MCDM Optimization of Characteristics in Resistance Spot Welding for Dissimilar Materials Utilizing Advanced Hybrid Taguchi Method-Coupled CoCoSo, EDAS and WASPAS Method



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1 Introduction

Resistance spot welding (RSW) is a high-speed process, wherein the actual time of welding is a small fraction of second and it is one of the cleanest and most efficient welding process that has been widely used in sheet metal fabrication [1–6]. The high speed of process, the case of operation and its adaptability for automation in the production of sheet metal assemblies are its major advantages. Limitations of RSW are equipment cost and power requirements, difficulty of disassembly for maintenance or repair of RSW joints, and the nature of the design needed for the process (lap joints are required) [5–9]. Resistance spot welding has steadily gained importance over the years because of its ability to join the variety of materials and complicated shapes with high accuracy and great precision. Resistance spot welding is a small fraction of second and it is one of the cleanest and most efficient welding processes that has been widely used in sheet metal fabrication [11–13]. The high speed of process, the case of operation and its adaptability for automation in the production of sheet metal fabrication [11–13]. The high speed of process, the case of operation and its adaptability for automation in the production of sheet metal assemblies are its major advantages. Over the last few years, the weight of

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automobiles has increased considerably due to the addition of safety related items, such as impact resistance bumpers and door impact beams, emission control equipment and convenience items, such as air conditioning. At the same time, fuel consumption has increased significantly primarily due to emission control equipment [1-15].

In this study, the Taguchi parameter design phase is the most important design phase and served the objective of determining the optimal resistance spot welding parameters to achieve the lowest weld time and the highest tensile-shear strength and nugget diameter in dissimilar (steel + Al) materials under varying resistance spot welding parameter conditions. The following are the questions considered in this study the relationship between the control factors (squeeze time, welding time and current) and output response factors (tensile-shear strength and nugget diameter and weld time). In this investigation, three parameters such as squeeze time, welding time, current were chosen and also optimized to know about the change of mechanical properties around the welded nugget area. In this study, Taguchi's design of experiment was used for experimental design, and multi-response optimization techniques, i.e., combined compromised solution (CoCoSo), evaluation based on distance from average solution (EDAS) and weighted aggregated sum product assessment (WASPAS) method were used to find optimum results.

2 Experimental Analysis and Methodology

AA1200 aluminum alloy sheets with a thickness of 2.5 mm and 50HS stainless steel of 3.0 mm thickness were used as base alloys in this investigation. The sheets were cut to required size by shear-off machine, followed by surface grinding to remove oxides and scales. The dimensions of the AA1200 sheet and 50HS are 114.3 mm \times 25.4 mm \times 3 mm and 114.3 mm \times 25.4 mm \times 3 mm respectively. The sheets were resistance spot welded in a 25.4 mm overlap configuration. The chemical composition and mechanical properties of the base alloys are presented in Tables 1 and 2. Prior to welding, the surface of all specimens from both types of material were first ground by abrasive paper using acetone, then thoroughly cleaned, and finally spot welded to prepare the similar and dissimilar welded joints using a spot welding machine SIP type PPV50. A tensile test machine (Tinius Olsen) was used to carry out all the tensile-shear tests for the dissimilar spot-welded specimens. The procedure of experimental work was planned to be conducted in three groups according to the type of weld joint for dissimilar (steel + Al) materials. Nine specimens from each group were spot welded according to the experimental design employed in the current work. During welding the aluminum with steel, it was needed to insert a 0.3 thick sheet of copper (AISI C10200) as a filler metal between the dissimilar materials of the specimen to be welded [8] (Fig. 1).

Table 1 Chemical	Element	50HS	AA1200
metals		Content (%)	Content (%)
metals	Chromium, Cr	20.5-23.5	-
	Nickel, Ni	11.5–13.5	-
	Manganese, Mn	46	≤ 0.050
	Molybdenum, Mo	1.5–3	-
	Silicon, Si	1 max	≤ 1
	Nitrogen, N	0.20-0.40	-
	Niobium, Nb	0.10-0.30	-
	Vanadium, Va	0.10-0.30	-
	Phosphorous, P	0.04 max	-
	Carbon, C	0.06 max	-
	Sulfur, S	0.010 max	-
	Zinc, Zn	-	≤ 0.10
	Aluminum, Al	-	\geq 99
	Iron, Fe	-	≤ 1
	Copper, Cu	-	\leq 0.050
	Titanium, Ti	-	≤ 0.050

 Table 2
 Parameters, codes
 and level values used for orthogonal array

Parameter	Unit	Code	Level 1	Level 2	Level 3
Squeeze time	(s)	А	13.75	15	16.25
Welding time	(s)	В	0.375	0.5	0.625
Current	(A)	С	60	65	70

Fig. 1 Dimensions of RSW specimen



3 **Optimization Methods**

Combined Compromise Solution Method (CoCoSo) 3.1

The following steps are used to solve CoCoSo decision problem [16, 17]:

1. Determination of initial decision-making matrix using Eq. (1)

$$X_{ij} = \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1n} \\ x_{21} & x_{22} & \dots & x_{2n} \\ \dots & \dots & \dots & \dots \\ x_{m1} & x_{m2} & \dots & x_{mn} \end{bmatrix}$$
(1)

2. Using compromise normalization equation, normalization of criteria values is done:

$$r_{ij} = \frac{x_{ij} - \min x_{ij}}{\max x_{ij} - \min x_{ij}}; \text{ for benefit criterion};$$
(2)

$$r_{ij} = \frac{\max x_{ij} - x_{ij}}{\max x_{ij} - \min x_{ij}}; \text{ for cost criterion}:$$
(3)

3. Determination of total weighted comparability sequence and whole of power of weight of comparability sequences for respective alternate as S_i and P_i , respectively:

$$S_i = \sum_{j=1}^n \left(w_j r_{ij} \right) \tag{4}$$

$$P_i = \sum_{j=1}^n \left(r_{ij} \right)^{w_j} \tag{5}$$

4. Three appraisal score are used for generation of comparative weights of other options derived using Eqs. (6, 7, 8):

$$k_{ia} = \frac{P_i + S_i}{\sum_{i=1}^{m} (P_i + S_i)}$$
(6)

$$k_{ib} = \frac{S_i}{\min S_i} + \frac{P_i}{\min P_i} \tag{7}$$

$$k_{ic} = \frac{\lambda(S_i) + (1 - \lambda)(P_i)}{(\lambda \max S_i + (1 - \lambda)\max P_i)}$$
(8)

5. Ranking of all alternatives is determined from higher to lower based on k_i values:

$$k_{i} = (k_{ia}k_{ib}k_{ic})^{\frac{1}{3}} + (k_{ia} + k_{ib} + k_{ic})$$
(9)

3.2 Weighted Aggregated Sum Product Assessment Method (WASPAS)

The chief technique of WASPAS method for solving MCDM problems is [18].

- 6. Initial decision matrix is set.
- 7. Decision matrix normalization using following Eqs. (10) and (11) for maximization and minimization criteria, respectively:

$$\overline{x}_{ij} = x_{ij} / \max_i x_{ij} \tag{10}$$

$$\overline{x}_{ij} = \min_i x_{ij} / x_{ij} \tag{11}$$

where x_{ij} is the assessment value of *i*th alternate with respect to *j*th measure.

8. Calculation of total comparative significance of *i*th alternate, based on weighted sum method (WSM) using Eq. (12):

$$Q_i^{(1)} = \sum_{j=1}^n \overline{x}_{ij} \cdot w_j \tag{12}$$

9. Calculation of total comparative significance of *i*th alternate, based on weighted product method (WPM) using Eq. (13):

$$Q_i^{(2)} = \prod_{j=1}^n \bar{x}_{ij}^{w_j}$$
(13)

10. Calculation of total relative significance of alternatives is done using Eq. (5) and ranked from higher value to lower value:

$$Q_i = \lambda \cdot Q_i^{(1)} + (1 - \lambda) \cdot Q_i^{(2)}$$

$$\tag{14}$$

3.3 Evaluation Based on Distance from Average Solution Method (EDAS)

EDAS method was developed by M. Keshavarz Ghorabaee et al. [19] for multi-criteria inventory classification. The steps for using the EDAS method are presented as follows [20]:

Step 1: Select the most important criteria that describe alternatives.

Step 2: Construct the decision-making matrix (X), shown as follows:

$$X = [x_{ij}]_{nXm} = \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1m} \\ x_{21} & x_{22} & \dots & x_{2m} \\ \dots & \dots & \dots & \dots \\ x_{n1} & x_{n2} & \dots & x_{nm} \end{bmatrix}$$
(15)

where X_{ij} denotes the performance value of *i*th alterative on *j*th criterion.

Step 3: Determine the average solution according to all criteria, shown as follows:

$$AV = \left[AV_j\right]_{1Xm} \tag{16}$$

where,

$$AV_j = \frac{\sum_{i=1}^n X_{ij}}{n} \tag{17}$$

Step 4: Calculate the positive distance from average (PDA) and the negative distance from average (NDA) matrixes according to the type of criteria (benefit and cost), shown as follows:

$$PDA = \left[PDA_{ij}\right]_{nXm} \tag{18}$$

$$NDA = \left[NDA_{ij}\right]_{nXm} \tag{19}$$

if *j*th criterion is beneficial,

$$PDA_{ij} = \frac{\max\left(0, \left(X_{ij} - AV_{j}\right)\right)}{AV_{j}}$$
(20)

$$NDA_{ij} = \frac{\max\left(0, \left(AV_j - X_{ij}\right)\right)}{AV_j}$$
(21)

and if *j*th criterion is non-beneficial,

$$PDA_{ij} = \frac{\max\left(0, \left(AV_j - X_{ij}\right)\right)}{AV_j}$$
(22)

$$NDA_{ij} = \frac{\max(0, (X_{ij} - AV_j))}{AV_j}$$
(23)

where PDA_{ij} and NDA_{ij} denote the positive and negative distance of *i*th alternative from average solution in terms of *j*th criterion, respectively.

Step 5: Determine the weighted sum of PDA and NDA for all alternatives shown as follows:

$$SP_i = \sum_{j=1}^m w_j PDA_{ij}$$
(24)

$$SN_i = \sum_{j=1}^m w_j NDA_{ij}$$
(25)

where w_i is the weight of *j*th criterion.

Step 6: Normalize the values of SP and SN for all alterative, shown as follows:

$$NSP_i = \frac{SP_i}{\max_i(SP_i)}$$
(26)

$$NSN_i = 1 - \frac{SN_i}{\max_i(SN_i)}$$
(27)

Step 7: Calculate the appraisal score (AS) for all alterative, shown as follows:

$$AS_i = \frac{1}{2} (NSP_i + NSN_i)$$
(28)

where $0 \leq AS_i \leq 1$.

Step 8: Rank the alternatives according to the decreasing values of appraisal score (AS). The alternative with the highest AS is the best choice among the candidate alternatives [21].

4 Results and Considerations

Samples are prepared by using Taguchi's experimental design which is shown in Table 3 and as per design of experiment, nine experimental runs are carried out. The analysis of the results of the above-mentioned welding conditions is being done on basis of tensile-shear strength, nugget diameter and weld time of the work piece. Table 3 elucidates that the maximum resulted force of (Steel + Al) spot-welded specimens are 8.39 MPa.

4.1 Optimization Using Combined Compromised Solution (CoCoSo)

The first step demonstrates forming of the normalized decision-making matrix (using compromise equation (max–min)), which is shown in Table 4. The further step is to generate the comparability sequence matrix. In this process, the weights of decision-making criteria are involved in the algorithm. The S_i and P_i vectors must be generated, and the values of K_a , K_b , and K_c are calculated using equations of CoCoSo approach used to calculate the ranking score by k shown in Table 4.

From Table 4, for a values of input, parameter in experiment number 1 has the highest k_i value. Therefore, experiment number 1 is an optimal parameter combination for RSW operation according to CoCoSo technique optimization. Now the k_i

Run no.	A	В	C	Tensile-shear strength (MPa)	Nugget diameter (mm)	Weld time (ms)
1	13.75	0.375	60	5.33	3.86	49
2	13.75	0.5	65	8.09	4.52	53
3	13.75	0.625	70	7.77	5.56	75
4	15	0.375	65	6.95	5.44	40
5	15	0.5	70	8.10	6.75	49
6	15	0.625	60	7.07	6.31	55
7	16.25	0.375	70	6.67	5.98	51
8	16.25	0.5	60	7.12	5.82	46
9	16.25	0.625	65	8.39	6.21	63

Table 3 Result table for tensile-shear strength and nugget diameter and weld time

Run no.	Si	P _i	k _{ia}	k _{ib}	k _{ic}	k _i	Rank
1	0.9317	2.9244	0.1663	9.8116	1.0000	4.8365	1
2	0.3253	2.0923	0.1042	4.1278	0.6270	2.2658	6
3	0.1775	1.5312	0.0737	2.5076	0.4431	1.4423	8
4	0.6137	2.5411	0.1360	6.8657	0.8181	3.5208	2
5	0.2585	1.5263	0.0770	3.1911	0.4629	2.0110	7
6	0.4294	2.2408	0.1151	5.1069	0.6925	2.7127	5
7	0.5535	2.4481	0.1294	6.2947	0.7784	3.2600	3
8	0.5170	2.4065	0.1261	5.9579	0.7581	3.1095	4
9	0.1180	1.5570	0.0722	2.0199	0.4344	1.2408	9

Table 4 Weighted comparability series (S_j) , exponentially weighted comparability sequence (P_i) , final aggregation and CoCoSo ranking of the alternatives



Fig. 2 S/N ratio by CoCoSo method

Source	DF	Seq SS	Adj MS	F	Р	% influence
А	2	2.258	1.129	0.70	0.589	1.96
В	2	75.017	37.509	23.18	0.041	65.09
С	2	34.746	17.373	10.74	0.085	30.15
Residual error	2	3.236	1.618			2.81
Total	8	115.257				

Table 5ANOVA result for k_i

values of alternatives were used to plot mean effect. In Fig. 2, A2 B1 C1 shows the smallest value combination in main effect plot for the three factors, i.e., A, B, C respectively which is optimum parameter arrangement for RSW operation.

Most influential factor

Table 5 gives the results of the ANOVA for the tensile-shear strength, nugget diameter and weld time using the calculated values from the k_i of alternatives of Table 4. According to Table 5, factor B, welding time with 65.09% is the most significant controlled parameters for RSW process followed by factor C, current with 30.15% of contribution and factor A, squeeze time with 1.96% of contribution if the minimization tensile-shear strength, nugget diameter and weld time are simultaneously considered.

S = 1.2720, R - Sq = 97.19% R - Sq(adj) = 88.77%

4.2 Optimization Using WASPAS

Since semantic terms, used to express the responses, have already been converted into crisp (real) values, the application of the WASPAS method starts with normalization of the decision matrix by applying WASPAS approach since the output has to be minimized. Subsequently, total relative importance of alternatives as per WSM and WPM is calculated by using equations of WASPAS approach. Finally, joint criterion of optimality of the WASPAS method is calculated by using WASPAS methodology. Table 6 provides the values of total relative importance (performance scores) for all the considered alternatives for a λ value of 0.5.

Based on the total relative importance values of alternatives, it is observed that trial 1 is determined as the best sample according to the ranking. Therefore, experiment no. 1 is an optimal parameter combination for RSW operation according to WASPAS technique optimization.

Run No.	$Q_{i}^{(1)}$	Q _i ⁽²⁾	Qi	Rank
1	0.9499	0.9461	0.9480	1
2	0.7072	0.7042	0.7057	6
3	0.6457	0.6416	0.6437	8
4	0.8226	0.8159	0.8193	2
5	0.6892	0.6845	0.6869	7
6	0.7255	0.7239	0.7247	5
7	0.7721	0.7703	0.7712	3
8	0.7702	0.7674	0.7688	4
9	0.6329	0.6329	0.6329	9

Table 6Computationaldetails of the WASPASmethod



Fig. 3 S/N ratio by WASPAS method

Source	DF	Seq SS	Adj MS	F	Р	% influence
А	2	0.24134	0.12067	9.79	0.093	2.52
В	2	6.53704	3.26852	265.30	0.004	68.24
С	2	2.77741	1.38870	112.72	0.009	28.99
Residual error	2	0.02464	0.01232			0.26
Total	8	9.58043				

Table 7 Analysis of variance for Q_i

Now the Q_i values of alternatives were used to plot mean effect. In Fig. 3, A1 B1 C1 shows the smallest value combination in main effect plot for the three factors, i.e., A, B, C respectively which is optimum parameter arrangement for RSW operation.

Most influential factor

Table 7 gives the results of the ANOVA for the tensile-shear strength, nugget diameter and weld time using the calculated values from the Qi of alternatives of Table 6. According to Table 7, factor B, welding time with 68.24%, is the most significant controlled parameters for RSW process followed by factor C, current with 28.99% of contribution and factor A, squeeze time with 2.52% of contribution if the minimization tensile-shear strength, nugget diameter and weld time are simultaneously considered.

S = 0.1110, R - Sq = 99.74%, R - Sq(adj) = 98.97%

Expt. No.	Tensile-shear strength		Nugget diameter		Weld time	
	PDA _{ij}	NDA _{ij}	PDA _{ij}	NDA _{ij}	PDA _{ij}	NDA _{ij}
1.	0.2674	0.0000	0.3121	0.0000	0.0000	0.0000
2.	0.0000	0.1113	0.1939	0.0000	0.0000	0.0001
3.	0.0000	0.0668	0.0091	0.0000	0.0000	0.3993
4.	0.0458	0.0000	0.0305	0.0000	0.1344	0.0000
5.	0.0000	0.1131	0.0000	0.2030	0.0000	0.0000
6.	0.0288	0.0000	0.0000	0.1252	0.0000	0.0375
7.	0.0838	0.0000	0.0000	0.0663	0.0000	0.0000
8.	0.0224	0.0000	0.0000	0.0372	0.0221	0.0000
9.	0.0000	0.1529	0.0000	0.1068	0.0000	0.1747

Table 8 Positive distance from average and negative distance from average of all output responses

 Table 9
 Weighted sum of PDA and NDA, normalized values of SP and SN, appraisal score and rank of all output responses

Expt. No.	SP	SN	NSP	NSN	AS	Rank
1.	0.2010	0.0000	1.0000	1.0000	1.0000	1
2.	0.0252	0.0668	0.1254	0.5630	0.3442	6
3.	0.0012	0.1479	0.0059	0.0987	0.0523	8
4.	0.0677	0.0000	0.3369	1.0000	0.6685	4
5.	0.0000	0.0942	0.0000	0.3832	0.1916	7
6.	0.0173	0.0264	0.7617	0.8272	0.7944	2
7.	0.0503	0.0086	0.2501	0.4496	0.3498	5
8.	0.0194	0.0048	0.5999	0.9683	0.7841	3
9.	0.0000	0.1528	0.0000	0.0000	0.0000	9

4.3 Optimization Using EDAS

The first step demonstrates forming of the normalized decision-making matrix and determines the average solution according to all criteria using EDAS method. The further step is to generate the positive distance from average (PDA) and the negative distance from average (NDA) matrixes according to the type of criteria, i.e., benefit criteria in this case using equation shown in table. Determination of the weighted sum of PDA and NDA for all alternatives was done in next step using equation shown in Table 8. After finding weighted sum of PDA and NDA, normalization is done using equations. Finally, the appraisal score (AS) was calculated for all alterative using equations of EDAS approach and ranking was done according to the decreasing values shown in Table 9.



Fig. 4 S/N ratio by EDAS method

Source	DF	Seq SS	Adj MS	F	Р	% influence
А	2	56.17	20.08	1.02	0.573	11.05
В	2	94.64	36.35	1.85	0.461	18.61
С	2	338.03	169.02	8.61	0.234	66.48
Residual error	2	19.64	19.64			3.86
Total	8	508.48				

Table 10 Analysis of variance for AS

Based on the total relative importance values of alternatives, it is observed that trial 1 is determined as the best sample according to the ranking. Therefore, experiment no. 1 is an optimal parameter combination for RSW operation according to EDAS technique optimization.

Now, the appraisal score (AS) calculated for all alterative was used to plot mean effect for SN ratios. Based on this study, one can select a mixture of the levels that provide the smaller average response. In Fig. 4, the combination of A3 B1 C1 shows the largest value of the SN ratio plot for the factors A, B and C respectively which is optimum parameter arrangement for RSW operation.

Most influential factor

Table 10 gives the results of the ANOVA for the tensile-shear strength, nugget diameter and weld time using the calculated values from the AS of alternatives of Table 9. According to Table 10, factor C, current with 66.48% is the most significant controlled parameters for RSW process followed by factor B, welding time of 18.61% contribution and factor A, squeeze time with 11.05% of contribution if

Optimization technique	Optimal setting	Predicted value	Experimental value
CoCoSo method	A2 B1 C1	4.75139	4.5208
WASPAS method	A1 B1 C1	0.956638	0.9480
EDAS method	A3 B1 C1	0.9807	0.9212

Table 11 Confirmatory test results

the minimization tensile-shear strength, nugget diameter and weld time are simultaneously considered.

4.4 Confirmation Experiment

The confirmation experiments were conducted using the optimum combination of the machining parameters obtain from Taguchi analysis. These confirmation experiments were used to predict and validate the improvement in the quality characteristics for RSW of AA1200 and 50HS. The final phase is to verify the predicted results by conducting the confirmation test [21-23]. The estimated total relative significance can be determined by using the optimum parameters as:

$$\mu_{\text{predicted}} = a_{2m} + b_{1m} - 3\mu_{\text{mean}} \tag{29}$$

where a_{2m} and b_{1m} are the individual mean values of total relative significance with optimum level values of each parameters and μ_{mean} is the overall total relative significance [21–23] where Table 11 shows the confirmatory test results.

5 Conclusions

This investigation clarifies the methodology for investigating the influence of the spot welding parameters on the tensile-shear force for dissimilar spot-welded joints of aluminum and steel materials. The "smaller is the better" approach was applied in Taguchi approach using Minitab 19 software to design the experiments and analyze the overall results. The Hybrid Taguchi methodologies, i.e., CoCoSo, WASPAS and EDAS were designed to predict which input variables give the optimum responses of resistance spot welding operation.

From this analysis, some important conclusions are drawn and listed below:

- 1. The optimum results can be achieved by a parametric optimization method, which provides a short period of time with a lower cost.
- 2. Analysis of the experimental results through the signal to noise ratio and means responses exhibited that the significant influence on the tensile-shear force for the similar material joint is the current. While, the squeeze time possesses a

major impact pursued by welding time and then current for the dissimilar material joint.

- 3. Tensile-shear force enhanced as the welding time was increased for the all welded joints. But the other parameters exhibited a different behavior, and the linear regression of the output results demonstrated this behavior. For the dissimilar joints, it is preferred to apply a lower squeezing time with a higher welding time and current.
- 4. The optimal setting of this investigation based on CoCoSo, WASPAS and EDAS is A₂ B₁ C₁, A₁ B₁ C₁ and A₃ B₁ C₁ respectively.
- 5. The results of confirmatory tests which were carried out at optimal setting are quite nearly come near the actual value with minimal error.
- 6. The CoCoSo and WASPAS methods have better result than EDAS because the P-value of input parameters comes less than 0.05 that means this experimental design fitted with 95% confidence interval.

It should be mentioned here that the current research can improve the spot welding process for similar and dissimilar welded joints through predicting the optimum input welding parameters for the optimal responses by applying Hybrid Taguchi approaches in order to avoid the encountered problems in the spot welding procedures of different structures as well as to reduce many expensive welding trials.

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