# **Chapter 14 Different Levels of Self-Sufficiency of the Velocity Sedimentation Method in the Study of Linear Macromolecules**

**Georges M. Pavlov**

**Abstract** The general principles for the interpretation of the sedimentation velocity for linear macromolecules are discussed in combination with the characteristics obtained by other hydrodynamic methods. The several levels of self-sufficiency of the sedimentation velocity method are demonstrated. They include scaling correlation between velocity sedimentation coefficient  $s<sub>0</sub>$  and concentration coefficient  $k_s = K_{\text{sk}} s_0^{\text{bks}}$ , application of the sedimentation parameter  $\beta_s$  for molar mass<br>estimation and qualitative conformation zoning of linear macromolecules using estimation, and qualitative conformation zoning of linear macromolecules using the normalized double logarithmic plots  $(k_sM_L$ vs [ $s$ ]/ $M_L$ ). The last example of self-sufficiency of the method is the study of the concentration dependence of the sedimentation velocity in combination with continuous  $c(s)$  distribution using general scaling law model of Sedfit software. This model allows to establish the relationship  $s_0 = K_s M^{bs}$  for flexible polymers and perform further gross conformational analysis and analysis of the molar mass distribution. It is shown that the  $K_s$  coefficient is strongly dependent on the polymer concentration.

**Keywords** Velocity sedimentation • Sedimentation coefficient • Sedit • Sedimentation parameter • Molar mass • Scaling relations

#### **14.1 Introduction**

Apparently, molecular hydrodynamics goes back to Archimedes of Syracuse and his concept of buoyancy which characterizes the difference in density between a particle/body and the surrounding liquid in which this particle moves (contrast of densities). Already in the new times, Stokes has obtained a relationship between

G.M. Pavlov  $(\boxtimes)$ 

Institute of Macromolecular Compounds, Russian Academy of Sciences, Bol'shoi prospect 31, St. Petersburg 199004, Russia

Department of Physics, St. Petersburg State University, 7-9, Universitetskaya nab., St. Petersburg 199034, Russia

e-mail: [g.m.pavlov@spbu.ru;](mailto:g.m.pavlov@spbu.ru) [georges.pavlov@mail.ru](mailto:georges.pavlov@mail.ru)

the translational friction coefficient of a rigid sphere and its radius. In 1911 Svedberg and Estrup used the precipitation rate of colloidal particles in the Earth's gravitational field (with acceleration of  $1 \text{ g}$ ) to assess their size. They obtained the following relation when the notion of the velocity sedimentation coefficient was not yet introduced:

<span id="page-1-0"></span>
$$
r_h = \left[ (9/2) (uh) / (d - d) g' \right]^{1/2} = \left[ (9/2) (s \eta \overline{\nu} / (1 - \overline{\nu} \rho_0)) \right]^{1/2}
$$
 (14.1)

The left side of the relationship  $(14.1)$  is the original one, and the right side is its modern paraphrase.

Here  $r_h$  is the hydrodynamic radius of the particle,  $\eta$  is the medium viscosity,  $\delta \equiv \rho_0$  is the density of the solvent,  $d = 1/\overline{v}$  is the density of the particle,  $\overline{v}$  is the partial specific volume, and  $u/g' \equiv s$  is the sedimentation coefficient according to the definition given later by Svedberg.

Conspicuously, in 1913, Dumanskiy, Jabotinsky, and Evseev (see also Introduction by T. Svedberg in Svedberg and Pedersen [\(1940\)](#page-36-0)) were the first to use a *centrifuge*. They studied the precipitation rate of colloidal particles at  $n = 2000$  rpm  $(\approx 300 \text{ g})$  to measure particle sizes using the same relationships [\(14.1\)](#page-1-0) which they have derived from the Stokes law. In 1913–1926, Svedberg and his coworkers have performed an enormous amount of creative and constructive work to design and build the *ultracentrifuge* which allows to achieve the fields of  $\approx$  200 000 g. On May 19, 1927, Svedberg gave his Nobel lecture entitled "The ultracentrifuge" (Svedberg [1927\)](#page-37-0). Thus, a new scientific direction has emerged in molecular biophysics and nascent polymer science – analytical ultracentrifugation. In fact, Svedberg's lecture predicted the widespread use of analytical ultracentrifugation in future studies of various dispersed systems. Further results of the analytical ultracentrifugation obtained before the 1940s were summarized in the book (Svedberg and Pedersen [1940\)](#page-37-1), which so far has not lost its value. The first investigations conducted by Svedberg himself were devoted to studying velocity sedimentation of globular proteins from different organic sources (e.g., Svedberg and Faehraeus [1926;](#page-37-2) Svedberg and Sjoegren [1928\)](#page-37-3). These data represent an extensive library of velocity sedimentation coefficients of proteins and are given in a special chapter (Pedersen in the monograph Svedberg and Pedersen [1940\)](#page-37-1). In a short while, the investigations of cellulose and its derivatives as well as the synthetic polymers were started (e.g., Stamm [\(1930\)](#page-37-4); Singer and Gross [\(1934a,](#page-37-5) [b\)](#page-37-6); Kraemers and Nichols [\(1940\)](#page-35-0)). In the mid-1950s, the study of DNA properties by AUC also began (see Peacocke and Schachman [\(1954\)](#page-36-1), Kawade and Watanabe [\(1956\)](#page-35-1)).

Currently, analytical ultracentrifugation methods are widely used in biophysics, polymer science, nanoscience, colloid science, and other related areas (Munk [1991;](#page-35-2) Schuster and Laue [1994;](#page-37-7) Laue and Stafford [1999;](#page-35-3) Lebowitz et al. [2002;](#page-35-4) Scott et al. [2005;](#page-37-8) Maechtle and Boerger [2006\)](#page-35-5). Analytical ultracentrifugation has some experimental variations, and the most important and used among them are sedimentation velocity and sedimentation equilibrium (Schachman [1959;](#page-37-9) Fujita [1975\)](#page-34-0). In this part, we will consider only the application of the first method.

In 1997 Beckman Instruments, Inc. (Palo Alto, USA) launched a new analytical ultracentrifuge. The progress made by Beckman Instruments in XLA/I model involves various aspects: up-to-date electrical drive, convenient temperature control of the apparatus, the development of optical detection systems, digital camera, and the online digitization of the measuring data. Since the XLI ultracentrifuge is equipped with two kinds of optics (the UV/Vis absorption detector and the Rayleigh interferometer), it became possible to use the new analytical ultracentrifuge to study a wide range of polymer molecules, both synthetic and natural.

The impressive breakthrough was made with the development of a commercial fluorescence detection system (FDS) for the analytical ultracentrifuge which has significantly extended the sensitivity of the boundary registration going up to picomolar concentrations of labeled solutes (MacGregor et al. [2004;](#page-35-6) Kroe and Laue [2009\)](#page-35-7). The only problem left is incorporation of the corresponding tags into macromolecules; then it would be virtually possible to follow the sedimentation of individual macromolecule. (It will be indeed gold "nuts and bolts.")

After development of the XLA/I ultracentrifuge, the amount of information obtained in the course of one sedimentation velocity experiment (i.e., number of scans) increased by several orders of magnitude. This change necessitated development of software for processing raw data, and these softwares have been worked out by different teams of researchers. Pioneering works in this area were made by Stafford [\(1992,](#page-37-10) 2000) and Stafford and Braswell [\(2004\)](#page-37-11); he elaborated the time derivative method dc/dt which is used in the Sedanal sedimentation velocity module. Several other methods have been developed for direct fitting of the sedimentation boundary; these methods are based both on approximate (Philo [1994;](#page-37-12) Behlke and Ristau [1997\)](#page-33-0) and numerical (Schuck [1998;](#page-37-13) Demeler and Saber [1998\)](#page-34-1) solutions of the Lamm equation. In these approaches, the diffusion process is directly taken into account. As a result, the distribution of sedimentation coefficients for the sample may be obtained, which in turn can be converted into the molar mass distribution. These software programs provide significant opportunities for extracting information from the impressive files of raw data obtained in the sedimentation velocity experiments by now.

The methods of molecular hydrodynamics are among the basic methods in polymer science and molecular biophysics (Tanford [1961;](#page-37-14) Volkenshtein [1963;](#page-38-0) Tsvetkov et al. [1970;](#page-38-1) Cantor and Schimmel [1980;](#page-34-2) Fujita [1990\)](#page-34-3). The information obtained by these methods is essential for understanding the structure and gross conformation of isolated macromolecules. Namely, these methods are useful for estimating the size and shape of the individual macromolecules, for judging how quick the chain is coiled; in other words, they help to understand the degree of rigidity or flexibility of macromolecules and get the information about the intrinsic nonideality of the chain state (i.e., strength of the long-range intrachain interactions).

This contribution considers the ways of the analysis of the results obtained in the study of individual linear synthetic and natural macromolecules using the hydrodynamic methods, especially velocity sedimentation. The main experimental studies of linear chain molecules have been carried out during the second half of the

twentieth century, but these studies are currently being continued with the aid of the modern analytical ultracentrifuge which is, however, now called "ProteomeLab<sup>TH</sup> XL-I Protein Characterization System" (strange nickname for the ultracentrifuge).

# **14.2 Essential Concepts of Molecular Hydrodynamics and Parameters Characterizing the Conformation of Linear Polymers**

The linear chain *macromolecules contract into a coil* due to free or hindered rotation around valence bonds between atoms which form the backbone. However, the selfcrossing configurations should be excluded from the consideration, i.e., *intrachain volume effects* should be taken into account. The *intrachain volume effects* lead to an increase in the chain size and also to changes of the chain size distribution function. In a weakly coiled chains, the *effects of intramolecular draining* are present, i.e., the flow of solvent molecules through a loose polymer coil is observed. This phenomenon leads to an increase in friction loss of the macromolecule moving in solution. The effects of the hydrodynamic interactions should be taken into consideration for the polymer coils moving in the solution. This interaction occurs not only between different macromolecules (*inter*coil interaction or concentration effects) but also within individual macromolecule (*intra*molecular interaction). The *intrachain hydrodynamic interaction* means that the moving chain element drags the solvent with it. The solvent is considered as a structureless continuum. The velocity of the adjacent solvent decreases proportionally to the distance from the chain element causing the flow. Other elements of the same chain involved in this velocity field are addicted by the driving fluid (solvent). These intrachain hydrodynamic interactions between the elements of the same chain in a moving liquid are described by the Oseen hydrodynamic tensor (Tanford [1961;](#page-37-14) Yamakawa [1971;](#page-38-2) Tsvetkov [1989;](#page-38-3) Doi [1996;](#page-34-4) Teraoka [2002;](#page-38-4) Rubinstein and Colby [2003\)](#page-37-15).

A linear polymer macromolecule is characterized by its molar mass (M), contour length (L), mean-square end-to-end distance  $(*h*<sup>2</sup>)$ , or mean-square radius of gyration  $(*R<sub>g</sub>*<sup>2</sup>)$  (Tanford [1961;](#page-37-14) Tsvetkov et al. [1970\)](#page-38-1); see Fig. [14.1.](#page-4-0) In the Gaussian coil limit, i.e., for the chains in the absence of intrachain excluded volume effects,  $\langle h^2 \rangle$  and  $\langle R_g^2 \rangle$  are related in a simple way:  $\langle h^2 \rangle = 6 \langle R_g^2 \rangle$ . It is<br>worth to mention that this relation is an exact result in the absence of excluded worth to mention that this relation is an exact result in the absence of excluded volume, but it also holds, in a proper approximation, for good solvents.

Hydrodynamic diameter (d), persistence length (a), or the Kuhn segment length  $(A = 2a)$ , and mass per unit length  $(M_L = M/L)$ , are the parameters being common for a homologous series of linear polymers which differs only by the contour lengths. For a homologous series of linear polymers, the mean-square end-to-end distance  $(\langle h^2 \rangle)$  and the mean-square radius of gyration  $(\langle R_g^2 \rangle)$  are related across the whole range of molar masses to the ratio of the contour length (L) to the



<span id="page-4-0"></span>**Fig. 14.1** Images of three coils having similar contour lengths  $(L_1 = L_2 = L_3)$  but different diameters *d* (1–3) and folded in varying degrees. These coils are characterized by the different statistical segment lengths  $(A: A_1 > A_2 = A_3)$ , different diameters  $(d: d_1 = d_2 > d_3)$ , different thermodynamic qualities of the solvent  $(\varepsilon_1 > 0, \varepsilon_2 = \varepsilon_3 = 0)$ , and different intracoil draining effects (drained (1), non-drained (2), and partially drained (3) coils)

persistence length (a) by the following relationships (Kratky and Porod [1949;](#page-35-8) Benoit and Doty [1953;](#page-33-1) Landau and Lifschitz [1963\)](#page-35-9):

<span id="page-4-1"></span>
$$
\langle h^2 \rangle = LA \left[ 1 - (1 - e^{-x}) / x \right], \tag{14.2}
$$

$$
\langle R_g^2 \rangle = a^2 \left\{ (x/3) - [1 - (2/x) [1 - ((1 - e^{-x})/x)] ] \right\} \tag{14.3}
$$

where  $x = L/a = 2 L/A$  is the reduced chain length.

The wormlike chain describes the behavior of chain molecules with the L/a values varying from very low to very high ones. For large (L/a) values, the wormlike chain has a Gaussian coil conformation. From this viewpoint, the wormlike chain is a more general model.

### **14.3 Relationships Between the Experimental Hydrodynamic Values and the Macromolecular Characteristics**

The main characteristics obtained by the methods of molecular hydrodynamics are the velocity sedimentation coefficient *s*0, the Gralen concentration coefficient  $k_s$ , the translational diffusion coefficient  $D_0$ , as well as the intrinsic viscosity [ $\eta$ ]. All the experimental values should be obtained in the limit of infinite dilution.

Different experimental measurements can be expressed as intrinsic values ([ $\eta$ ], [D],  $[s]$ ,  $k_s$ ) which are independent of the solvent properties at a first approximation. Each of these hydrodynamic characteristics is related to common macromolecular characteristics, which are, in the case of linear polymers, *M* and  $\langle h^2 \rangle$  (Svedberg) and Pedersen [1940;](#page-37-1) Flory [1953;](#page-34-5) Tanford [1961;](#page-37-14) Tsvetkov et al. [1970;](#page-38-1) Yamakawa [1971;](#page-38-2) Cantor and Schimmel [1980;](#page-34-2) Pavlov and Frenkel [1986,](#page-35-10) [1988\)](#page-36-2):

<span id="page-5-0"></span>
$$
[\eta] = \Phi < h^2 > ^{3/2} / M,\tag{14.4}
$$

$$
[D] \equiv D_0 \eta_0 / T = k / (P < h^2 >^{1/2}), \qquad (14.5)
$$

<span id="page-5-2"></span>
$$
[s] \equiv s_0 \eta_0 / \left( \Delta \rho / \Delta c \right) = M / P < h^2 > ^{1/2} N_A \Big), \tag{14.6}
$$

$$
k_s = B < h^2 > \frac{3}{2} / M,\tag{14.7}
$$

<span id="page-5-3"></span><span id="page-5-1"></span>where T is the absolute temperature, k is Boltzmann's constant, and  $N_A$  is Avogadro's number. The density increment  $(\Delta \rho / \Delta c)$  or buoyancy (Archimedes) factor  $(1 - \overline{v} \rho_0)$  is used to obtain a partial specific volume  $(\overline{v})$ , and  $\rho_0$  is the solvent<br>density  $\Phi$  and  $P$  are the Elory hydrodynamic parameters: B is also a hydrodynamic density.  $\Phi$  and P are the Flory hydrodynamic parameters; B is also a hydrodynamic dimensionless parameter. The values of  $\Phi = \Phi(L/A, d/A, \varepsilon)$  and  $P = P(L/A, d/A, \varepsilon)$  $\varepsilon$ ) are functions of the relative contour length (L/A) and relative diameter (d/A), and parameter  $\varepsilon$  characterizes the thermodynamic quality of the solvent (or the long intrachain interactions). In the case of the absence of the excluded volume effects, when  $\varepsilon = 0$ , the values of  $\Phi = \Phi(L/A, d/A, \varepsilon = 0)$  and  $P = P(L/A, d/A, \varepsilon = 0)$  are tabulated in the frame of the wormlike cylinder theory (Yamakawa and Fujii [1973,](#page-38-5) [1974\)](#page-38-6).

In the case of linear polymers of non-globular conformation, the sensitivity of the hydrodynamic characteristics to the changes in the molar mass decreases in the following order: Eq.  $(14.4) \approx$  $(14.4) \approx$  Eq.  $(14.7)$  > Eq.  $(14.5)$  > Eq.  $(14.6)$ .

The comparison of Eqs.  $(14.5)$  and  $(14.6)$  immediately leads to the second Svedberg relationship, which is an essence of one of the absolute method of the molar mass determination, i.e., sedimentation-diffusion analysis:

$$
M_{sD} = (RT / (1 - \overline{v} \, \rho_0)) (s_0 / D_0) = R [s] / aD \Big]
$$
 (14.8)

(The first Svedberg relationship is the relation [\(14.6\)](#page-5-3).)

#### **14.4 Degree of Solution Dilution**

The use of  $[\eta]$ , s<sub>0</sub>, and  $D_0$  requires extrapolation of the experimentally determined values to zero concentration of polymer *c*. In the vicinity of zero concentration, the following relationships (Tsvetkov et al. [1970;](#page-38-1) Yamakawa [1971\)](#page-38-2) are applied:

<span id="page-6-1"></span>
$$
\eta = \eta_0 \left( 1 + k_{1\eta} c + k_{2\eta} c^2 + \cdots \right) \text{ or } \left( \left( \eta / \eta_0 \right) - 1 \right) / c = k_{1\eta} + k_{2\eta} c + \cdots \quad (14.9)
$$

$$
D = D_0 \left( 1 + (2A_2 M - (k_s + \overline{\upsilon})) c + \cdots \right)
$$
 (14.10)

<span id="page-6-0"></span>
$$
s^{-1} = s_0^{-1} \left( 1 + (k_s + \overline{\upsilon}) c + \cdots \right) \tag{14.11}
$$

<span id="page-6-2"></span>where  $\eta$  and  $\eta_0$  are the dynamic viscosity of solution and solvent, A<sub>2</sub> is the second thermodynamic virial coefficient, and  $k_{1\eta}$ ,  $k_{2\eta}$ ,  $k_s$  are the concentration coefficients. All concentration coefficients in Eqs.  $(14.9, 14.10,$  $(14.9, 14.10,$  $(14.9, 14.10,$  and  $14.11)$  contain molecular information. Two of them are very useful, namely, the *first viscosity concentration coefficient*  $k_{1\eta} \equiv [\eta]$ , the so-called intrinsic viscosity, and the concentration sedi-<br>mentation coefficient k, the so-called Gralen coefficient mentation coefficient  $k_s$ , the so-called Gralen coefficient.

In order to satisfy the linear regressions  $(14.9, 14.10, \text{ and } 14.11)$  the solutions under study should belong to the zone of *dilute solutions*. This means that the neighboring coils in the solution must be spaced each other by a distance greater than their own size. The *degree of dilution* is usually characterized by dimensionless Debye parameter c[ $\eta$ ] (c is polymer concentration expressed in  $g \times cm^{-3}$ , [ $\eta$ ] is intrinsic viscosity expressed in cm<sup>3</sup>  $\times$   $\sigma^{-1}$ ). The product of the intrinsic viscosity intrinsic viscosity expressed in  $\text{cm}^3 \times \text{g}^{-1}$ ). The product of the intrinsic viscosity<br>and the concentration of the solution represents a good approximation of the and the concentration of the solution represents a good approximation of the volume fraction  $\phi$  of the polymer substance in solution, with  $\phi = nv_1/V = mv_1$  $N_A/VM = c \times 0.36 < h^2 >^{3/2} \times N_A/M = (0.36N_A/\Phi)c[\eta] \approx c[\eta]$ , where  $v_1 = 0.36$ <br>  $c h^2 >^{3/2}$  is the volume occupied by the macromolecular coil in solution and m  $\langle h^2 \rangle^{3/2}$  is the volume occupied by the macromolecular coil in solution and m is the overall mass of the polymer dispersed in overall volume of solution V. The condition  $c[\eta] = 1$  corresponds to the situation when each coil may contact with others and the coils start to overlap. The dilute solution regime corresponds to the others, and the coils start to overlap. The dilute solution regime corresponds to the inequality  $c[\eta] \ll 1$ ; the lower limit of concentration is determined by the sensitivity<br>of the optical detection system used. Thus, the concentration of the solutions of of the optical detection system used. Thus, the concentration of the solutions of linear macromolecules cannot characterize the degree of dilution of the solution. For example, the polymer solution with a concentration of  $\approx 0.4$  mg/ml =  $0.4 \times 10^{-3}$ <br>g/cm<sup>3</sup> may be not diluted if the intrinsic viscosity [n] is bigher than 2000 cm<sup>3</sup>/g (for g/cm<sup>3</sup> may be not diluted if the intrinsic viscosity [ $\eta$ ] is higher than 2000 cm<sup>3</sup>/g (for instance, this is the case for the high molar mass polystyrene Meyerhoff and Appelt [\(1979\)](#page-35-11)).

Note that since the  $k<sub>s</sub>$  value also characterizes the specific volume occupied by the macromolecule, the product  $k<sub>s</sub>c$  will characterize the degree of dilution too. However, for the flexible chain polymers, the condition  $k<sub>s</sub>c < 1$  will be stronger than the condition  $[\eta]c < 1$ , as far as  $k_s/[\eta] \approx 1.7$ . Meanwhile, for the rigid-chain

polymers, condition  $k_s c < 1$  will overestimate the degree of dilution, because in this case  $k_s/[\eta]$  is usually lower than 1.

#### **14.5 Error of** *ks* **Determination**

The concentration range should be wide enough to obtain a reliable extrapolation to zero concentration, i.e., to make estimation of both values with good accuracy: intercept  $(s_0)$  and slope  $(k_s/s_0)$ . We shall analyze the errors of determination of the  $s_0$  and  $k_s$  values. The mean square errors were determined by the mean square linear approximation of the dependences  $s^{-1} = f(c)$  following the relation [\(14.11\)](#page-6-2). By<br>way of example, let us consider the results obtained in the sedimentation study of way of example, let us consider the results obtained in the sedimentation study of chitosan and nitrate chitin solutions (Table [14.1](#page-8-0) and Fig. [14.2\)](#page-9-0) (Pavlov and Frenkel [1986\)](#page-35-10). Obviously, the error of  $k_s$  value is larger because it includes the error of  $s_0$ value and the error of the slope of the linear dependency  $(Eq, 14.11)$  $(Eq, 14.11)$ . The correlation between the relative errors of  $s_0$  and  $k_s$  values is given in Fig. [14.2.](#page-9-0)

#### **14.6** Scaling Relation Between  $k_s$  and  $s_0$

Since the publication of Newman and Eirich [\(1950\)](#page-35-12) where  $k<sub>s</sub>$  values were compared with the corresponding values of the intrinsic viscosity, attempts were made to determine the molecular meaning of the  $k<sub>s</sub>$  coefficient. But in the first place, it was a matter of optimizing the study of the concentration dependence of sedimentation coefficient for a number of polymer-homologous series of fractions/samples, sometimes reaching up to 30–40. For this purpose, the direct comparison between  $s_0$  and *ks* represents the most advantageous way.

The comparison of  $k_s$  and  $s_0$  allows establishing the cross-scaling relation between two experimental values (Pavlov and Frenkel [1982\)](#page-35-13). Replacing the  $\langle h^2 \rangle$  value in the relation  $k_s = B \langle h^2 \rangle^{3/2}/M$  with help of the Svedberg relation  $(s_0 = (1 - \overline{v} \rho_0)M/N_A P_0 \eta_0 < h^2 >^{1/2})$  allows to obtain the following relationship:

<span id="page-7-0"></span>
$$
k_s = B((1 - \overline{\nu}\rho_0) / N_A P_0 \eta_0) (M^2 / s_0^3)
$$
 (14.12)

Using Kuhn-Mark-Houwink-Sakurada-type scaling relation  $(s_0 = K_s M^{bs})$ , the following correlation may be obtained:

$$
k_s = \left(\left(1 - \overline{\nu}\rho_0\right) / N_A P_0 \eta_0\right) \left(B / K_s^{2/3}\right) s_0^{(2-3bs)/bs} = K_{kss} s_0^{v} \tag{14.13}
$$

where  $v \equiv v_1 = (2 - 3b_s)/b_s$ .<br>Alternative scaling relations

Alternative scaling relations  $(k_s \sim s_0^{\nu})$  can be obtained:  $\nu_2 = (4 - 3b_s)/3b_s$  from<br>Peterson theory (1964) of straight cylinder sedimentation (see also Fujita et al. the Peterson theory [\(1964\)](#page-37-16) of straight cylinder sedimentation (see also Fujita et al.





<span id="page-8-0"></span>the repeating unit of  $M_0 = 109$ . Chilosan fractional material mater sedimentation of these fractions was investigated using the analytical ultracentrifuge MOM 3170 (Hungary) at a rotor speed of 40 x 10<sup>3</sup> rpm in a double-sector synthetic boundary cell; the height of the centerpiece was 12 mm (Pavlov and Selyunin 1986). The optical system of recording the sedimentation boundary was 0.3 M NaCl. In this solvent of high  $\tilde{\mathsf{x}}$  $\times 10^{-2}$ . Velocity  $\times 10^3$  rpm in a double-sector synthetic boundary cell; the height of the centerpiece was 12 mm (Pavlov and Selyunin [1986\)](#page-36-3). The optical system of recording the sedimentation boundary was  $_0 = 1.05$  mPa  $\breve{ }$ ionic strength, the polyelectrolyte effects are suppressed. This solvent was characterized by the density  $\rho_0 = 1.015 \text{ g/cm}^3$  and the viscosity  $\eta$  $v\rho_0$ ) = 0.38 with a mean relative error of 4.7 sedimentation of these fractions was investigated using the analytical ultracentrifuge MOM 3170 (Hungary) at a rotor speed of 40  $M_0 = 169$ . Chitosan fractions were investigated in the following buffer solvent: 0.33 M CH<sub>3</sub>COOH values at 294 K. Buoyancy factor was determined pycnometrically and was equal to (1 the Lebedev's polarizing interferometer (Tsvetkov et al. 1970) the Lebedev's polarizing interferometer (Tsvetkov et al. [1970\)](#page-38-1)the repeating unit of



<span id="page-9-0"></span>**Fig. 14.2** Comparison of the relative errors of velocity sedimentation coefficient  $s_0$  and Gralen coefficient  $k_s$  for the chitosan fractions studied in buffer solvent 0.33 M CH<sub>3</sub>COOH + 0.3 M NaCl (*1*) and chitin nitrate fractions in dimethylformamide (*2*)



<span id="page-9-1"></span>**Fig. 14.3** Dependencies of the scaling coefficients  $\nu$  on  $b_s$ : (*I*)  $\nu \equiv \nu_1 = (2 - 3b_s)/b_s$  (Pavlov and Frenkel 1982): (*2*)  $\nu_2 = (4 - 3b_s)/3b_s$  for the straight cylinder (Peterson 1964): and (3) and Frenkel [1982\)](#page-35-13); (2)  $v_2 = (4 - 3b_s)/3b_s$  for the straight cylinder (Peterson [1964\)](#page-37-16); and (3)<br> $v_2 = (1 - b_s)/b_s$  for the coils under  $\theta$ -conditions (Imai 1970; Freed 1983; Muthukumar and de  $v_3 = (1 - b_s)/b_s$  for the coils under  $\theta$ -conditions (Imai [1970;](#page-34-6) Freed [1983;](#page-34-7) Muthukumar and de Mense 1983) Mense [1983\)](#page-35-14)

[1966\)](#page-34-8) and  $v_3 = (1 - b_s)/b_s$  for the random-coil macromolecules under  $\theta$ -conditions (Imai 1970; Freed 1983; Muthukumar and de Mense 1983). Figure 14.3 shows the (Imai [1970;](#page-34-6) Freed [1983;](#page-34-7) Muthukumar and de Mense [1983\)](#page-35-14). Figure [14.3](#page-9-1) shows the dependence of  $\nu$  on  $b_s$ .

The values of  $v_1$  and  $v_2$  are close to each other in the range of  $b_s < 0.3$ corresponding to rigid-chain macromolecules. At  $b_s = 0.5$  (random coils under  $\theta$ conditions), we have  $v_1 = v_3$ . Consequently, the cross-scaling dependence

<span id="page-10-0"></span>
$$
k_s = K_{kss} s_0^{(2-3bs)/bs} \tag{14.14}
$$

has a general meaning and can be used for  $b<sub>s</sub>$  value estimation for all spectrum of linear macromolecules.

Thus, the study of concentration dependence of sedimentation coefficient for three or four fractions in the possibly wide range of  $s_0$  allows to establish the correlation given in Eq. [14.13](#page-7-0) and to obtain a reliable estimation of the concentration coefficients  $k_s$  for other fractions of the studied series. Furthermore, the  $b_s$  value may be determined (Eq.  $14.14$ ); this is a key parameter in transformation of the sedimentation coefficient distribution of a sample into the molar mass distribution, as  $ds_0/dM = b_s K_s^{1/bs} s_0^{(bs-1)/bs}$ . The b<sub>s</sub> value is also necessary for the application<br>of the continuous  $c(s)$  model with general scaling law of Sedfit suite to treat the of the continuous  $c(s)$  model with general scaling law of Sedfit suite to treat the velocity sedimentation data.

It should be noted that the  $k_s$  values can vary within wide limits (from a few to several thousand of  $\text{cm}^3/\text{g}$  for the same homologous series of linear polymer systems. The  $k<sub>s</sub>$  values are different for linear macromolecules of various conformational status and scale differently with  $s_0$  values (Fig. [14.4\)](#page-10-1). In the case of globular structures, the values of  $k_s$  vary slightly ( $\approx$ (4–10) cm<sup>3</sup>/g) and are weakly dependent on the sedimentation coefficient (see Fig. [14.4](#page-10-1) and Table [14.2\)](#page-11-0). In the case of more rigid macromolecules, the more of them are draining, the greater are the values of  $k_s$  and the steeper is the dependence of  $k_s$  on  $s_0$  (Fig. [14.4\)](#page-10-1).

<span id="page-10-1"></span>



<span id="page-11-0"></span>

### **14.7 Scaling Relations Between Other Hydrodynamic Values and Molar Mass**

To quote from Fujita [\(1990\)](#page-34-3), "one of the most surprising generalities in the world of polymers is that  $[\eta]$  for a series of homologous polymers under a fixed solvent condition follows a simple power law over an extended range of M." We can add that such relationships are also observed for all other hydrodynamic characteristics:  $s_0, k_s$ , and  $D_0$  and between them; this was shown above for the  $s_0 - k_s$  correlation.<br>In principle, this kind of dependence is characteristic of fractal systems in which In principle, this kind of dependence is characteristic of fractal systems in which any part of the object is similar to the whole (de Gennes [1979;](#page-34-10) Mandelbrot [1982\)](#page-35-15). The comparison of hydrodynamic characteristics with each other and with molar mass allows to obtain cross (among hydrodynamic characteristics) and canonic (among hydrodynamic characteristics and molecular mass) relationships of Kuhn-Mark-Houwink-Sakurada type or hydrodynamic scaling relationships. In general, they may be given as the following:

<span id="page-12-0"></span>
$$
P_i = K_{ij} P_j^{bij} \tag{14.15}
$$

where  $P_i$  is one of the hydrodynamic characteristics  $[\eta]$ ,  $D_0$ ,  $s_0$ , or  $k_s$  and  $P_j$  is another hydrodynamic characteristic from this array or molar mass. In the case of homologous series of linear polymers, the scaling indices  $b_{ii}$  are intercorrelated (Tsvetkov et al. [1970;](#page-38-1) Pavlov and Frenkel [1995\)](#page-36-5) in the following ways:  $b_{sD} = b_s/b_D$ ,  $b_{D\eta} = b_D/b_{\eta}$ ,  $b_{s\eta} = b_s/b_{\eta}$ ,  $|b_D| = (1 + b_{\eta})/3$ ,  $|b_D| + b_s = 1$ , and  $b_{kss} = (2 - 3b_s)/b_s$ , where the double underline index refers to cross-correlations and the single where the double underline index refers to cross-correlations and the single underline index refers to correlations of appropriate hydrodynamic characteristic with molar mass. (For instance,  $b_{sD}$  is the index of the power function between *s*<sub>0</sub> and *D*<sub>0</sub>, which is represented as  $s_0 = K_{sD}D_0^{bsD}$ .  $b_s$  and  $b_D$  are the indices of the nower functions between **M** and *s*<sub>0</sub> and between **M** and *D*<sub>0</sub> respectively:  $s_0 = K M^{bs}$ power functions between M and  $s_0$  and between M and  $D_0$ , respectively:  $s_0 = K_s M^{bs}$ ,  $D_0 = K_D M^{bD}$ .)

It is important to note that further molecular interpretation of the hydrodynamic characteristics will be the more accurate the wider is the molar mass range of investigated homologous series. At the same time, the  $b_{ii}$  value may vary in different ways during the transition *from very high to very low molar masses (contour lengths)* (Bloomfield [1968;](#page-34-11) Budtov [1992\)](#page-34-12) (Fig. [14.5\)](#page-13-0).

For any kind of linear macromolecules, there is a certain range of contour lengths where the coil maturation happens. Just in this range of the molar masses, the changes in the slopes of KMHS plots may be observed. The change of the slope in the KMHS plots is more easy to observe for  $[\eta]$  dependence ( $b_{\eta}$  value) and less easy to see for the s<sub>0</sub> dependence (*b<sub>s</sub>* value), because  $[\eta] \sim \langle h \rangle^{3/2}$  and  $s_0 \sim \langle h \rangle^{1/2}$ , i.e. the value of [n] is more sensitive to changes in the size and shape of the coil i.e., the value of  $[\eta]$  is more sensitive to changes in the size and shape of the coil than the  $s_0$  value.

The analyzed polymer can be referred to a certain class according to the type of the change in the respective slope. This is illustrated in Fig. [14.5a.](#page-13-0) The data obtained for polyvinylpyrrolidone [\(14.1\)](#page-1-0) demonstrate a decrease in slope from  $b_{\eta} = 0.74$  in



<span id="page-13-0"></span>**Fig. 14.5** Scaling plots of the hydrodynamic characteristics: (**a**) canonical Kuhn-Mark-Houwink-Sakurada (KMHS) plot  $[\eta] = K_{\eta} M^{b\eta}$  and (b) dependencies of velocity sedimentation coefficient<br>on the molar mass in double logarithmic scale or KMHS-type plot  $s_0 = K M^{b\delta}$ on the molar mass in double logarithmic scale or KMHS-type plot  $s_0 = K_s M^{bs}$ 

The comparison of the linear macromolecules of different structures and equilibrium rigidity ric comparison of the finear macromotecules of unferent structures and equinorium rigidity<br>was made: flexible, poly(1-vinyl-2-pyrrolidone) (PVP) in 0.1 *M* sodium acetate solutions (*1*)<br>(Paylov et al. 1990); brushlike, st (Pavlov et al. [1990\)](#page-36-4); brushlike, styrene-methyl methacrylate brush copolymer in bromoform (*2*) (Magarik et al. 1978); rigid,  $poly(2,2'-p$ -phenylene-(5-benzimidazole)) isophthalamide (PBIA) in dimethylacetamide  $+3\%$ LiCl (3) (Pavlov and Selyunin [1986\)](#page-36-3); and extra-rigid, the triple helix of *Schizophyllum commune* polysaccharide (schizophyllan) in water (*4*) (Yanaki et al. [1980\)](#page-38-7)

the high molar mass region to  $b_n \approx 0.50$  in the low molar mass region; this pattern<br>corresponds to the behavior of flexible macromolecules in thermodynamically good corresponds to the behavior of flexible macromolecules in thermodynamically good solvents. Thus, in this case, the deviation of  $b<sub>η</sub>$  value from 0.5 in the high molar mass region is attributed to the intrachain volume effects (intrinsic nonideality). System 2 in Fig. [14.5a](#page-13-0) represents a thick macromolecule which is characterized by a large transverse dimension. In this case, a decrease in the slope of the  $[\eta]$  dependence *vs.* molar mass in the region of small contour lengths of the main chain is also observed. The  $b_{\eta}$  value can be significantly less than 0.5, which is explained by the comparability of longitudinal and transverse dimensions of the coil when the chain length is short enough. The systems 3 and 4 describe the behavior of the rigid polymer for which is characteristic the approaching of molecular conformation to slightly bending rod with decrease in chain contour length, and  $b_{\eta}$  becomes higher than 1. In this case, deviation of the  $b_{\eta}$  value from 0.5 is attributed to the effects of intramolecular draining associated with high equilibrium rigidity of the chains (high values of persistent length). The  $[\eta]$  dependence *vs*. molar mass for rigid macromolecules is concave downward in the opposite direction as compared with that for flexible macromolecules which is concave upward (system 1). Figure [14.5b](#page-13-0) shows the dependence of  $s_0$  *vs.* molar mass for the same systems. In this connection, two circumstances should be noted. First, the changes in the slopes of the curves shown in this figure are much weaker than the slope for the intrinsic viscosity values; second, these changes should show the opposite trend.

Table [14.2](#page-11-0) gives the comparison between the  $b_s$ ,  $b_\eta$ , and  $b_{kss}$  indexes for linear macromolecules with different conformational status. Comparison of variation of the  $b_{\eta}$  and  $b_{\text{kss}}$  indices with changing conformational type of the macromolecules shows that the direct comparison between the sedimentation coefficient  $s_0$  and the Gralen coefficient *ks* is more sensitive to conformational changes of macromolecules than the comparison between  $[\eta]$  and M. This fact has led to the establishment of conformational zones of macromolecules considering the normalized plot of  $k_s M_l$ vs.  $[s]/M_L$ . It is one of the examples of self-sufficiency of the sedimentation velocity method in the conformational analysis of linear polymers (Pavlov and Frenkel 1986; Pavlov [1997\)](#page-36-6).

### **14.8 Another Level of Self-Sufficiency of Velocity Sedimentation Data: Sedimentation Parameter and Hydrodynamic Invariant**

Wales and van Holde [\(1954\)](#page-38-8) were the first to suggest estimating molar masses of polymers from the experimental data obtained in the study of the concentration dependence of sedimentation velocity. As was shown by Wales and van Holde [\(1954\)](#page-38-8), using the  $s_0$  and  $k_s$  values, it is possible to estimate the molar mass of the flexible polymer chains by the following relation:

<span id="page-14-1"></span><span id="page-14-0"></span>
$$
M = 4.85 \pi N_A [s]^{3/2} k_s^{1/2}
$$
 (14.16)

A reexamination of this problem from the original theoretical standpoint was carried out later by Rowe [\(1977\)](#page-37-17). The definitive result for the sedimentation of solvated molecules is given in the following equation:

$$
M = N_A (6\pi)^{3/2} [s]^{3/2} \{ (3\overline{\upsilon}/4\pi) \left[ (k_s/2\overline{\upsilon}) - (v_s/)\right] \}^{1/2}
$$
 (14.17)

where  $v_s$ , according to Rowe, is the specific volume occupied by the sedimenting component (solute  $+$  entrained solvent  $+$  bound solvent). Rowe gave the following approximation for the  $v_s/\overline{v}$  ratio:

$$
v_s/\overline{\upsilon} = k'(k_s/[\eta])^{-1}
$$
\n(14.18)

where  $k'$  is the Huggins parameter. For the majority of polymer systems, the second term in brackets in Eq. [\(14.17\)](#page-14-0) is negligible as compared with the first one and is far lower than the error of  $k<sub>s</sub>$  determination, so Eq.  $(14.17)$  can be rearranged as:

<span id="page-14-2"></span>
$$
M \cong 9\pi N_A[s]^{3/2} k_s^{1/2} \tag{14.19}
$$

Equations [\(14.16\)](#page-14-1) and [\(14.19\)](#page-14-2) differ only in numerical coefficients, and for some comparative purposes (e.g., scaling relation), they can give the same results.

The Wales-van Holde-Rowe Eqs. [\(14.16](#page-14-1) and [14.19\)](#page-14-2) were presented in general form with the introduction of the sedimentation parameter  $\beta$ <sub>s</sub> (Pavlov and Frenkel [1986\)](#page-35-10). In fact, this idea has been already implicitly contained in the paper of Wales and van Holde [\(1954\)](#page-38-8). Actually, the sedimentation coefficients  $s_0$  (first Svedberg equation) and  $k_s$  depend differently on molecular mass and size of macromolecules (Eqs. [14.6](#page-5-3) and [14.7\)](#page-5-1). The exclusion of  $\langle h^2 \rangle$  from Eqs. [\(14.6\)](#page-5-3) and [\(14.7\)](#page-5-1) allows to obtain the following expression:

<span id="page-15-1"></span>
$$
\beta_s \equiv B_s^{1/3} P_0^{-1} = N_A \left[ s \right] \ k_s^{1/3} M^{-2/3} \tag{14.20}
$$

where  $\beta_s$  is the sedimentation parameter introduced by Pavlov and Frenkel [\(1986,](#page-35-10) [1988,](#page-36-2) [1995\)](#page-36-5).

Obviously, the sedimentation parameter  $\beta_s$  is an analogue of the hydrodynamic invariant  $\beta$  (Mandelkern and Flory [1952\)](#page-35-17).

The introduction of the sedimentation parameter was supported by the extensive set of experimental data available in the literature for linear uncharged polymers, both synthetic and natural. Analysis of almost entire data library on the velocity sedimentation of macromolecules indicates that the value of parameter  $\beta_s$  is practically invariant both in terms of molar mass and with respect to the structure of the repeating unit of the linear polymer (Pavlov and Frenkel [1995;](#page-36-5) Pavlov [1997\)](#page-36-7). Table [14.3](#page-15-0) lists the average experimental values of the sedimentation parameter  $\beta_s$ , parameter  $B_s$  for different polymer classes, and also classical hydrodynamic invariant  $\beta = A_0/k$ .

The invariance of  $\beta_s$  value makes it possible to use Eq. [14.20](#page-15-1) for determining molar mass of the polymer macromolecules using the data obtained only from

invariant $\beta$ (and $A_0$ ), and parameter $B_s$						
	$\beta_s^a 10^{-7}$	$B_{s}10^{-23}$	$\beta^{**}10^{-7}$			
Polymer-solvent	$mol-1/3$	$mol-1$	$mol-1/3$	$A_0{}^b 10^{10}$		
Flexible-chain polymers under $\theta$ -conditions	1.0	1.33	1.08	3.21		
Flexible-chain polymers in thermodynamically good solvents.	1.25	2.61	1.08	3.21		
Rigid-chain polymers	1.0	1.33	1.24	3.69		
$\beta$ 1-4 glucanes and their derivatives	1.0	1.33	1.14	3.39		
Globular proteins	1.17	2.14	1.01	3.00		

<span id="page-15-0"></span>**Table 14.3** Averaged experimental values of the sedimentation parameter  $\beta_s$ , hydrodynamic invariant  $\beta$  (and  $A_0$ ), and parameter  $B_s$ <br>  $\beta_s^a 10^{-7}$   $B_s 10^{-23}$   $\beta^{**} 10^{-7}$ 

<sup>a</sup>Mean-square errors are  $\approx 6 \%$ ,  $P_0 = 5.11$ 

 ${}^{\text{b}}A_0 = k\beta$  – Mandelkern-Flory-Tsvetkov-Klenin hydrodynamic invariant, *k* is Boltzmann constant Note that expressed in the same unit the both  $\beta$  and  $\beta_s$  values are close to each other (see Table [14.3,](#page-15-0) columns 2 and 4)



<span id="page-16-1"></span>Fig. 14.6 Comparison of the molar mass values for chitosan (1) and chitin nitrate (2) calculated from the data of the sedimentation-diffusional analysis ( $M_{sD}$ ) and from the  $s_0$  and  $k_s$  values ( $M_{ks}$ , Eq. [14.21\)](#page-16-0). Chitosan fractions were investigated in a buffer solvent: 0.33 M CH<sub>3</sub>COOH  $+$  0.3 M NaCl. Chitin nitrate fractions were investigated in dimethylformamide. *Dashed line* is drawn with a slope equal to 1

velocity sedimentation experiments:

<span id="page-16-0"></span>
$$
M_{ks} = (N_A/\beta_s)^{3/2} [s]^{3/2} k_s^{1/2}
$$
 (14.21)

Good correlation is observed between independently measured  $M_{sD}$  values and those determined from the  $s_0$  and  $k_s$  values. Figure [14.6](#page-16-1) demonstrates this kind of correlation observed for fractions of chitosan and chitin nitrate.

Knowledge of the molar masses opens up the possibilities for further molecular interpretation of  $s_0$  and  $k_s$  values. Useful applications of this concept have been demonstrated in various publications for different polymers (Tarabukina et al. [1991;](#page-37-18) Pavlov et al. [1995,](#page-36-8) [2003;](#page-36-9) Harding et al. [2011a;](#page-34-13) Morris and Harding [2013\)](#page-35-18).

One of the definitions of Flory-Mandelkern-Tsvetkov-Klenin hydrodynamic invariant  $\beta$  (or  $A_0 = k\beta$ ) (Mandelkern and Flory [1952;](#page-35-17) Tsvetkov and Klenin [1953\)](#page-38-9) is given by the following relation:

<span id="page-16-2"></span>
$$
\beta \equiv \Phi^{1/3} P^{-1} = N_A \left[ s \right] [\eta]^{1/3} M^{-2/3}
$$
 (14.22)

(Traditionally, in this case, the intrinsic viscosity is denominated in  $100 \text{ cm}^3/\text{g}$ .)

The ratios  $\Phi^{1/3}/P$  and  $B^{1/3}/P$  and thus  $A_0$  and  $\beta_s$  are not strictly constant even theoretically (Table [14.4\)](#page-17-0); they are experimentally found to be invariant (i.e., within the incertitude of the measurements) in the case of homologous polymers with different chain lengths. The theoretical values of the Flory hydrodynamic parameters  $P_0$  and  $\Phi_0$  depend on the models and mathematical approximations. The limiting theoretical values of  $\Phi$  and P for a Gaussian coil ( $M \to \infty$ ), obtained after a preliminary averaging of the hydrodynamic Oseen's tensor, are  $\Phi_0 = 2.87 \cdot 10^{23}$ 

$P_0$	$\Phi_0 10^{-23}$ mol <sup>-1</sup>	$A_0$ 10 <sup>10</sup>	References
(Sphere) $6\pi^a$	(Sphere) $2.5^{\text{a}}$	2.914	Tanford $(1961)$
$7.35^{b}$	4.3	3.05	Kuhn et al. $(1953)$ and Tsvetkov et al. $(1970)$
5.11 <sup>c</sup>	3.62	4.15	Kirkwood and Riseman (1948)
5.11 <sup>c</sup>	2.19	3.51	Hearst and Tagami (1965)
5.11 <sup>c</sup>	2.86	3.84	Hearst and Stokmayer (1962) and Yamakawa and Fujii (1973, 1974)
5.99 <sup>d</sup>	2.51	3.13	Zimm (1980) and de la Torre et al. (1982, 1984)
5.3 <sup>d</sup>	1.9	3.23	Bernal et al. $(1991)$
6.20 <sup>e</sup>	2.36	2.96	Oono (1985)

<span id="page-17-0"></span>**Table 14.4** Theoretical values of Flory hydrodynamic parameters  $P_0$ ,  $\Phi_0$ , and hydrodynamic invariant  $A_0 = kP_0 \Phi_0^{-1/3}$  (g cm<sup>2</sup> s<sup>-2</sup> K<sup>-1</sup> mol<sup>-1/3</sup>) for polymer chains in the absence of intrachain<br>excluded volume effects<br> $P_0$   $\phi_0$  10<sup>-23</sup>mol<sup>-1</sup>  $A_0$  10<sup>10</sup> References 1 values of Flory hydro<br>  $1/3$  (g cm<sup>2</sup> s<sup>-2</sup> K<sup>-1</sup> mol<sup>-1</sup> excluded volume effects mvariant  $A_0 = kP_0 \Phi_0^{-1}$ <br>xcluded volume effects<br> $P_0$   $\rho_0$  10<sup>-</sup>

<sup>a</sup>For sphere  $f_0 = 6\pi \eta_0 R$ ;  $[\eta] = 2.5 (4\pi/3) N_A (R^3/M)$ <br><sup>b</sup>Obtained with macroscopic models of polymer chains

bObtained with macroscopic models of polymer chains

cObtained with preaveraging approximation of the tensor of the hydrodynamic interactions

dObtained by Monte Carlo simulation without preaveraging approximation

eObtained with renormalization groups theory



<span id="page-17-1"></span>**Fig. 14.7** The Flory parameters *P* (*A*) and  $\Phi$  (*B*) as function of the relative contour length  $L/A$ of wormlike cylinder in semilogarithmic scale for different relative thickness *d*/*A* of cylinder from  $d/A = 0.001$  up to  $d/A = 1$  (Yamakawa and Fujii [1973,](#page-38-5) [1974\)](#page-38-6)

and  $P_0 = 5.11$  (Yamakawa [1971;](#page-38-2) Tsvetkov [1989,](#page-38-3) Fig. [14.7\)](#page-17-1). They are affected by the preaveraging of the Oseen hydrodynamic tensor, as studied by the Monte Carlo simulation method (Zimm [1980;](#page-38-10) de la Torre et al. [1982,](#page-34-16) [1984;](#page-34-17) Bernal et al. [1991\)](#page-34-18) and by renormalization group calculations (Oono [1985\)](#page-35-21).

Thus, the basis of the similarity of two invariants is the same physical dimensions (cm<sup>3</sup>/g); in other words, both [ $\eta$ ] and  $k_s$  are the functions of the specific volume of macromolecules. At the same time, Eqs. [14.20](#page-15-1) and [14.22](#page-16-2) expose the fundamental difference between  $\beta$  (or  $A_0$ ) and  $\beta_s$ . This difference consists of the following. The value  $\beta$  is obtained from M and from two experimental values  $s_0$  and  $[\eta]$  which, in turn, are obtained in different kinds of experiments. In these experiments, a macromolecule performs different kinds of movement, namely, translational  $(s_0)$ and rotational ([ $\eta$ ]). The sedimentation parameter  $\beta_s$  is obtained from M and two experimental values  $s_0$  and  $k_s$  obtained in a single series of experiments where the macromolecule is studied under exactly the same translational conditions.

The calculation of the hydrodynamic invariants  $A_0$  and  $\beta_s$  is a check for the mutual coherence of a set of the experimental data. These values should not go beyond a certain range of values indicated in Tables [14.3](#page-15-0) and [14.4.](#page-17-0) Positioning of the  $A_0$  and  $\beta$ <sup>*s*</sup> values in these ranges allows further interpretation of the hydrodynamic characteristics. Otherwise, we need to analyze the causes of mismatch in the primary experimental data or to admit that the sizes of macromolecules are not equivalent in different types of movements.

## **14.9 Relationship Between Hydrodynamic Values and Conformational Parameters A and d in the Model of Wormlike Chain**

In the limit of low molar mass chains  $(L/A < 2.3; L \gg d)$ , a model of a weakly bending rod or a cylinder can be used that provides *ML* and *d* through a linear regression (Broersma [1969;](#page-34-19) Yamakawa and Fujii [1973\)](#page-38-5):

<span id="page-18-0"></span>
$$
[s] = (M_L/3\pi N_A) [lnM - ln (M_L d) + 0.386)
$$
 (14.23)

In principle, the slope of  $[s] = f(lnM)$  in the range of lowest *L*/*A* values (<2) allows estimating linear density of the chain *ML*. For this purpose, a sufficient number of experimental data in the corresponding range of molar masses should be available. However, these conditions are not frequently realized. The rare examples are the cases of extra-rigid macromolecules (Yanaki et al. [1980;](#page-38-7) Sato et al. [1984\)](#page-37-19). The more flexible are the macromolecules, the lower molar mass samples must be studied (Fig. [14.8\)](#page-19-0). This condition imposes significant restrictions on using velocity sedimentation data to obtain the *ML* value.

A similar relationship was obtained for the intrinsic viscosity of slightly bending rods:

$$
M^2/[\eta] = (45M_L^3/2\pi N_A) [\ln M - \ln (M_L d) - 0.697] \tag{14.24}
$$

It should be noted that the intrinsic viscosity data must be obtained in the region of smaller contour lengths (i.e., molar masses) than that used in velocity sedimentation experiments. This condition renders it more difficult to use intrinsic viscosity for determining the *ML* value.

The dimensions of long linear chains are determined by two main factors: the short- and long-range interactions. The stronger is the short-range interaction, the stiffer is the chain; therefore, the coil becomes spongy, i.e., permeable for solvent



<span id="page-19-0"></span>**Fig. 14.8** Determination of mass per unit length *ML*, the ratio of mass *M* to contour length *L*, and **Eig. 14.8** Determination of mass per unit length  $M_L$ , the ratio of r<br>the hydrodynamic diameter d of heparin in 0.2 *M* NaCl (1and 1<sup>1</sup>) the hydrodynamic diameter d of heparin in  $0.2 M$  NaCl (1 and 1') (Pavlov et al. [2003\)](#page-36-9), poly  $\{4-$ **Fig. 14.8** Determination of mass per unit length  $M_L$ , the ratio of mass the hydrodynamic diameter d of heparin in 0.2 M NaCl (1 and 1') (Paper-<br>[4-(hexyloxy)phenyl]ethynylphenyl methacrylate} in toluene (2 and 2'nolv(2 ) (Pavlov et al. [2012\)](#page-36-10), and rig. 14.6<br>the hydro<br>[4-(hexyl<br>poly(2,2' poly(2,2'-p-phenylene-(5-benzimidazole)) isophthalamide in dimethylacetamide + 3 % LiCl (3 and 3') (Pavlov et al. 1985) from the plot of  $s_0$  versus ln M. The linear extrapolation (dashed line 1', 2', and 3') was made us  $[4-(hea)$ <br> $poly(2)$ <br>and 3<sup>'</sup> and 3') (Pavlov et al. [1985\)](#page-35-22) from the plot of  $s<sub>0</sub>$  versus ln *M*. The linear extrapolation (dashed line  $1'$ ,  $2'$ , and  $3'$ ) was made using the fractions of smallest *M*. The slope and intercept allow to determine *ML* and *d*, respectively, within the framework of the weakly bending rod model or the cylinder model (Eq. [14.23\)](#page-18-0), usable in the theoretical limit of  $L/A < 2.3$ . For heparin chain, the following results and *d*, respectively, within the framework of the weakly bending rod model or<br>the cylinder model (Eq. 14.23), usable in the theoretical limit of  $L/dA < 2.3$ . For heparin chain, the<br>following results were poly $\{4-[4-(\text{hexyloxy})\text{phenyl}]\}$ ethynylphenyl methacrylate} chain  $M_L$  was equal to (1520  $\pm$  60) and d was equal to  $(2.1 \pm 0.1)$ . The data obtained for polyamide benzimidazole macromolecules did not contradict to the theoretical value of  $M_L = 190$ 

molecules. The long-range effects are apparent in very long chains regardless of their stiffness, but it is easier to observe and study the long-range interactions in the flexible polymers. In the case of flexible polymers, the chain is contracted significantly, and there is a high probability of interaction between the remote chain monomer units. The most part of polymer coil becomes impermeable for a solvent; flexible macromolecules manifest the effects of thermodynamic interaction between polymeric material and solvent molecules.

The detailed modeling theories of hydrodynamic characteristics are elaborated for two models of macromolecules *without the volume effects*: wormlike necklace (Hearst and Stokmayer [1962;](#page-34-15) Hearst [1964\)](#page-34-20) and wormlike cylinder (Yamakawa and Fujii [1973,](#page-38-5) [1974\)](#page-38-6). These model theories do not take into account the excluded volume effects and attribute the change in coil size solely to the change in persistence length. Note that in the case of chains without volume interactions, the  $b_{\eta}$  index varies from 1.8 for slightly bending rod (very stiff and/or very short chains) to 0.5 for a Gaussian coil (very long chain independently of the rigidity). Meanwhile, in the case of the chain with volume interactions, the  $b_{\eta}$  index varies

from 0.8 for long chains with strong volume interactions to 0.5 for a Gaussian coil (no volume interactions or very short flexible chains). The procedure taking into account the influence of volume effects on transport characteristics was developed on the basis of linear approximation of the dependence of swelling coefficient of flexible macromolecules  $(\alpha)$  on the excluded volume parameter  $(z)$ ,

$$
\alpha = \left[ \langle h^2 \rangle / \langle h^2 \rangle \theta \right]^{1/2} = 1 + Cz + \cdots, \tag{14.25}
$$

where  $\langle h^2 \rangle$ ,  $\langle h^2 \rangle$  are the size of the swelling coil and the size of the coil in  $\theta$ -conditions, respectively. The numerical coefficient *C* for short chains depends on the relative contour length  $(L/A)$ ,  $C = C(L/A)$ , and with increasing chain length, the *C* value tends to the limit  $C = 4/3$  (Yamakawa and Stockmayer [1972\)](#page-38-11). The excluded volume parameter *z* describes the number of collisions between chain segments per unit volume occupied by the macromolecule. Finally for flexible chains with moderate excluded volume effects, the data on translation friction are treated with the aid of the Cowie-Bywater plot [\(1965\)](#page-34-21), and the data on intrinsic viscosity are processed using the Burchard-Stockmayer-Fixman plot [\(1961;](#page-34-22) [1963\)](#page-37-20). In this case, the change of the coil size is related exclusively to the change in the thermodynamic quality of the solvent.

Up to now, the more complete theory that takes into account the simultaneous influence of draining and excluded volume effects on the translation friction coefficient is Gray-Bloomfield-Hearst (GBH) theory [\(1967\)](#page-34-23). Unfortunately, this translation friction (sedimentation) coefficient theory has found insufficient dissemination and application, apparently, because the corresponding equation has not been represented in an easy form to use. In the case of the intrinsic viscosity theory (Sharp and Bloomfield [1968\)](#page-37-21), the authors have received only an asymptotic expression for extremely large values of molar mass.

The sedimentation coefficient calculations (Gray et al. [1967\)](#page-34-23) were carried out for distant segment pairs using the parameter  $\varepsilon$  which characterizes the deviations of the mean-square end-to-end distance from the Gaussian form due to volume swelling effects ( $\langle h^2 \rangle \sim M^{1+\epsilon}$ ). For close segment pairs, when volume interactions are small, the Porod-Kratky statistics have been applied. The analytical result for the velocity sedimentation coefficient is given in Eq. [\(14.10\)](#page-6-1) in Gray et al. [\(1967,](#page-34-23) p.1495). This equation may be rearranged for *L*/*A* > 2.3 in a more compact form as shown in Pavlov et al. [\(1990\)](#page-36-4):

<span id="page-20-0"></span>
$$
[s]P_0N_A = (3/(1 - \varepsilon)(3 - \varepsilon)(M_L^{(1+\varepsilon)/2}/A^{(1-\varepsilon)/2})M^{(1-\varepsilon)/2}
$$
  
+  $(M_L P_0/3\pi) [ln (A/d) - (d/3A) - \varphi(\varepsilon)]$  (14.26)

where  $P_0$  and  $\Phi_0$  are Flory hydrodynamic coefficients and  $\varphi(\varepsilon) = 1.431 + 2.635\varepsilon$  $+4.709\varepsilon^2 + \cdots$ 

In the case of  $\varepsilon = 0$ , i.e., in the absence of the intrachain excluded volume effects, Eq. [14.26](#page-20-0) is transformed into the expressions obtained in the theories of Hearst and Stockmayer [\(1962\)](#page-34-15) and Yamakawa and Fujii [\(1973\)](#page-38-5):

<span id="page-21-0"></span>
$$
[s] N_A P_0 = (M_L/A)^{1/2} M^{1/2} + (P_0 M_L/3\pi) [ln(A/d(A/d) - \varphi(0)] \qquad (14.27)
$$

where  $\varphi(0)$  depends on the model used  $(\varphi(0) = 1.431$  for the wormlike necklace model (Hearst and Stokmayer [1962\)](#page-34-15) or  $\varphi(0) = 1.056$  for the wormlike cylinder model (Yamakawa and Fujii [1973\)](#page-38-5), respectively).

Viscometry data in the range of the molar mass values when  $L/A > 2.3$  may be treated by changing the variables  $[s]P_0N_A = (M^2\Phi_0/[\eta])^{1/3}$  according to Pavlov et al.<br>(1990) and using the corresponding relationship (Eq. 14.26). When  $L/4 > 2.3$  linear [\(1990\)](#page-36-4) and using the corresponding relationship (Eq. [14.26\)](#page-20-0). When *L*/*A* > 2.3, linear approximations of the  $s_0$  and/or  $(M^2/[\eta])^{1/3}$  vs.  $M^{(1-\epsilon)/2}$  may be applied (Eqs. [14.26](#page-20-0)) and [14.27\)](#page-21-0). The slope of these straight lines allows evaluation of the chain persistence length, and the intercept allows estimating the hydrodynamic diameter of the chain. Some examples are presented in Fig. [14.9,](#page-21-1) i.e., the treatments of data using the  $s_0$  and  $[\eta]$  values for two different systems (polyamide benzimidazole in DMAA + 3 % LiCl at  $21^{\circ}$  C (Pavlov et al. [1985\)](#page-35-22) and polyisobutylene in n-heptane at  $25^{\circ}$  C (Abe et al. [1993\)](#page-33-2)).



<span id="page-21-1"></span>**Example 14.5** Dependences of  $s_0$  (a) and  $(M^2|I|)$  (b) on  $M^2$  used for the estimation of the statistical segment length *A* (or the persistent length  $a = A/2$ ) and the hydrodynamic diameter benzimidazole fractions in d in correspondence with the Gray-Bloomfield-Hearst theory (relationships (25)) for polyamide benzimidazole fractions in DMAA + 3 % LiCl at 21  $^{\circ}$ C (a) and polyisobutylene in n-heptane at 25  $^{\circ}$ C (b) of different sizes. For polyamide benzimidazole macromolecules (Pavlov et al. [1985\)](#page-35-22), the following estimations were obtained: the parameter  $\varepsilon = 0$ , the values  $A_f = (6.9 \pm 0.7)$  nm, and  $d_f = (0.4 \pm 0.2)$  nm with  $P_0 = 6.0$  (Fig. [14.9a\)](#page-21-1). For polyisobutylene macromolecules (Abe et al. [1993\)](#page-33-2), correspondingly,  $\varepsilon = 0.10$ ,  $A_{\eta} = (1.40 \pm 0.01)$  nm, and  $d_{\eta} = (0.20 \pm 0.07)$  nm with  $\Phi_0 = 2.3 \times 10^{23}$  (Fig. 14.9b)  $\Phi_0 = 2.3 \times 10^{23}$  (Fig. [14.9b\)](#page-21-1)

#### **14.10 Multi-Hydfit Program**

In the relatively recent works of de la Torre and his colleagues (Ortega and de la Torre [2007,](#page-35-23) [2013;](#page-35-24) Amoros et al. [2011\)](#page-33-3), a method of computer processing of the experimental data obtained in independent experiments is developed. The aim of this approach is to obtain the structural and conformational parameters of linear macromolecules. The authors introduce the dimensionless ratio of the experimental values to the corresponding values for the rigid sphere (concept of bead-model hydrodynamics (de la Torre and Bloomfield [1981\)](#page-34-24)). The persistence length, diameter, and mass per unit length can be evaluated using Multi-Hydfit program; this program performs a minimization procedure aimed at finding the best values of a, d, and  $M<sub>L</sub>$ , satisfying the equations which describe hydrodynamic behavior of persistence cylinders without the excluded volume effects (Yamakawa and Fujii [1973,](#page-38-5) [1974\)](#page-38-6). The Multi-Hydfit program then "floats" the variable parameters in order to find a minimum of the multi-sample error function (Ortega and Torre [2007\)](#page-35-23), which is calculated using equivalent radii. The equivalent radius is defined as a radius of an equivalent sphere having the same value as the determined characteristic (translation diffusion and/or velocity sedimentation coefficients and intrinsic viscosity). The error function is a dimensionless estimate of the agreement between the experimentally measured characteristic and the theoretical values of a, d, and ML calculated for the selected hydrodynamic characteristic and for a particular molar mass. The last version of program also includes the option for chains with the excluded volume effects, e.g., for poly(isobutylene) in n-heptane (Amoros et al. [2011\)](#page-33-3). This important addition concerns on a huge class of flexible chain polymers, both synthetic and natural origin.

The final results of Multi-Hydfit program are presented as the maps of conformation-structural parameters like the topographic maps. This is illustrated in Fig. [14.10](#page-23-0) which demonstrates the result of handling hydrodynamic data by Hydfit program. The measurements were performed on a series of samples of alternating styrene/diphenylethylene copolymers functionalized with terpyridine in toluene solutions; the molecular mass range was  $1.7 < M \times 10^{-3}$  g/mol <25.2 (Pavlov et al. 2009) [2009\)](#page-36-11).

# **14.11 Further Steps of the Analysis of the Hydrodynamics Data of Homologous Series of Linear Macromolecules**

It should be noted that as well as for non-computerized procedures, the sought-for estimates are more adequate, the wider is the range of studied molecular masses. It is especially important to have a sufficient number of samples of low molecular masses, when  $L/A$  is less than 2, to obtain the reliable and adequate value of  $M_L$ . However, the choice between intramolecular effects of excluded volume and/or of intrachain draining in doubtful cases of semiflexible macromolecules is beyond the



<span id="page-23-0"></span>**Fig. 14.10** Hydfit contour plot of the percent typical deviation,  $100\Delta$ , of the alternating styrene/diphenylethylene copolymers functionalized with terpyridine molecule in toluene with a fixed value of  $M_L = 564$  g/(mol nm), showing the minimum of the deviation at the following values of persistence length,  $a = 2$  nm and  $d = 1.1$  nm (Pavlov et al. [2009\)](#page-36-11)

capabilities of these approaches. One unresolved macromolecular hydrodynamic problem concerns the partition of the influence of the draining and volume effects on the size of the macromolecular chain. The value of parameter  $\varepsilon$  can/should be divided into two components: one is responsible for the volume effects  $(\varepsilon_v)$  and the other one for the flow of solvent molecules through the polymer coil  $(\varepsilon_d)$ :  $\varepsilon = \varepsilon_v + \varepsilon_d$ . In Eq. [14.26,](#page-20-0) only the  $\varepsilon_v$  part should be used for estimating statistical segment length and hydrodynamic diameter.

Finally, generalization of the hydrodynamic data, namely, the intrinsic viscosity and velocity sedimentation coefficient values can be made by the double normalization of the canonical KMHS equations by the structural parameter  $M<sub>L</sub>$  and the statistical segment length *A* taking into account the both parameters (Pavlov et al. [1999;](#page-36-12) Pavlov [2005,](#page-36-13) [2007\)](#page-36-14). In this procedure, the chain contour length *L* is calculated for a unit of the statistical segment length *A*, i.e., *(L/A)*. The fundamental



<span id="page-24-0"></span>**Fig. 14.11** Double normalized plots of  $[\eta]M<sub>L</sub>A<sup>2</sup>$  (a) and  $[s]M<sub>L</sub><sup>-1</sup>(b)$  vs. relative contour length *LA*- $LA^{-1}$  presented in double logarithmic scale. This figure interprets the data given in Fig. [14.5.](#page-13-0) Comparison of linear macromolecules of different structures, different equilibrium rigidities, and different scaling indices was made; these macromolecules are poly(1-vinyl-2-pyrrolidone) in 0.1 M sodium acetate solutions (*1*), styrene-methyl methacrylate brush copolymer in bromoform (*2*), comparison of mean macromotecules of unferent structures, unterest equinorium rigidates, and<br>strifferent scaling indices was made; these macromolecules are poly(1-vinyl-2-pyrrolidone) in 0.1 M<br>poly(2,2'-p-phenylene-(5-benz and the triple helix of *Schizophyllum commune* polysaccharide (schizophyllan) in water (*4*). The following lengths of the statistical segment  $A \times 10^8$  cm and the relative hydrodynamic diameters  $(d/A)$  are obtained for comparing macromolecules: 22 and 0.2 (1), 90 and 0.5 (2), 90 and 0.06 (3), 4000 and 0.007 (4)

Flory-Fox [\(14.4\)](#page-5-0) and Svedberg [\(14.6\)](#page-5-3) equations can be transformed into the following relationships:

$$
[\eta] M_L / A^2 = \Phi (L / A, d / A, \varepsilon) \times (L / A)^{1/2}
$$
 (14.28)

$$
[s] / M_L = (P (L/A, d/A, \varepsilon) N_A)^{-1} \times (L/A)^{1/2}
$$
 (14.29)

where *L/A* is the relative contour length and *d/A* is the relative chain diameter.

Figure [14.11](#page-24-0) shows the data plotted in Fig. [14.5](#page-13-0) in new coordinates  $[\eta] M_L/A^2$ and  $[s]/M_L$  *vs.* relative contour length  $L/A$ . These plots (Fig. [14.11\)](#page-24-0) illustrate the earlier conclusion (Pavlov [2013;](#page-36-15) Pavlov et al. [2014\)](#page-36-16) that the entire set of the linear macromolecules, regardless of the stiffness realization mechanism (free/hindered rotation around valence bonds, multistrand helix structures, electrostatic and/or thermodynamic interactions, specific interactions that lead to the globule formation), obeys the same laws.

## **14.12 Examples of Handling of Velocity Sedimentation Data with Sedfit Suite**

To estimate the value of sedimentation coefficient for a series of fractions/samples of polymers from the files of raw data obtained with the XLI analytical ultracentrifuge (usually, using the interference optics), the Sedfit suite software may be chosen. This program provides the opportunity to process the velocity sedimentation data (Schuck [2000;](#page-37-22) Dam and Schuck [2004;](#page-34-25) Schuck and Zhao [2011\)](#page-37-23). Within the framework of this suite, the raw data can be processed using various programs, and the results can be compared to each other. The treatment of the results obtained in the sedimentation experiments with different linear polymers in the wide range of molar masses will be discussed below.

# *14.12.1 Model-Less Method for Calculating the Apparent Differential Sedimentation Coefficient Distribution g\*(s)*

*First*, the model-less method for calculating the apparent differential sedimentation coefficient distribution *<sup>g</sup>*\*(*s*) denoted by ls-*g*\*(*s*) (Schuck and Rossmanith [2000\)](#page-37-24) is employed; this method involves direct linear least-squares boundary modeling with the aid of superposition of sedimentation profiles of ideal *nondiffusing particles* (Figs. [14.12](#page-26-0) and [14.13\)](#page-27-0). This model is appropriate for the high molar mass polymer when the diffusion flow is slow and the s/D ratio is more than  $\approx 0.3$  svedberg/fick (1 svedberg =  $10^{-13}$  s and 1 fick =  $10^{-7}$  cm<sup>2</sup>/s). Despite the fact that the average sedimentation coefficient does not differ from the values obtained using other sedimentation coefficient does not differ from the values obtained using other models, the obtained distribution ls-*g*\*(*s*) does not reflect the real distribution of sedimentation coefficients (molar masses) because it contains unaccounted diffusion spreading.

In some cases, the additional  $ls-g^*(s)$  model with one discrete Lamm equation<br>*propent* completes the distribution curve in the region of small s values and *component* completes the distribution curve in the region of small *s* values and, respectively, in the range of large *D* values (Fig. [14.13\)](#page-27-0). This variation of the model not only serves an aesthetic purpose but also is entirely consistent with the general idea that linear synthetic and natural polymers have the essentially continuous molar mass distributions.

The results obtained using different up-to-date software should be compared to those obtained by the classical method based on the definition of sedimentation coefficient:  $s \equiv (d \ln r/dt) \omega^{-2}$ , where *r* is the position of sedimentation boundary,  $\omega$  is the angular velocity, and *t* is the time of sedimentation (Syedberg and Pedersen is the angular velocity, and *t* is the time of sedimentation (Svedberg and Pedersen [1940\)](#page-36-0). The integral curves can be transformed into differential ones. Two kinds of differentiation are possible. First, the value of *dJ*/*dr* is calculated by differentiation of the raw interference curve with the subsequent smoothing. The second way is to compute *dJ*/*dt* curves as the difference of the adjacent interference curves when the



<span id="page-26-0"></span>**Fig. 14.12** Results obtained in the velocity sedimentation experiments using a pullulan stan-Fig. 14.12 Results obtained in the velocity sedimentation experiments using a pullulan standard (Polymer Standards Service GmbH) with  $M_w = 1\,660\,$  kg mol<sup>-1</sup> and a concentration  $c = 0.54$  ms cm<sup>-3</sup> in H<sub>2</sub>O at 25 °C, at **Fig. 14.12** Results obtained in the velocity sedimentation experiments using a pullulan standard (Polymer Standards Service GmbH) with  $M_w = 1\,660\,$  kg mol<sup>-1</sup> and a concentration  $c = 0.54$  mg cm<sup>-3</sup> in H<sub>2</sub>O at 25 °C, superposition of the integral distribution of the pullulan concentration inside the cell collected by interference optics every 240 s; *middle*, corresponding residuals plot obtained by the Sedfit –  $c(s)$ ; *bottom*, distribution obtained with *c*(*s*) model. (**b**) Corresponding differential distribution of the sedimentation profiles  $dJ/dt$ . (**c**) Dependence of  $\Delta ln x$  on  $\Delta t$ ; the slope of this dependence yields  $s = dln r/d(t\omega^{$ sedimentation profiles  $dJ/dt$ . (c) Dependence of  $\Delta lnx$  on  $\Delta t$ ; the slope of this dependence yields  $^{2}$ ) = 12.8 S, 1 - dJ/dt, 2 - dJ/dr. (**d**) Comparison of the differential distributions coefficient obtained by different model of Sedfit suite; (1)  $c(s)$ , s = 12.78 S; of the sedimentation coefficient obtained by different model of Sedfit suite: (1)  $c(s)$ ,  $s = 12.78$  S; (2)  $ls - g*(s)$ ,  $s = 12.79$  S; and (3)  $c(s) - bs$ ,  $s = 12.64$  S. Thus, the average of the four values  $s = (12.75 + 0.04)$  S, and the maximum difference between the obtained values  $\Delta s = 0.16S$ is  $s = (12.75 \pm 0.04)$  S, and the maximum difference between the obtained values  $\Delta s = 0.16S$ amounts 1.2 % from the mean value (insignificant deviation)

shift in time is small (Stafford [1994\)](#page-37-25) (Fig. [14.12b, c\)](#page-26-0). The slope of the dependence of the sedimentation boundary shift logarithm lnr on  $\omega^2 t$  allows to evaluate the sedimentation coefficient by its definition.

It is necessary to point out that the study of the concentration dependence of the velocity sedimentation is an important task in the hydrodynamic investigation of linear polymers (Eq[.14.11](#page-6-2) and Fig. [14.14\)](#page-28-0).



<span id="page-27-0"></span>**Fig. 14.13** Comparison of differential distributions obtained with different model of Sedfit suite. (a) Differential distributions  $dJ/ds$  of a pullulan sample with  $M_w = 11.8$  kg/mol in H<sub>2</sub>O at  $c = 5.38$  mg/cm<sup>3</sup> obtained with  $ls - g*(s)$  model (1) and with  $ls - g*(s)$  with one discrete Lamm<br>For component model (14.2). The last model gives more realistic dependence in the region of very Eq. component model [\(14.2\)](#page-4-1). The last model gives more realistic dependence in the region of very low s values. (**b**) The distributions of sedimentation coefficients obtained for the same sample. The following values were obtained with the different model of Sedfit program: continuous  $c(s)$ distribution  $-s = 1.65$  S (2); continuous  $c(s) - bs$ ,  $b_s = 0.458 - s = 1.66$  S (1); and  $ls - s = 1.7$  S (3) In the case of the low molar mass sample which is characterized by t distribution –  $s = 1.65$  S (2); continuous  $c(s) - bs$ ,  $b_s = 0.458 - s = 1.66$  S (1); and  $ls - g*(s)$  $s = 1.7$  S (3). In the case of the low molar mass sample which is characterized by the high<br>diffusion coefficient  $(D_0 \approx 10 \times 10^{-7} \text{ cm}^2/\text{s})$  there is a striking difference in the form of  $s = \sigma^*(s)$ distribution  $- s = 1.65$  S (2); continuated<br>  $s = 1.7$  S (3). In the case of the lot<br>
diffusion coefficient (*D*<sub>0</sub>  $\approx$  10 × 10<sup>-</sup><br>
distributions Here the diffusion process  $^7$  cm<sup>2</sup>/s), there is a striking difference in the form of  $ls-g^*(s)$ <br>ress is not taken into account which leads to a fictitious broad distributions. Here, the diffusion process is not taken into account, which leads to a fictitious broad distribution as compared with two other methods  $(c(s)$  and  $c(s)$ —*bs*). These two methods take<br>into account the dominant diffusion flux during sedimentation. At the same time, the average into account the dominant diffusion flux during sedimentation. At the same time, the average sedimentation coefficient obtained by  $ls-g^*(s)$  method virtually is the same as those obtained<br>with two other methods. For this sample, the ratio so/D<sub>0</sub> is  $\approx 0.17$  svedberg/fick (c) Distributions with two other methods. For this sample, the ratio  $s_0/D_0$  is  $\approx 0.17$  svedberg/fick. (**c**) Distributions of sedimentation coefficients obtained for the fraction of poly(N-methyl-N-vinylacetamide) with  $M_{sD}$  = 5.2 kg/mol in H<sub>2</sub>O at  $n = 40,000$  rpm. The following values were obtained using the different models included in Sedfit program at the concentration  $c = 3.03$  mg/cm<sup>3</sup> (1 and 2): continuous  $c(s)$  distribution  $-s = 0.43$ S (1); continuous  $c(s) - bs$ ,  $b_s = 0.43 - s = 0.43$ S (2); at the concentration  $c = 1.5$  mg/cm<sup>3</sup> (3 and 4) continuous  $c(s)$  distribution  $-s = 0.44$ S (3); continuous concentration  $c = 1.5$  mg/cm<sup>3</sup> (3 and 4), continuous  $c(s)$  distribution  $-s = 0.44S$  (3); continuous  $c(s) - bs$   $h = 0.43 - s = 0.43S$  (4). It is noteworthy that in the case when the sedimentation flow  $c(s) - bs$ ,  $b_s = 0.43 - s = 0.43S$  (4). It is noteworthy that, in the case when the sedimentation flow<br>becomes wilted and the diffusion flow is growing  $(D_0 \approx 13 \times 10^{-7} \text{ cm}^2/\text{s})$  the  $(s-a^*(s) \text{ model})$ committed contraction  $c = 1.5$  mg/cm<sup>3</sup> (3 and 4), continuous  $c(s)$  distribution  $c(s) - bs$ ,  $b_s = 0.43 - s = 0.43S$  (4). It is noteworthy that, in the case wilted, and the diffusion flow is growing ( $D_0 \approx 13 \times 10^{-1}$ ) is no lo  $7 \text{ cm}^2$ /s), the  $ls-g*(s) \text{ model}$ <br>efficient For this sample the is no longer applicable for evaluating the velocity sedimentation coefficient. For this sample, the ratio  $s_0/D_0$  is  $\approx 0.03$  svedberg/fick (Pavlov et al. [2010a\)](#page-36-18)

#### *14.12.2 Continuous c(s) Model in Sedfit Suite*

*Second*, the differential distribution of sedimentation coefficient  $c(s)$  is calculated by numerical solution of Lamm equation in which both opposite flows (sedimentation and diffusion) are taken into account (*continuous c(s) model*, Schuck [2000\)](#page-37-22). In order to achieve one-parametric distribution, a scaling law between the diffusion and sedimentation coefficient is invoked in the  $c(s)$  method. The choice of the scaling law is based on the  $D_0 = K_{DS} s_0^{-1/2}$  relation which is correct for roughly globular<br>particles with the frictional ratio (*f*/*f*, ,) as a scaling parameter (*f* is the frictional particles, with the frictional ratio (*f*/*f<sub>sph</sub>*) as a scaling parameter (*f* is the frictional coefficient of the solute macromolecule; *fsph* is the frictional coefficient of a rigid sphere with the same "anhydrous" volume (free of solvent) as the macromolecule). Fitting for  $(f/f_{sph})$  in a nonlinear regression will provide the estimate of the weightaverage frictional ratio of all macromolecules in solution that actually leads to



<span id="page-28-0"></span>**Fig. 14.14** Concentration dependence of velocity sedimentation for pullulan molecules in  $H_2O$ , **Fig. 14.14** Concentration dependence of velocity sedimentatio  $n = 42,000$  rpm, at 25°C. (a) Distributions obtained using  $ls = 1660$  kg/mol at different concentrations: (1)  $c = 167$  (2)  $c = 167$  $n = 42,000$  rpm, at 25°C. (a) Distributions obtained using  $ls - g*(s)$  model for sample with  $M_w$ =1660 kg/mol at different concentrations: (1)  $c = 1.67$ , (2)  $c = 1.10$ , and (3)  $c = 0.54$  mg/cm<sup>3</sup>. The area under the distribution curve gives the number of fringes *J* and corresponds to polymer concentration c. The refractive index increment was calculated from  $(\Delta n/\Delta c) = J\lambda/Kcl$ , where  $\lambda$  is the wavelength,  $K$  is the magnifying coefficient, and  $l$  is the optical path length. (**b**) Concentration concentration c. The refractive index increment was calculated from  $(\Delta n/\Delta c) = J\lambda/Kcl$ , where  $\lambda$  is the wavelength, K is the magnifying coefficient, and l is the optical path length. (b) Concentration dependences of the (r molar masses and corresponding characteristics  $s_0$  and  $k_s$ : (1)  $M_w = 1$  660 kg/mol,  $s_0 = 14.8$  S,  $k_s = 290 \text{ cm}^3/\text{g};$  (2)  $M_w = 404$ ,  $s_0 = 9.1$ ,  $k_s = 130$ ; (3)  $M_w = 212$ ,  $s_0 = 6.8$ ,  $k_s = 80$ ; (4)  $M_w = 22.8$ ,  $s_0 = 2.3, k_s = 15$ ; and (5)  $M_w = 11.8, s_0 = 1.7, k_s = 8$ 

determination of the average value of the translational diffusion coefficient *D*:

$$
D_0 = kT(1 - \nu \rho_0)^{1/2} / \eta_0^{3/2} \left(9\pi 2^{1/2}\right) \left(f / f_{sph}\right)_0^{3/2} (s_0 \nu)^{1/2} \tag{14.30}
$$

The distribution of the sedimentation coefficients for the sample in Sedfit software is denoted as *c* (*s*). Usually this kind of designation is used for integral distribution. Indeed, *c* is a concentration; in the case of interference optics, it is expressed as a number of fringes *J*, which is unambiguously associated with the concentration; see the relation [\(14.31\)](#page-28-1). However, the Sedfit program gives the distribution in a differential form. The area under the differential curve is equal to the number of interference fringes (i.e., concentration). Therefore, it is logical and more consistent to denote this distribution by *dc*(*s*)/*ds* or *dJ*(*s*)/*ds*. Finally, the differential distribution  $\left(\frac{dc(s)}{ds}\right)$  of the sample is obtained (Figs. [14.12](#page-26-0) and [14.13\)](#page-27-0). The area under the  $\frac{dc(s)}{ds}$  curve gives the loading concentration of the macromolecules between the minimum and maximum *s*-value occurring (expressed in number of fringes, *J*). Note that the concentration dependence of *J* (fringes number) allows defining an additional parameter – the refractive index increment  $\Delta n/\Delta c$ 

<span id="page-28-1"></span>
$$
\Delta n/\Delta c = J\lambda/Kcl \tag{14.31}
$$

where  $\lambda$  is the wavelength, *K* is the magnifying coefficient, and *l* is the optical path length. The value of  $\Delta n/\Delta c$  is a characteristic of polymer-solvent system and should be virtually constant in a series of polymer homologues until the oligomer region. Obviously, such correlation will be performed in the case of an absorption boundary registration:  $OD_{solution} = OD_{solvent} + K_{ab}c$ , where  $K_{ab}$  is the increment of the polymer absorption in a given solvent ( $K_{ab} \equiv dOD/dc$ ). However, this relationship will hold within the range of much smaller concentration due to quick absorbance saturation.

Needless to say, the series of globular particles is not the best model to describe hydrodynamic behavior of linear macromolecules. Nevertheless, the continuous *c*(*s*) distribution model leads to reasonable values of the velocity sedimentation coefficients for many linear polymers.

### *14.12.3 Continuous c(s) Model with General Scaling Law in Sedfit Suite*

Third, recently Sedfit suite has been implemented with *continuous c(s) model with general scaling law* (designated below as *c*(*s*)–*bs*). Some information about this add-in program is contained in a publication by Harding et al. (2011b). In this add-in program is contained in a publication by Harding et al. [\(2011b\)](#page-34-26). In this paper, the implementation is called "extended Fujita approach." For direct boundary modeling with distributions of the Lamm equation solutions (Schuck [2000\)](#page-37-22), the measured interference (or absorbance) profiles *a*(*r*, *t*) were modeled as an integral over the differential concentration distribution *c*(*s*)

$$
a(r, t) = \int c(s) \chi(s, D(s), r, t) \, ds + b_{nr}(r) + b_{nt}(t) \tag{14.32}
$$

with  $b_{nr}$  (*r*) and  $b_{nt}(t)$ , denoting systematic baseline noise components, and  $\chi(s)$ ,  $D(s)$ ,  $r$ ,  $t$ ) denoting the solution of the Lamm equation at unit loading concentration of a species with sedimentation coefficient s and diffusion coefficient *D*

<span id="page-29-0"></span>
$$
d\chi/dt = r^{-1}d\left[rD(s)\left(\frac{d\chi}{dr}\right) - s\omega^2r^2\chi\right]/dr\tag{14.33}
$$

where r is the distance from the center of rotation and  $\omega$  is the rotor angular velocity. Equation [14.33](#page-29-0) was solved by finite element methods in a static or moving frame of reference as described in Claverie et al. [\(1975\)](#page-34-27), Schuck [\(1998\)](#page-37-13), and Schuck [\(1998\)](#page-37-13). For each species, the diffusion coefficient  $D(s)$  was estimated as a function of the sedimentation coefficient *s* based on the general scaling law, which may be presented as

<span id="page-29-1"></span>
$$
D_0 = \left(RT/\left(1 - \nu \rho_0\right) K_s^{1/bs} s_0^{(bs-1)/bs} = K_{Ds} \times s^{(bs-1)/bs} \right) \tag{14.34}
$$

where the parameters  $b_s$  and  $K_s$  define the scaling relation between  $s_0$  and M  $(s_0 = K_s M^{bs})$ . It should be emphasized that the  $D_0 = K_{D_s} s_0^{-1/2}$  relation known for globular species is a special case of general Eq. 14.34. To solve the Lamm for globular species is a special case of general Eq. [14.34.](#page-29-1) To solve the Lamm equation numerically, the range of possible velocity sedimentation coefficient values is typically discretized into 100–200 values. Actually, it is modern paraphrase of the "graphic fractionation" approach (Gralen [1944;](#page-34-28) Kinell and Ranby [1950\)](#page-35-25). For any reasons, a researcher specifies the power law exponent  $b<sub>s</sub>$ , and the program fits the best value of  $K_s^*$ . The asterisk means that this value is obtained at some known concentration, and these values must be extrapolated to zero concentration to obtain the non-disturbed  $K_s$  value. In the finite element method, the solutions of the ideal Lamm equation are obtained using the adaptive grid algorithm which allows fitting the best *Ks* \* value; finally, each *s*-value gets the corresponding *D*-value. As a result, the differential distribution (*dc*(*s*)/*ds*) of the sample is also fitted. The relation [\(14.34\)](#page-29-1) has a general meaning and may be applied to any kind of homologous series of the macromolecular compounds. In principle, the  $c(s) - bs$  implementation is more appropriate to treat the velocity sedimentation data on any macromolecules due to appropriate to treat the velocity sedimentation data on any macromolecules due to the possibly large variation of the  $b_s$  value. The  $K_s$  value (Eq. [14.15\)](#page-12-0) should not be confused with the Gralen concentration coefficient  $k_s$  (Eqs. [14.7\)](#page-5-1).

Note that the distributions of the sedimentation coefficients for the samples of high molar masses obtained using different models  $(c(s), c(s) - bs$ , and  $ls - g*(s)$ <br>are virtually indistinguishable (Fig. 14.12d). The lower the molar mass, the higher are virtually indistinguishable (Fig. [14.12d\)](#page-26-0). The lower the molar mass, the higher the deviation of the  $ls - g^*(s)$  distribution from the real one (Fig. [14.13b\)](#page-27-0). However,<br>up to a certain value of the  $s/D$  ratio ( $>0$  2), the average value of sedimentation up to a certain value of the  $s/D$  ratio (>0.2), the average value of sedimentation coefficient s obtained using the  $ls - g^*(s)$  model is almost equal to the average values<br>of s obtained with the use of other models of *s* obtained with the use of other models.

Another important question arises: How do the fitted  $K_s^*$  values sort with those obtained by the straightforward procedure of comparison between the  $s_0$  values and molar masses for a series of samples? The results obtained for the flexible polymers are summarized in Figs. [14.15,](#page-31-0) [14.16,](#page-31-1) and [14.17,](#page-32-0) and the following conclusions can be draw from these data. Uppermost, the  $K_s^*$  value strongly depends on concentration. This fact highlights the importance of studying the concentration dependencies of the hydrodynamic characteristics in the appropriate range of concentrations and extrapolating the sought-for characteristics to infinite dilution. This means that the use of a single concentration for estimating samples polydispersity is unlikely to give the reliable results.

The sign of the slope of concentration dependence is determined by the thermodynamic quality of the solvent (compare Figs. [14.15](#page-31-0) and [14.17](#page-32-0) with Fig. [14.16\)](#page-31-1). The  $K_s^*$  values depend in a unified manner on the parameters characterizing the degree of dilution  $(c[\eta]$  or  $ck_s$ ) of samples of different molar masses. The fitted  $K_s$  values extrapolated to the infinite dilution are close to those obtained in the traditional way. Here is another proof of self-sufficiency of the velocity sedimentation method coupled with the Sedfit  $c(s)$ — $bs$  model in the determination<br>of molecular characteristics of linear polymers of molecular characteristics of linear polymers.

Explicitly, the use of new software for primary processing of the experimental data should lead to results, which must not contradict with the main conclusions on



<span id="page-31-0"></span>**Fig. 14.15** Concentration dependences of fitted  $K_s^*$  value parameter (a) for polystyrenes of different molar masses in toluene (which is thermodynamically good solvent for polystyrene): (1)  $M = 1760$ , (2)  $M = 17$  kg/mol; dependences of  $K_s$  on the  $c[\eta]$  parameter (**b**). Triangle point (3) is the  $K_s$  value from the independent literature data (Meverboff and Appelt 1979) point (3) is the  $K_s$  value from the independent literature data (Meyerhoff and Appelt [1979\)](#page-35-11). point (3) is the  $K_s$  value from the independent literature data (Meyerhoff and Appelt 1979).<br>  $K_s^*$  values are fitted within the framework of the continuous *c*(*s*) model with general scaling<br>  $\int \ln w \cdot D_0 = RT/(1 - v_0 \alpha)K^{1$  $\Omega_0 = RT/(1 - \upsilon \rho_0) K_s^{-1/bs} s_0^{(bs-1)/bs}$ <br>concentration Gralen coefficient *k*, in E dependent literature data (Meyerhoff and Appelt 1979).<br>work of the continuous  $c(s)$  model with general scaling<br> $= K_{Ds} \times s^{(bs-1)/bs}$ .  $K_s^*$  is not to be confused with the concentration Gralen coefficient *ks* in Eq. [14.11](#page-6-2)



<span id="page-31-1"></span>**Fig. 14.16** Concentration dependences of fitted  $K_s^*$  value (a) for two mixtures of polystyrene standards of different molar masses studied in MEK (which is a marginal solvent for polystyrene) and dependences of  $K_s^*$  on the dilution parameter  $c[\eta]$  (**b**). Full triangle point is the  $K_s$  value from the independent literature data (Pavlov et al. [2011\)](#page-36-19). (1)  $(1760 + 1060 + 710 + 311 + 194) \times 10^3$  g/mol, 20 % of each in the mixture,  $[\eta]_w = \Sigma (0.2[\eta]_i) = 90.2$  cm<sup>3</sup>/g; (2)  $(95 + 43 + 9 + 4 + 1.8) \times 10^3$  g/mol, 20 % of each in the mixture  $[\eta] = \Sigma (0.2[\eta]_i) = 11.6$  cm<sup>3</sup>/g where  $[\eta]$  is the intrinsic viscosity value of the the mixture,  $[\eta]_w = \Sigma(0.2[\eta]_i) = 11.6$  cm<sup>3</sup>/g, where  $[\eta]_i$  is the intrinsic viscosity value of the individual sample individual sample

conformational states of linear macromolecules that have been previously received on the basis of the velocity sedimentation coefficients obtained with the fundamental relations. This is true, at least for the flexible linear polymers.



<span id="page-32-0"></span>**Fig. 14.17** Concentration dependences of fitted  $K_s^*$  value (a) for pullulan of different molar masses (kg/mol) in  $H_2O$  (which is thermodynamically good solvent for pullulan): (1)  $M = 1660 \times 10^3$  g/mol, (2)  $M = 404$ , (3) 212, (4) 22.8, (5)  $11.8 \times 10^3$  g/mol (*left side*) and  $K_3^*$  dependences on the *ck*, parameter characterizing the degree of solution dilution (b). Open triangle dependences on the  $ck<sub>s</sub>$  parameter characterizing the degree of solution dilution (**b**). Open triangle point is the  $K_s$  value from the literature data (Pavlov et al. [1994](#page-36-20) and the references therein).  $K_s^*$  is not to be confused with the concentration Gralen coefficient  $k_s$  in Eq. [14.11](#page-6-2)

#### **14.13 Conclusions**

Self-sufficiency of the velocity sedimentation method manifests itself (1) in the qualitative analysis of the conformational status of linear macromolecule from the  $lgk_{s}M_{L}$  vs.  $lg$  [s]/ $M_{L}$  plot, (2) in the possibility of an adequate assessment of polymer molar masses and further conformational analysis using the sedimentation parameter  $\beta_s$ , and (3) in the fact that numerical solution of the Lamm equation using the  $c(s)$ —*bs* model within Sedfit suite allows to set the scaling relation  $s_0 = K_s M^{bs}$ <br>which opens up possibilities for further conformational analysis, as well as molar which opens up possibilities for further conformational analysis, as well as molar mass distribution analysis.

In outcome conclusion, we propose the following algorithm for the study of homologous series of macromolecules using XLI coupled with *<sup>c</sup>*(*s*)-*bs* model inside of Sedfit suite.

The proposed algorithm involves the following stages:

- 0. First of all, for the comprehensive and exhaustive study of any polymer system, the researcher should have a set of samples/fractions with narrow polydispersity and the possibly broadest range of molar masses.
- 1. Studying of the concentration dependence of the available number of samples/fractions using  $c(s)$  or/and  $ls - g^*(s)$  models of Sedfit suite.<br>Determining the so and k, values from the concentration dependent
- 2. Determining the  $s_0$  and  $k_s$  values from the concentration dependencies of  $s^{-1}$  and subsequently establishing the  $k_s = K_{\text{sky}} s_0 b^k s$  correlation in order to define the scal-<br>ing index *b* in the KMHS-type relation  $s_0 = K M^{bs}$  from the *b*<sub>1</sub>  $-(2-3b)/b$ ing index *b<sub>s</sub>* in the KMHS-type relation  $s_0 = K_s M^{bs}$  from the  $b_{ks} = (2 - 3b_s)/b_s$ <br>relationship relationship.
- 3. Using the obtained  $b_s$  value, the rehandling of raw set of data must be done using  $c(s)$ —*bs* model and  $K_s^*(c)$  parameter must be fitted. The concentration

dependencies of  $K_s^*$  must be plotted and extrapolated to zero concentration conditions. Thus, the unperturbed value of  $K_s$  will be estimated and the scaling relation  $s_0 = K_s M^{bs}$  is known.

- 4. The molar masses *M* may be calculated. It is necessary to check the  $b_s$  and  $K_s$ values using the double logarithmic plot  $(lgs_0 \text{ vs. } lgM)$ . The difference of about  $\Delta b_s \approx 0.01$  can be considered as insignificant. But if, for example, instead of  $b_s = 0.41$ , the  $b_s$  value turns out to be  $b_s = 0.46$ , it is necessary to go back to step 3 and repeat the process using the new value  $b_s = 0.46$ . In other words, the method of successive approximations is necessary to achieve the consistency in the *b<sub>s</sub>* value.
- 5. With the final set of  $s_0$ ,  $k_s$ , and M values, further molecular interpretation may be reached: assessments of the sedimentation parameter  $\beta_s$  values, Kuhn segment length, the value of hydrodynamic diameter, the degree of macromolecular coiling, etc. Finally, the obtained estimations should be compared with the chemical structure of the repeating unit of the polymer.
- 6. If successful, this path gives the full set of molecular and conformation characteristics of studied linear polymer and will illustrate self-sufficiency of the sedimentation velocity method in the study of a homologous series of linear polymers.

Finally, it is interesting to analyze possible scope of measuring sedimentation coefficients with the help of the modern analytical ultracentrifuge. The upper limit can be represented by sedimentation of nanoparticles and nano-complexes, and it totals hundreds of thousands of svedberg (e.g., Perevyazko et al. [2010,](#page-37-26) [2012\)](#page-37-27). Up to now, the lower limit has been apparently achieved in the studies of the cyclodextrins, and it is about one tenth of svedberg (Pavlov et al. [2010b\)](#page-36-21). Thus, one XLI instrument enables us to measure the values of a physical quantity differing by six orders of magnitude (by varying the rotation speed and/or solvent). This is a rare opportunity in the practice of physical experiments.

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