# Chapter 2 Fundamentals of Membrane Processes

In this chapter the common fundamentals of different membrane processes are described. In the first part a general description of the different membrane structures, such as porous and dense homogeneous or symmetric and asymmetric membranes, and their function is discussed. In the second part membrane materials such as inorganic, organic, and composite materials and their function in membrane bioreactors are described. Third, the preparation of synthetic membranes via the phase inversion method is described in detail. Finally, alternative techniques of membrane fabrication are presented.

# 2.1 Membrane Classification by Membrane Structure

Synthetic membranes display a broad range in their physical structure and the material they are made from (Strathmann [2011\)](#page-22-0). They can be classified according to their morphology, as shown in Fig. [2.1.](#page-1-0)

The first group is dense homogeneous polymer membranes. Usually they are prepared (i) from solution by solvent evaporation only or (ii) by extrusion of the melted polymer (Nunes and Peinemann [2006](#page-21-0)). However, dense homogeneous membranes only have a practical usefulness when they are made from a highly permeable polymer such as silicone. Commonly, the permeate flow across the membrane is quite low, since a minimal thickness is required to grant the membrane mechanical stability. The majority of membranes currently are porous or consist of a dense top layer on a porous structure (Mulder [1984,](#page-21-0) [1997;](#page-21-0) Nunes and Peinemann [2001;](#page-21-0) Strathmann et al. [2006\)](#page-22-0).

<span id="page-1-0"></span>

The second category is porous membranes, which can also be divided into two main groups. They are divided according to their pore diameter: microporous  $(d_p < 2$  nm), mesoporous  $(2 \text{ nm} < d_p < 50 \text{ nm})$  and macroporous  $(d_p > 50 \text{ nm})$ (Gallucci et al. [2011b](#page-18-0)).

The first groups of membranes are referred to as symmetric (isotropic) and the second type is referred to as asymmetric (anisotropic) membranes. Within the asymmetric membranes, there are several distinctly different structures including integrally skinned membranes (where the pore structure gradually changes from very large pores to very fine pores, essentially forming a "skin" on top of the membrane, giving rise to the name "integrally skinned"). Alternatively, the skin may be nonporous. A third, and industrially very important type of asymmetric membrane is the thin-film composite membrane, where a dense, selective, thin layer is deposited or polymerised at the surface/interface of a porous substrate.

Symmetric membranes refer to the membranes with uniform structure (uniform pore size or nonporous) throughout the entire membrane thickness (Buonomenna et al. [2011\)](#page-18-0). Symmetric membranes are used today mainly in dialysis, electrodialysis, and to some extent also in microfiltration (Strathmann [2000,](#page-22-0) [2011\)](#page-22-0). The thickness of symmetric membranes is usually between 30 and 500 µm. The total resistance of the mass transfer relies on the total thickness of the membranes. Hence, a decrease in membrane thickness results in an increased permeation rate.

Asymmetric membranes have a gradient in structure. They consist of a  $0.1-5 \mu m$ thick "skin" layer on a highly porous 100–300 µm thick structure (Strathmann [2011\)](#page-22-0). The skin represents the actual selective barrier of the asymmetric substructure. Its separation properties are thoroughly determined by the nature of the material or the size of pores in the skin layer. The porous substrate layer serves as a support for the mostly very thin top layer, or "skin" (relatively dense) and has little effect on the separation properties of the membrane or the mass transfer rate of the membrane (Strathmann [2011\)](#page-22-0). The dense surface layer is considered to be responsible for the membrane selectivity. Consequently, the controlled structure of the dense surface layer has become a serious concern in the membrane design (Zhenxin and Matsuura [1991](#page-24-0)). Also, the resistance to the mass transfer is mainly determined by the top layer (Buonomenna et al. [2011](#page-18-0); Nunes and Peinemann [2001\)](#page-21-0). Asymmetric membranes are primarily employed in pressure driven membrane processes such as reverse osmosis, ultrafiltration, gas separation and sometimes in microfiltration. High fluxes (high permeate flow per unit area), a reasonable mechanical stability providing very thin selective layer are the unique properties of asymmetric membranes (Strathmann [2011](#page-22-0); Nunes and Peinemann [2006](#page-21-0)). Two procedures are used to prepare asymmetric membranes: the first method is based on phase inversion process which leads to integral structure (Kesting [1971](#page-19-0)), The second method resembles a composite structure in a two-step process in which a thin barrier layer is deposited on a microporous substructure (Cadotte and Petersen [1981;](#page-18-0) Strathmann [2011\)](#page-22-0).

# 2.2 Membrane Materials

In general, there are three fundamentally different categories of membrane materials: Organic (polymeric), inorganic (ceramic) materials and biological materials. Organic materials are either cellulose—based or composed of modified organic polymers. By contrast, inorganic materials such as ceramics and metals are used in niche industrial applications but are usually cost-prohibitive in wastewater treatment. Biological membrane (bio membranes) is a selective barrier within or around a cell in a living organism. The biomembrane is capable of recognising what is necessary for the cell to receive or block for its survival. These membranes cannot meet the industrial requirements due to thermomechanical stability and productivity. It should be pointed out that, a large majority of membranes in research and commercial use are polymeric-based (organic membrane) as a result of their facile processing into viable membrane structures and the diverse polymers available, as well as the capability to synthesise novel polymer structures (Peyravi et al. [2012\)](#page-21-0). Recently, composite membranes and inorganic membranes have gained tremendous attention owing to their potentially high performance, long lifetime and even their availability that outweigh the benefits/advantages of using polymeric membranes.

### 2.2.1 Inorganic Membranes

Inorganic membranes posses excellent thermal and chemical stability in comparison to polymeric membranes and hive higher antifouling property due to the hydrophilic nature of in organic material (Gallucci et al. [2011a;](#page-18-0) Mulder [1997\)](#page-21-0). Nevertheless, there has been some limitation in their use despite their wide use and application. The main application of inorganic membranes in the past was enrichment of uranium hexafluoride  $U^{235}$  via Knudsen flow through porous ceramic membranes. Recently, many more applications are found in the field of ultrafiltration and microfiltration. Inorganic membranes are generally divided into four groups: glass membranes, ceramic membranes, metallic membranes, carbon membranes, and zeolitic membranes.

Metallic membranes can generally be obtained via the sintering of metal powders (e.g. stainless steel, molybdenum, or tungsten). According to (Gallucci et al. [2011a](#page-18-0)), the main materials for preparing metallic membranes are palladium and its alloys due to their high solubility and permeability of hydrogen. These membranes are employed for separation of hydrogen from gas mixtures and in the membrane reactor area for producing pure hydrogen (Lin [2001](#page-20-0)). These membranes have both advantages and disadvantages. The advantages are considerable mechanical strength and higher permeating flux (Gallucci et al. [2011a](#page-18-0)). The limitations of metallic membranes are (1) highly cost (very expensive) due to the low availability of palladium in nature and (2) surface poisoning, which is significantly more for thin metal membranes. There have been numerous studies reporting that the impact of poisons such as  $CO$  or  $H_2S$  on Pd-based membranes is a major problem. These gases  $(H<sub>2</sub>S$  or CO) adsorb on the palladium surface that block the dissociation sites for hydrogen. Therefore, these membranes have received limited attention today because they do not relate to MBR technology (Judd [2006](#page-19-0)).

Ceramic membranes are of great importance in separation technology as they have a higher chemical, thermal and mechanical stability compared to organic membranes (Belfer et al. [2000](#page-18-0)). This stability makes these UF or MF membranes suitable in different fields of industry such as (food, biotechnology and pharmaceutical applications). They have been proposed for gas separation and the application of membrane reactor. Ceramic membranes are prepared through the combination of a metal (e.g. aluminium, titanium, silicium or zirconium, zinc, tin, and iron) with a non-metal in the form of oxide, nitride, or carbide to form a variety of inorganic nanoparticles (fillers) such as carbon nanotubes, alumina, or aluminium oxide (Al<sub>2</sub>O<sub>3</sub>), titanium oxide (TiO<sub>2</sub>), zirconium dioxide or zirconia (ZrO<sub>2</sub>), zinc oxide (ZnO), Silver, tin oxide (SnO<sub>2</sub>), and Fe<sub>3</sub>O<sub>4</sub>. All these membranes have been used to fabricate inorganic—polymer composite membranes (Arthanareeswaran et al. [2008;](#page-17-0) Huang et al. [2006](#page-19-0); Jian et al. [2006](#page-19-0); Liang et al. [2012](#page-20-0); Yang et al. [2007;](#page-23-0) Zoppi and Soares [2002;](#page-24-0) Leo et al. [2013](#page-20-0); Celik and Choi [2011;](#page-18-0) Celik et al. [2011a,](#page-18-0) [b;](#page-18-0) Bae and Tak [2005a,](#page-17-0) [b](#page-17-0); Maximous et al. [2010;](#page-20-0) Gallucci et al. [2011a;](#page-18-0) Leo et al. [2012;](#page-20-0) Lu et al. [2005;](#page-20-0) Mulder [1997](#page-21-0); Rahimpour et al. [2008,](#page-21-0) [2009;](#page-21-0) Razmjou et al. [2011a,](#page-21-0) [b;](#page-21-0) Sawada et al. [2012;](#page-22-0) Yu et al. [2009a,](#page-23-0) [b;](#page-23-0) Livari et al. [2012;](#page-20-0) Moghimifar et al. [2014\)](#page-20-0). Sintering or sol–gel techniques are usually used to prepare ceramic membranes.

#### <span id="page-4-0"></span>2.2 Membrane Materials 17

Glass membranes can be regarded as ceramic membranes. Issues associated with ceramic membranes are the difficulties faced in proper sealing of the membranes in modules operating at high temperature, extremely high sensitivity of membranes to temperature gradient, leading to membrane cracking, and chemical instability of some perovskite-type materials (Gallucci et al. [2011a\)](#page-18-0). Glass membranes (silica,  $SiO<sub>2</sub>$ ) are generally prepared by leaching techniques.

Carbon membranes (also called carbon molecular sieve membranes CMS) have been regarded as a promising candidate for applications of gas (Gallucci et al. [2011a](#page-18-0)). CMS are porous solids membranes, containing constricted holes that are responsible for approaching the molecular dimensions of diffusing gas molecules. Therefore, molecules with different size can be efficiently separated through molecular sieving (Gallucci et al. [2008](#page-19-0)). CMS membranes can be prepared by pyrolysis of thermosetting polymers such as poly acrylonitrile (PAN), cellulose triacetate, phenol formaldehyde, and poly (furfural) alcohol.

Recently, a new class of membranes have been developed and studied, such as the zeolitic membranes. These membranes have a very narrow pore size and can be employed in gas separation, pervaporation and separation of ions from aqueous solution by reverse osmosis. These membranes have some limitations; first the main limitation is relatively low gas fluxes in comparison to other inorganic membranes. Second, its thermal effect, as noted by Cejka et al.  $(2007)$  $(2007)$ , the zeolite layer exhibits negative thermal expansion, in which the zeolite layer shrinks when the region temperature is high, but the support layer expands continuously, causing thermal stress issues for the attachment of the zeolite layer to the support and for the connection of the individual microcrystals within the zeolite layer.

Inorganic membranes have both advantages and disadvantages as presented in Table 2.1. The major advantages of inorganic membranes when compared with polymeric membranes, is their high chemical, thermal, and mechanical stability and wide tolerance to pH (Belfer et al. [2000;](#page-18-0) Gallucci et al. [2011a](#page-18-0)). They can operate at high temperatures. As a fact of matter, inorganic membranes are stable at

Advantages	Disadvantages
1. Long-term stability at high temperatures	1. High capital cost
2. Resistance to harsh environments (e.g. chemical degradation, pH, etc.)	2. Embrittlement phenomenon (in the case of dense) Pd membranes)
3. Resistance to high pressure drops	3. Low membrane surface per module volume
4. Inertness to microbiological degradation	4. Difficulty of achieving high selectivities in large-scale microporous membranes
5. Easy cleanability after fouling	5. Low permeability of the highly hydrogen selective (dense) membranes at low temperatures
6. Easy catalytic activation	6. Difficult membrane to module sealing at high temperature

Table 2.1 Advantages and disadvantages of inorganic membranes with respect to polymeric membranes (Gallucci et al. [2011a\)](#page-18-0)

temperatures ranging from 300 to 800  $^{\circ}$ C and in some cases, ceramic membranes usable over 1000  $\rm{^{\circ}C}$  (van Veen et al. [1996\)](#page-23-0). They also have a high resistance to chemical degradation. Judd et al. ([2004](#page-19-0)) stated that ceramic membranes did not foul substantially at fluxes up to 60 L  $m^{-2}$   $h^{-1}$ , whilst polymeric membranes fouled at a lower flux of 36 L m<sup>-2</sup> h<sup>-1</sup>. Applicability of inorganic membranes is of great interest in non—aqueous filtration due to stability in organic solvents (Tsuru et al. [2000a](#page-22-0), [b\)](#page-22-0). Despite their potential in waste water treatment, certain limitations deter membrane processes from large scale and continuous operation (Lee et al. [1999\)](#page-20-0). One of the major limitations arises from membrane fouling caused by different inorganic salts (Bhattacharjee and Johnston [2002\)](#page-18-0) which increases feed pressure, reduces permeate flux, decreases product quality and finally shortens membrane lifespan (Lee and Lee [2000](#page-20-0); Seidel and Elimelech [2002](#page-22-0)).

Another limitation of inorganic membranes that probably hampers their application is the high capital costs of both the manufacturing process and material (Gallucci et al. [2011a](#page-18-0)). Therefore, the inorganic membranes might be used only in some special applications such as anaerobic biodegradation (Fan et al. [1996](#page-18-0)) and high temperature waste water treatment (e.g. high-strength industrial waste) (Luonsi et al. [2002](#page-20-0); Scott et al. [1998\)](#page-22-0). Despite, the high expense of inorganic membranes and their susceptibility to membrane fouling, they are still a competitive product in many applications. It is expected that inorganic membranes will have more applications in the future. Table [2.1](#page-4-0) summarises the advantages and disadvantages of inorganic membranes over polymeric membranes.

# 2.2.2 Polymeric Membranes

Although polymer membranes are less resistance to high temperature and aggressive chemicals than inorganic or metallic membranes, they are still the most widely used materials in wastewater treatment applications. This is mainly owing to easy preparation, reasonable expense (low cost), high efficiency for removing dispersed oil, particles, and emulsified, small size, lower energy requirement, flexibility in membrane configuration, and relatively low operating temperature which is also associated with less stringent demands for the materials need in the construction of module (Buonomenna et al. [2011](#page-18-0); Nunes and Peinemann [2010\)](#page-21-0). Among many homopolymeric materials presented in Table [2.1,](#page-4-0) polyethersulfone (PES) is one of the most vital polymeric materials and is widely used in producing microfiltration (Li et al. [2008,](#page-20-0) [2009a](#page-20-0), [b](#page-20-0); Ulbricht et al. [2007](#page-22-0); Zhao et al. [2003a](#page-23-0), [b](#page-23-0); Shin et al. [2005;](#page-22-0) Liu and Kim [2011\)](#page-20-0), ultrafiltration (Chaturvedi et al. [2001;](#page-18-0) Marchese et al. [2003](#page-20-0); Xu and Qusay [2004](#page-23-0); Wang et al. [2006a](#page-23-0), [b,](#page-23-0) [c](#page-23-0)) as well as nanofiltration membranes (Boussu et al. [2006](#page-18-0); Ismail and Hassan [2007\)](#page-19-0), either on the laboratory or industrial scale (Razali et al. [2013\)](#page-21-0) Polyethersulfone (PES) has been recognised or acknowledged as a high performance polyaromatic polymer possessing toughness and thermal stability (Huang et al. [2012](#page-19-0); Li et al. [2004](#page-20-0); Shi et al. [2008;](#page-22-0) Shin et al. [2005;](#page-22-0) Zhao et al. [2013\)](#page-23-0).

PES is a thermoplastic polymer and is typically amorphous in nature and shows one prominent XRD peak at  $2\theta = 19.9^\circ$  (Nair et al. [2001;](#page-21-0) [Kumar](#page-20-0) et al. 2006; Guan et al. [2005](#page-19-0)). PES membranes show a high glass transition temperature (Tg  $\approx$  503 K). PES structure has a harder benzene ring and a softer ether bond; so crystalline properties can be expected (Barth et al. [2000;](#page-17-0) Ismail and Hassan [2007\)](#page-19-0). Additional properties include

- Good chemical resistance (inertness): PES exhibits excellent chemical resistance to aliphatic hydrocarbons, alcohols, and acids. It is also soluble in some aprotic polar solvents (Zhu et al. [2014\)](#page-24-0).
- Blood compatibility.
- Outstanding oxidative stability.
- Outstandingly high mechanical strength.
- Easy processing and environmental endurance.
- Wide temperature and pH tolerance.
- Moderate good chlorine resistance.
- Easy to fabricate membranes in a wide variety of modules and configurations as well as wide range of pore size available for UF and MF from 10 A to 0.2  $\mu$ m.
- PES also shows other good qualities such as good membrane forming properties.
- Commercially available and relatively inexpensive (Bolong et al. [2009\)](#page-18-0).

Polyethersulfone has been affirmed as the membrane material in many processes such as in biomedical fields for blood purification (haemodialysis and plasma collection) (Barzin et al. [2004;](#page-18-0) Samtleben et al. [2003;](#page-22-0) Tullis et al. [2002;](#page-22-0) Werner et al. [1995;](#page-23-0) Zhao et al. [2001;](#page-23-0) Unger et al. [2005\)](#page-23-0), hollow fibres (Khulbe et al. [2003](#page-19-0)) (Yang et al. [2007\)](#page-23-0), stable substrate for the deposition and thermal processing of semiconductor thin films (Nair et al. [2001](#page-21-0)), sensors applications [\(Gerlach](#page-19-0) et al. 1998), sterilisation and pharmaceutical (Baker [2012](#page-17-0); Song et al. [2000\)](#page-22-0), water purification, beverage filtration, protein separation, and pre-treatment of reverse osmosis (Bolong et al. [2009](#page-18-0); Yu et al. [2011\)](#page-23-0).

However, its main limitations is related to the relatively high hydrophobic property, which can lead to severe membrane fouling (Kim et al. [1999](#page-19-0); Van der Bruggen et al. [2002a,](#page-23-0) [b](#page-23-0)) owing to the adsorption of nonpolar solutes and hydrophobic particles or bacteria onto its surface (Khulbe et al. [2000](#page-19-0), [2010](#page-19-0); Koh et al. [2005](#page-19-0); Rahimpour and Madaeni [2010](#page-21-0)). This would lead to the gradual reduction of permeation flux, frequent membrane cleaning, impacting on the useable lifetime of the membrane and its applications (Daraei et al. [2013a](#page-18-0), [b](#page-18-0), [c](#page-18-0); Luo et al. [2005](#page-20-0); Yamamura et al. [2007a](#page-23-0), [b](#page-23-0); Zhao et al. [2013](#page-23-0); Rahimpour et al. [2011\)](#page-21-0). Therefore, achieving the desired surface properties without modification of the advantageous properties of PES membrane is a paramount goal for membrane researchers and industry.

Regarding of the preparation of PES membranes, (Zhao et al. [2013](#page-23-0)) stated that the structure of PES membranes is always symmetric and is prepared by phase inversion methods. The structure of PES membrane is affected by the composition

(e.g. concentration, solvent, and additives), temperature of PES solution, the nonsolvent or the mixture of nonsolvents, and the coagulation bath or even the environment (Barth et al. [2000\)](#page-17-0).

Many other polymeric materials can also be employed for fabricating membranes as explained schematically in Table [2.2](#page-8-0). This table illustrates some examples of polymeric materials used for microfiltration, ultrafiltration, reverses osmosis, and some membrane processes.

Recently, copolymer is another important polymeric material in the manufacture of membranes. It is gaining more attention by a number of researchers. The copolymers are composed of at least two different types of structural units with different properties. The properties of copolymers rely on the properties of the units that are connected in the polymer and their relative proportions. Hence, polymers that are employed for the preparation of membrane and require different properties can be copolymerised carefully by selecting various polymeric units. To date, many membranes with high performance have been fabricated by different copolymers with different molecular structures (for example, block copolymers: poly (ethylene oxide)–polysulfone block copolymer (Hancock et al. [2000\)](#page-19-0), graft copolymers: poly (ethylene glycol)-graft-polyacrylonitrile copolymer (Su et al. [2009b\)](#page-22-0), and so on.

## 2.2.3 Composite Membranes

Composite membranes are often referred to as thin-film composite (TFC) membranes and they have received tremendous attention in recent years for desalination of brackish and sea water, waste water reclamation, and the separation and purification of chemical and biological products (Buch et al. [2008\)](#page-18-0). TFC membranes are composed of at least two layers (with different (polymeric) materials), with a very selective membrane material being deposited as a dense ultrathin layer formed upon a more or less porous support layer (sublayer), which usually is an ultrafiltration membrane and serves as support as shown in Fig. [2.2](#page-10-0) (Strathmann [1989;](#page-22-0) Wu [2012](#page-23-0)). The advantage of TFC membranes is each layer (i.e. top selective layer and bottom porous substrate) is thoroughly optimised and controlled independently to achieve the desired selectivity and permeability while presenting excellent compression resistance and mechanical strength (Jahanshahi et al. [2010;](#page-19-0) Lau et al. [2012](#page-20-0); Rahimpour [2011;](#page-21-0) Kosaraju and Sirkar [2008](#page-19-0)). The porous support layer (bottom layer) is generally prepared through phase inversion method. On the other hand the top selective layer is prepared from elastomer, which is hard to prepare it through phase inversion method. The first generation TFC membranes were prepared by pouring a thin layer of polymer solution on a liquid of water or mercury (Mulder [1997\)](#page-21-0). Numerous coating procedures have been used to prepare TFC membranes, including plasma polymerisation, dip coating, in situ polymerisation, and interfacial polymerisation. These techniques will be discussed in this chapter.

<span id="page-8-0"></span>

Table 2.2 Overview of polymeric materials used for membranes, the type of membranes formed and the membrane processes they are used in Ulbricht



 $\overline{\phantom{a}}$ 

Table 2.2 (continued)

<span id="page-10-0"></span>

Fig. 2.2 Examples of the preparation of composite membranes by interfacial polymerization (Mulder [1997](#page-21-0))

Another type of procedure used to prepare composite membranes, is the coating layer, which plugs the pores in the sublayer. In this procedure, the unique characteristics of the sublayer compared to those of the coating layer highlight the overall properties. With other techniques like stretching, sintering, leaching out and track-etching, porous membranes can be obtained. Porous membranes are mainly used as sublayer for composite membranes. Using phase inversion method is frequently possible to obtain open or dense structures. Various techniques have been implemented to prepare the ultrathin barrier layer upon the supporting layer. These techniques include (Lau et al. [2012](#page-20-0); Mulder [1997;](#page-21-0) Seman et al. [2012](#page-22-0)).

(a) Interfacial polymerization (IP): It is a technique that is used for depositing the thin selective layer onto the porous layer. Polymerisation reactions emerge between two reactive monomers that react on the interface of two immiscible phase (an aqueous phase and an organic solvent such as hexane) through

interfacial polymerization, and form a denser polymeric top layer on the supporting layer surface. The benefits of this technique are self-inhibiting through passage of a limited supply of reactants through the already formed layer, causing an extremely thin film of thickness in the range of 50 nm. Figure [2.2](#page-10-0) illustrates some examples of monomers and pre-polymers that can be used to prepare composite membranes by interfacial polymerization.

- (b) Dip coating: It is a straightforward and effective technique to prepare composite membranes with a very thin structure but dense toplayer. Membranes obtained by this technique can be used in gas separation, pervaporation and reverse osmosis applications. The principle of this method is dip coating a polymer solution onto the supporting layer's surface and then drying the coated layer (using oven).
- (c) Lamination: In this technique, casting an ultrathin layer and then the microporous layer is covered with the casted ultrathin layer.
- (d) Plasma-initiated polymerization: This technique involves depositing the barrier film directly on the microporous support layer by gaseous phase monomer plasma using an electrical discharge at high frequencies up to 10 MHz (Mulder [1997\)](#page-21-0).

### 2.2.4 Formation of Membranes by Phase Inversion Method

Generally, various techniques have been extensively used to prepare synthetic membranes either inorganic membranes (e.g. ceramics, metals, glass, Zeolites) or organic membranes that includes all sorts of polymers (Mulder [1997;](#page-21-0) Nunes and Peinemann [2006;](#page-21-0) Strathmann et al. [2006\)](#page-22-0). The purpose of preparation is to modify the material using an appropriate technique to obtain a membrane structure with an appropriate morphology for a specific separation. The preparation method is limited by the materials used, the membrane morphology obtained and the separation principle applied.

The techniques that are being employed for the preparation of synthetic membrane are phase inversion, stretching of films, irradiation and etching of films, sintering of powders, track-etching, sol–gel process, microfabrication vapour deposition and coating (Hoek and Elimelech [2003](#page-19-0); Hoek et al. [2002;](#page-19-0) Jeong et al. [2007;](#page-19-0) Mulder [1997](#page-21-0); Tang et al. [2008;](#page-22-0) Ulbricht [2006](#page-22-0)). One of the most important methods is phase inversion.

Phase inversion method is arguably one of the most common and versatile technique used to prepare all sorts of morphologies (both symmetric and asymmetric types) due to the significance of immersion precipitation (Boom et al. [1992;](#page-18-0) Buonomenna et al. [2011](#page-18-0); Madaeni and Rahimpour [2005a,](#page-20-0) [b](#page-20-0); Mulder [1997;](#page-21-0) Rahimpour and Madaeni [2010;](#page-21-0) Rahimpour et al. [2007a](#page-21-0), [b,](#page-21-0) [2009](#page-21-0), [2010a](#page-21-0), [b\)](#page-21-0). It is a process whereby a polymer is transformed in a controlled manner from a liquid state to a solid state. Throughout this technique, a thermodynamically stable

<span id="page-12-0"></span>polymer solution with a multiple components is subjected to a liquid–liquid demixing whereby the cast polymer film separates into a polymer—rich phase (membrane matrix) and a polymer—lean phase (membrane pores) (Buonomenna et al. [2011\)](#page-18-0). The mechanism of phase inversion during membrane formation can be concisely described by a polymer/solvent/nonsolvent system, as explained typically by a ternary phase diagram shown in Fig. 2.3 (Buonomenna et al. [2011\)](#page-18-0).

The corners of the triangle act the three components (polymer, solvent, nonsolvent), whilst at any point within the triangle represents a mixture of three components (starting compositions of the casting solution); the binodal curve divides the triangle into two phase regions; a one-phase region where all components are miscible to and a two-phase region where the system is separated into a polymer-rich, generally a solid phase and a polymer-poor which is generally liquid phase (although the one-phase region in the phase diagram is continuous thermodynamically).

For practical purposes it can conveniently be divided into a liquid and a solid region. The tie lines within the two-phase region connect two equilibrium states on the binodal curve, which also represent the compositions of two coexisting phases generated during the phase separation. The region between the spinodal and the binodal curves is called metastable region, where phase separation appears under certain initiation (nucleation). The region within the spinodal curve corresponds to unstable composition where immediate demixing occurs after entering this region.



Fig. 2.3 Ternary phase diagram (solvent/polymer/nonsolvent) for membrane formation via phase inversion process (Machado et al. [1999](#page-20-0))

By immersing a thin layer casting solution into a coagulation bath, the solvent of the casting solution is exchanged with a nonsolvent (Rahimpour and Madaeni [2007\)](#page-21-0). The composition of the coagulation and casting solution are the most considerable factor, as it determines the phase inversion path of a membrane forming system (Albrecht et al. [2001\)](#page-17-0).

The filled square represents the initial state of casting solution. The exchange between solvent and nonsolvent changes the composition in the casting film. Once demixing polymer solution arrives in the metastable region between the binodal and the spinodal, the region is referred to "binodal demixing" and therefore represents path A (Fig. [2.3](#page-12-0)). In this region, the polymer solution is separate into a polymer-lean phase and a polymer-rich phase (Buonomenna et al. [2011](#page-18-0)). Another pathway towards miscibility gap (path B) is called "spinodal decomposition". In this pathway, the composition path passed through the thermodynamically unstable zone (critical point), in which the binodal and spinodal curve converge, and two co-continuous phases formed. This process yields asymmetric membranes with a dense top layer and porous sublayer containing macrovoids, pores, and micropores (Rahimpour and Madaeni [2007\)](#page-21-0).

The general concept of phase inversion method covers a variety of different techniques, including:

- (a) Precipitation by solvent evaporation: Precipitation by solvent evaporation is a straightforward technique used to prepare phase inversion membranes. The polymer is dissolved in a solvent and form homogenous solution (casting or dope solution). Then, the dope solution is casted on a suitable support (e.g. glass plate) or another type of support that may be nonporous (polymer) or porous (non-woven fabric). Later, the solvent is allowed to evaporate in an inert gas (e.g. nitrogen) to exclude water vapour, allowing a dense homogenous membrane to be obtained (Mulder [1997\)](#page-21-0).
- (b) Precipitation by controlled evaporation: In the early years this technique has been used. In this method, the polymer is dissolved in a mixture of solvent and nonsolvent. Even though, the solvent is more volatile than the nonsolvent, the evaporation step leads to polymer precipitation own to higher nonsolvent content. The structure of membrane prepared by this technique is skinned membranes.
- (c) Thermal precipitation: Polymeric solution in a mixed or single solvent is cooled to allow phase separation to occur. Evaporation of the solvent usually allows the formation of a skinned membrane (Cheryan [1998](#page-18-0); Oh et al. [2009](#page-21-0); Su et al. [2009a](#page-22-0), [b\)](#page-22-0). This method is thoroughly used to prepare microfiltration membranes.
- (d) Precipitation from the vapour phase: In this method, a dope solution, which consists of a polymer and a solvent, is placed in a vapour atmosphere whereas vapour phase consists of a nonsolvent saturated with the same solvent. The high solvent concentration in the vapour phase prohibits the evaporation of solvent from the cast film. As a result of diffusion of nonsolvent into the cast film, the membrane formation appears. This leads to formation of porous membrane without a toplayer.

#### 2.2 Membrane Materials 27

(e) Immersion precipitation or nonsolvent induced phase inversion: This is one of the most common methods in the preparation of the most polymeric microfiltration and ultrafiltration and some of nanofiltration which is used for separation processes (Ismail and Hassan [2007](#page-19-0)). In this procedure, a film of homogenous polymeric solution is cast on a suitable substrate after preparing it by dissolving polymer into solvent. Then the cast film is immersed in a coagulation bath containing deionised water or methanol. Precipitation occurs as a consequence of the exchange between the solvent and nonsolvent. The membrane structure essentially is obtained from a combination of mass transfer and phase separation method (Rahimpour et al. [2010a\)](#page-21-0). Keeping in mind, that thermodynamic behaviour of a polymer solution is attributed to immersion—precipitation and is represented by polymer/solvent/nonsolvent systems (Buonomenna et al. [2011\)](#page-18-0). This precipitation is also called dry/wet method (Zhao et al. [2008](#page-23-0); Oh et al. [2009](#page-21-0)).

#### 2.3 Membrane Fabrication Techniques

Membranes of different arrangements are formed in order to meet different industrial and domestic demands; thus, various casting techniques have been implemented to obtain different types of the membrane such as flat sheet membrane (casting), hollow fibre membrane (spinning) and composite membrane (dip coating). The first two, will be discussed in this chapter. The third one is discussed previously.

# 2.3.1 Flat Sheet Membranes

For research purposes, flat sheet membrane is a relatively simple method used to fabricate/prepare membranes. In industrial scale, the casting method employed is usually a continuous mode as shown below in Fig. [2.4](#page-15-0) (Mulder [1997\)](#page-21-0).

The principle of this method is the polymer is initially dissolved in an appropriate solvent mixture (which may include additives) and forms a homogeneous (dope) solution. Molecular weight of a polymer, concentration of the polymer and the kind of solvent used (mixture) are three factors (parameters) affect the viscosity of the dope solution. Afterward, the polymer solution is spread (poured) and cast directly to a thin film of a homogenous polymer solution using one of the supporting layer (for example, clean glass plate, or polyethylene non-woven fabric, polyester, metal, and Teflon) by means of steel casting knife and adjusting the thickness of the membranes. The casting thickness can roughly vary from 50 to 500  $\mu$ m. The thin film of a homogenous polymer solution (protomembrane) is immediately immersed in a second liquid, which is a nonsolvent for the polymer;

<span id="page-15-0"></span>

Fig. 2.4 Schematic of continuous flat sheet membrane preparation. Adapted from Mulder [\(1984](#page-21-0), [1997\)](#page-21-0)

however, it is miscible with the polymer solvent. Exchange between the solvent and nonsolvent occurs and ultimately introduces phase separation in polymer film and would lead to the formation of membranes (Rahimpour and Madaeni [2010;](#page-21-0) Rahimpour et al. [2010a,](#page-21-0) [b;](#page-21-0) Mulder [1997\)](#page-21-0). Water is used as a nonsolvent (second liquid), as it is a powerful nonsolvent. Organic solvents (e.g. methanol) can be used for the same purpose as well. Since the solvent/nonsolvent pair is a very important characteristic in obtaining the desired structure, the nonsolvent cannot be chosen at will.

A non-continuous mode is usually employed in a laboratory scale. The three-component polymer solution (polymer/solvent/additive) is prepared and stirred under particular temperatures in order to ensure complete dissolution of the polymer. After the polymer solution is placed for some time and the complete release of bubbles is confirmed, the homogenous solution is cast on glass plates using a casting knife with a specific thickness (for example, filmographe Dr. Blade 150  $\mu$ m; Erichsen blade 150  $\mu$ m). This is immediately moved to the coagulation bath (which is usually deionised water) for immersion at room temperature without any evaporation. Then, the membranes are peeled off the glass and subsequently rinsed with deionised water and stored in fresh deionised water for at least one day to leach out all residual solvents (Rahimpour and Madaeni [2010](#page-21-0); Rahimpour et al. [2009,](#page-21-0) [2010a](#page-21-0), [b](#page-21-0)). At the final stage, membrane is sandwiched by placing between two sheets of filter paper or placing in air for 24 h at room temperature.

In Summary, flat sheet membranes are relatively straightforward to prepare, as they are very effective for characterising on laboratory scale. A dead end cell station is usually used for measuring water flux of membranes.

For very small membrane surface area (less than  $1000 \text{ cm}^2$ ), the membranes are mostly cast by hand or semi-automatically using glass plate, not on non-woven polyester.

#### 2.3.2 Hollow Fibre Membranes

Spinning is another technique used to prepare hollow fibre membranes. For industrial applications, hollow fibre membranes are more applicable, more effective and cheaper than flat sheet membranes because hollow fibre membranes have relatively higher (surface/volume) ratio compared to flat sheet membranes, which can have a greater resistance to pressure. Additionally very few manufactures supply flat sheet membranes (Zhao et al. [2013\)](#page-23-0). Hollow fibre membranes have a minimum dead space; therefore it can be physically cleaned by frequent backwash, yielding longer life to the membranes. It has been designed with specific dimensions that are suitable to minimise membrane fouling in a given application. Many scholars believe that hollow fibre membranes and flat membranes can exhibit similar performance. But, the procedures for their preparation are thoroughly different, considering hollow fibre membranes are self-supporting. The fibre dimensions are a paramount aspect and should be taken into account when preparing hollow fibre membranes.

In general, hollow fibre membranes can be prepared by three methods:

- (a) Wet spinning method: possible but rarely used to prepare hollow fibre membranes,
- (b) Melt spinning, and
- (c) Dry spinning (dry-wet spinning): this method is more applicable to prepare hollow fibre membranes and is based on the phase inversion method (Khayet and García-Payo [2009](#page-19-0)).

A schematic drawing illustrating the preparation of hollow fibre membranes is displayed in Fig. [2.5.](#page-17-0) The polymer solution is prepared and stored in a thermostated tank. Then, the solution is pumped and extruded through a tube–in-orifice spinneret; the polymer solution (being filtered before it) enters the spinneret. The viscosity of the polymer solution should be high (more than 100 poise). The bore injection liquid (nonsolvent liquid or gas) is also delivered or passed through the inner tube of the spinneret. The primary function (goal) of the bore liquid is to keep the fibre open and to assist in controlling the interior surface morphology of the hollow fibre through phase inversion.

After a short residence time in air or atmosphere, the fibre is immersed in a coagulation bath where precipitation appears outside the liquid filament due to solvent evaporation. After immediate coagulation, asymmetric hollow fibre are formed with density gradient along the radial direction (Machado et al. [1999](#page-20-0)). The fibres are then rinsed and cut with the desired length and collected upon a godet. Cutting the fibre is favourable in the hollow fibre process to assist in promoting the flow of bore liquid inside the hollow. The main parameters in the spinning technique are (Mulder [1997](#page-21-0)):

- (a) The extrusion rate of the polymer solution,
- (b) The bore fluid rate,
- (c) The tearing rate,

<span id="page-17-0"></span>

Fig. 2.5 Hollow fibre spinning apparatus. Adapted from Machado et al. [\(1999](#page-20-0)), Mulder [\(1997\)](#page-21-0)

- (d) The residence time in the air gap (between spinneret and coagulation bath), and
- (e) The dimensions of the spinneret.

These parameters strongly interact with the membrane forming parameters such as the composition of the polymer solution, the composition of the coagulation bath and its temperature.

In summary, the configurations of flat sheet and hollow fibre membrane can be used as membrane bioreactors (MBRs) for applications of wastewater treatment, and both have their advantages and disadvantages.

### **References**

- Albrecht W, Weigel T, Schossig-Tiedemann M, Kneifel K, Peinemann KV, Paul D (2001) Formation of hollow fiber membranes from poly(ether imide) at wet phase inversion using binary mixtures of solvents for the preparation of the dope. J Membr Sci 192(1–2):217–230. doi:[10.1016/S0376-7388\(01\)00504-X](http://dx.doi.org/10.1016/S0376-7388(01)00504-X)
- Arthanareeswaran G, Sriyamuna Devi TK, Raajenthiren M (2008) Effect of silica particles on cellulose acetate blend ultrafiltration membranes: Part I. Sep Purif Technol 64(1):38–47
- Bae TH, Tak TM (2005a) Effect of TiO<sub>2</sub> nanoparticles on fouling mitigation of ultrafiltration membranes for activated sludge filtration. J Membr Sci 249(1–2):1–8
- Bae TH, Tak TM (2005b) Interpretation of fouling characteristics of ultrafiltration membranes during the filtration of membrane bioreactor mixed liquor. J Membr Sci 264(1–2):151–160
- Baker R (2012) Membrane technology and application, 3rd edn. Wiley, United Kingdom
- Barth C, Gonçalves MC, Pires ATN, Roeder J, Wolf BA (2000) Asymmetric polysulfone and polyethersulfone membranes: effects of thermodynamic conditions during formation on their performance. J Membr Sci 169(2):287–299
- <span id="page-18-0"></span>Barzin J, Feng C, Khulbe KC, Matsuura T, Madaeni SS, Mirzadeh H (2004) Characterization of polyethersulfone hemodialysis membrane by ultrafiltration and atomic force microscopy. J Membr Sci 237(1–2):77–85
- Belfer S, Fainchtain R, Purinson Y, Kedem O (2000) Surface characterization by FTIR-ATR spectroscopy of polyethersulfone membranes-unmodified, modified and protein fouled. J Membr Sci 172(1–2):113–124
- Bhattacharjee S, Johnston GM (2002) A model of membrane fouling by salt precipitation from multicomponent ionic mixtures in crossflow nanofiltration. Environ Eng Sci 19(6):399–412
- Bolong N, Ismail AF, Salim MR, Rana D, Matsuura T (2009) Development and characterization of novel charged surface modification macromolecule to polyethersulfone hollow fiber membrane with polyvinylpyrrolidone and water. J Membr Sci 331(1–2):40–49
- Boom RM, Wienk IM, Den Van, Boomgaard T, Smolders CA (1992) Microstructures in phase inversion membranes. Part 2. The role of a polymeric additive. J Membr Sci 73(2–3):277–292
- Boussu K, Van der Bruggen B, Volodin A, Van Haesendonck C, Delcour JA, Van der Meeren P, Vandecasteele C (2006) Characterization of commercial nanofiltration membranes and comparison with self-made polyethersulfone membranes. Desalination 191(1–3):245–253
- Buch PR, Jagan Mohan D, Reddy AVR (2008) Preparation, characterization and chlorine stability of aromatic-cycloaliphatic polyamide thin film composite membranes. J Membr Sci 309(1– 2):36–44
- Buonomenna M, Choi S, Galiano F, Drioli E (2011) Membranes prepared via phase inversion. In: Basile A, Gallucci F (eds) Membranes for membrane reactors, preparation, optimization and selection, 1st edn. Wiley, UK, pp 475–490
- Cadotte J, Petersen R (1981) Thin film reverse osmosis membranes: origin, development, and recent advances. In: Synthetic membranes, ACS symposium series 153, vol 1, pp 305–325
- Cejka J, Corna HV, Corma A, Schuth F (2007) Introduction to zeolite science and practise, studies in surface science and catalysis. Elsevier
- Celik E, Choi H (2011) Carbon nanotube/polyethersulfone composite membranes for water filtration. In: ACS Symposium Series, vol 1078
- Celik E, Liu L, Choi H (2011a) Protein fouling behavior of carbon nanotube/polyethersulfone composite membranes during water filtration. Water Res 45(16):5287–5294
- Celik E, Park H, Choi H, Choi H (2011b) Carbon nanotube blended polyethersulfone membranes for fouling control in water treatment. Water Res 45(1):274–282
- Chaturvedi BK, Ghosh AK, Ramachandhran V, Trivedi MK, Hanra MS, Misra BM (2001) Preparation, characterization and performance of polyethersulfone ultrafiltration membranes. Desalination 133(1):31–40
- Cheryan M (1998) Ultrafiltration and microfiltration handbook. Technomic Publishing Company Inc, USA
- Daraei P, Madaeni SS, Ghaemi N, Khadivi MA, Astinchap B, Moradian R (2013a) Enhancing antifouling capability of PES membrane via mixing with various types of polymer modified multi-walled carbon nanotube. J Membr Sci 444:184–191
- Daraei P, Madaeni SS, Ghaemi N, Khadivi MA, Astinchap B, Moradian R (2013b) Fouling resistant mixed matrix polyethersulfone membranes blended with magnetic nanoparticles: study of magnetic field induced casting. Sep Purif Technol 109:111–121
- Daraei P, Madaeni SS, Ghaemi N, Khadivi MA, Rajabi L, Derakhshan AA, Seyedpour F (2013c) PAA grafting onto new acrylate-alumoxane/PES mixed matrix nano-enhanced membrane: preparation, characterization and performance in dye removal. Chem Eng J 221:111–123
- Fan XJ, Urbain V, Qian Y, Manem J (1996) Nitrification and mass balance with a membrane bioreactor for municipal wastewater treatment. Water Sci Technol 34. doi[:10.1016/0273-1223](http://dx.doi.org/10.1016/0273-1223(96)00502-1) [\(96\)00502-1](http://dx.doi.org/10.1016/0273-1223(96)00502-1)
- Gallucci F, Basile A, Hai F (2011a) Membranes for membrane reactors: preparation, optimization and selection, 1st edn. Wiley, UK
- Gallucci F, Basile A, Hai FI (2011b) Introduction—a review of membrane reactors. In: Membranes for membrane reactors: preparation, optimization and selection. Wiley, Chichester, pp 1–61. doi:[10.1002/9780470977569.ch](http://dx.doi.org/10.1002/9780470977569.ch)
- <span id="page-19-0"></span>Gallucci F, Tosti S, Basile A (2008) Pd-Ag tubular membrane reactors for methane dry reforming: a reactive method for  $CO_2$  consumption and  $H_2$  production. J Membr Sci 317(1–2):96–105. doi:[10.1016/j.memsci.2007.03.058](http://dx.doi.org/10.1016/j.memsci.2007.03.058)
- Gerlach G, Baumann K, Buchhold R, Naklal A (1998) German Patent D E 19853732
- Guan R, Zou H, Lu D, Gong C, Liu Y (2005) Polyethersulfone sulfonated by chlorosulfonic acid and its membrane characteristics. Eur Polym J 41(7):1554–1560
- Hancock LF, Fagan SM, Ziolo MS (2000) Hydrophilic, semipermeable membranes fabricated with poly(ethylene oxide)-polysulfone block copolymer. Biomaterials 21(7):725–733
- Hoek EMV, Elimelech M (2003) Cake-enhanced concentration polarization: a new fouling mechanism for salt-rejecting membranes. Environ Sci Technol 37(24):5581–5588
- Hoek EMV, Kim AS, Elimelech M (2002) Influence of crossflow membrane filter geometry and shear rate on colloidal fouling in reverse osmosis and nanofiltration separations. Environ Eng Sci 19(6):357–372
- Huang J, Zhang K, Wang K, Xie Z, Ladewig B, Wang H (2012) Fabrication of polyethersulfone-mesoporous silica nanocomposite ultrafiltration membranes with antifouling properties. J Membr Sci 423–424:362–370
- Huang ZQ, Chen ZY, Guo XP, Zhang Z, Guo CL (2006) Structures and separation properties of PAN-Fe3O4 ultrafiltration membranes prepared under an orthogonal magnetic field. Ind Eng Chem Res 45(23):7905–7912
- Ismail AF, Hassan AR (2007) Effect of additive contents on the performances and structural properties of asymmetric polyethersulfone (PES) nanofiltration membranes. Sep Purif Technol 55(1):98–109
- Jahanshahi M, Rahimpour A, Peyravi M (2010) Developing thin film composite poly (piperazine-amide) and poly(vinyl-alcohol) nanofiltration membranes. Desalination 257(1– 3):129–136
- Jeong BH, Hoek EMV, Yan Y, Subramani A, Huang X, Hurwitz G, Ghosh AK, Jawor A (2007) Interfacial polymerization of thin film nanocomposites: a new concept for reverse osmosis membranes. J Membr Sci 294(1–2):1–7
- Jian P, Yahui H, Yang W, Linlin L (2006) Preparation of polysulfone-Fe3O<sub>4</sub> composite ultrafiltration membrane and its behavior in magnetic field. J Membr Sci 284(1–2):9–16
- Judd S (2006) Principles and applications of membrane bioreactors in water and waste water treatment, 1st edn. Elsevier, UK
- Judd S, Robinson R, Holdner J, Vazquez HA, Jefferson B (2004) Impact of membrane material on membrane bioreactor permeability. In: Proceedings of the water environment-membrane technology conference, Seoul, Korea
- Kesting R (1971) Synthetic polymeric membranes. McGraw-Hill, New York
- Khayet M, García-Payo MC (2009) X-Ray diffraction study of polyethersulfone polymer, flat-sheet and hollow fibers prepared from the same under different gas-gaps. Desalination 245  $(1-3):494-500$
- Khulbe KC, Feng C, Matsuura T, Kapantaidakis GC, Wessling M, Koops GH (2003) Characterization of polyethersulfone-polyimide hollow fiber membranes by atomic force microscopy and contact angle goniometery. J Membr Sci 226(1–2):63–73. doi[:10.1016/j.](http://dx.doi.org/10.1016/j.memsci.2003.08.011) [memsci.2003.08.011](http://dx.doi.org/10.1016/j.memsci.2003.08.011)
- Khulbe KC, Feng CY, Matsuura T (2010) Surface modification of synthetic polymeric membranes for filtration and gas separation. Recent Pat Chem Eng 3(1):1–16
- Khulbe KC, Matsuura T, Singh S, Lamarche G, Noh SH (2000) Study on fouling of ultrafiltration membrane by electron spin resonance. J Membr Sci 167(2):263–273
- Kim IC, Choi JG, Tak TM (1999) Sulfonated polyethersulfone by heterogeneous method and its membrane performances. J Appl Polym Sci 74(8):2046–2055
- Koh M, Clark MM, Howe KJ (2005) Filtration of lake natural organic matter: adsorption capacity of a polypropylene microfilter. J Membr Sci 256(1–2):169–175
- Kosaraju P, Sirkar K (2008) Interfacially polymerized thin film comopsite membranes on microporous polypropylene supports for solvent-resistant nanofiltration. Membr Sci 321:155–161

<span id="page-20-0"></span>Kumar R et al (2006) Nucl Instr Meth Phys Res 248B: 279–283

- Lau WJ, Ismail AF, Misdan N, Kassim MA (2012) A recent progress in thin film composite membrane: a review. Desalination 287:190–199
- Lee S, Kim J, Lee CH (1999) Analysis of  $CaSO<sub>4</sub>$  scale formation mechanism in various nanofiltration modules. J Membr Sci 163(1):63–74
- Lee S, Lee CH (2000) Effect of operating conditions on  $CaSO<sub>4</sub>$  scale formation mechanism in nanofiltration for water softening. Water Res 34(15):3854–3866
- Leo CP, Ahmad Kamil NH, Junaidi MUM, Kamal SNM, Ahmad AL (2013) The potential of SAPO-44 zeolite filler in fouling mitigation of polysulfone ultrafiltration membrane. Sep Purif Technol 103:84–91
- Leo CP, Cathie Lee WP, Ahmad AL, Mohammad AW (2012) Polysulfone membranes blended with ZnO nanoparticles for reducing fouling by oleic acid. Sep Purif Technol 89:51–56
- Li B, Zhao W, Su Y, Jiang Z, Dong X, Liu W (2009a) Enhanced desulfurization performance and swelling resistance of asymmetric hydrophilic pervaporation membrane prepared through surface segregation technique. J Membr Sci 326(2):556–563
- Li JF, Xu ZL, Yang H, Yu LY, Liu M (2009b) Effect of  $TiO<sub>2</sub>$  nanoparticles on the surface morphology and performance of microporous PES membrane. Appl Surf Sci 255(9): 4725–4732
- Li Y, Cao C, Chung TS, Pramoda KP (2004) Fabrication of dual-layer polyethersulfone (PES) hollow fiber membranes with an ultrathin dense-selective layer for gas separation. J Membr Sci 245(1–2):53–60
- Li Y, Chung TS, Xiao Y (2008) Superior gas separation performance of dual-layer hollow fiber membranes with an ultrathin dense-selective layer. J Membr Sci 325(1):23–27
- Liang S, Xiao K, Mo Y, Huang X (2012) A novel ZnO nanoparticle blended polyvinylidene fluoride membrane for anti-irreversible fouling. J Membr Sci 394–395:184–192
- Lin YS (2001) Microporous and dense inorganic membranes: current status and prospective. Sep Purif Technol 25(1–3):39–55. doi:[10.1016/S1383-5866\(01\)00089-2](http://dx.doi.org/10.1016/S1383-5866(01)00089-2)
- Liu SX, Kim JT (2011) Characterization of surface modification of polyethersulfone membrane. J Adhes Sci Technol 25(1–3):193–212
- Livari AE, Aroujalian A, Raisi A, Fathizadeh M (2012) The effect of  $TiO<sub>2</sub>$  nanoparticles on PES UF membrane fouling in water oil separation. Process Eng 44:1783–1785
- Lu Y, Yu S, Chai B (2005) Preparation of PVDF ultrafiltration membrane modified by nano-sized alumina( $AI2O<sub>3</sub>$ ) and its antifouling research. Polymer  $46:7701-7706$
- Luo ML, Zhao JQ, Tang W, Pu CS (2005) Hydrophilic modification of poly(ether sulfone) ultrafiltration membrane surface by self-assembly of  $TiO<sub>2</sub>$  nanoparticles. Appl Surf Sci 249(1– 4):76–84
- Luonsi A, Laitinen N, Beyer K, Levänen E, Poussade Y, Nyström M (2002) Separation of CTMP mill-activated sludge with ceramic membranes. Desalination 146(1–3):399–404
- Machado PST, Habert AC, Borges CP (1999) Membrane formation mechanism based on precipitation kinetics and membrane morphology: Flat and hollow fiber polysulfone membranes. J Membr Sci 155(2):171–183
- Madaeni SS, Rahimpour A (2005a) Effect of type of solvent and non-solvents on morphology and performance of polysulfone and polyethersulfone ultrafiltration membranes for milk concentration. Polym Adv Technol 16(10):717–724
- Madaeni SS, Rahimpour A (2005b) Preparation of polyethersulfone ultrafiltration membranes for milk concentration and effects of additives on their morphology and performance. Chin J Polym Sci (English Edition) 23(5):539–548
- Marchese J, Ponce M, Ochoa NA, Prádanos P, Palacio L, Hernández A (2003) Fouling behaviour of polyethersulfone UF membranes made with different PVP. J Membr Sci 211(1):1–11
- Maximous N, Nakhla G, Wan W, Wong K (2010) Performance of a novel  $ZrO<sub>2</sub>/PES$  membrane for wastewater filtration. J Membr Sci 352(1–2):222–230
- Moghimifar V, Raisi A, Aroujalian A (2014) Surface modification of polyethersulfone ultrafiltration membranes by corona plasma-assisted coating  $TiO<sub>2</sub>$  nanoparticles. J Membr Sci 461:69–80
- <span id="page-21-0"></span>Mulder M (1984) Basic principles of membrane technology, 1st edn. Kluwer Academic Publishers, Dordrecht
- Mulder M (1997) Basic principles of membrane technology, 2nd edn. Kluwer Academic Publishers, Dordrecht
- Nair PK, Cardoso J, Gomez Daza O, Nair MTS (2001) Polyethersulfone foils as stable transparent substrates for conductive copper sulfide thin film coatings. Thin Solid Films 401(1–2):243–250
- Nunes S, Peinemann K (2001) Membrane technology. Wiley, Weinheim

Nunes S, Peinemann K (2006) Membrane technology. Wiley, Weinheim

- Nunes S, Peinemann K (2010) Membranes for water treatment, 4th edn. Wiley, Weinheim
- Oh SJ, Kim N, Lee YT (2009) Preparation and characterization of PVDF/TiO<sub>2</sub> organic-inorganic composite membranes for fouling resistance improvement. J Membr Sci 345(1–2):13–20
- Peyravi M, Rahimpour A, Jahanshahi M (2012) Thin film composite membranes with modified polysulfone supports for organic solvent nanofiltration. J Membr Sci 423–424:225–237
- Rahimpour A (2011) Preparation and modification of nano-porous polyimide (PI) membranes by UV photo-grafting process: ultrafiltration and nanofiltration performance. Korean J Chem Eng 28(1):261–266
- Rahimpour A, Jahanshahi M, Peyravi M, Khalili S (2011) Interlaboratory study of highly permeable thin film composite polyamide nanofiltration membrane. Polym Adv Technol 23:884–893
- Rahimpour A, Madaeni SS (2007) Polyethersulfone (PES)/cellulose acetate phthalate (CAP) blend ultrafiltration membranes: preparation, morphology, performance and antifouling properties. J Membr Sci 305(1–2):299–312
- Rahimpour A, Madaeni SS (2010) Improvement of performance and surface properties of nano-porous polyethersulfone (PES) membrane using hydrophilic monomers as additives in the casting solution. J Membr Sci 360(1–2):371–379
- Rahimpour A, Madaeni SS, Mansourpanah Y (2007a) The effect of anionic, non-ionic and cationic surfactants on morphology and performance of polyethersulfone ultrafiltration membranes for milk concentration. J Membr Sci 296(1–2):110–121
- Rahimpour A, Madaeni SS, Mansourpanah Y (2007b) High performance polyethersulfone UF membrane for manufacturing spiral wound module: preparation, morphology, performance, and chemical cleaning. Polym Adv Technol 18(5):403–410
- Rahimpour A, Madaeni SS, Mansourpanah Y (2010a) Fabrication of polyethersulfone (PES) membranes with nano-porous surface using potassium perchlorate  $(KClO<sub>4</sub>)$  as an additive in the casting solution. Desalination 258(1–3):79–86
- Rahimpour A, Madaeni SS, Mansourpanah Y (2010b) Nano-porous polyethersulfone (PES) membranes modified by acrylic acid (AA) and 2-hydroxyethylmethacrylate (HEMA) as additives in the gelation media. J Membr Sci 364(1–2):380–388
- Rahimpour A, Madaeni SS, Taheri AH, Mansourpanah Y (2008) Coupling TiO<sub>2</sub> nanoparticles with UV irradiation for modification of polyethersulfone ultrafiltration membranes. J Membr Sci 313(1–2):158–169
- Rahimpour A, Madaeni SS, Zereshki S, Mansourpanah Y (2009) Preparation and characterization of modified nano-porous PVDF membrane with high antifouling property using UV photo-grafting. Appl Surf Sci 255(16):7455–7461
- Razali NF, Mohammad AW, Hilal N, Leo CP, Alam J (2013) Optimisation of polyethersulfone/ polyaniline blended membranes using response surface methodology approach. Desalination 311:182–191
- Razmjou A, Mansouri J, Chen V (2011a) The effects of mechanical and chemical modification of TiO2 nanoparticles on the surface chemistry, structure and fouling performance of PES ultrafiltration membranes. J Membr Sci 378(1–2):73–84
- Razmjou A, Mansouri J, Chen V, Lim M, Amal R (2011b) Titania nanocomposite polyethersulfone ultrafiltration membranes fabricated using a low temperature hydrothermal coating process. J Membr Sci 380(1–2):98–113
- <span id="page-22-0"></span>Samtleben W, Dengler C, Reinhardt B, Nothdurft A, Lemke HD (2003) Comparison of the new polyethersulfone high-flux membrane DIAPES® HF800 with conventional high-flux membranes during on-line haemodiafiltration. Nephrol Dial Transplant 18(11):2382–2386
- Sawada I, Fachrul R, Ito T, Ohmukai Y, Maruyama T, Matsuyama H (2012) Development of a hydrophilic polymer membrane containing silver nanoparticles with both organic antifouling and antibacterial properties. J Membr Sci 387–388(1):1–6
- Scott JA, Neilson DJ, Liu W, Boon PN (1998) A dual function membrane bioreactor system for enhanced aerobic remediation of high-strength industrial waste. Water Sci Technol 38(4– 5):413–420
- Seidel A, Elimelech M (2002) Coupling between chemical and physical interactions in natural organic matter (NOM) fouling of nanofiltration membranes: implications for fouling control. J Membr Sci 203(1–2):245–255
- Seman MA, Khayet M, Hilal N (2012) Development of anti-fouling properties and performance of nanofiltration membranes by interfacial polymerization and photografting In: Hilal N, Khayet M, Wright B (eds) Membrane modification technology and applications. Boca Raton, Taylor & Francis Group: CRC press, pp 119–153
- Shi Q, Su Y, Zhao W, Li C, Hu Y, Jiang Z, Zhu S (2008) Zwitterionic polyethersulfone ultrafiltration membrane with superior antifouling property. J Membr Sci 319(1–2):271–278
- Shin SJ, Kim JP, Kim HJ, Jeon JH, Min BR (2005) Preparation and characterization of polyethersulfone microfiltration membranes by a 2-methoxyethanol additive. Desalination 186  $(1-3):1-10$
- Song YQ, Sheng J, Wei M, Yuan XB (2000) Surface modification of polysulfone membranes by lowtemperature plasma-graft poly(ethylene glycol) onto polysulfone membranes. J Appl Polym Sci 78(5):979–985
- Strathmann, H (1989) Economical evaluation of membrane technology In: Cecille L, Toussaint JC (eds) Future industrial prospects of membrane processes. Elsevier, London & New York, pp 41–55
- Strathmann H (2000) Introduction to membrane science and technology. Wiley-VCH, Weinheim
- Strathmann H (2011) Introduction to membrane science and technology. Wiley-VCH, Weinheim
- Strathmann H, Giorno L, Drioli E (2006) An introduction to membrane science and technology. In: Consiglio Nazionale delle Ricerche, Rome
- Su Y, Mu C, Li C, Jiang Z (2009a) Antifouling property of a weak polyelectrolyte membrane based on poly(acrylonitrile) during protein ultrafiltration. Ind Eng Chem Res 48(6):3136–3141
- Su YL, Cheng W, Li C, Jiang Z (2009b) Preparation of antifouling ultrafiltration membranes with poly(ethylene glycol)-graft-polyacrylonitrile copolymers. J Membr Sci 329(1–2):246–252
- Tang B, Huo Z, Wu P (2008) Study on a novel polyester composite nanofiltration membrane by interfacial polymerization of triethanolamine (TEOA) and trimesoyl chloride (TMC). I. Preparation, characterization and nanofiltration properties test of membrane. J Membr Sci 320(1–2):198–205
- Tsuru T, Izumi S, Yoshioka T, Asaeda M (2000a) Temperature effect on transport performance by inorganic nanofiltration membranes. AIChE J 46(3):565–574
- Tsuru T, Sudou T, Kawahara SI, Yoshioka T, Asaeda M (2000b) Permeation of liquids through inorganic nanofiltration membranes. J Colloid Interface Sci 228(2):292–296
- Tullis RH, Duffin RP, Zech M, Ambrus JL Jr (2002) Affinity hemodialysis for antiviral therapy. I. Removal of HIV-1 from cell culture supernatants, plasma, and blood. Ther Apheresis 6(3):213–220
- Ulbricht M (2006) Advanced functional polymer membranes. Polymer 47(7):2217–2262
- Ulbricht M, Schuster O, Ansorge W, Ruetering M, Steiger P (2007) Influence of the strongly anisotropic cross-section morphology of a novel polyethersulfone microfiltration membrane on filtration performance. Sep Purif Technol 57(1):63–73
- <span id="page-23-0"></span>Unger RE, Peters K, Huang Q, Funk A, Paul D, Kirkpatrick CJ (2005) Vascularization and gene regulation of human endothelial cells growing on porous polyethersulfone (PES) hollow fiber membranes. Biomaterials 26(17):3461–3469. doi:[10.1016/j.biomaterials.2004.09.047](http://dx.doi.org/10.1016/j.biomaterials.2004.09.047)
- Van der Bruggen B, Braeken L, Vandecasteele C (2002a) Evaluation of parameters describing flux decline in nanofiltration of aqueous solutions containing organic compounds. Desalination 147 (1–3):281–288
- Van der Bruggen B, Braeken L, Vandecasteele C (2002b) Flux decline in nanofiltration due to adsorption of organic compounds. Sep Purif Technol 29(1):23–31
- van Veen HM, Bracht M, Hamoen E, Alderliesten PT (1996) Chapter 14 Feasibility of the application of porous inorganic gas separation membranes in some large-scale chemical processes. Membr Sci Technol 4
- Wang Y, Su Y, Sun Q, Ma X, Ma X, Jiang Z (2006a) Improved permeation performance of Pluronic F127-polyethersulfone blend ultrafiltration membranes. J Membr Sci 282(1–2):44–51
- Wang YQ, Su YL, Ma XL, Sun Q, Jiang ZY (2006b) Pluronic polymers and polyethersulfone blend membranes with improved fouling-resistant ability and ultrafiltration performance. J Membr Sci 283(1–2):440–447
- Wang YQ, Wang T, Su YL, Peng FB, Wu H, Jiang ZY (2006c) Protein-adsorption-resistance and permeation property of polyethersulfone and soybean phosphatidylcholine blend ultrafiltration membranes. J Membr Sci 270(1–2):108–114
- Werner C, Jacobasch HJ, Reichelt G (1995) Surface characterization of hemodialysis membranes based on streaming potential measurements. J Biomater Sci Polym Ed 7(1):61–76
- Wu H (2012) Improving the anti-fouling and fouling release of PVDF UF membrane by chemically modified SiO<sub>2</sub> nanoparticles. New South Wales, Sydney, Australia
- Xu ZL, Qusay FA (2004) Polyethersulfone (PES) hollow fiber ultrafiltration membranes prepared by PES/non-solvent/NMP solution. J Membr Sci 233(1–2):101–111
- Yamamura H, Kimura K, Watanabe Y (2007a) Mechanism involved in the evolution of physically irreversible fouling in microfiltration and ultrafiltration membranes used for drinking water treatment. Environ Sci Technol 41(19):6789–6794
- Yamamura H, Okimoto K, Kimura K, Watanabe Y (2007b) Influence of calcium on the evolution of irreversible fouling in microfiltration/ultrafiltration membranes. J Water Supply Res Technol —AQUA 56(6–7):425–434
- Yang Y, Zhang H, Wang P, Zheng Q, Li J (2007) The influence of nano-sized TiO<sub>2</sub> fillers on the morphologies and properties of PSF UF membrane. J Membr Sci 288(1–2):231–238
- Yu LY, Shen HM, Xu ZL (2009a) PVDF-TiO2 composite hollow fiber ultrafiltration membranes prepared by  $TiO<sub>2</sub>$  sol-gel method and blending method. J Appl Polym Sci 113(3):1763–1772
- Yu LY, Xu ZL, Shen HM, Yang H (2009b) Preparation and characterization of PVDF-SiO<sub>2</sub> composite hollow fiber UF membrane by sol-gel method. J Membr Sci 337(1–2):257–265
- Yu Y, Seo S, Kim IC, Lee S (2011) Nanoporous polyethersulfone (PES) membrane with enhanced flux applied in forward osmosis process. J Membr Sci 375(1-2):63-68. doi[:10.1016/j.memsci.](http://dx.doi.org/10.1016/j.memsci.2011.02.019) [2011.02.019](http://dx.doi.org/10.1016/j.memsci.2011.02.019)
- Zhao C, Liu T, Lu Z, Cheng L, Huang J (2001) An evaluation of a polyethersulfone hollow fiber plasma separator by animal experiment. Artif Organs 25:3–60
- Zhao C, Liu X, Rikimaru S, Nomizu M, Nishi N (2003a) Surface characterization of polysulfone membranes modified by DNA immobilization. J Membr Sci 214(2):179–189
- Zhao C, Xue J, Ran F, Sun S (2013) Modification of polyethersulfone membranes—A review of methods. Prog Mater Sci 58(1):76–150
- Zhao Q, Qian J, An Q, Zhu Z, Zhang P, Bai Y (2008) Studies on pervaporation characteristics of polyacrylonitrile-b-poly(ethylene glycol)-b-polyacrylonitrile block copolymer membrane for dehydration of aqueous acetone solutions. J Membr Sci 311(1–2):284–293
- Zhao ZP, Wang Z, Wang SC (2003b) Formation, charged characteristic and BSA adsorption behavior of carboxymethyl chitosan/PES composite MF membrane. J Membr Sci 217(1– 2):151–158
- <span id="page-24-0"></span>Zhenxin Z, Matsuura T (1991) Discussions on the formation mechanism of surface pores in reverse osmosis, ultrafiltration, and microfiltration membranes prepared by phase inversion process. J Colloid Interface Sci 147(2):307–315
- Zhu J, Guo N, Zhang Y, Yu L, Liu J (2014) Preparation and characterization of negatively charged PES nanofiltration membrane by blending with halloysite nanotubes grafted with poly (sodium 4-styrenesulfonate) via surface-initiated ATRP. J Membr Sci 465:91–99
- Zoppi RA, Soares CGA (2002) Hybrids of poly(ethylene oxide-b-amide-6) and  $ZrO<sub>2</sub>$  sol-gel: Preparation, characterization, and application in processes of membranes separation. Adv Polym Technol 21(1):2–16