

# Design of Novel Radial Folded Microstrip Patch Antenna for WiMAX Application



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**Abstract** In recent years, the study of microstrip patch antennas (MPA) has made great progress because of its advantages in terms of weight, volume, cost, fabrication, and dimension. This paper presents a novel radial folded microstrip patch antenna, which operates at 3.55 GHz frequency. The microstrip design composed radial folded resonator with partial ground plane. The folded structure is used in order to achieve the compactness, and partial ground is used to suppress the high order harmonic. The proposed antenna shows mono narrowband behavior with the  $-10$  dB bandwidth of 480 MHz (3.3–3.78 GHz), which is one of the 5G bands used for Worldwide Interoperability for Microwave Access (WiMAX) application. The obtained results through simulation depict return loss below  $-30$  dB, VSWR below 0.6, and peak gain of 5.1 dB at operating frequency of 3.55 GHz. These results are obtained through HFSS software.

**Keywords** Microstrip antenna · Radial folded resonator · WiMAX

## 1 Introduction

The rapid development in mobile communication and emergence of newer technologies require design of antenna with smaller size, higher gain, lower power loss, high

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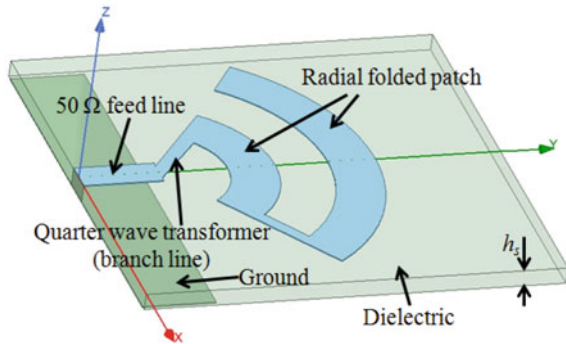
bandwidth, and higher data speed. In order to reach tradeoffs amid these requirements, several antenna configurations are developed [1–3]. The advent of integrated devices in modern communication system popularizes microstrip patch antenna due to its properties like light weight, integration compatibility with passive and active devices, low volume, low cost, and easier fabrication. The microstrip patch antenna includes a metallic radiating patch at the top of dielectric substrate with metallic ground on the bottom of the substrate.

The antenna is vital element in wireless system used to transmit and receive the electromagnetic signals through the air media. Nowadays, its use is not limited to only human communication but is used in variety of applications like microwave imaging [4], e-health [5], satellite communication, IoT (Internet of things), radar, military, cognitive radio, energy harvesting, and so on. The individual applications need the antenna performance as per their requirement. Many researches had been already done in the designing of antenna, and many more are going on due to regular escalation in technology with improved performance and addition of newer technologies within the same volume of the equipment, as one can easily see from 1 to 5G wireless communication. In order to achieve these, a variety of antenna designs with numerous radiations patterns and performance parameters had presented [6]. Numerous patch shapes are also researched to realize miniaturized antenna structure, enhanced bandwidth, multiband operations such as Z-shape [4], Koch Fractal [7], T-shape [8], U-shape [9], spline shape [10], and so on.

There are different methods proposed in literature for wideband and narrow-band performance. As specific frequency bands are allotted for different applications like for wireless local area network (WLAN), WiMAX, wireless fidelity (Wi-Fi), Global Positioning System (GPS) etc. So, these systems need multi or mono narrow-band antennas, and for easier portability microstrip technology is best choice due to its light weight and easier integration capability. In past, many application-specific mono-band antennas are presented like E-shaped microstrip antenna [11] for WLAN (5–6 GHz) application, metamaterial-based antenna with bowtie stub for WLAN (2.45 GHz) [12], Coplanar waveguide-fed antenna for WiMAX (5.5 GHz) application [13], microstrip rectangular patch antenna [14] with defected ground structure comprise of array of complementary split ring slots in ground plane for WiMAX (2.6 GHz), fractal patch antenna with partial ground [15] for WiMAX (3.5 GHz) application.

This paper illustrates a narrowband microstrip patch antenna (MPA) with partial ground plane for WiMAX application at 3.55 GHz. The microstrip line fed is used with quarter wave transformer for impedance matching. The novelty of the work is in terms of patch configuration which shows compactness due to radial folded configuration and its narrowband performance. HFSS software is used for all the simulations in this work. The achieved bandwidth, VSWR, and realized gain show its suitability for WiMAX.

**Fig. 1** Three-dimensional view of the proposed radial folded patch antenna



## 2 Antenna Design Methodology and Configuration

Initially, the dielectric substrate with a particular height and dielectric constant and the desired operating frequency are chosen or known in the typical antenna design procedure. The designed antenna is radial folded microstrip patch. The overall volume of the antenna geometry is  $W_s \times L_s \times h_s$ , i.e.,  $40 \times 40 \times 1.6 \text{ mm}^3$ ; however, the overall dimension of the radiating patch is only  $W_g \times L_p$ , i.e.,  $39 \times 29 \text{ mm}^2$ . The proposed antenna system has been simulated on FR4 glass-reinforced epoxy laminate material with relative permittivity, dielectric loss tangent, and height of 4.4, 0.02, and 1.6 mm, respectively. For effective radiation from the antenna, impedance matching must be ensured by the designer in between the radiating patch and feed line for maximum power transfer from the input to the patch and less reflection. Here, a branch line of quarter wavelength is used for the matching purpose. The width of the branch line can be calculated easily after the evaluation of its characteristic impedance ( $Z_{\lambda/4}$ ), which can be determined by using (1).

$$Z_{\lambda/4} = \sqrt{Z_o Z_e} \tag{1}$$

Here,  $Z_o$  is characteristic impedance of main feed line ( $50 \Omega$ ) and  $Z_e$  is input impedance at patch edge. The three-dimensional view of the designed antenna is illustrated in Fig. 1. Figure 2 depicts the top and bottom view of the design with dimensional variables. The optimized dimensional parameters are specified in Table 1.

## 3 Results

The mono and narrowband antenna presented in this paper use partial ground plane and radiating element as radial folded patch. The simulated results demonstrate the applicability of the proposed antenna for WiMAX band at 3.55 GHz. The operating

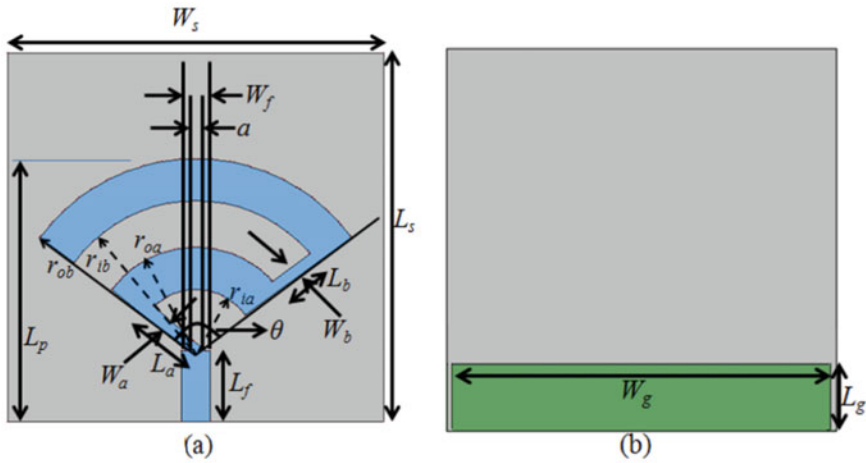


Fig. 2 Two-dimensional view (a) radiating patch at top and (b) partial ground at bottom

Table 1 Antenna design variables

Variables	Dimension
$W_s$	40 mm
$L_s$	40 mm
$W_g$	39 mm
$L_g$	7 mm
$W_f$	3 mm
$L_f$	7.6 mm
$A$	2 mm
$W_a$	1.3 mm
$L_a$	6.5 mm
$r_{ia}$	6.5 mm
$r_{oa}$	11 mm
$W_b$	1.3 mm
$L_b$	5 mm
$r_{ib}$	16 mm
$r_{ob}$	20.5 mm
$L_p$	29 mm
$\Theta$	108°

frequency and bandwidth of the antenna are achieved by optimizing the dimensional parameters shown in Table 1. The partial ground concept is utilized in the design to excite the higher mode and enhance the return loss. The effect of the partial ground plane can be easily demonstrated by analyzing the return loss (S11) plot in Fig. 3.

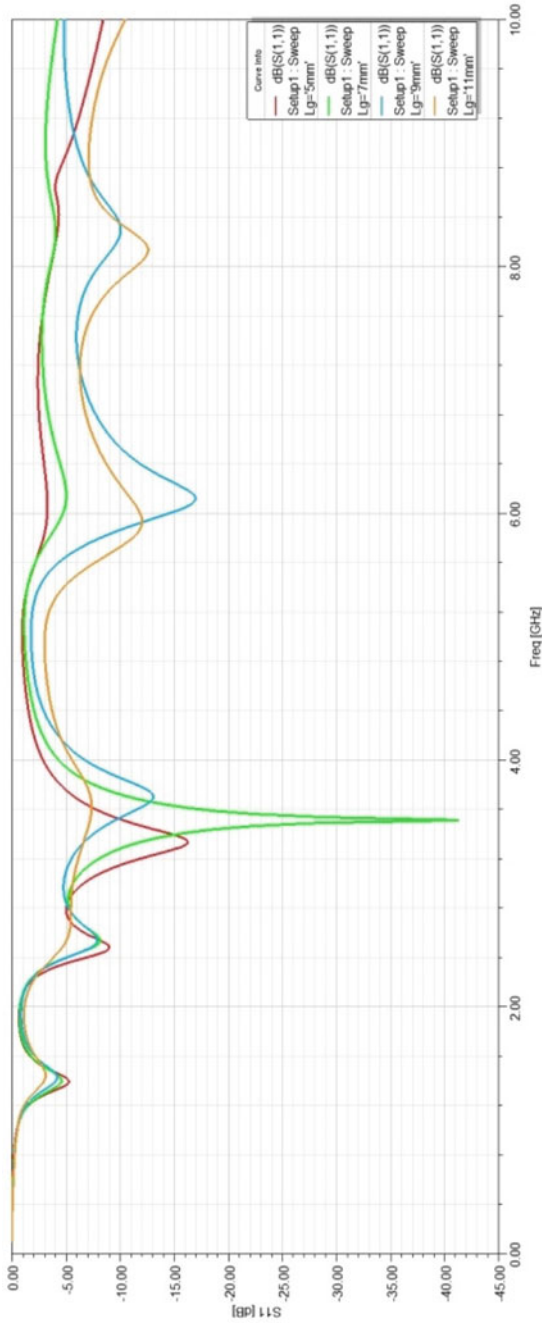


Fig. 3 Simulated return loss (S11) of designed antenna with variation in length of ground conductor ( $L_g$ )

The return loss of the final structure with  $L_g = 7$  mm, is illustrated in Fig. 4. The designed antenna resonates at 3.55 GHz and shows  $-10$  dB bandwidth of 480 MHz (3.3–3.78 GHz) i.e. 14%. The simulated S-parameter illustrates a return loss at the operating frequency well below  $-30$  dB.

In Fig. 5 VSWR plot is shown, which demonstrates the VSWR level within 6 dB for 3.3–3.78 GHz frequency range; however, the VSWR at 3.55 GHz is below 0.6 dB. Figure 6 illustrates the polar plot of radiation pattern at the resonant frequency 3.55 GHz for 0 and 90 phi angle. The 3-D radiation plot for total gain at 3.3, 3.55 and 3.7 GHz are depicted in Fig. 7, which show peak gain of 5.6, 5.1 and 4.7 dB, respectively. This demonstrates the applicability of the antenna over the bandwidth.

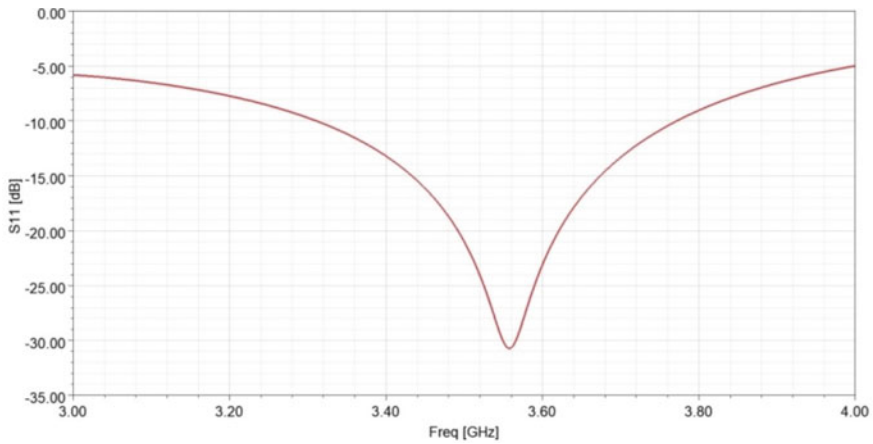


Fig. 4 Simulated S11 plot for proposed antenna configuration ( $L_g = 7$  mm)

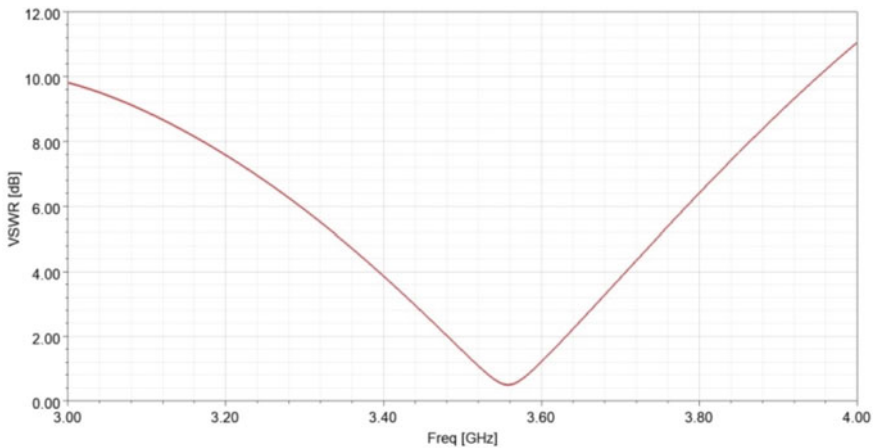


Fig. 5 The simulated VSWR plot of the proposed antenna

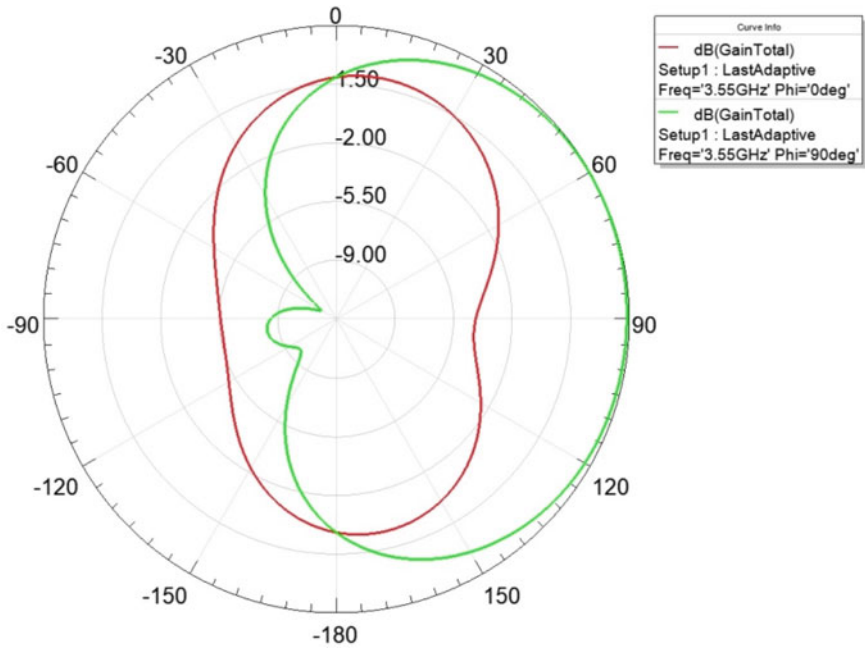


Fig. 6 Polar plot for radiation pattern at 3.55 GHz for  $\phi = 0^\circ$  and  $90^\circ$

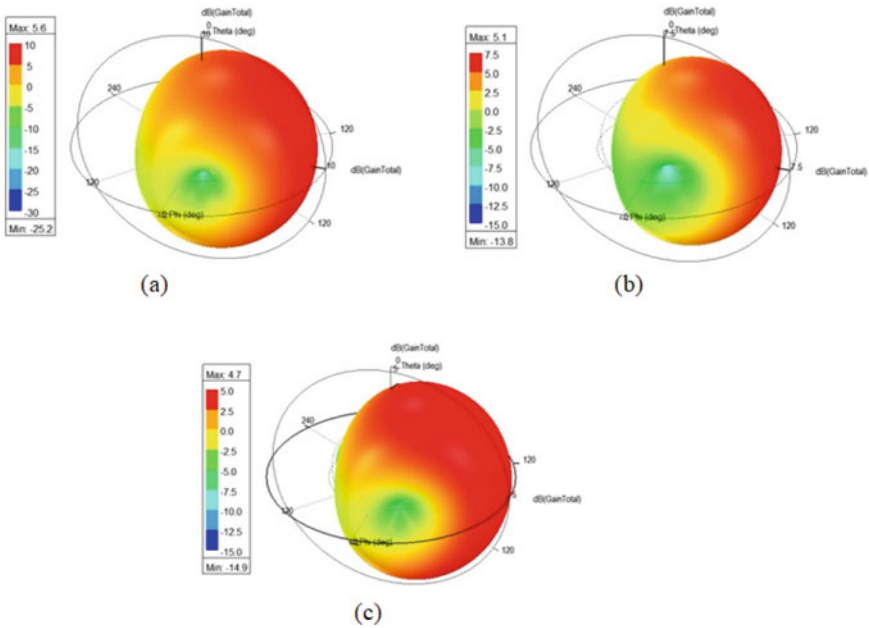


Fig. 7 3-D plot of total gain a at 3.3 GHz, b at 3.55 GHz and c at 3.7 GHz

## 4 Conclusion

In this work, a novel radial folded MPA has been presented. The design of radial folded MPA is done by using HFSS simulator. A radial folded MPA is simulated and it provides 3.55 GHz resonating frequency which is used for WiMAX applications. The folding of the resonator is done in order to achieve miniaturization. The Radial folded MPA gives a gain of 5.1 dB for 3.55 GHz. The VSWR at operating frequency is below 0.6 dB and the  $-10$  dB bandwidth is 480 MHz (3.3–3.78 GHz). This proposed antenna depicts appreciable gain, bandwidth and return loss, which makes the antenna suitable for WiMAX applications.

## References

1. Jacobs IS (1963) Fine particles, thin films and exchange anisotropy. *Magnetism* 1963:271–350
2. Maxwell JC (1873) *A treatise on electricity and magnetism*. Clarendon press
3. Outerelo DA, Alejos AV, Sanchez MG, Isasa MV (2015) Microstrip antenna for 5G broadband communications: Overview of design issues. In: 2015 IEEE international symposium on antennas and propagation and USNC/URSI national radio science meeting. IEEE pp 2443–2444
4. Ullah S, Ruan C, Sadiq MS, Haq TU, He W (2020) High efficient and ultra wide band monopole antenna for microwave imaging and communication applications. *Sensors* 20:115
5. Nafis F, Yahyaouy A, Aghoutane B (2019) Ontologies for the classification of cultural heritage data. In: 2019 international conference on wireless technologies, embedded and intelligent systems (WITS). IEEE, pp 1–7
6. Balanis CA (2016) *Antenna theory: analysis and design*, p 318
7. Tripathi S, Mohan A, Yadav S (2014) Hexagonal fractal ultra-wideband antenna using Koch geometry with bandwidth enhancement. *IET Microwaves Antennas Propag* 8:1445–1450
8. Paga P, Nagaraj HC, Rukmini TS, Nithin NE (2015) Design and fabrication of a microstrip printed T monopole antenna for ISM application. In: 2015 International conference on microwave, optical and communication engineering (ICMOCE). IEEE, pp 264–267
9. Tiwari RN, Singh P, Kanaujia BK (2020) Asymmetric U-shaped printed monopole antenna embedded with T-shaped strip for bluetooth. *WLAN/WiMAX appl Wirel Netw* 26:51–61
10. Lizzi L, Azaro R, Oliveri G, Massa A (2011) Printed UWB antenna operating over multiple mobile wireless standards. *IEEE Antennas Wirel Propag Lett* 10:1429–1432
11. Logan B, Healey J (2005) Robust detection of atrial fibrillation for a long term telemonitoring system. In: *Computers in cardiology*. IEEE, pp 619–622
12. Mulchandani JD, Gupta D, Sharma SK, Mishra N, Chaudhary RK (2016) Narrow-band electrically small metamaterial-inspired antenna with bowtie-shaped stub for WLAN. In: 2016 11th International conference on industrial and information systems (ICIIS). IEEE, pp 32–36
13. Sahitya V, Kumar SA, Shanmuganatham T (2019) Design of CPW fed antenna for WiMAX applications. In: 2019 TEQIP III sponsored international conference on microwave integrated circuits, photonics and wireless networks (IMICPW). IEEE, pp 95–97
14. Ajay VG, Parvathy AR, Mathew T (2019) Microstrip antenna with DGS based on CSRR array for WiMAX applications. *Int J Electr Comput Eng* 9:157
15. Sanap K, Labade RP (2020) Fractal patch antenna with exalted bandwidth and harmonic suppression for WiMAX applications. In: ICCCE 2019. Springer pp 143–149