

## Application of a Geomechanical Model to Wellbore Stability Analysis: A Case Study X-Well, Bach Ho Field in Vietnam

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**Abstract.** Selection of proper failure criterion is one of the most important task in analyzing wellbore stability analysis. While the Mohr-Coulomb criterion is still commonly used, its prediction of the safe mud weight supporting the wellbore wall is usually too high because this zone is predicted to yield without any shear failure around the borehole. The main purpose of the paper is to discuss pros and cons of some existing criteria such as Mohr-Coulomb, Hoek-Brown and modified Lade failure criterion. Then the allowable drilling mud pressures calculated by using these methods are compared with each other and with the field data. Two wellbores in two Bach Ho oilfields are considered as case studies in order to identify the criterion that is able to provide the closest agreement with the field data.

Keywords: Wellbore stability  $\cdot$  Geomechanical models  $\cdot$  Bach Ho field

## 1 Introduction

Geomechanical model is used for well design process in petroleum exploration and production in Vietnam. The aim of this application is to prevent well problems during drilling or production such as breakout, mud loss, lost circulation, wellbore collapse and drilling cost reduction. In well trajectory design, engineers based on various calculation models [1] which is similar with wellbore stability analysis in minimum mud weight determination by using failure analysis rock. Generally these applications require several geomechanical parameters, for instance well condition (azimuth angle, inclination angle), in-situ stress (vertical, horizontal stress), rock mechanical properties (poisson's ratio, cohesion, internal friction angle, uniaxial compressive strength UCS, TWC external collapse). In some cases, non-destructive strength tests is essential solution of rock properties determination with the indicators of rock detected by logging tools (gamma Ray GR, density, sonic compressional transit time DTCO, and sonic shear transit time DTSM logs).

In terms of wellbore stability analysis, there are there important parameters should be stated: reasonable mud weight (MW), drilling fluid inhibition and sealing ability with several impact factors such as in situ stresses, pore pressure, rock strength, drilling operation. In the present paper, we consider only the mud weight selection which can result to shear failure around the wellbore, as a result there is hole enlargement or breakout, washout, even hole-collapse. There are a number of published geomechanical models, rock mechanical properties estimation. These results are developed for particular rock type, age, depth range, field or even a basin while their applications to another rock may not reliable. This paper first will present briefly analytical solution for wellbore stability, and then a specific case study application for X-well of Bach Ho field in Vietnam.

# 2 Analytical Solution for Wellbore Stability of a Deviated Well

#### 2.1 Stress Distribution Around a Wellbore

The rock material is generally assumed as a continuous homogeneous and isotropic porous media.

$$\sigma_{r} = P_{w}$$

$$\sigma_{\theta} = \sigma_{H} + \sigma_{h} - 2(\sigma_{H} - \sigma_{h})\cos 2\theta - P_{w}$$

$$\sigma_{z} = \sigma_{v} - 2v(\sigma_{H} - \sigma_{h})\cos 2\theta$$

$$\tau_{\theta z} = \tau_{r\theta} = \tau_{rz} = 0$$

$$\sigma_{r} = P_{w}$$

$$\sigma_{\theta} = (\sigma_{v} + \sigma_{h}) - 2(\sigma_{v} - \sigma_{h})\cos 2\theta - P_{w}$$

$$\sigma_{z} = \sigma_{H} - 2v(\sigma_{v} - \sigma_{h})\cos 2\theta$$

$$\tau_{\theta z} = \tau_{r\theta} = \tau_{rz} = 0$$
(1)

Figure 1 illustrates the stress distribution around a deviated well path subjected to in-situ on different coordinate systems, which was reported in [2].

The stress components at the boundary of the plane-strain problem can be expressed in the follow equation for vertical and horizontal well respectively.

#### 2.2 Rock Failure Criteria

Well design process generally requires a careful selection of rock failure criterion. The common criterion used for wellbore stability analysis is the Mohr-Coulomb criterion (Eq. 1) [3]. However this criterion involves only the maximum principal stress and the minimum principal stress, and so the intermediate stress has no influence on rock strength. There was some new proposed criteria to ameliorate this disadvantage but the determination of parameters were complicate. This paper mainly focuses on two criteria



Fig. 1. Stress coordinate transformation around wellbore [2]. (a) deviated well trajectory under in-situ stress; (b) coordinate conversion for deviated well.

named Hoek-Brown and Modified Lade, which are summarised in the Eqs. (4) and (5) respectively.

$$\sigma_1 = UCS + K_p \sigma_3 \tag{3}$$

$$\sigma_1 = \sigma_3 + \sqrt{mC_0\sigma_3 + sC_0^2} \tag{4}$$

$$P_{w} = \left(B - C^{1/2}\right)(2A)$$

$$A = \sigma_{z} + S + P_{0}$$

$$B = A\sigma_{\theta d} - \sigma_{\theta z}^{2}$$

$$D = \left(\sigma_{\theta d} + \sigma_{z} + 3S - 3P_{0}\right)^{3}/(27 + \eta)$$

$$C = B^{2} - 4A\left\{D - \left(S - P_{0}\right)\left[A(\sigma_{\theta d} + S - P_{0}) - \sigma_{\theta z}^{2}\right]\right\}$$
(5)

Where:  $\sigma_r$ ,  $\sigma_\theta$ ,  $\sigma_z$ ,  $\tau_{\theta z}$ ,  $\tau_{r\theta}$ ,  $\tau_{rz}$ ,: stress components in cylindrical coordinate;  $\sigma_v$ ,  $\sigma_H$ ,  $\sigma_h$ : in-situ principal stresses, vertical stress, major horizontal stress, minor horizontal stress respectively;  $\sigma_1$ ,  $\sigma_2$ ,  $\sigma_3$ : principal stresses; Pw: internal wellbore pressure;  $\theta$ : rotation angle;  $\tau_0$ ,  $\varphi$ : cohesion of the material, and angle of internal friction; *S*,  $\eta$ , *v*: material constants, Poison's ratio;  $K_p = \frac{1 + \sin \phi}{1 - \sin \phi}$ .

#### **3** Wellbore Stability Analysis and Discussions

Based on X-well data of Bach Ho field in Vietnam, the data shown in the Table 1 for the depth of TVD = 98,437 ft, vertical well, vertical stress  $\sigma_v = 822.56$  psi, horizontal stress ( $\sigma_H = 7236.31$  psi,  $\sigma_h = 6702.42$  psi), uniaxial compressive strength UCS = 4493.33 psi, pore pressure Pp = 4180.93 psi. The calculation of tangential stress shows in the Fig. 2. Since the tangential stresses with max value of approximately 9000 psi are lower than uniaxial tress strength of 9100,31 psi it could be concluded that there is no compressive damage around the wellbore.

Depth	D	98,437	ft
Stress	$\sigma_v$	8222.56	psi
	$\sigma_H$	7236.31	psi
	$\sigma_h$	6702.42	psi
Pore pressure	Рр	4180.93	psi
Cohension	с	1200	psi
Friction angle	$\phi$	0.53	radian
Poisson's ratio	v	0.22	
Uniaxial compressive strength	UCS	9100.31	psi
Mud pressure	Pw	6000	psi

Table 1. Principle stress at borehole and rock criteria



Fig. 2. Tangential stress for X-well, Bach Ho Field, Vietnam, at the depth TVD = 98,437 ft.

Regarding the wellbore stability problems, a number of running tests with the data in the Table 1 but the mud weight of this works is unknown. The task is to choose the mud weight which is below value in the Fig. 3 corresponding shear stress and in this paper we have considered all three criteria given in the Eqs. (3)–(5). The figure illustrates that the similar trend of change mud weight versus inclination angle of the well. Overall, the higher inclination angle of the well will requires the higher value of mud weight, exception azimuth angle of 90°. The lowest mud weight can be used is for vertical well for Mohr-Coulomb, Hoek Brown, and Modified Lade, around 7.6 lb/gal, 7.5 lb/gal, 6.1 lb.gal respectively, except the well with azimuth angle of 90° which has the lowest mud weight requirement for well inclination of 50°.

By contrast, the highest mud weight need to used is for horizontal well for three criteria. In addition, there is no different of mud weight can be used for two wells with azimuth angle of  $0^{\circ}$  and  $30^{\circ}$ . The results also show that wells which are drilled at azimuth angle of  $90^{\circ}$  require lowest mud weight for any well inclination compared to other cases of azimuth angle.



Fig. 3. Mud weight estimation versus wellbore inclination at four value of azimuth angles, corresponding three criteria Mohr-Coulomb, Hoek-Brown, and Modified Lade.

### 4 Conclusion

This paper has presented campaign test on stress distribution around wellbore and results of three rock failure criteria applied to a case study of X-well data in Bach Ho field, Vietnam. The following concluding remarks could be drawn from the study:

- There is no rock damage around wellbore
- Modified Lade predicts the lowest mud weight requirement while the Mohr-Coulomb gives the highest value
- Safest wellbore stability of drilled well at azimuth angle of 90°.

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