

# Experimental Investigation of Unmodified Diesel Engine on Performance, Combustion and Emission with Various Proportions of Jatropha Biofuel in Diesel



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## Nomenclature

ASTM	American Society for Testing Materials
CI	Compression ignition
CO	Carbon monoxide
HC	Hydrocarbon
CO <sub>2</sub>	Carbon dioxide
NO <sub>x</sub>	Oxides of nitrogen
HRR	Heat release rate
J20	20% transesterified Jatropha oil and 80% diesel in volume
J40	40% transesterified Jatropha oil and 60% diesel in volume
J60	60% transesterified Jatropha oil and 40% diesel in volume
J80	80% transesterified Jatropha oil and 20% diesel in volume
J100	100% volume of transesterified Jatropha oil in volume

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## 1 Introduction

The compression ignition engine is used for an extensive range of applications in the transportation division, and it also has applications in agricultural and power generation sectors due to its higher thermal efficiency. But due to fossil fuel depletion, researchers all over the world are impelled to develop an alternative fuel source that has comparable properties with diesel oil. Biogas, vegetable oils and methanol have been considered as alternative fuels for diesel. The previous experimental studies suggested that esterified vegetable oil has been recognized as the best alternative for diesel [1–3]. It also has a higher cetane number, calorific value and latent heat of vaporization compared with diesel. Table 1 shows the various vegetable oil biodiesel fuels whose chemical properties are closer to those of diesel. The availability, plantation and extraction of oil from seeds or crops do not pose a problem. The vegetable oils have the advantage of being biodegradable, non-toxic and pollution-free. The oils extracted from seeds or plants can simply be transesterified to produce biodiesel. Pure vegetable oil also has the potential to run a diesel engine restricted to lower viscosity [4, 5].

For better combustion and performance, the viscosity of vegetable oil is decreased by the transesterification process. During this process, the viscosity of the biodiesel gets reduced and turns equivalent to diesel [10–14]. The effect of viscosity will influence combustion, performance and emissions through fuel droplets, vaporization and atomization. Some researchers have reported that preheated oils also lead to better performance and emission characteristics [15–19]. It has been observed that preheating gives better emissions of HC, CO and particulate matter emissions due to the reduction of viscosity. It has also been noted that for higher compression ratios, biodiesel improves performance. In recent years, biodiesel has achieved significant consideration as an alternative renewable fuel. Biodiesel has several advantages over other petroleum products. Recent researches have shown that exhaust gases have less

**Table 1** Property of various biodiesels

Property	Diesel	Cottonseed biodiesel	Jatropha biodiesel	Neem biodiesel	Palm biodiesel	Soybean biodiesel	Sunflower biodiesel
Calorific value (MJ/kg)	41–45.9	40.32	42	40.1	40.39	39.76	40.56
Cetane number	45–55	51.2	46–70	51	50–65	40–53	49–52
Kinematic viscosity at 40 °C (cSt)	2.5–5.7	4	3.7–5.8	7.2	4.5	4.08	4.5
Relative density	0.82–0.867	0.874	0.878–0.885	0.87	0.87	0.885	0.878
References	[1]	[6]	[1]	[7]	[8]	[8]	[9]

unburned hydrocarbon, particulate matter, carbon monoxide and sulfur levels while using biodiesel as a fuel. But the oxides of nitrogen have increased. Nowadays, to reduce smoke and  $\text{NO}_x$  with improved performance, considerable research is going on with water emulsion fuel, EGR and SCR.

Priyabrata Pradhan [20] investigated on the impact of Jatropha on the performance, emission and combustion on CI engine and reported that Jatropha biodiesel had a marginal decrease in brake thermal efficiency compared with mineral diesel, and it also had a reduction in  $\text{CO}_2$ , HC and  $\text{NO}_x$  and increased in CO emissions. Anand et al. [21] investigated the Jatropha biodiesel for injection pressure that ranges from 200 bar and 250 bar on diesel engine.

It was reported that there was a negligible decrease in BTE and a rise in emissions of emissions for Jatropha blends. Higher density, viscosity and molecular weight make it challenging to atomize the biodiesel at low temperatures and the low loads, causing more CO emissions. A significant cause for the lower CO emissions at high loads from the combustion of biodiesel is the inbuilt oxygen content, which makes the burning of biodiesel more complete when the engine works at higher loads.

Nabi et al. [22] investigated the influence of cottonseed oil on single-cylinder water-cooled, four-stroke, DI diesel engines. It was noted that preferred biodiesel resulted in lower CO, particulate matter, smoke and higher  $\text{NO}_x$  emissions than diesel at all load conditions. At full load condition, it also resulted, in B10, in lower smoke emission and particulate matter by 14 and 24% to mineral diesel. Blend B30 showed that the CO emissions decreased by 24% and increased  $\text{NO}_x$  emissions of 10%, and it was owing to the existence of oxygen in their molecular structure. Cottonseed blend has slightly lower thermal efficiency than mineral diesel due to its more moderate calorific content. However, higher density, higher volatility and higher viscosity might be the reasons for its reduction in its efficiency. Table 2 shows the study of various biodiesel fuels and their performance, emission and combustion characteristics.

From Table 1, it can be observed that properties such as calorific value, cetane number, kinematic viscosity and relative density of Jatropha oil are highly relative to mineral diesel compared to other biofuels. So these properties will influence in better performance, combustion and emission characteristics of Jatropha diesel blend used as fuel in the CI engine. The government of India launched the biofuel mission in 2003 to develop the Jatropha biodiesel industry. The planning commission reported that 13.4 million hectares of land available for Jatropha plantation [31]. Jatropha is an off-seasonal crop. So it can be cultivated at a slack agricultural season.

From the literature analysis, it can be perceived that only very limited researches have investigated in the field of Jatropha biodiesel with preheating of oil using the engine exhaust. In the current investigation, raw Jatropha oil was transformed into biodiesel using the transesterification process and converted into the fuel of various proportions on a volume basis. And during its operation in the engine, it was preheated with the engine exhaust for the betterment of engine behavior. The chemical and the physical properties of the fuel models have been analyzed on ASTM biodiesel standards. The objective of the present investigation was to determine the extent to which biodiesel blending could improve the combustion and emission characteristics

**Table 2** Effect of biodiesel usage in diesel engine

Investigator	Biodiesel type	Engine type	Test conditions	Engine characteristics								
				Performance		Combustion		Emission				
				BTE	BSFC	HRR	ICP	CO	HC	NO <sub>x</sub>		
Tarbet et al. [23]	Eucalyptus oil	Single cylinder, four stroke, direct ignition, CR:18:1, 4.5 kW power	Varying load at 1500 RPM	↓	↑	↓	↑	↓	↑	↑	↑	↓
Rehman et al. [1]	Jatropha oil	Single cylinder, four stroke, direct ignition, CR:17.5, RP:7.4 kW	Varying load at 1500 RPM	↓	↑	-	-	-	-	↑	↑	↑
Gogoi et al. [24]	Korach seed oil methyl ester (KSOME)	Single cylinder, four stroke, direct ignition, CR:12-18, RP:3.5 kW	Varying load at 1500 RPM	↓	↑	↓	↓	-	↓	-	-	-
Lenin et al. [25]	Mahua oil methyl ester	Single cylinder, four stroke, direct ignition, CR:17.5, RP:5.2 kW	Varying load at 1500 RPM	↓	↑	↓	↓	↓	↓	↑	↓	↑
Agarwal et al. [26]	Karanja oil	Single cylinder, four stroke, direct ignition, CR:17.5, RP:7.4 kW	Varying load at 1500 RPM	↓	↑	↓	↓	↓	↓	↓	↓	↑
Nithyananda et al. [27]	Neem and mixed Pongamia coconut methyl esters	Single cylinder, four stroke, direct ignition, CR:16.5:1, RP:3.75 kW	Varying load at 1500 RPM	↓	↑	-	-	-	-	-	-	-

(continued)

**Table 2** (continued)

Investigator	Biodiesel type	Engine type	Test conditions	Engine characteristics								
				Performance		Combustion		Emission				
				BTE	BSFC	HRR	ICP	CO	HC	NO <sub>x</sub>		
Anand et al. [21]	Turpentine oil	Single cylinder, four stroke, direct ignition, CR:17.5, RP:5.2 kW	Varying load at 1500 RPM	↓	↑	↓	↓	↓	↓	↓	↓	↓
Sajid et al. [28]	Mustard Biodiesel (MB)	Four cylinders, four stroke, direct ignition, CR: 21:1	Varying load at 1500 RPM	↓	↑	-	-	↓	↓	↓	↑	↑
Nalgundwar et al. [29]	Palm and Jatropa	Single cylinder, four stroke, direct ignition, CR:17.5, RP:5.2 kW	Varying load at 1500 RPM	↑	↑	-	-	↓	↓	↓	↑	↑
Kakati and Gogoi [30]	Kultura fruit seed oil	Single cylinder, four stroke, direct ignition, CR:18:1, RP:3.5 kW	Varying load at 1500 RPM	↑	↓	-	-	↓	↓	↓	↑	↑

↑—increase/high; ↓—decrease/low; CR—compression ratio; DI—direct ignition; RP—rated power; rpm—revolution per minute

without sacrificing its performance in an unmodified diesel engine. For that purpose, the experiment was conducted with a biodiesel blend in an unmodified diesel engine at all load conditions. The performance characteristics such as BTE, BSFC and emission characteristics such as  $\text{CO}_2$ , CO, HC,  $\text{NO}_x$  and smoke opacity were measured for *Jatropha* biodiesel and compared with mineral diesel. The combustion features such as rate of heat release and peak in-cylinder pressure graphs were constructed against the crank angle to find the effectiveness of combustion.

## 2 Materials and Methods

### 2.1 *Jatropha*

*Jatropha* is one of the flowering plants in the spurge family, & it is also called Euphorbiaceae. The *Jatropha* fruits are yellow color, and their dried seeds are black in color and oval in shape. The oil extracted from the seeds is golden yellow in color and fragrance-free. *Jatropha* has usually been used in basket creation and dye production. It had origin from tropical America and also many portions of the jungles in Africa [32, 33]. It is a drought-resistant, permanent plant, grown-up to fifty years, and it grows on any kind of soil. It has a yield of about 1 kg per square meter per year [34]. The toxin is the only drawback in it. In World War II, it was used as biodiesel for engines [35, 36]. In *Jatropha* seed oil, phorbol esters are considered toxic. The phorbol esters are destroyed by chemical refining (degumming, neutralization, silica/bleaching, mild deodorization) and physical refining (stripping at  $240^\circ$  and vacuum). The *Jatropha* seeds oil is highly viscous used in the manufacture of soap and candles. In cosmetics production, it is used as a diesel/paraffin additional or extender [37, 38]. It has significant inferences for fixing the demand for rural energy usage and also exploring useful substitutes for fossil fuels to reduce greenhouse gas addition in the atmosphere. Figure 1 shows the *Jatropha* plant and its fruit.

### 2.2 *Biodiesel Preparation Process—Transesterificaton*

The energy content of the vegetable oils is similar to that of diesel. The vegetable oils cannot be used as fuels in unmodified diesel engines as they are too viscous due to their high molar mass. Triglycerides react with methanol in the presence of a catalyst to form glycerol, and methyl ester is called biodiesel, and the same is shown in Fig. 2. Vegetable oil can be converted into a usable fuel, known as biodiesel, in a transesterification reaction. The triglycerides in *Jatropha* oil react with methanol, which is one of the alcohols, in the existence of a strong base such as sodium hydroxide to produce glycerol and *Jatropha* methyl ester, which is also known as *Jatropha* biodiesel. The chemical reaction between them is shown in Fig. 3.



Fig. 1 Jatropha plant

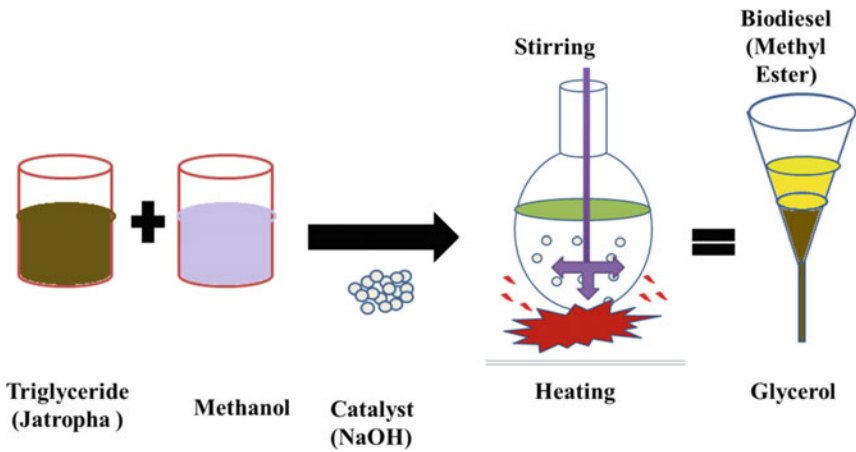


Fig. 2 Transesterification process

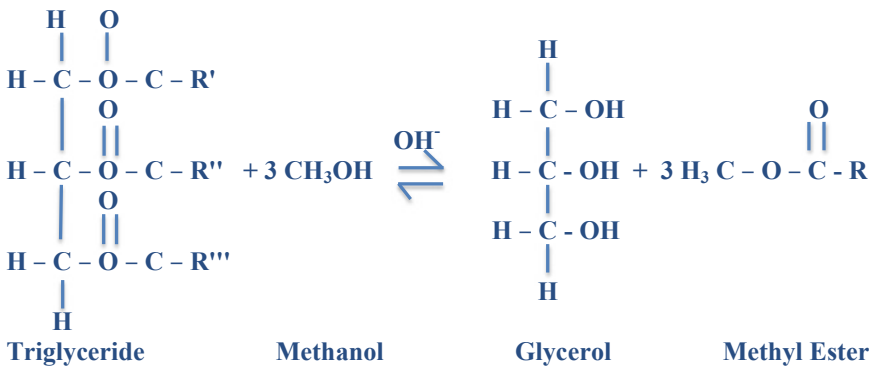


Fig. 3 Transesterification reaction

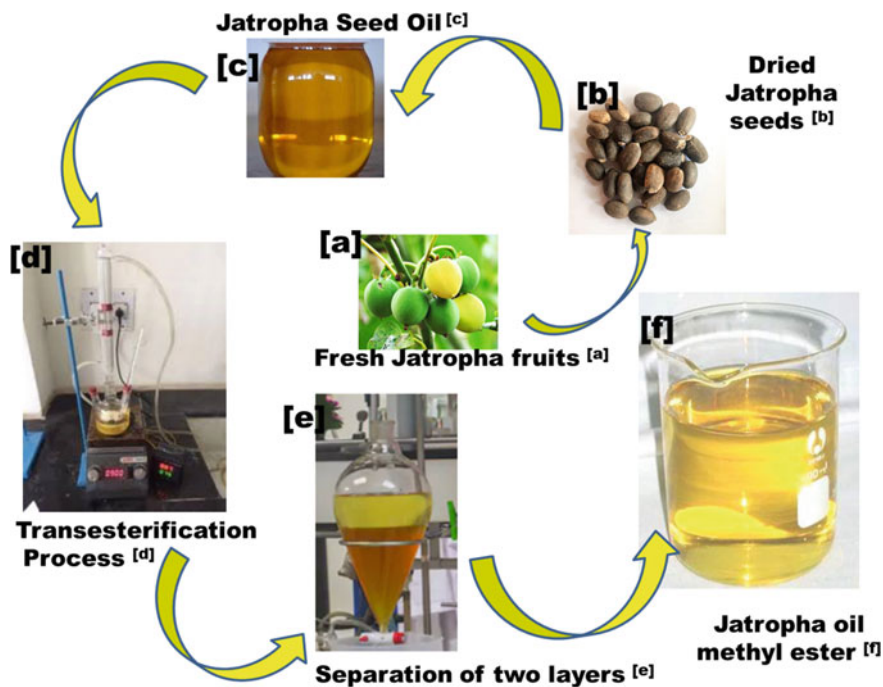


Fig. 4 Process of Jatropha biodiesel production

**Table 3** Weight composition of Jatropha oil

Fatty acid	Weight composition %
Linoleic 18:2	30.8
Oleic 18:1	46.3
Palmitic 16:0	14.5
Stearic 18:0	6.9
Linolenic 18:3	0.2
Palmitoleic 16:1	0.7
Unrecognized components	0.3
Arachidic 20:0	0.3

In this reaction, an excess of alcohol is used to drive the position of equilibrium to the right in favor of the products. The three alkyl ester molecules produced have similar energy content to the triglyceride but are less viscous due to their lower molar mass, and they are suitable for use in diesel engines.

Biodiesel is much less toxic and more biodegradable than regular diesel. In the industrial sector, the alkali-catalyzed transesterification process is followed for mass production [39, 40]. The whole process, which contains the conversion of



Jatropha seeds into Jatropha biofuel, is as shown in Fig. 4. Table 3 shows the weight composition of fatty acid [41].

### 2.3 Experimental Setup

A water-cooled, single-cylinder and four-stroke direct-injection compression engine with a compression ratio of 17.5:1 and power of 5.2 kW run at a speed of 1500 rpm was used for the present research work. The high viscosity is the major drawback of using Jatropha oil in an unmodified compression ignition engine. So, it is imperative to reduce the fuel viscosity before its use in the engine. Its higher viscosity is reduced by preheating the Jatropha biodiesel up to 90 °C by the heat exchanger, which utilizes the heat from exhaust gases that pass through it. Its viscosity is also reduced by blending with diesel. Experiments were conducted on various proportions of Jatropha biodiesel blend (J20, J40, J60, J80 and J100) and mineral diesel. The properties of diesel and Jatropha blends at 90 °C were measured, as given in Table 4 and other technical specifications of the engine used for this work are given in Table 5.

The performance, combustion and emission of the Jatropha oil with diesel in various proportions were measured. The eddy current dynamometer was used for multiple loading conditions. The schematic experimental setup for our investigation is shown in Fig. 5.

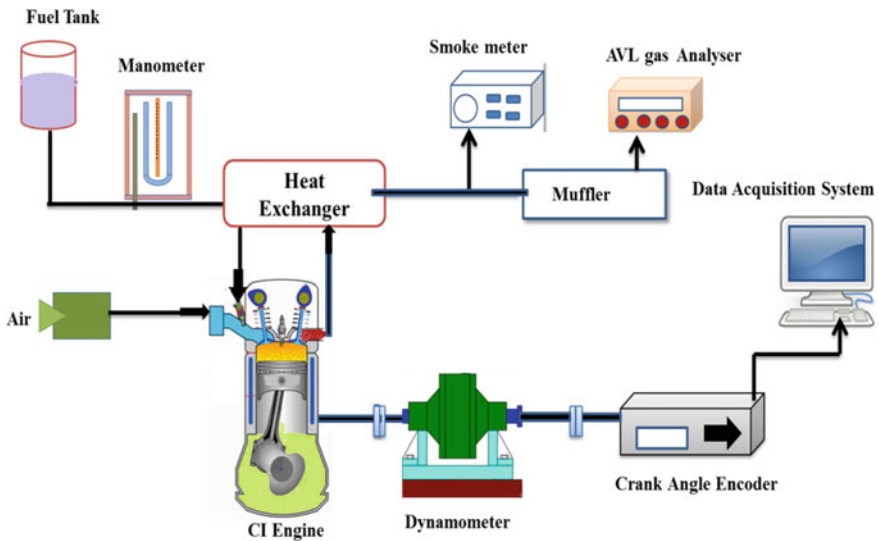
The Jatropha and diesel oils were filled in separate fuel tanks, which are our major components. The heat exchanger, exhaust gas analyzer, smoke meter, dynamometer and data acquisition system were also used as main components. The engine was started with diesel first and then with Jatropha oil for the purpose of warm-up. It also reduced deposits and cold-starting problems in the fuel line and injection system. The

**Table 4** Properties of Jatropha blends and diesel

Fuel used	Kinematic viscosity	Calorific value	Flash point	Density	Cetane number
Unit	(mm <sup>2</sup> /s)	(MJ/kg)	(°C)	(kg/l)	–
Apparatus utilized	Redwood viscometer	Bomb calorimeter	Pensky–Martens	Hydrometer	Ignition quality tester
Apparatus standard	ASTM D445	ASTM D240	ASTM D93	ASTM D941	ASTM D613
J20	4.2	43.1	79	0.868	54.17
J40	4.5	42.8	92	0.876	54.53
J60	4.8	42.3	110	0.889	54.65
J80	5	41.5	131	0.908	55.62
J100	5.3	40.2	168	0.939	56.88
Diesel	2.71	44.8	70	0.836	54

**Table 5** Specifications of the engine

Engine specifications	Manufacturer Kirloskar Ltd., India
Engine type	Single cylinder, four stroke, direct injection, vertical, water cooled and constant speed
Rated power	5.2 kW
Speed	1500 RPM
Bore/Stroke	102/ 116 (mm)
Compression ratio	17.5:1
Displacement volume in cylinder	0.9481 mm <sup>3</sup>
Injection pressure	210 bar
Injection timing	26° before top dead center
Brake mean effective pressure at 1500 RPM	6.34 kg/cm <sup>2</sup>



**Fig. 5** Schematic diagram of the engine setup

voltage and the current spent by the load were measured by voltmeter and ammeter. The exhaust gas composition was measured using an exhaust gas analyzer. Figure 5 represents the schematic diagram of the experimental setup test rig.

The physical, thermal and chemical properties of the Jatropa and diesel are given in Table 4. Jatropa oil has a high pour point, density and cloud point compared with diesel. The fire and flash points are higher for Jatropa oil than diesel and make it safe to use. Increased carbon deposit is due to the higher carbon content

from the Jatropha oil. The emissions and combustion properties are enhanced by the existence of oxygen, but the calorific value of the Jatropha oil decreases. The Jatropha oil has around 80% calorific value compared with diesel. Higher viscosity in Jatropha oil is the main issue of its use as a fuel in the diesel engine. In this experimental examination, viscosity was minimized by preheating and blending the Jatropha oil with diesel. The viscosity of Jatropha oil was maintained at 90 °C in this investigation because, at this temperature, it had a relative viscosity closer to diesel. Hence, Jatropha must be heated up to 90 °C before its injection into the engine to attain fuel properties close to diesel. Viscosity decrease depends upon its concentration of the combination.

### 2.4 Analysis of Uncertainty

The range of error in the experimental results represents the uncertainty analysis. It arises due to multiple factors such as instrument selection, condition, calibration, environment, reading, observation and test procedure. The experiments were performed thrice to minimize the effect of errors in the results. The uncertainty of various measuring units is given in Table 6. The uncertainty percentage was calculated by the square root of the sum of squares of the uncertainty values of brake power, brake specific fuel consumption, brake thermal efficiency, total fuel consumption, carbon monoxide, hydrocarbon, oxides of nitrogen, smoke, temperature and pressure [42].

**Table 6** Experimental uncertainty of various measuring units

Parameter	Methodology of measuring	Accuracy	Errors (±)
Load	Strain gauge load cell	±10 N	±0.2
Temperature	Thermocouple	±1 °C	±0.15
Pressure	Magnetic pickup principle	±0.1 kg	±0.1
Engine speed	Magnetic pickup principle	±10 rpm	±0.1
Fuel flow measurement	Volumetric measurement	±0.1 cc	±1
Crank angle encoder	Magnetic pickup principle	±1°	±0.2
Time	Stopwatch	±0.1 s	±0.2
Manometer deflection	Balancing of the column of liquid	±1 mm	±1
CO	NDIR technique	±0.02 vol%	±0.2
HC	NDIR technique	±10 ppm	±0.1
NO <sub>x</sub>	NDIR technique	±12 ppm	±0.2
Smoke	NDIR technique	±1 HSU	±1

$$\begin{aligned}
 \text{Total uncertainty} &= \sqrt{(\text{BP uncertainty})^2 + (\text{BFSC uncertainty})^2 + (\text{BTE uncertainty})^2} \\
 &= \sqrt{(\text{TFC uncertainty})^2 + (\text{CO uncertainty})^2 + (\text{HC uncertainty})^2} \\
 &\quad + (\text{NO}_x \text{ uncertainty})^2 + (\text{Smoke uncertainty})^2 + (\text{EGT uncertainty})^2 \\
 &\quad + (\text{Press uncertainty})^2} \\
 &= \sqrt{(0.2)^2 + (1)^2 + (1)^2 + (1)^2 + (0.2)^2 + (0.1)^2 + (0.2)^2 + (1)^2} \\
 &\quad + (0.15)^2 + (1)^2} \\
 &= \pm 2.26\%
 \end{aligned}$$

±2.26% was calculated as uncertainty values for the current experimental setup. The experimental uncertainty of various measuring units is given in Table 6.

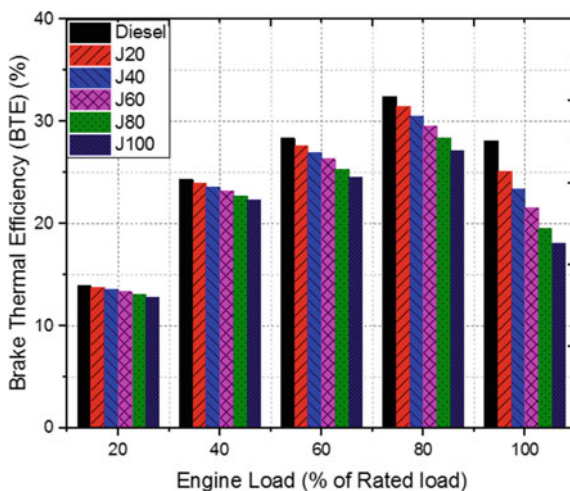
### 3 Results and Discussion

#### 3.1 Analysis of Performance Characteristics

##### 3.1.1 Brake Thermal Efficiency (BTE)

The BTE of Jatropha oil and diesel blends increases with increases in engine load, as presented in Fig. 6. It is witnessed that the calorific value of Jatropha oil is lesser than that of diesel oil. As a result of increasing the proportion of Jatropha biodiesel in blend decreases, the calorific value is proportional, which affects in increased BSFC, and it reduces BTE. BTE of Jatropha blends lower than that of diesel. However, BTE of J20 stays very nearer to diesel, and all other combinations have lesser BTE

Fig. 6 Thermal efficiency versus engine load



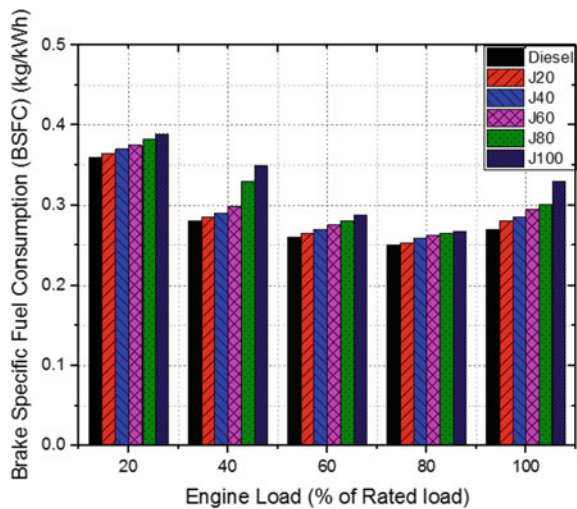
compared with J20 and mineral diesel. The combustion characteristics of the fuel molecules were increased by the presence of oxygen content in the biodiesel.

The higher viscosity and reduced volatility of the *Jatropha* biodiesel oil affect the atomization and combustion characteristics [43]. Therefore, BTE was found to be lesser for higher blend concentrations related to diesel. The BTEs of diesel and its blends were found increased with increases in load, but it tended to decrease with further increase in peak load. The maximum BTE of 31.1% was attained for J20, while for diesel, it was 32.5% at 80% of its full load condition.

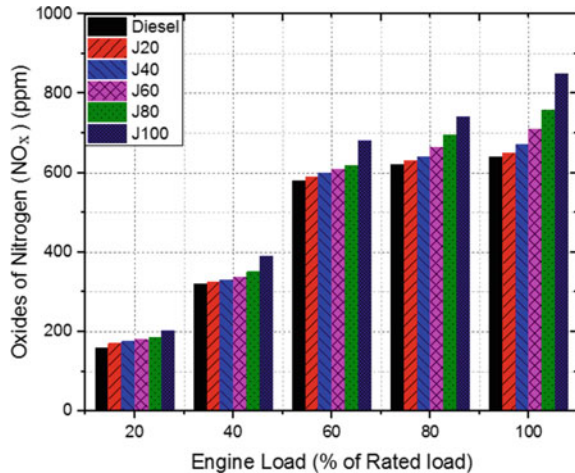
### 3.1.2 Brake Specific Fuel Consumption (BSFC)

Brake specific fuel consumption has been found to increase with a higher proportion of *Jatropha* biodiesel in the blend-related diesel in the various engine load range (Fig. 7). It is owing to the collective effects of the fuel density, viscosity and heating value of the blends. BSFC has increased owing to the high density of the *Jatropha* biodiesel oil blends based on its proportion levels. The higher bulk modulus has resulted in higher fuel discharge for the same value in BSFC. The usage of a low percentage of *Jatropha* biodiesel in diesel has resulted in lesser BSFC compared with diesel in all loads. The low BTE for J100 could be owing to lower calorific value and an increase in fuel consumption as related to J20. However, on the whole, by running the engine with *Jatropha* biodiesel, BSFC is always higher than the biodiesel as well as diesel.

**Fig. 7** Brake specific fuel consumption versus engine load



**Fig. 8** Oxides of nitrogen ( $\text{NO}_x$ ) versus engine load



## 3.2 Analysis of Emission Characteristics

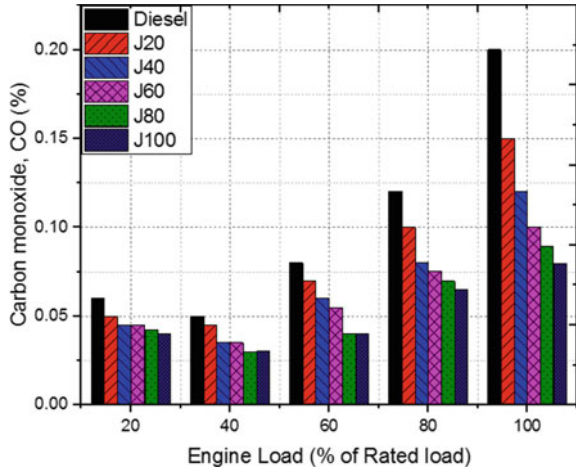
### 3.2.1 Emissions of Nitrogen Oxides ( $\text{NO}_x$ )

$\text{NO}_x$  emission is a highly harmful gaseous emission compared with other engine exhaust emissions. Hence, its reduction in an engine has always been one of the key aims of engine researchers all over the world. The  $\text{NO}_x$  emissions of diesel fuel were related to various proportions of Jatropa biodiesel at different loads as shown in Fig. 8. It is observed that the emission of oxides of nitrogen increases with increases in load for all fuels. It is also observed that if the amount of Jatropa in the blend increases, then emissions of  $\text{NO}_x$  also increase. This increase is due to Jatropa oil being an oxygenated fuel and that leads to improved combustion, and therefore, higher combustion temperature is attained. The higher temperature promotes  $\text{NO}_x$  formation. The  $\text{NO}_x$  emissions have increased enormously between 40 and 60% of the rated load for all blends and mineral diesel. However, the emissions of  $\text{NO}_x$  of blend J20 are nearer to diesel compared with others.

### 3.2.2 Carbon Monoxide

The development of CO emission mainly depends upon the physical and chemical properties of the fuel used. Figure 9 shows that the engine discharges lesser CO for Jatropa blends when related to diesel. When the proportion of Jatropa biodiesel in the blend increases, the percentage of emission of CO decreases. But all Jatropa blends are far below the percentage of CO emissions than that of mineral diesel. The decrease in CO emission of Jatropa blend is due to the high cetane number and oxygen present in the molecular structure of Jatropa oil, and it supplies the necessary oxygen to convert CO to  $\text{CO}_2$  when combustion takes place. Kumar et al.

**Fig. 9** Carbon monoxide (CO) versus engine load

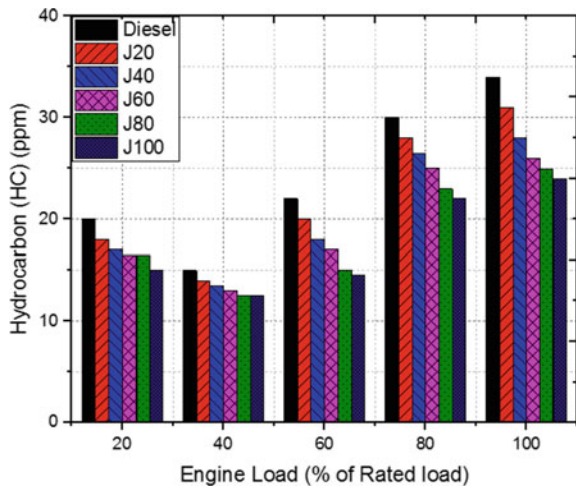


[44], in his investigation, reported that an increase in cetane number, there was a reduction in ignition delay, increased the injection pressure, thereby making the fuel particles finer, giving lower CO emissions. The emissions of CO for all blends are closer to those of diesel at 20% and 40% of the rated load. But the variation increases as 0.2% for diesel and 0.08% for J100 at full load conditions.

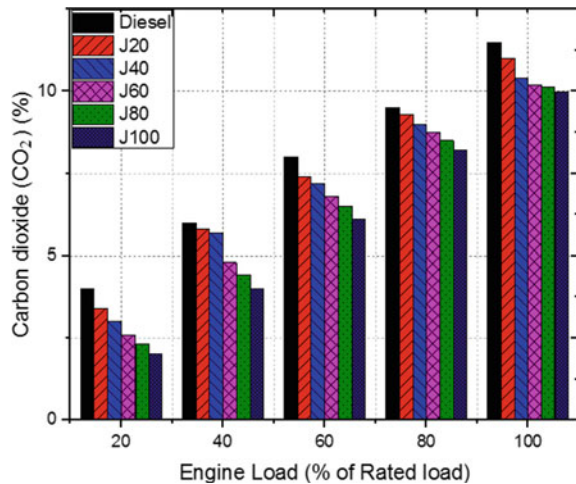
### 3.2.3 Hydrocarbon

The HC emission variation for various proportions of blends is shown in Fig. 10. It is observed that for diesel and Jatropa blends, the HC emissions are showing a

**Fig. 10** Hydrocarbon versus engine load



**Fig. 11** Carbon dioxide (CO<sub>2</sub>) versus engine load



decreasing trend first up to 40% of its load and then increasing trend with increasing load. It is owing to the existence of a rich fuel mixture at higher loads. It is witnessed that an increasing proportion of Jatropha in the blend decreases HC emissions. It is due to the presence of oxygen in the Jatropha oil, and the higher combustion temperature promotes the oxidation of HC. Elango and Senthilkumar [45] concluded that the effect of viscosity increased the HC emissions level of the blend at higher load conditions. The emissions of HC for all Jatropha blends are closer to those of diesel at 40% rated load as the emission values are 15% for diesel and 12.5% for J100. However, the variations of HC are maximum at its full load condition as the emissions values are 34.2% for diesel and 24.4% for J100.

### 3.2.4 Carbon Dioxide

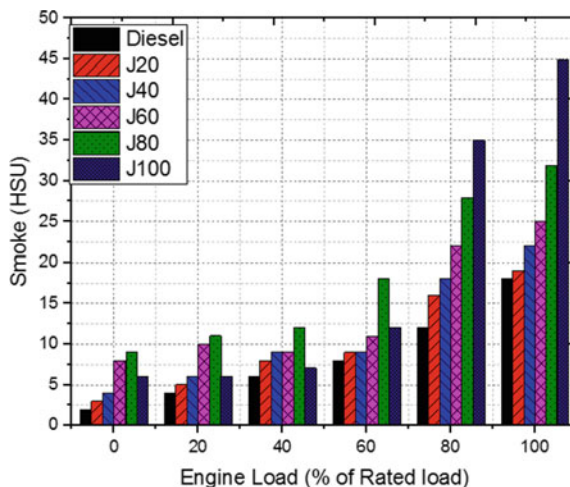
The emission intensities of CO<sub>2</sub> for various proportions of biodiesel and diesel is shown in Fig. 11. At full load conditions, the CO<sub>2</sub> emissions for diesel, J20, J40, J60, J80 and J100 are found to be 11.5%, 11.01%, 10.4%, 10.21%, 10.15% and 10.11%, respectively. It is shown that the CO<sub>2</sub> emission of Jatropha blends is less than that of diesel at all load conditions. It may be pointed out that Jatropha blends contain lower carbon content than diesel. The Jatropha oil contains more oxygen content, which is also one of the reasons for lower CO<sub>2</sub> emissions of Jatropha blend compared with diesel.

### 3.2.5 Smoke Density

The emissions of smoke opacity with the varying load are shown in Fig. 12. It indicates that as Jatropha biodiesel concentration increases, the smoke opacity also



**Fig. 12** Smoke versus engine load



increases irrespective of the load condition. At full load conditions, the smoke opacity for diesel, J20, J40, J60, J80 and J100 are found to be 18.2, 19.1, 22.4, 25.2, 32.7 and 45.1 HSU, respectively. It is owing to reduced volatility and improper mixing of fuel droplets with air because of the higher viscosity of the Jatropa blends. At full load condition, the value of the smoke density of Jatropa biodiesel J100 is two times the value of diesel at the same load condition. The  $\text{NO}_x$  and smoke emissions are controlled by combustion treatments (exhaust gas recirculation, emulsified biodiesel), exhaust after treatments (selective catalytic reduction, lean  $\text{NO}_x$  traps) and fuel treatments (fuel additives) [46].

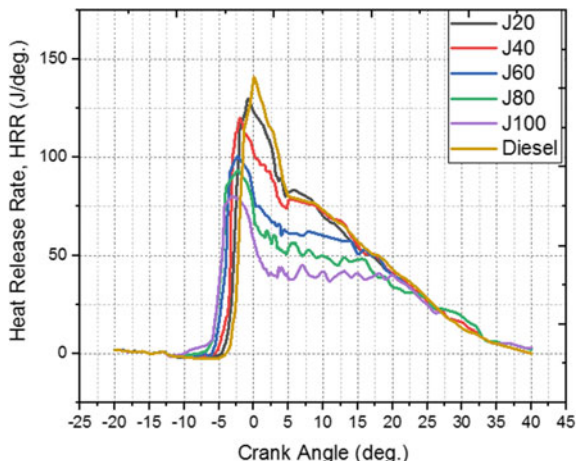
### 3.3 Analysis of Combustion Characteristics

#### 3.3.1 Heat Release Rate Versus Crank Angle

The heat release rates (HRR) versus crank angle for all Jatropa blends and diesel at full loading conditions are shown in Fig. 13. HRR attains negative value at the beginning of the combustion due to the vaporization of the fuel. After the start of the combustion phase (SOC), HRR turns into positive. All the proportions of Jatropa blends have almost identical combustion as mineral diesel at all stages, such as ignition delay, premixed combustion and diffusion combustion.

From Fig. 13, it is witnessed that at full engine load condition, combustion starts earlier for Jatropa blends. At the time of fuel injection, thermal cracking happens due to high cylinder temperature. It leads to shorter ignition delay for Jatropa blend compared to diesel. At the premixed combustion stage, the HRR is greater for diesel due to its high volatility and improved air–fuel mixing characteristics. It is also because of the longer ignition delay, which leads to a large amount of fuel addition.

**Fig. 13** Heat release rate versus crank angle

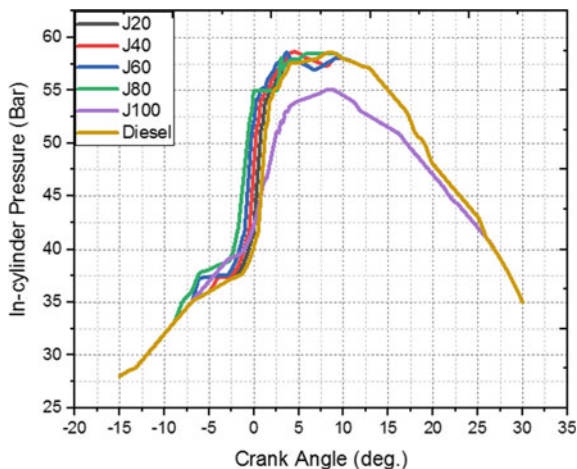


At diffusion combustion, Jatropa blends have high HRR in higher load conditions. The higher HRR for mineral diesel is 145.1 J/degree, and for J100, it is 76.3 J/degree, which is two times that of mineral diesel. However, the combustion duration for diesel is less than that of Jatropa blends.

### 3.3.2 In-Cylinder Pressure Versus Crank Angle

The variations of cylinder pressure for the crank angle for diesel and Jatropa blends J20, J40, J60, J80 and J100 at full engine loads are shown in Fig. 14. From these figures, it is observed that cylinder pressure rates are almost comparable with diesel for all fuel blends at low engine load conditions.

**Fig. 14** In-cylinder pressure versus crank angle



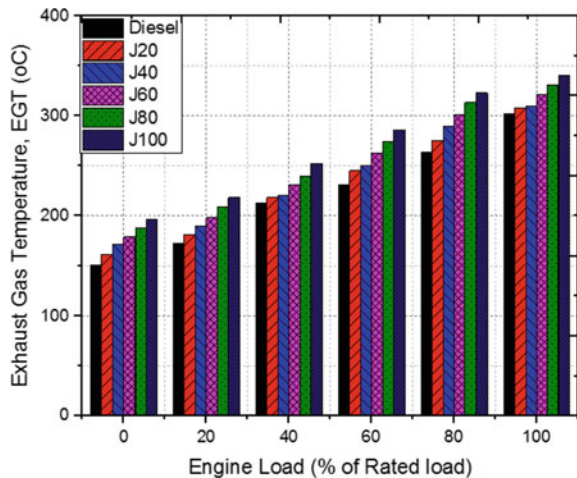
At higher load conditions, Jatropha blends have earlier pressure rise than diesel, and mineral diesel had higher peak pressure. The Jatropha blends had initial combustion compared to diesel, and the pressure rise rate is slower for Jatropha blends at full load conditions. Hence, it is due to the slower burning characteristics. The starting point of combustion for all fuels gets advanced as the engine load is increased. The combustion starts earlier for Jatropha blends. It is because of shorter ignition delay and partly due to advanced injection timing and also due to higher density and higher bulk modulus of Jatropha oil. It is due to the complex and pre-flame chemical reaction at high temperature. In the high cylinder temperature existing during fuel injection, Jatropha attained thermal cracking, and it leads to formation of lighter compounds [26]. Therefore, it causes in earlier ignition and shorter ignition delay for Jatropha blend compared to diesel.

Jatropha blend J40 has higher peak pressure of 58.5 bar, and it is higher compared with all blends and diesel. J100 has a peak pressure of 54.2 bar, and it is lower compared with all blends and mineral diesel.

### 3.3.3 Exhaust Gas Temperature

The influence of BTE and BSFC was reflected in exhaust gas temperature as well. The exhaust gas temperature with blends having a higher proportion of biodiesel blend was higher than that of diesel at greater loads, as shown in Fig. 15. When biodiesel concentration was increased, the exhaust gas temperature rose by a small value. Upon using 100% Jatropha oil, a higher value of exhaust gas temperature was obtained, which indicated more loss of energy. Elango et al. suggested that combustion is delayed for the blends, and more of the heat is released during mixing controlled combustion phase in which higher amount of heat goes with exhaust gas [45]. Hence, exhaust gas temperatures are higher. The EGT improved with an increase in load for

**Fig. 15** Exhaust gas temperature versus engine load



all blends. The rise in EGT with load was evident, and it showed that more fuel was required to take additional capacity. EGT is a sign of the range of conversion of heat into work, which occurs inside the cylinder. It was found that EGT for various fuel blends at different load conditions were almost identical. EGT increased with a rise in power for all fuel blends. As the biodiesel fuel concentration was improved, the exhaust gas temperature also got enhanced. The highest exhaust gas temperature was 340 °C at higher power for J100.

## 4 Conclusion

The principal objective of the current investigation was to measure the performance, combustion and emission characteristics of the compression ignition engine fueled with various proportions of Jatropha blends with diesel and mineral diesel. Accordingly, an experimental investigation was conducted. The investigation revealed that if the viscosity of Jatropha could be nearer to diesel, it would give better performance and emission characteristics. Hence, the viscosity of the Jatropha oil was reduced by the transesterification process and then by blending it with diesel with a preheating technique from the exhaust gas.

- The experimentation was conducted for raw diesel and various proportions of Jatropha diesel blends (J20, J40, J60, J80 and J100) at different load conditions and constant speed (1500 rpm).
- Brake thermal efficiency (BTE) decreased as Jatropha concentration in the blend increased. In contrast, maximum brake thermal efficiency of 31.1% was achieved for J20, while for diesel, it was 32.5% at full load conditions. At the same time, the brake specific fuel consumption (BSFC) and exhaust gas temperature were higher for Jatropha biodiesel blends than for diesel.
- Jatropha blends had higher peak pressure at lower loads, and mineral diesel had higher peak pressure at higher loads. NO<sub>x</sub> and smoke emissions were higher than diesel for Jatropha blends because of reduced volatility and higher viscosity of mixtures. In contrast, the emissions CO, HC and CO<sub>2</sub> were lower for Jatropha blends than for diesel due to low carbon content, high oxygen content and high cetane number of biodiesel.

From the detailed experimental investigation on performance, combustion and emission on Jatropha biodiesel, it could be inferred that J20 was the best alternative fuel, and it gave better efficiency and emissions similar to those of diesel. And hence, it can be directly used in the CI engine without any engine modification.

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### Declaration of Competing Interest

The authors announce that they have no recognized competing financial interests or personal relationships that could have seemed to influence the work described in this article.

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