tau \neq 0$. All coefficients of this polynomial equation are functions of s . Continuing as in the proof of Proposition 3.1, we have $k_\beta = 0$ and thus S is a circular cylinder.

This completes the Proof of Theorem 1.1.

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Thomas Hasanis
Department of Mathematics
University of Ioannina
451 10 Ioannina
Greece
e-mail: thasanis@uoi.gr

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