Parameter Study on Remediating Cr(VI) in Water Using Activated Charcoal

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Abstract. Commercial activated charcoal was investigated for removal of Cr(VI) from aqueous solutions. The effects of altering the initial Cr(VI) concentration, pH, contact time and amount of activated charcoal were studied. Maximum adsorption of Cr(VI) was achieved between pH 1–3 and after a contact time of 120 min. The percentage of Cr(VI) removed decreased from 99.99–90.83% when the initial Cr(VI) concentration was increased from 0.05–0.5 mg ml⁻¹ at pH 2 and 26 ± 2 °C. Various kinetic models such as pseudo first-order and pseudo second-order models were used to evaluate the mechanism of Cr(VI) adsorption on activated charcoal. The Cr(VI) removal process was found to be governed by second-order kinetics and the rate constant of the adsorption (k₂) was 0.1800 g kg⁻¹ min⁻¹ for an initial Cr(VI) concentration of 0.1 mg ml⁻¹. The adsorption of Cr(VI) was evaluated using Langmuir, Freundlich, and Temkin isotherms and their constants were determined. The maximum adsorption capacity obtained using the Langmuir isotherm model was 45.24 g kg⁻¹ at pH 2.

Keywords: Parameter \cdot Activated charcoal \cdot Adsorption \cdot Water \cdot Cr(VI)

1 Introduction

All over the world industry is forced to diminish down to acceptable level contents of heavy metal in water and industrial waste waters. Conventional methods like precipitation are a favorable especially when dealing with large volume of matter which contains heavy metal ions in low concentration. Typically these ions are precipitated as hydrated metal oxides or hydroxides using calcium oxide. Precipitation is accompanied by flocculation or coagulation, and one major problem is the formation of large amounts of sediments containing heavy metal ions. In recent years, considerable attention has been devoted to fine new adsorbents. One of the suitable methods for removing heavy metals from water and waste water is using surface adsorption process.

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Activated carbon is the most widely used adsorbent for this purpose because it has a high capacity for adsorption of organic matter, but its use is limited because of its high cost (Battacharya and Venkobachar 1984; Khare et al. 1987). This has led to search for cheaper substitutes. Coal, fly ash, wood, silica gel, clay materials (bentonite, mont-morillonite, etc.), agricultural wastes (bagasse pith, maize cob, coconut shell, rice husk, etc.), and cotton wastes have been tried with varying success for metal ions removal (Mande Seyf-Laye et al. 2009; Singh and Rawat 1994; Theng and Wells 1995).

The objective of this study was to investigate the use of activated charcoal as an adsorbent material for removing Cr(VI) from wastewater.

Batch experiments were carried out for kinetic studies on the removal of Cr(VI) from aqueous solutions. The influence of various important parameters such as the pH, contact time, adsorbent amount, and initial Cr(VI) concentration were investigated by varying any one of the process parameters and holding the other parameters constant. The Langmuir and Freundlich equations were used to fit the equilibrium isotherm models. Pseudo first-order and second-order kinetic models were used to evaluate the mechanism of adsorption.

2 Experimental

Commercial activated carbon in granular form (CAC) (Table 1) was obtained from Sinopharm Chemical Reagent Co. Ltd (Beijing, China) and crushed and sieved to a particle size of 450 µm. A Cr(VI) stock solution (1 mg.ml⁻¹) was prepared by dissolving 99.9% K₂Cr₂O₇ (2.8287 g) in distilled water (1 L). This solution was diluted as required to obtain 0.05–0.5 mg.ml⁻¹ Cr(VI) standard solutions. The initial pH of the solution was adjusted using either 0.5 M NaOH or 0.5 M H₂SO₄. The batch experiments were carried out in 100 ml conical flasks by agitating a pre-weighed amount of the activated charcoal with 50 ml of the aqueous Cr(VI) solution for a predetermined period of time (based on prior kinetic studies) at 26 ± 2 °C on a water bath-mechanical shaker (198 rpm). The effect of altering the initial pH was studied with 0.05 mg.ml⁻¹ Cr(VI). The effect of altering the contact time was studied with 0.1-0.4 mg.ml⁻¹ Cr(VI) solutions at pH 2. Experiments were also conducted to investigate the effect of varying the amount of activated charcoal from 2-24 g.L⁻¹ with a Cr(VI) concentration of 0.250 mg.ml⁻¹ at pH 2. Adsorption isotherm studies were carried out with the different standard solutions $(0.05-0.5 \text{ mg.ml}^{-1} \text{ Cr}(\text{VI}))$ while maintaining the adsorbent dosage at 10 g.L⁻¹ and the pH at 2. An UV-visible spectrophotometer was employed with 1,5-diphenylcarbazide in acid medium to determine the concentrations of Cr(VI) remaining in the sample. The absorbance of the purple-violet colored solution was recorded at 540 nm. The filtrate was analyzed for the remaining Cr(VI) concentration. The amount of Cr(VI) adsorbed (g kg⁻¹) at time t was calculated using Eq. (1):

$$q_t = \frac{C_0 - C_t}{m_s} \times V \tag{1}$$

Langmuir isotherm						
Linear regression equation	q _m	b	R ²			
Ce = 0.0221Ce + 0.0727	45.25	0.3039	0.9800			
Freundlich isotherm						
Linear regression equation	K _f	n _f	\mathbb{R}^2			
$\log q_e = 0.2259 \log Ce + 1.2139$	16,364	0.2259	0.9886			

Table 1. Linear regression equations, coefficients of determination (R^2) and isotherm constants for the Freundlich and Langmuir isotherm models for adsorption of Cr(VI) by activated charcoal.

Where C_0 and C_t are the Cr(VI) concentrations in g L⁻¹ at time 0 and time t, respectively, V is the volume of the Cr(VI) solutions in L, and m_s is the weight of activated charcoal in kg.

3 Results and Discussion

3.1 Effect of Initial PH

The percentage of Cr(VI) adsorbed by activated charcoal decreased from 99.9–39.54% when the pH was increased from 1–7 (Fig. 1). The maximum percent removal of Cr (VI) was obtained between pH 1–3, and therefore pH 2 was selected for the rest of the experiments. Chromium exists mostly in two oxidation states which are Cr(VI) and Cr(III) and the stability of these forms is dependent on the pH of the system (Cimino et al. 2000; Selomulya et al. 1999; Shama and Forster 1994). It is well known that the dominant form of Cr(VI) at pH 2 is $HCrO_4^-$. Increasing the pH will shift the concentration of $HCrO_4^-$ to other forms; CrO_4^{2-} and $Cr_2O_7^{2-}$. Maximum adsorption at pH 1.0 indicates that it is the $HCrO_4^-$ form of Cr(VI), which is the predominant species between pH 1 and 4, which is adsorbed preferentially on the activated charcoal.

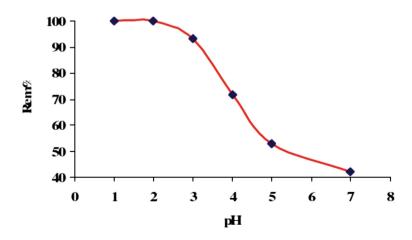


Fig. 1. Effect of initial pH on the percentage of Cr(VI) adsorbed by activated charcoal (10 g L^{-1}) at a Cr(VI) concentration of 0.05 mg ml⁻¹.

3.2 Effect of Contact Time

The contact time was found to be an important parameter for the adsorption of Cr(VI) on activated charcoal (Fig. 2). Over the first 20 min the percent removal of Cr(VI) from the aqueous solution increased rapidly and reached 60.21-97.43% (for 0.4–0.1 mg. ml⁻¹ Cr(VI) solutions. After this the percent removal tapered off until at 120 min it reached 99.76% and 90.83% for solutions containing 0.1 and 0.4 mg.ml⁻¹ of Cr(VI), respectively. Further increase in the contact time had a negligible effect on the percent removal. Therefore, a contact time of 120 min was used for Cr(VI) adsorption on activated charcoal in all the batch studies.

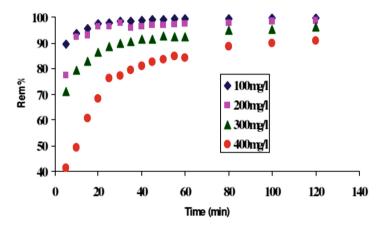


Fig. 2. Effect of contact time on the percentage of Cr(VI) adsorbed by activated charcoal (10 g L⁻¹) at pH 2 for solutions with different initial Cr(VI) concentrations (0.1–0.4 mg.ml⁻¹).

3.3 Effect of Initial Cr(VI) Concentration

When the initial Cr(VI) concentration was varied from 0.05–0.5 mg.ml⁻¹, the percentage of Cr(VI) removed decreased from 99.99–88.21% (Fig. 3). However, the absolute amount of Cr(VI) removed per unit mass of activated charcoal (or absorption capacity) significantly increased from 4.99–44.10 g.kg⁻¹ with the increase in initial Cr (VI) concentration.

3.4 Effect of Adsorbent Amount on Cr(VI) Removal

When the amount of activated charcoal was increased from 2–24 g L^{-1} , the percentage of Cr(VI) removed increased from 56–99.44% (Fig. 4). The amount of activated charcoal selected for subsequent experiments was 10.0 g L^{-1} as above this amount the removal of Cr(VI) remained stable.

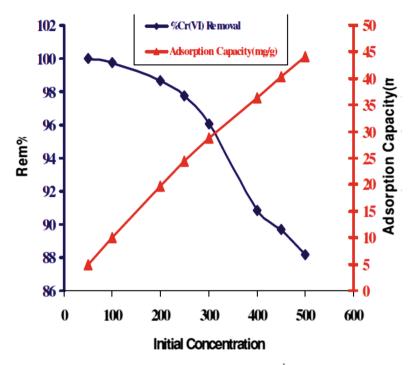


Fig. 3. Effect of initial Cr(VI) concentration $(0.05-0.5 \text{ mg.ml}^{-1})$ on the absorption capacity and percentage of Cr(VI) adsorbed by activated charcoal (10 g L⁻¹) at pH 2 with a contact time of 120 min.

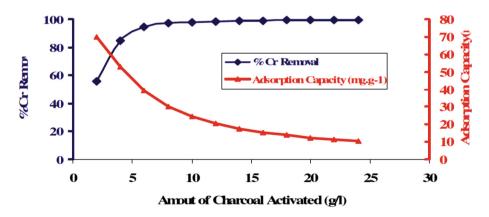


Fig. 4. Effect of the amount of activated charcoal on the percentage of Cr(VI) adsorbed at an initial Cr(VI) concentration of 0.250 mg.ml⁻¹, a contact time of 120 min, and pH 2.

3.5 Adsorption Isotherm

The equilibrium of adsorption is an important physicochemical parameter for evaluation of the adsorption process. The adsorption isotherm (q_e versus C_e) obtained in this study showed that the adsorption capacity (g kg⁻¹) increased with increasing equilibrium Cr(VI) concentrations (C_e) and eventually attained a constant value (Fig. 5).

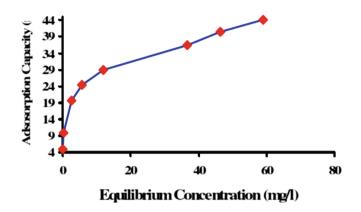


Fig. 5. Adsorption isotherm obtained for Cr(VI) absorption by activated charcoal (10 g/l) at initial concentrations (0.05, 0.1, 0.2, 0.25, 0.3, 0.4, 0.45, 0.5 mg ml), pH 2 and contact time 120 min.

To model the adsorption behavior, three adsorption isotherms were studied and their correlation with the experimental data was assessed. These included the Freundlich and Langmuir isotherms, which are the earliest and simplest known relationships describing the adsorption equation (Muhamad et al. 1998; Jalali et al. 2002). Table 1 shows the adsorption capacities of various adsorbents. It is clear from this table that the adsorption capacity of the commercial activated carbon used in this study far exceeded that of other activated carbons prepared from different materials.

• Langmuir isotherm

The linear form of the Langmuir equation is shown in Eq. (2) (Bulut and Aydin 2006; Langmuir 1996; Ravikumar et al. 2007).

$$\frac{C_e}{q_e} = \frac{1}{bq_m} + \frac{C_e}{q_m} \tag{2}$$

Where *b* and q_m are constants related to the apparent energy of adsorption and the adsorption capacity, respectively; and q_e is the amount adsorbed per unit mass of the adsorbent (g kg⁻¹) with an equilibrium concentration of C_e (mg ml⁻¹). A plot of (C_e/q_e) vs. C_e was linear and the constants q_m and *b* were determined from the slope and intercept of the plot (Table 3). The correlation coefficient obtained with the Langmuir equation was high ($R^2 = 0.98$), which indicated a good fit between the

parameters. The dimensionless parameter ($R_L = 1/1 + bC_0$), which is a measure of adsorption favorability, was found to be in the range of 0.00653–0.06174 ($0 < R_L < 1$) and confirmed that Cr(VI) removal using activated charcoal at pH 2 and 26 ± 2 °C was a favorable adsorption process.

• Freundlich isotherm

The Freundlich isotherm is expressed by Eq. (3) (Freundlich 1906)

$$q_e = K_f C_e^{n_f} \tag{3}$$

Where K_f (g^{1-1/n} l^{1/n} kg⁻¹) is the Freundlich constant, which indicates the relative adsorption capacity of the adsorbent related to the bonding energy, and n_f is the heterogeneity factor representing how the absorption deviates from linearity. Values of n_f less than one are an indication that significant adsorption takes place at low concentration, while high K_f values indicate greater adsorption intensity. The linear form of the Freundlich isotherm is Eq. (4):

$$logq_e = logK_f + n_f logC_e \tag{4}$$

The Freundlich coefficients were determined from a plot of log q_e versus log (C_e) and are given in Table 2. The Freundlich model clearly agreed very well with the experimental data.

Co (mg/L)	qe (g kg^{-1})	Pseudo first-order			Pseudo second-order		
		kinetics model			kinetics model		
	(Experimental)	k ₁	q _e	R ²	k ₂	q _e	R ²
100	9.97	0.0199	0.77	0.9652	0.1800	10.02	1.000
200	19.73	0.0159	2.23	0.8456	0.0451	19.88	1.000
300	28.81	0.0155	7.06	0.9751	0.0141	29.32	0.9999
400	36.33	0.0172	21.2	0.9815	0.0032	38.75	0.9998

 Table 2. Kinetic constants for pseudo first-order and pseudo second-order models of the Cr(VI) adsorption by activated charcoal.

3.6 Adsorption Kinetics

Pseudo first-order kinetics

Kinetic modeling of the removal of Cr(VI) by activated charcoal was carried out using the well-known Lagergren model (Hameed 2009; Tabak et al. 2009).

$$\log(q_e - q_t) = \log q_e - k_{ad}t/2.303$$
(5)

Where q_e and q_t are the amounts of Cr(VI) adsorbed (g kg⁻¹) at equilibrium and time *t*, respectively, and k_{ad} (L min⁻¹) is the rate constant of the pseudo first-order adsorption operation.

A plot of log $(q_e - q_t)$ versus t was linear and represents the pseudo first-order kinetics for the removal of Cr(VI) using activated charcoal. The first-order rate constants k_1 and q_e were calculated for a range of initial Cr(VI) concentrations (0.1–0.4 mg L⁻¹) with a constant amount of activated charcoal (10 g L⁻¹) (Table 2). The regression correlation coefficient was in the range 0.97–0.982, which is good and shows the applicability of the pseudo first-order kinetic model to the removal of Cr(VI) using activated charcoal. The experimental values of q_e obtained using initial Cr(VI) concentrations of 100, 200, 300, and 400 mg L⁻¹ were 9.97, 19.73, 28.81, and 36.33 g kg⁻¹, respectively, which do not agree with the values predicted by the pseudo first-order model.

• Pseudo second-order kinetics

The pseudo second-order adsorption kinetic rate equation is expressed as Eq. (6) (Ho et al. 2000):

$$\frac{1}{(q_e - q_t)} = \frac{1}{q_e} + k_2 t \tag{6}$$

Where k_2 is the rate constant of pseudo second-order adsorption $(g kg^{-1} min^{-1})$. Equation (6) can be rearranged to obtain Eq. (7), which has the linear form:

$$\frac{t}{q_t} = \frac{1}{h} + \frac{1}{q_e}t\tag{7}$$

With $h (g kg^{-1} min^{-1})$, the initial adsorption rate, expressed by: Eq. (8)

$$h = k_2 q_e^2 \tag{8}$$

The plot of (t/q_t) and t of Eq. (9) was linear (Fig. 10), and q_e and k_2 were determined from the slope and intercept, respectively. Because pseudo first-order kinetics were not applicable to the adsorption of Cr(VI) on activated charcoal, the second-order kinetic model was evaluated. The calculated q_e values agreed with the experimental values, and the values obtained for the regression correlation coefficients were more than 0.9998. These results indicate that the kinetics of Cr(VI) adsorption using activated charcoal are explained better by a second-order kinetic model than a first-order one.

3.7 Comparison of Cr(VI) Removal with Different Adsorbents Reported in Literature

The adsorption capacities of the adsorbents for the removal of Cr(VI) have been compared with those of others reported in literature and the values of adsorption capacities have been presented in Table 3. The values reported areas in the form of

Absorbent	Adsorption capacities $(g kg^{-1})$	Reference	
Coconut tree sawdust	3.46	Selvi et al. 2001	
Rind of orange (Citrus sinensis), (L.) Osbeck	10.74	Poojari et al. 2015	
Sawdust	20.70	Bhattacharya et al. 2006	
Banana peels	24.61	Mande Seyf-Laye et al 2009	
Rice husk ash	25.64	Bhattacharya et al. 2006	
Clarified sludge	26.31	Bhattacharya et al. 2006	
Maize cob	28.57	Mande Seyf-Laye et al. 2009	
Leaf mould	43	Sharma and Forster 1994	
Commercial activated charcoal	45.24	Present work	

Table 3. Comparison of adsorption capacities $(g kg^{-1})$ of the adsorbents for the removal of Cr(VI) with those of other adsorbents

monolayer adsorption capacity. The experimental data of the present investigations are comparable with the reported values.

4 Conclusion

Activated charcoal has been successfully used to remove Cr(VI) from aqueous solution. The adsorption of Cr(VI) fitted well at low pH values, and the removal of Cr(VI) depended on the initial concentration, contact time and amount of activated charcoal. The Freundlich and Langmuir isotherm models agreed with the experimental data. Cr(VI) adsorption obeyed a second order rate equation, and the rate constant was found to be 0.0032 kg.g⁻¹ min⁻¹ with an initial Cr(VI) concentration 0.4 mg.ml⁻¹.

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