# **Non-isothermal kinetic studies for binary TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system**

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A study of  $TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub>$  glass system has been carried out by Differential Thermal Analysis (DTA) to elucidate the kinetics of crystallization for these glassy samples. The results of DTA performed at different heating rates are discussed. The values of the glass transition temperature,  $T_{q}$ , as well as the glass crystallization temperature,  $T_{q}$ , are found to be dependent upon the heating rate. From this dependence, the values of activation energy for both the glass transition and crystallization are evaluated and discussed

### **1. Introduction**

The TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system has the ability to form glasses from 0 up to 100%  $TeO<sub>2</sub>$  content. This ability seems to be connected with chemical ordering in the liquid states [1], and the ability of TeO<sub>2</sub> and  $P_2O_5$  to form glasses on their own.

Many workers  $[2-6]$  have studied the different physical properties of oxide glasses, but little work has been done on the crystallization kinetics of these glasses.

Kinetic studies are mostly connected with the concept of activation energy. Two separate phenomena are associated with the glass crystallization, both of which need some kind of activation energy. These phenomena are the nucleation and growth processes that dominate the devitrification of most glassy solids. The nucleation and growth are separate steps in the transformation, although they have been combined into an activation energy representative of the overall crystallization process [7-9].

In the present work, the dependencies of the glass transition temperature,  $T_g$ , and the glass crystallization temperature,  $T_c$ , upon the composition and heating rate have been studied. From the heating rate dependence of  $T_g$  and  $T_g$ , the activation energy of the glass transition and the activation energy of crystallization have been evaluated.

Crystallization studies have been made under nonisothermal conditions with the samples heated at several uniform rates. Valuable information about the crystallization process has been obtained for the binary TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system using a recent analysis developed for non-isothermal crystallization studies.

# **2. Experimental procedure**

### 2.1. Glass preparation

For each binary  $TeO_2-P_2O_5$  glass system in the present study, the thermal history (i.e. melting temperature, melting time, annealing temperature and time, and all other preparation conditions were as similar as possible.

The binary  $TeO_2-P_2O_5$  glasses were prepared by melting appropriate mixtures of Analar phosphorus pentoxide  $P_2O_5$ , 99.99% purity, and Analar tellurium oxide TeO<sub>2</sub>, 99.99% purity, using open alumina crucibles heated in an electric furnace open to the atmosphere. The mixture was heated first at 300 °C for one hour and then transferred to a second furnace held at  $800^{\circ}$ C for 45 min. The glass melts were stirred occasionally with an alumina rod, to ensure homogeneous melts. The highly viscous melt was cast into a cylindrically shaped split-mould of mild steel. The produced glass was annealed at 300 °C in a second furnace for one hour. Finally, the furnace was switched off and the glass allowed to cool *in situ* for 24 h.

### 2.2. Differential Thermal Analysis (DTA)

The characteristic of the prepared glasses (such as the transition temperature,  $T_{\text{g}}$ , melting temperature,  $T_{\text{m}}$ , chemical transformations, etc.) were studied using the Shimadzu Differential Thermal Analysis system. This is a'sensitive instrument for the ready evaluation of thermal behaviour over the temperature range of ambient to 1575 K. When the sample and reference substance are heated at a constant rate, their temperatures rises. The temperature of the reference substance, which is thermally inactive, rises uniformly, while the temperature of the sample stops rising when an endothermic reaction (e.g. fusion) occurs, because the heat supplied from outside is consumed by the reaction. When the reaction is over, the sample temperature is very much less than ambient. Initially, its temperature rises rapidly, then more uniformly. The temperature difference  $\Delta T$  is detected, amplified and recorded, as a peak. The temperature in the sample holder is measured by a thermocouple, the signal of which is compensated for the ambient temperature and fed to the temperature controller. This signal is compared with program signal and the voltage applied to the furnace is adjusted. Thus the sample and reference substance are heated or cooled at the desired rate.

#### **3. Results** and discussion

A small amount of powdered sample ( $\sim$  0.1 g) and a thermally inert standard sample of  $\gamma$ -alumina were placed in the furnace. Fig. 1 shows typical DTA traces for the TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass samples with different TeO<sub>2</sub> content heated at different heating rates. It is evident from the figure that at the glass transition temperature,  $T_{\rm g}$ , there is a drop in output due to the change in the heat capacity and also an increase in the specific heat of the glass samples. Before and after  $T_{g}$ , the structure remains unchanged, softening of the originally hard material only occurring at  $T_g$ . On further heating the DTA curves show an exothermic peak representing devitrification. This temperature corresponds to a change in the glassy material to a crystalline structure. Since the glass structure exhibits higher energy state than the corresponding crystal phase, this is indicated by the evolution of heat. On further heating, a drop in the output (an endothermic peak) is observed. In this region the crystal absorbs the latent heat on changing to the liquid state.

The glass transition temperature, or the softening temperature,  $T_{g}$ , as well as the crystallization temperature,  $T_c$ , which have been obtained using the DTA charts of Fig. 1 are tabulated in Tables I and II. It was noted that both  $T<sub>g</sub>$  and  $T<sub>c</sub>$  are increased with increasing  $TeO<sub>2</sub>$  content at different heating rates. The glass transition temperature,  $T_g$ , plotted in Fig. 2 is found to vary linearly with TeO<sub>2</sub> content. The changes in  $T_g$ with  $TeO<sub>2</sub>$  are due to the closeness of the network structure of these glasses and correspond to the increase in density [2]. Also, the increase of  $T<sub>g</sub>$  with TeO<sub>2</sub> may be due to the fact that, as  $TeO<sub>2</sub>$  increases, the fraction of phosphorus atoms participating in terminal charged  $PO_4$  units increases and therefore the chains become shorter. Also, with increasing  $TeO<sub>2</sub>$ mole %, the ratio of tellurite to phosphate increases and therefore the crosslink density increases. Both the increase in the fraction of shorter, stiffer chains and the increase in strong ionic crosslinks serve to increase

TABLE I Composition,  $T_{\epsilon}$ , density and number of bonds per unit volume for binary TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system

Glass type	TeO, $(mole \%)$ chemically analysed	$T_{\rm g}$ $(^{\circ}C)$	Density $(g cm^{-3})$	$n_{\rm b}\times 10^{-22}$
Pure $P_2O_5$		290	2.52	6.42
$T_{1}$	28.18	312	3.13	6.89
$T_{2}$	32.38	314	3.17	6.92
$T_3$	36.15	317	3.30	7.08
$\rm T_4$	40.16	319	3.34	7.01
$T_{5}$	45.72	322	3.47	7.14
$T_{6}$	52.55	327	3.65	7.19
т,	59.42	333	3.80	7.22
$\rm T_s$ .	62.80	336	3.91	7.30
T,	64.28	337	3.95	7.32
$T_{10}$	68.40	340	4.06	7.36
$T_{11}$	73.51	346	4.34	7.65
$T_{12}$	76.49	350	4.47	7.78
$T_{13}$	81.09	355	4.82	8.14
Pure TeO <sub>2</sub>	98.40	320	5.13	7.74



*Figure 1* Typical DTA traces of TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system recorded at different heating rates.

TABLE II Glass transition temperatures,  $T_{\text{ex}}$ , and crystallization temperatures,  $T_{\text{ex}}$ , recorded at different heating rates for TeO<sub>2</sub>-P<sub>2</sub>O<sub>s</sub> glass system

Glass type	Glass transition temperature, $T_{\rm g}$ , recorded at different heating rates							
	$5^{\circ}$ C min <sup>-1</sup>	$10^{\circ}$ C min <sup>-1</sup>	$15^{\circ}$ C min <sup>-1</sup>	$20^{\circ}$ C min <sup>-1</sup>	$25^{\circ}$ C min <sup>-1</sup>	$30^{\circ}$ C min <sup>-1</sup>	$50^{\circ}$ C min <sup>-1</sup>	
$\mathbf{T}_1$	305	309	312	314	316	318	322	
$T_{3}$	307	313	317	320	323	325	332	
$T_5$	309	317	322	325	329	332	340	
$T_6$	311	321	327	331	335	338	346	
$T_{s}$	314	326	333	338	342	345	356	
$\rm T_{10}$	316	330	340	346	350	355	367	
$T_{12}$	320	340	350	360	365	370	385	





*Figure 2* Glass transition temperature as a function of  $TeO<sub>2</sub>$  content for  $TeO_2-P_2O_5$  glass system.

the transition temperature of the  $TeO_2-P_2O_5$  glass system with increasing  $TeO<sub>2</sub>$  content.

The glass transition temperature can be taken as a measure of the onset of diffusion motion and thus it corresponds to the fixed value of viscosity (or of reciprocal fluidity). In such a case, the  $T_{\rm g}$  can be connected with

(i) the average number of bonds per atom  $(N)$  which must be broken to obtain fluidity;

(ii) the bond strength, which can be related to the optical gap.

Based on this idea, attempts are made to calculate the number of bonds per unit volume  $(n<sub>b</sub>)$  for each glass sample using the following expression:

$$
n_{\rm b} = n_{\rm f} N_{\rm A} \rho / M_{\rm g} \tag{1}
$$

where  $n_f$  is the co-ordination number,  $N_A$  is Avogadro's number,  $\rho$  is density and  $M_{\rm g}$  is the molecular mass of the glass sample, which is given by

$$
M_{\rm g} = xM_1 + (1 - x) M_2 \tag{2}
$$

where  $M_1$  and  $M_2$  are the atomic masses, and x and  $1-x$  the fractional atomic concentrations, of the oxides used. The calculated number of bonds per unit volume using the above equations are presented in Table I. From Table I it was found that the number of bonds per unit volume increases with increasing  $TeO<sub>2</sub>$ content and thus the average crosslink density also increases leading to compactness of this binary glass system, confirming the increase in density and  $T_{g}$  for the same glass system.

Since  $T_c$  depends upon the heating rate, crystallization must be a kinetic rather than an equilibrium thermodynamic process for the glasses. Thermodynamically, the metastable condition of glass differs from the stable condition of the crystal by virtue of its higher free energy. The transition (vitreous-crystalline) takes place via two kinds of reaction: nucleation and crystal growth. The first is an endothermic process, while the latter is exothermic. As early as 1993, Tammann [10] established that these processes are based on different rate-controlling mechanisms.

It must be added that according to the Tammann interpretation of devitrification at a constant temperature below  $T_m$ , nuclei can be formed at a constant rate. Tuszyhski [11], on the other hand, explains the phenomenon of crystallization in glasses in such a manner that an endless number of nuclei of the phase to be formed can be assumed. The maximum crystal nucleation occurs either next to or just. above  $T_{\rm g}$ . This can be theoretically substantiated by the impediment of nucleation as a result of elastic deformation below  $T_g$  [12], as well as on an atomistic basis in terms of resonance of thermal vibrations at the point of conversion  $T_{g}$  or in its immediate vicinity (up to about 15 degrees above  $T<sub>g</sub>$ ).

Three approaches are used to discuss the dependence of  $T<sub>e</sub>$  and  $T<sub>e</sub>$  on the heating rate  $\alpha$ . One of them is the empirical relationship

$$
T_g = A + B \log \alpha \tag{3}
$$

where  $A$  and  $B$  are constants for a given glass composition [13]. Fig. 3 shows the variation of  $T_g$  as a function of log  $\alpha$  and indicates the validity of this relationship for the present glass system.

The second approach is the so-called Kissinger formula [14] for the evaluation of the activation energy of the glass transition. It has been shown [15, 16] that the dependence of  $T_c$  upon  $\alpha$  is given by

$$
\log (T_c^2/\alpha) + \text{constant} = E/(RT_c) \tag{4}
$$

where  $E$  is the effective activation energy and  $R$  is the universal gas constant. It was found that this expression is valid for the glass transition [17] and has been used to calculate values of the glass transition activation energy  $\lceil 15-18 \rceil$ . Kissinger assumed that the temperature of maximum deflection in DTA is also the temperature at which the reaction rate is maximal. Plots of both log  $(T_e^2/\alpha)$  versus  $1/(T_e)$  and  $(T_e^2/\alpha)$ versus  $1(T_c)$  for these glasses are shown in Figs 4 and 5, respectively; these indicate linearity with heating rate and yield values for the glass transition activation energy and the activation energy of crystallization. The glass transition activation energy was found to decrease with increasing  $TeO<sub>2</sub>$  content, from 345 kJ mol<sup>-1</sup> to 104 kJ mol<sup>-1</sup>. When the TeO<sub>2</sub> content increased from 28.18 to 76.49 mole %. The activation energy of crystallization was found to be higher than the activation energy of glass transition and



*Figure 3* Glass transition temperature as a function of heating rate,  $\alpha$ , for TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system.

shows anomalous behaviour with  $TeO<sub>2</sub>$  content. The third approach uses the Ozawa relationship [19] which is based on the shift in the peaks as the heating rate is changed, as indicated from the following equation:

$$
\log \alpha = E/4.57 \times 1/T_{\rm g} + \text{constant} \tag{5}
$$

Plotting log  $\alpha$  versus  $1/T_g$  and  $1/T_g$  gives straight lines (see Figs 6 and 7), the gradients of which give values for the glass transition activation energy and the activation energy of crystallization. By inspection of Figs 4-7, one can see that the glass transition



*Figure 4* Log  $(T_a^2/\alpha)$  versus 1000/T<sub>g</sub> obtained from DTA traces for Te $O_2-P_2O_5$  glass system.



*Figure 5* Log  $(T_c^2/\alpha)$  versus 1000/ $T_c$  obtained from DTA traces for  $TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub>$  glass system.



*Figure 6* Log  $\alpha$  versus 1000/T<sub>g</sub> obtained from DTA traces for  $TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub>$  glass system.



*Figure 7* Log  $\alpha$  versus 1000/T<sub>c</sub> obtained from DTA traces for Te $O_2-P_2O_5$  glass system.

activation energy and the activation energy of crystallization (which are summarized in Table III) calculated by the Kissinger and Ozawa relationships are in agreement.

# **4. Conclusion**

The general trend for the  $P_2O_5$ -TeO<sub>2</sub> glass system is that both the glass transition temperature and the glass crystallization temperature  $T_c$  increase with in-

TABLE III Glass transition activation energy,  $E<sub>e</sub>$ , and crystallization activation energy,  $E_c$ , calculated using Kissinger and Ozawa methods for TeO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass system

Glass type	Glass activation energies, kJ/mol						
		Kissinger method	Ozawa method				
	$E_{\rm g}$	E.	$E_{\varepsilon}$	$E_c$			
$T_{1}$	82.40	113.84	86.14	121.65			
$T_3$	58.36		65.44				
$T_5$	48.90	84.04	51.28	91.13			
$T_{6}$	46.30		48.76				
$T_{\rm R}$	38.60	114.71	42.41	122.93			
$T_{10}$	31.10		32.81				
$T_{12}$	24.76	77.00	27.28	78.42			

creasing  $TeO<sub>2</sub>$  content. It seems that as the heating rate,  $\alpha$ , increases, the glass transition temperature and the activation energy of crystallization shift to higher temperatures for all compositions. Also, we noted that as  $\alpha$  increased, the area under the crystallization and melting peaks of the DTA traces increased. Smaller areas mean that only small amounts of the sample material have been crystallized and may be increased at higher heating rates. The activation energies calculated by either the Kissinger or Ozawa methods are in good agreement and their values decrease with increasing  $TeO<sub>2</sub>$  content.

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