



CO₂ Flooding and Geological Storage Potential Evaluation Method for Low Permeability Reservoirs in Dagang Oilfield

Hai-ying Cheng¹, Xin-wei Liao²(✉), Ming-jun Cai¹, Yang Zhang¹,
and Rong-tao Li²

¹ Petrochina Dagang Oilfield, Tianjin, China
{chenghaiying, caimjun, zhangyang08}@petrochina.com.cn

² China University of Petroleum, Beijing, China
xinwei@cup.edu.cn, lirongtao2015@126.com

Abstract. Permanently sequestering carbon dioxide during carbon dioxide flooding is the most realistic way to meet carbon dioxide emission reduction obligations in developing countries. In order to effectively evaluate the potential of carbon dioxide flooding and geological storage of low permeability reservoirs in Dagang Oilfield, it is necessary to establish a reliable CO₂ flooding and geological storage potential evaluation method. Based on the characteristics of low permeability reservoirs in Dagang Oilfield, this paper establishes a CO₂ enhanced oil recovery (EOR) and geological storage potential evaluation method based on fractional flow theory. Through theoretical analysis and numerical simulation method, the carbon dioxide storage coefficient, carbon dioxide storage and CO₂ flooding efficiency of low permeability reservoirs in Dagang Oilfield under carbon dioxide miscible and immiscible flooding conditions were determined, and these values were analyzed and evaluated. The results show that the CO₂ flooding efficiency and storage coefficient of miscible flooding are significantly higher than that of immiscible flooding. In addition, as the amount of carbon dioxide injected increases, the carbon dioxide flooding oil increase and the amount of storage increase. Through the evaluation of 272 oil layers in the low-permeability oil area of Dagang Oilfield, the enhanced oil recovery and geological storage potential of CO₂ in this area were analyzed. It can be seen from the analysis and evaluation results that CO₂ miscible flooding is an effective displacement and storage method. The conclusions drawn can

Copyright 2019, IPPTC Organizing Committee.

This paper was prepared for presentation at the 2019 International Petroleum and Petrochemical Technology Conference in Beijing, China, 27–29, March, 2019.

This paper was selected for presentation by the IPPTC Committee following review of information contained in an abstract submitted by the author(s). Contents of the paper, as presented, have not been reviewed by the IPPTC Technical Committee and are subject to correction by the author(s). The material does not necessarily reflect any position of the IPPTC Technical Committee, its members. Papers presented at the Conference are subject to publication review by Professional Team of Petroleum Engineering of the IPPTC Technical Committee. Electronic reproduction, distribution, or storage of any part of this paper for commercial purposes without the written consent of Shaanxi Petroleum Society is prohibited. Permission to reproduce in print is restricted to an abstract of not more than 300 words; illustrations may not be copied. The abstract must contain conspicuous acknowledgment of IPPTC. Contact email: paper@ipptc.org.

© Springer Nature Singapore Pte Ltd. 2020

J. Lin (ed.), *Proceedings of the International Petroleum and Petrochemical Technology Conference 2019*, pp. 70–79, 2020.

https://doi.org/10.1007/978-981-15-0860-8_6

provide technical reference for the implementation of CO₂ flooding and storage in low permeability reservoirs in Dagang Oilfield.

Keywords: CO₂ flooding · CO₂ geological storage · Potential evaluation method · Low permeability reservoir

1 Introduction

With the increasing global warming and climate deterioration, greenhouse gas emissions, especially CO₂ emissions, have attracted more and more attention of countries. Achieving the geological storage of CO₂ in reservoirs can not only greatly reduce the emission of CO₂ in the atmosphere, but also greatly improve the oil recovery. Research on CO₂ flooding and its storage has been carried out earlier, and a more complete theory of displacement and storage has been formed [1–12]. In 1997, Taber et al. summarized the screening criteria for CO₂ flooding reservoirs based on the successful case of CO₂ enhanced oil recovery [2]. In 2002, Shaw et al. screened the reservoir parameters suitable for CO₂-EOR on the basis of summarizing the previous research results, and graded the target reservoir by setting the optimal value and parameter weight [5, 6]. The potential of CO₂ flooding enhanced recovery was evaluated in the Alberta reservoir [8]. CO₂ sequestration is widely evaluated using CO₂ utilization coefficient in American and European countries, which is defined as total sequestration amount divided by cumulative oil production [9–12]. Shen Pingping et al. also proposed a similar approach in 2009 [13]. At present, China has a relatively late start in this field, especially for the potential of carbon dioxide storage in China's major oil areas, it is necessary to further establish a reasonable evaluation system. There are a large number of low permeability reservoirs in Dagang oilfield. After decades of exploitation, the effect of water injection development has been worse year by year. Comparatively speaking, CO₂ flooding has the advantages of low injection pressure and fast formation energy replenishment, and can obtain lower solvent/crude oil mobility ratio when miscible flooding is realized, which improves sweep efficiency and realizes geological storage of CO₂ while increasing production and tapping potential. Based on the establishment of CO₂ enhanced oil recovery and geological storage potential evaluation method, 272 oil layers in the low-permeability oil area of Dagang Oilfield are used as the evaluation objects, and the CO₂ enhanced oil recovery and geological storage potential in this area are analyzed.

2 Method

2.1 Numerical Simulation Calculation Models

The current CO₂ flooding enhanced recovery and geological storage numerical simulation calculation models mainly include four types: component model, black oil model, streamline model and split model. The advantage of the split model is that the three-dimensional problem is transformed into a one-dimensional flow problem, that

the data volume needs to be reduced, and the operation speed is faster. The leakage characteristics of the split model are simplified. Considering that Dagang Oilfield CO₂ flooding enhanced oil recovery and geological storage potential evaluation workload is large, detailed data is difficult to obtain, we adopted the split model.

According to the principle of conservation of mass, the following conservation equations are established:

$$\frac{\partial C_{ij}}{\partial t_D} + \frac{\partial F_{ij}}{\partial X_D} = 0 \quad (1)$$

$$C_{ij} = C_{i0}S_0 + C_{i1}S_1 + C_{i2}S_2 \quad (2)$$

$$F_{ij} = C_{i0}f_0 + C_{i1}f_1 + C_{i2}f_2 \quad (3)$$

Here, C_{ij} is concentration of component i in j phase; S_j is j phase saturation; i is component of fluid; $i = 0$ is water component; $i = 1$ is crude oil component; $i = 2$ is injection gas component; t is time; X is length distance; f is split flow; D represents dimensionless.

Based on the traditional model, the calculation model considers the following main influencing factors in combination with the characteristics of Dagang oilfield reservoir: (1) viscous fingering and heterogeneity; (2) gas injection gravity differentiation; (3) introducing the minimum miscibility pressure calculation method to define the state of CO₂ flooding phase; (4) the difference of area sweep coefficient between miscible flooding and immiscible flooding; (5) the influence of interfacial tension effect on relative permeability change.

From this model, the CO₂ flooding enhanced oil recovery range can be determined, and the amount of CO₂ storage in the reservoir can be calculated from the following formula.

$$M_{CO_2t} = \rho_{CO_2r} \times [R_f \times A \times h \times \varphi \times (1 - S_{wi}) - V_{iw} + V_{pw}] \quad (4)$$

Here, M_{CO_2t} is CO₂ storage potential, t; ρ_{CO_2r} is CO₂ density in the formation, t/m³; R_f is oil recovery; A is reservoir area, m²; h is reservoir thickness, m; φ is reservoir porosity; S_{wi} is reservoir irreducible water saturation; V_{iw} is injected water volume, m³; V_{pw} is produced water volume, m³.

2.2 Model Reliability Analysis

Based on the CO₂ flooding enhanced recovery calculation model, a numerical simulation calculation program was developed. The program runs fast and the calculation results show that the reservoir engineering theory can be effectively reflected. Taking the typical reservoir of Dagang Oilfield as the research object, as shown in Fig. 1, the calculation results of the calculation software using this study are close to the calculation results of the commercial software Eclipse, and the difference between the two is within 10%, and the precision is high.

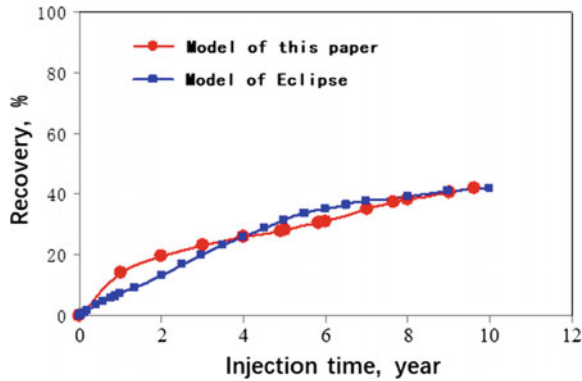


Fig. 1 The calculation results of this study and the commercial software Eclipse

2.3 Analysis of Influencing Factors

2.3.1 Influence of Reservoir Thickness

As shown in Fig. 2, as the thickness of the reservoir increases, the recovery of crude oil decreases. Mainly because the greater the thickness, the gravity differentiation causes the sweep volume coefficient to decrease.

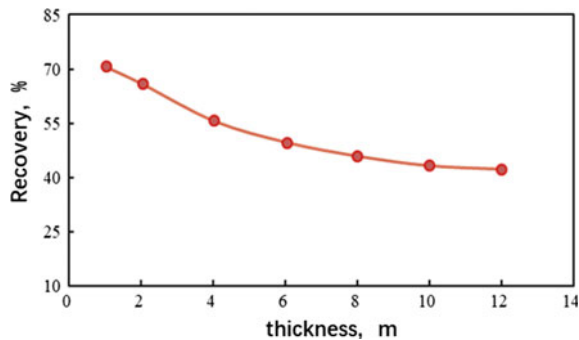


Fig. 2 Relationship between recovery factor and thickness

2.3.2 Influence of Reservoir Heterogeneity

As shown in Fig. 3, as the heterogeneous coefficient increases, the gas injection process leads to the intrusion of gas, and the volume coefficient of the sweep decreases, which in turn reduces the recovery factor.

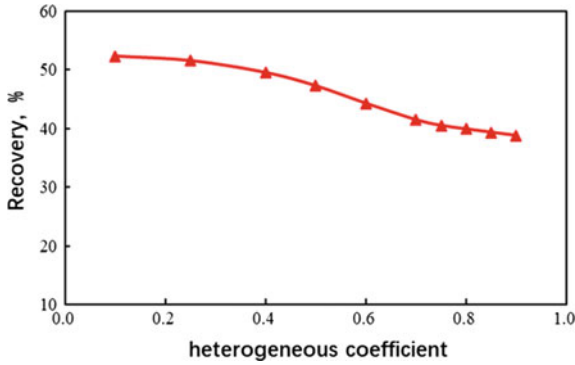


Fig. 3 Relationship between recovery factor and heterogeneous coefficient

2.3.3 Influence of Reservoir Crude Oil Viscosity

As shown in Fig. 4, as the viscosity of the crude oil decreases, the flow performance of the crude oil becomes better, the relative permeability of the oil phase increases, and the recovery factor increases exponentially.

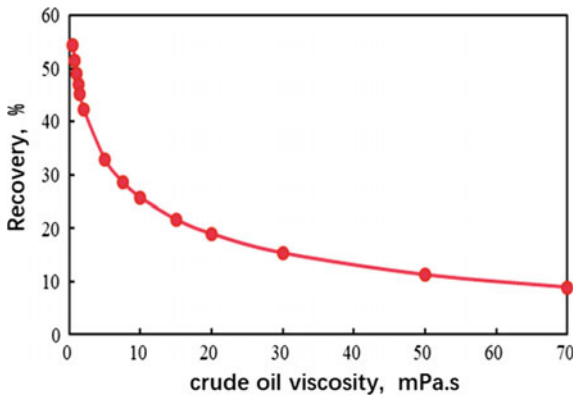


Fig. 4 Relationship between recovery factor and crude oil viscosity

2.3.4 Influence of Reservoir Oil Saturation

As shown in Fig. 5, as the oil saturation increases, the recovery factor has an upward trend with a large increase. It indicates that the better the oil bearing of the reservoir, the better the development of gas flooding.

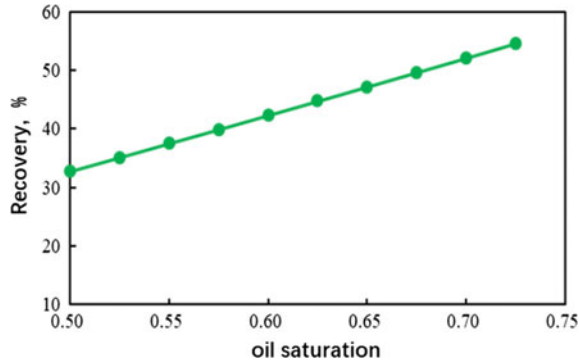


Fig. 5 Relationship between recovery factor and oil saturation

2.3.5 Influence of Reservoir Permeability

As shown in Fig. 6, as the reservoir permeability increases, the recovery rate increases, but when the permeability reaches a certain level, it is prone to gas enthalpy, resulting in a downward trend in oil recovery.

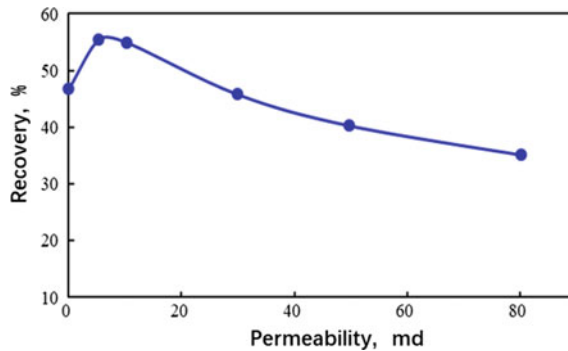


Fig. 6 Relationship between recovery factor and permeability

Based on the above analysis, the sensitivity rankings of factors affecting CO₂ flooding enhanced oil recovery are: crude oil viscosity > permeability > oil saturation > heterogeneity > reservoir thickness.

3 CO₂ EOR and Storage Potential Evaluation

3.1 Evaluation Process

We designed and developed the software, including four basic modules: basic data input, solution design, simulation calculation analysis, and report output. Based on the

software, CO₂ flooding and geological storage potential evaluation can be performed through the process shown in Fig. 7.

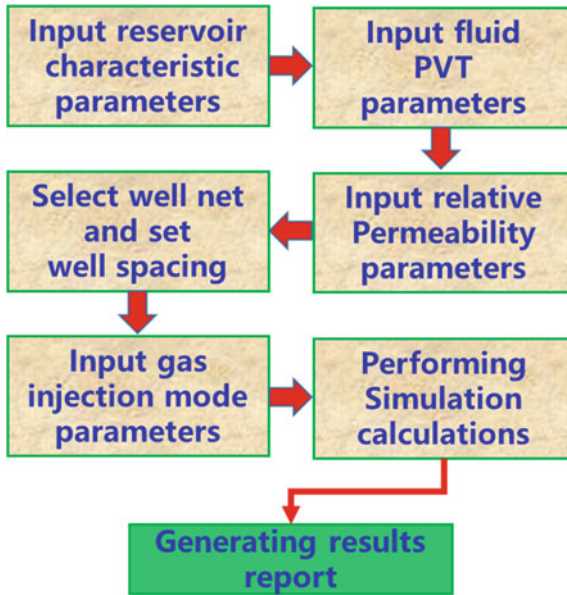


Fig. 7 Potential evaluation process

3.2 CO₂ EOR and Storage Potential Evaluation

3.2.1 CO₂ EOR Potential Evaluation

Through the evaluation of the potential of CO₂ flooding enhanced recovery in the low-permeability reservoirs developed in Dagang Oilfield, the results show that the geological reserves of the miscible flooding are great potential, and the number of miscible flooding blocks is 16. These low-permeability reservoirs can enhance oil recovery by 8.6% by CO₂ flooding, of which the average miscible flooding can be increased by 15.5%, and the average of immiscible flooding can be improved. 5.6%.

The evaluation results of the CO₂ flooding enhanced oil recovery potential of the undeveloped low-permeability reservoirs in Dagang Oilfield indicate that 144 blocks can achieve miscible flooding, accounting for the total amount. 65%. These low-permeability reservoirs can enhance oil recovery by an average of 9.9% by CO₂ flooding, of which the average recovery of miscible flooding is 12.3%, and the average of immiscible flooding increased oil recovery by 5.4%.

3.2.2 CO₂ Storage Potential Evaluation

Figures 8 and 9 show the results of CO₂ geological storage potential of 272 oil layers in the low-permeability oilfield of Dagang Oilfield. Figure 8 shows the CO₂ geological storage potential of the miscible flooding area, and Fig. 9 shows the CO₂ geological storage potential of the immiscible flooding area.

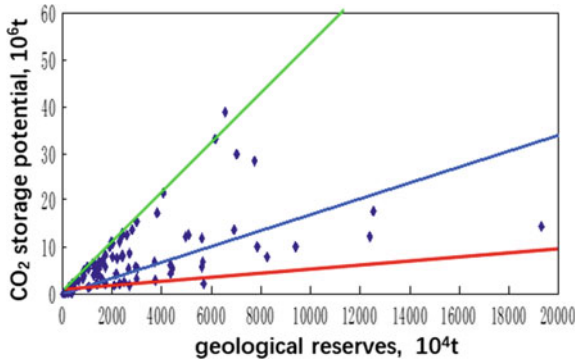


Fig. 8 Storage potential of miscible flooding area

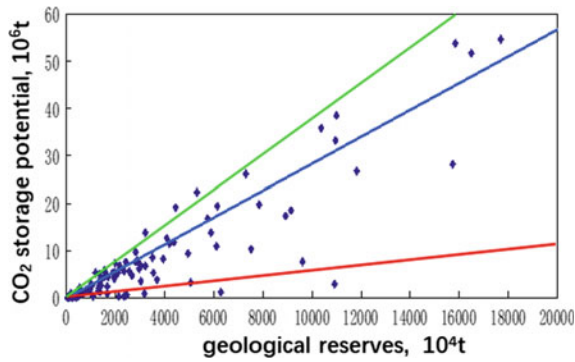


Fig. 9 Storage potential of immiscible flooding area

Shen Pingping et al. [9] predict storage potentials as below:

$$M_{CO_2t} = R_{CO_2} \cdot N \quad (5)$$

In which, M_{CO_2t} is CO₂ storage potentials, t; R_{CO_2} is sequestration storage coefficient, dimensionless; N is geological reserves, t.

According to the formula (5), the sequestration storage coefficients of Figs. 8 and 9 can be obtained. Here, we divide the sequestration storage coefficients into three levels of the highest value, the median value and the lowest value, as shown in Table 1.

Table 1 Sequestration storage coefficients

Values	Miscible area	Immiscible area
The highest value	0.50	0.41
The median value	0.17	0.28
The lowest value	0.06	0.06

4 Conclusion

- (1) This paper establishes a method for evaluating the enhanced recovery and storage potential of CO₂ flooding in actual reservoirs of Dagang Oilfield. This method can effectively evaluate CO₂ flooding and geological sequestration potential of low permeability reservoirs in similar oilfields.
- (2) By evaluating the CO₂ flooding potential of low-permeability reservoirs in Dagang Oilfield, the results show that Dagang Oilfield has a huge potential for CO₂ flooding to enhance oil recovery.
- (3) By evaluating the geological storage potential of CO₂ flooding in low-permeability reservoirs in Dagang Oilfield, the results show that Dagang Oilfield has a considerable amount of CO₂ geological storage, and the highest sequestration storage coefficients can reach 0.5.

Acknowledgements. At the completion of the article, I would like to thank Professor Liao Xinwei of China University of Petroleum (Beijing). We thank the supports from Chinese National Major Science and Technology Projects (2017ZX05009004-005) and Chinese National Major Science and Technology Projects (2017ZX05030002-005). We also thank the help of experts from Dagang Oilfield for their correlation study.

References

1. Robl, F.W., Emanuel, A.S., Van Meter, O.E.: The 1984 Natl. petroleum council estimate of potential EOR for miscible processes. *J. Pet. Technol.* **20**(8), 875–882 (1986)
2. Taber, J.J., Martin, F.D., Seright, R.S.: EOR screening criteria revisited—part 1: introduction, to screening criteria and enhanced recovery field projects. *SPE Reserv. Eng.* **12**(3), 189–198 (1997)
3. Stevens, S.H., Kuuskraa, V.A., Taber, J.J.: Sequestration of CO₂ in depleted oil and gas fields: barriers to overcome in implementation of CO₂ capture and storage (disused oil and gas fields). IEA, USA (1999)
4. Winter, E.M., Dergman, P.D.: Availability of depleted oil and gas reservoirs for disposal of carbon dioxide in the United States. *Energy Convers. Manag.* **34**(6), 1177–1187 (2001)
5. Bradshaw, J., Bachu, S.: Screening, evaluation, and ranking of oil reservoirs suitable for CO₂-flood EOR and carbon dioxide sequestration. *J. Can. Pet. Technol.* **41**(9), 51–61 (2002)
6. Bachu, S., Stewart, S.: Geological sequestration of anthropogenic carbon dioxide in the Western Canada sedimentary basin: suitability analysis. *J. Can. Pet. Technol.* **41**(2), 32–40 (2002)
7. Kovseck, A.R.: Screening: criteria for CO₂ storage in oil reservoirs. *Pet. Sci. Technol.* **20**(7–8), 841–866 (2003)
8. Bachu, S., Shaw, J.: Evaluation of the CO₂ sequestration capacity in Alberta's oil and gas reservoirs at depletion and the effect of underlying aquifers. *J. Can. Pet. Technol.* **42**(9), 31–41 (2003)
9. Bachu, S., Shaw, J., Robert, M.: Estimation of oil recovery and CO₂ storage capacity in CO₂ EOR incorporating the effect of underlying aquifers. *SPE*, 89340 (2004)

10. Bradshaw, J., Bachu, S., Bonijoly, D., et al.: A taskforce for review and development of standards with regards to storage capacity measurement. <http://www.cslforum.org/documents/TaskforceStorageCapacityEstimationVersion2.pdf> (2005)
11. Bradshaw, J., Bachu, S., Bonijoly, D., et al.: Estimation of CO₂ storage capacity in geological media. <http://www.cslforum.org/documents/PhaseIIReportStorageCapacityMeasurementTaskForce.pdf> (2007)
12. Bradshaw, J., Bachu, S., Bonijoly, D., et al.: Comparison between methodologies recommended for estimation of CO₂ storage capacity in geological media. <http://www.cslforum.org/documents/PhaseIIIReportStorageCapacityEstimationTaskForce0408.pdf> (2008)
13. Shen, P., Liao, X., Liu, Q.: Methodology for estimation of CO₂ storage capacity in reservoirs. *Pet. Explor. Dev.* **36**(2), 216–220 (2009)