Chapter 1 Dynamic Robust Bifurcation Analysis

Masaki Inoue, Jun-ichi Imura, Kenji Kashima and Kazuyuki Aihara

1.1 Introduction

In dynamical systems theory, bifurcation phenomena have been studied extensively [\[1](#page-14-0)[–3\]](#page-14-1). Bifurcation is a phenomenon whereby a slight parametric perturbation in a dynamical system produces qualitative changes in structure of the solutions. It can be interpreted as bifurcation that because of a slight parameter change a stable equilibrium of differential equations is suddenly destabilized, and a stable periodic orbit can arise near the equilibrium. In order to analyze such phenomena, bifurcation theory has been studied and widely used for analysis and synthesis of complex behavior in many research fields; systems biology and synthetic biology $[4-14]$ $[4-14]$, power system

M. Inoue (\boxtimes)

J. Imura

This research was done when M.I. was with FIRST, Aihara Innovative Mathematical Modelling Project, Japan Science and Technology Agency/Graduate School of Information Science and Engineering, Tokyo Institute of Technology.

Faculty of Science and Technology, Keio University, 3-14-1 Hiyoshi, Kohoku-ku, Yokohama, Kanagawa 223-8521, Japan e-mail: minoue@appi.keio.ac.jp

Graduate School of Information Science and Engineering, Tokyo Institute of Technology, 2-12-1 O-Okayama, Meguro-ku, Tokyo 152-8552, Japan e-mail: imura@mei.titech.ac.jp

K. Kashima Graduate School of Informatics, Kyoto University, Yoshida-honmachi, Sakyo-ku, Kyoto, Japan e-mail: kashima@bode.amp.i.kyoto-u.ac.jp

K. Aihara Institute of Industrial Science, The University of Tokyo, 4-6-1 Komaba, Meguro-ku, Tokyo 153-8505, Japan e-mail: aihara@sat.t.u-tokyo.ac.jp

[©] Springer Japan 2015 K. Aihara et al. (eds.), *Analysis and Control of Complex Dynamical Systems*, Mathematics for Industry 7, DOI 10.1007/978-4-431-55013-6_1

analysis [\[15](#page-15-1)[–18\]](#page-15-2), epidemic model analysis [\[19](#page-15-3)[–22\]](#page-15-4), and so on. For example, bifurcation theory has contributed to recent breakthroughs in systems biology and synthetic biology. Bifurcation analysis methods have been adopted to study the functions or characteristics of artificial bio-molecular systems, such as bio-molecular oscillators [\[4,](#page-14-2) [10](#page-15-5), [11\]](#page-15-6) and bio-molecular switches [\[5](#page-14-3), [9](#page-14-4), [14\]](#page-15-0). In addition, the robustness of such functions is identified with the volume of a parameter region in which the system has oscillatory property or bistable equilibria.

Conventional bifurcation theory is not always applicable to the analysis and synthesis of dynamical systems with uncertainties. Bifurcation analysis methods assume that mathematical models such as differential equations are completely known. Hence, they are not applicable to dynamical systems with uncertainties, in particular, large dynamic uncertainties . However, practical systems in the real world inevitably involve not only static but dynamic uncertainties [\[23](#page-15-7), [24\]](#page-15-8). In order to apply the theory to such real-world systems, bifurcation analysis methods for uncertain dynamical systems are required.

In this chapter, we study local bifurcation of an equilibrium for systems with dynamic uncertainties. Note that a bifurcation point, i.e., a parameter value on which bifurcation occurs, depends on each model in general. If a system contains uncertainties and is described by a model set, we cannot find the specific bifurcation point. Therefore, we evaluate the potential bifurcation region: the parameter region that consists of all possible bifurcation points for a given model set. In other words, the region consists of all parameter points on which bifurcation can potentially occur. Evaluating the potential bifurcation region is referred to as the dynamic robust bifurcation analysis problem in this chapter. To this end, we first propose a condition for existence of equilibria independently of uncertainties and evaluate their location. Then, we derive a condition for robust hyperbolicity of potential equilibrium points, which implies that the dimension of unstable manifolds is independent of uncertainties. We consider parameter-dependent nonlinear systems with dynamic uncertainties, and using the robust hyperbolicity condition we identify the region that contains all potential bifurcation points. Finally, illustrative examples for robustness analysis of normal forms for various types of bifurcation are presented.

Notation: The symbols $\overline{\sigma} \{\cdot\}$ and $\rho \{\cdot\}$ represent the maximum singular value and the spectrum radius of a matrix, respectively. RH_{∞} is the space that consists of all proper and complex rational stable transfer function matrices. The H_{∞} norm and L_{∞} norm of a linear system *S* are defined by

$$
||S||_{H_{\infty}} := \sup_{\text{Re}[s]>0} \overline{\sigma} \{ \overline{S}(s) \}, \quad ||S||_{L_{\infty}} := \sup_{\text{Re}[s]=0} \overline{\sigma} \{ \overline{S}(s) \},
$$

where $\bar{S}(s)$ is a transfer function matrix representation of *S*. The poles (system poles) of a linear system $\dot{x} = Ax$ are defined by the roots of the characteristic polynomial $\phi(s) := \det(sI - A)$. In addition, a stable pole, an unstable pole, and a neutral pole are defined as poles lie in the open left half-plane, open right half-plane, and the imaginary axis of the complex plane, respectively.

1.2 Problem Formulation: Dynamic Robust Bifurcation Analysis

Consider the feedback system (Σ, Δ) illustrated in Fig. [1.1.](#page-2-0) In the figure, Σ is the nominal dynamical system composed of the linear dynamical system Σ_L and the nonlinear static function *f*. The linear system Σ_L is described by the state equations

$$
\Sigma_L: \begin{cases} \n\dot{x} = A(\mu)x + B_1(\mu)u_1 + B_2(\mu)u_2, \\ \ny_1 = C_1(\mu)x + D_{11}(\mu)u_1 + D_{12}(\mu)u_2, \\ \ny_2 = C_2(\mu)x + D_{21}(\mu)u_1 + D_{22}(\mu)u_2, \n\end{cases} \tag{1.1}
$$

where $x \in \mathbb{R}^n$ is the state, $u_1 \in \mathbb{R}^q$ and $u_2 \in \mathbb{R}^m$ are the inputs, $y_1 \in \mathbb{R}^p$ and $y_2 \in \mathbb{R}^{\ell}$ are the outputs, respectively, $\mu \in \mathcal{P} \subset \mathbb{R}^r$ is a static bifurcation parameter, and $A \in \mathbb{R}^{n \times n}$, $B_1 \in \mathbb{R}^{n \times q}$, $B_2 \in \mathbb{R}^{n \times m}$, $C_1 \in \mathbb{R}^{p \times n}$, $C_2 \in \mathbb{R}^{\ell \times n}$, $D_{11} \in \mathbb{R}^{p \times q}$, $D_{12} \in \mathbb{R}^{p \times m}$, $D_{21} \in \mathbb{R}^{\ell \times q}$, and $D_{22} \in \mathbb{R}^{\ell \times m}$ are parameter-dependent matrices. The input-to-output responses of the system Σ_L can be characterized by the transfer function representation as follows:

$$
\begin{aligned}\n\left[\begin{array}{c}\n\bar{y}_1(s) \\
\bar{y}_2(s)\n\end{array}\right] &= \bar{\Sigma}_L(s) \begin{bmatrix}\n\bar{u}_1(s) \\
\bar{u}_2(s)\n\end{bmatrix}, \quad \bar{\Sigma}_L(s) := \begin{bmatrix}\n\bar{\Sigma}_{L11}(s) & \bar{\Sigma}_{L12}(s) \\
\bar{\Sigma}_{L21}(s) & \bar{\Sigma}_{L22}(s)\n\end{bmatrix}, \\
\bar{\Sigma}_{Lij}(s) &= C_i(\mu)(sI_n - A(\mu))^{-1}B_j(\mu) + D_{ij}(\mu), \\
(i,j) &= (1, 1), (1, 2), (2, 1), (2, 2),\n\end{aligned}
$$

where $s \in \mathbb{C}$ and $\bar{u}_1(s), \bar{u}_2(s), \bar{y}_1(s)$, and $\bar{y}_2(s)$ represent the Laplace transformations of the signals $u_1(t)$, $u_2(t)$, $y_1(t)$, and $y_2(t)$, respectively. The function $f : \mathbb{R}^{\ell} \times \mathbb{R}^r \to$ \mathbb{R}^m is in $C^2(\mathbb{R}^{\ell} \times \mathbb{R}^r, \mathbb{R}^m)$ and satisfies

$$
u_2 = f(y_2, \mu).
$$

The symbol Δ in Fig. [1.1](#page-2-0) expresses a dynamical system as well, but exact dynamics and even the dimension of the inner state of Δ are uncertain. This Δ is called a dynamic uncertainty. If there is no assumption on the dynamic uncertainty Δ, it is

Fig. 1.1 Feedback representation of an uncertain dynamical system: A feedback system is composed of the linear dynamical system Σ*L*, nonlinear function *f* , and dynamic uncertainty Δ

impossible to further analyze the feedback system illustrated in Fig. [1.1.](#page-2-0) We assume that the uncertainty is in the class of linear time-invariant systems.

$$
\Delta : \begin{cases} \dot{\delta} = A_d \delta + B_d y_1, \\ u_1 = C_d \delta + D_d y_1, \end{cases}
$$
 (1.2)

where $\delta \in \mathbb{R}^k$ is the state of Δ and the matrices $A_d \in \mathbb{R}^{k \times k}$, $B_d \in \mathbb{R}^{k \times p}$, $C_d \in \mathbb{R}^{q \times k}$, and $D_d \in \mathbb{R}^{q \times p}$ are uncertain. Then, the input-to-output responses of Δ can be characterized by the transfer function matrix $\overline{\Delta}(s) := C_d(sI - A_d)^{-1}B_d + D_d$. In addition, assume that the uncertainty Δ belongs to the given set of linear timeinvariant systems as

$$
\Delta\in\mathscr{U}.
$$

Discussion below is independent of the realization of Δ . The approach of this chapter uses only an input-output relation of the uncertainty as $\Delta \in \mathcal{U}$. Although we assumed above that the dynamic uncertainty Δ is a linear dynamical system for simplifying discussion below, we can extend the results of the paper to nonlinear uncertain cases.

For the uncertain feedback system (Σ, Δ) , we consider the bifurcation analysis, i.e., qualitative change of the flow by parametric variations in μ . In this formulation, the uncertain feedback system (Σ, Δ) is described by a model set. Since a bifurcation point depends on each model, we cannot find a specific bifurcation point for such a model set (see Fig. [1.2\)](#page-3-0). For uncertain dynamical systems, the location and even existence of equilibrium points are uncertain as well. We consider the following dynamic robust bifurcation analysis problem of identifying the sets of all potential bifurcation points for a given model set.

Definition 1.1 (*Potential Bifurcation Region*) For a given parameter region *P* and a given set of dynamic uncertainties \mathcal{U} , the potential bifurcation region $\mathcal{P}_{PB} \subseteq \mathcal{P}$ is the set of parameter points that are bifurcation points of the feedback system (Σ , Δ) for some $\Delta \in \mathcal{U}$.

Problem 1.1 (*Robust Bifurcation Analysis*) Consider the feedback system (Σ , Δ) and $\Delta \in \mathcal{U}$. Then, find the potential bifurcation region $\mathcal{P}_{PB} \subseteq \mathcal{P}$.

Fig. 1.2 Bifurcation analysis: A pitchfork bifurcation diagram for a nominal dynamical system is illustrated in the *left figure*. A robust bifurcation diagram for an uncertain dynamical system is illustrated in the *right figure*, where the location and hyperbolicity of the equilibria are uncertain

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In dynamical systems theory, there is a similar concept called imperfect bifurcation [\[25\]](#page-15-9), which is a bifurcation phenomenon for dynamical systems with small uncertainties. The uncertainties treated in the imperfect bifurcation problem are restricted to the ones represented by a finite number of uncertain parameters. Thus, our formulation covers a much wider class of uncertainties including dynamic uncertainties.

Bifurcation is defined as qualitative change of the structure of the solution in the state space by small parametric variation in $\mu \in \mathcal{P}$ (see e.g., [\[3\]](#page-14-1)). In such phenomena, we focus only on local bifurcation of an equilibrium. Suppose that for the feedback system (Σ, Δ) and at a parameter point $\mu_1 \in \mathbb{R}$, the number of equilibria is constant and they are robustly hyperbolic for all $\Delta \in \mathcal{U}$. Further suppose that at a point $\mu_2(\neq \mu_1) \in \mathbb{R}$ there exists Δ such that the number of equilibria is varied from the nominal system (Σ , 0) or an equilibrium loses hyperbolicity. Then, a potential bifurcation point is included in (μ_1, μ_2).

In addition, at a bifurcation point, an equilibrium for a dynamical system disappears or loses its hyperbolicity. Therefore, we evaluate the potential bifurcation region by finding the existence and location of an equilibrium and testifying its hyperbolicity for the feedback system (Σ, Δ) . The content of the next section is composed of the three parts: Sect. [1.3.1](#page-5-0) equilibrium analysis for the feedback system (Σ, Δ) , Sect. [1.3.2](#page-8-0) hyperbolicity analysis, and Sect. [1.3.3](#page-11-0) a solution to the dynamic robust bifurcation analysis.

In the following, we assume that the uncertainty Δ is in the set of norm-bounded linear stable systems $\mathcal{U}(\gamma)$ as follows:

$$
\mathscr{U}(\gamma) := \{ S(s) \in RH_\infty : ||S||_{H_\infty} \leq \gamma \},\
$$

where a positive constant γ is an upper bound of the maximum gain of Δ . The set $\mathcal{U}(\gamma)$ can represent signal distortions, unknown signal delays, approximation errors from PDEs to ODEs, and truncated errors of high index ODEs as long as their gains are bounded [\[23](#page-15-7), [24\]](#page-15-8). Utilizing this characterization by the value of γ , we solve the dynamic robust bifurcation analysis problem.

Some types of bifurcation phenomena, such as saddle-node bifurcation, are said to be robust. We *qualitatively* know the fact that if the constant γ is small so that $\Delta \in \mathcal{U}(\gamma)$ has little effect to the dynamics of the feedback system (Σ, Δ) , then, the same bifurcation can occur generically by parametric variations in μ . On the other hand, in this chapter, we will propose an analysis method to *quantitatively* evaluate the parameter points that can be a bifurcation point for some Δ .

1.3 Equilibrium, Stability/Instability, and Robustness Analysis

In Sects. [1.3.1](#page-5-0) and [1.3.2,](#page-8-0) the parameter value of μ is fixed at a non-bifurcation point in \mathscr{P} . We first consider the uncertain feedback system (Σ , Δ) to derive an existence condition for an equilibrium $[x_e^T \delta_e^T]^T$. Then, we derive a robust hyperbolicity condition for nonlinear systems with uncertainty-dependent equilibria.

1.3.1 Equilibrium Analysis

We evaluate the existence and location of equilibria in an uncertain feedback system (Σ, Δ) . They are dependent on the steady-state gain of Δ , i.e., $\overline{\Delta}(0)$. To this end, we make an assumption on the system Σ*L*.

(A1) Σ_L has no neutral poles.

The assumption A1, i.e., hyperbolicity of the origin of Σ_L , is a technical assumption that is used only for simplifying an existence condition of equilibria. This assumption can be satisfied in any uncertain feedback system applying the loop transformation technique to the feedback loop in Σ_L and f.

If A1 holds, the matrix $A(\mu)$ is nonsingular. Then, we can evaluate the steady state gain of $\bar{\Sigma}_L(s)$ as

$$
\bar{\Sigma}_L(0) = -\left[\frac{C_1(\mu)}{C_2(\mu)}\right] A^{-1}(\mu) \left[B_1(\mu) B_2(\mu)\right] + \left[\frac{D_{11}(\mu) D_{12}(\mu)}{D_{21}(\mu) D_{22}(\mu)}\right].
$$

The steady state gain of $\bar{\Delta}(s)$ can also be defined as

$$
\bar{\Delta}(0) = -C_d A_d^{-1} B_d + D_d \in \mathcal{U}_0(\gamma),
$$

$$
\mathcal{U}_0(\gamma) := \{D_0 \mid \bar{\sigma}(D_0) \in [-\gamma, \gamma] \}.
$$

We focus on the steady state output $y_2 = y_{2e}$ to derive an existence condition for an equilibrium $[x_e^T \delta_e^T]^T$. In the following, we consider the static nonlinear equation

$$
y_2 = F_u(\Sigma_L(0), D_0)f(y_2, \mu), \tag{1.3}
$$

where $D_0 \in \mathbb{R}^{q \times p}$ is a constant matrix and $F_u(X, Y)$ is the upper LFT representation of matrices *X* and *Y* as follows:

$$
F_{\rm u}(X,Y) = X_{21}Y(I - X_{11}Y)^{-1}X_{12} + X_{22}.
$$

We also define the matrix

$$
M(D_0) := F_{\rm u} \left\{ \left[\begin{array}{cc} \bar{\Sigma}_{L11}(0) & \bar{\Sigma}_{L12}(0) \\ B_1(\mu) & B_2(\mu) \end{array} \right], D_0 \right\}
$$

to state the conditions of a theorem. We derive a condition for the existence of equilibria as follows.

Theorem 1.1 *For a given* $\gamma > 0$ *, assume that A1 and* $\bar{\sigma} \{\bar{\Sigma}_{L11}(0)\} < 1/\gamma$ *. Then, for a fixed* $\mu \in \mathcal{P}$, (T1) *holds.*

(T1) *The feedback system* (Σ, Δ) *has no equilibrium for all* $\Delta \in \mathcal{U}(\gamma)$ *if and only if* [\(1.3\)](#page-5-1) *admits no real solution for all* $D_0 \in \mathcal{U}_0(\gamma)$ *.*

In addition, suppose that the matrix M(*D*₀) *is of full column rank for all D*₀ $\in \mathcal{U}_0(\gamma)$ *. Then,* (T2) *holds.*

(T2) *The feedback system* (Σ, Δ) *has* $N(>0)$ *isolated equilibria for all* $\Delta \in \mathcal{U}(y)$ *if and only if* [\(1.3\)](#page-5-1) *admits N isolated real solutions* $y_2 = y_2(D_0)$ *for all* $D_0 \in$ $\mathscr{U}_0(\gamma)$.

Proof From A1, at the steady state, we have

$$
x_e = -A^{-1} \{ B_1 \bar{\Delta}(0) y_{1e} + B_2 f(y_{2e}, \mu) \},\tag{1.4}
$$

$$
\delta_e = -A_d^{-1} B_d y_{1e},\tag{1.5}
$$

 *y*1*^e y*2*^e* $= \bar{\Sigma}_L(0) \left| \begin{array}{c} u_{1e} \\ u_{2e} \end{array} \right|$ *u*2*^e* $|, u_{1e} = \bar{\Delta}(0)y_{1e}.$

From the assumption that $\bar{\sigma} \{\bar{\Sigma}_{L11}(0)\} < 1/\gamma$ holds, the matrix $F_u(\bar{\Sigma}_L(0), D_0)$ is well-defined, and we can derive the static equations (1.3) and

$$
y_{1e} = \bar{\Sigma}_{L12}(0) \{ I_q - \bar{\Delta}(0) \bar{\Sigma}_{L11}(0) \}^{-1} f(y_{2e}, \mu).
$$

Then, for fixed $\bar{\Delta}(0)$ and μ , all equilibria $[x_e^T \delta_e^T]^T$ can be parametrized only by the steady state output y_{2e} as [\(1.4\)](#page-6-0) and [\(1.5\)](#page-6-0). The existence of a real solution y_{2e} of [\(1.3\)](#page-5-1) is equivalent to the existence of an equilibrium $[x_e^T \delta_e^T]^T$. From this equivalence, we can prove $(T1)$.

By using the representation $M(D_0)$, the equilibrium x_e of [\(1.4\)](#page-6-0) can be written as $x_e = -A^{-1}(\mu)M(\bar{\Delta}(0))f(y_{2e})$. From the assumption that $M(D_0)$ is of full column rank for all $D_0 \in \mathcal{U}_0(\gamma)$, the map from $f(y_{2e})$ to x_e is one-to-one. In other words, two equilibria x_e and $x'_e \neq x_e$ are distinguishable by two vectors $f(y_{2e}, \mu)$ and $f(y'_{2e}, \mu)$ ($\neq f(y_{2e}, \mu)$). In addition, a solution of the static equation [\(1.3\)](#page-5-1) is determined by an intersection of linear and nonlinear functions. Then, $f(y_{2e}, \mu) \neq f(y'_{2e}, \mu)$ if and only if $y_{2e} \neq y'_{2e}$. The number of the isolated real solutions y_{2e} of [\(1.3\)](#page-5-1) is equivalent to that of the isolated equilibria x_e . This completes the proof of Theorem [1.1.](#page-5-2)

A solution of the static equation [\(1.3\)](#page-5-1) with $D_0 = \Delta(0) \in \mathcal{U}_0(\gamma)$ is denoted by $y_{2ei}(\Delta)$, $i = \{1, 2, ..., N\}$. The sets of such potential steady state outputs $y_{2ei}(\Delta)$, $i = \{1, 2, ..., N\}$ for all $\Delta \in \mathcal{U}(\gamma)$ are denoted by

$$
\mathscr{Y}_{2ei}(\gamma) := \{ y_{2ei}(\Delta) \mid \Delta \in \mathscr{U}(\gamma) \}, \quad i = \{1, 2, \dots, N \}. \tag{1.6}
$$

In the next subsection, we analyze hyperbolicity of the equilibria determined by the elements of $\mathscr{Y}_{\text{rel}}(\gamma)$.

To evaluate the set $\mathcal{Y}_{2ei}(\gamma)$, we need to solve the nonlinear static equation [\(1.3\)](#page-5-1) for all $D_0 \in \mathcal{U}_0(\gamma)$. In general, it is hard to precisely solve such equations. However, in the case that f is monotonic, we can easily solve the equation. See the following two remarks and two examples with single-input and single-output nonlinear feedback systems.

Remark 1.1 Assume that $f(y_2, \mu)$, $y_2 \ge 0$, $\ell = m = 1$ is a positive and monotonically decreasing function as illustrated in Fig. [1.3.](#page-7-0) In that case, there exists a unique equilibrium. In addition, we can evaluate $\mathcal{Y}_{2e1}(\gamma)$ as follows. First, we evaluate the range of the function

$$
h(d_0) = \left\{ \frac{d_0 \bar{\Sigma}_{L21}(0) \bar{\Sigma}_{L12}(0)}{1 - d_0 \bar{\Sigma}_{L11}(0)} + \bar{\Sigma}_{L22}(0) \right\}
$$

for all $d_0 \in [-\gamma, \gamma]$. If min $h(d_0) > 0$ holds, then $\mathscr{Y}_{2e1}(\gamma)$ is given by [y_{2emin} , *y*₂*e*max], where *y*₂*e*min and *y*₂*emax* are the unique solutions of *y*₂=(min *h*(*d*₀))*f*(*y*₂, μ) and $y_2 = (\max h(d_0)) f(y_2, \mu)$, respectively. We can evaluate $\mathcal{Y}_{2e1}(\gamma)$ by simple calculations.

Remark 1.2 Assume that $f(y_2, \mu)$, $y_2 \ge 0$, $\ell = m = 1$ is monotonically increasing and satisfies $f(0) = 0$ as illustrated in Fig. [1.4.](#page-7-1) Then, the equilibrium uniquely exists and $\mathscr{Y}_{2e}(\gamma_0) = \{0\}$ if there is no solution of $y_2 = (\max h(d_0))f(y_2, \mu)$ except for $y_2 = 0$. There possibly exist multiple equilibria for such an activation function as illustrated in Fig. [1.4,](#page-7-1) which connects to the saddle-node bifurcation and its robustness analysis.

1.3.2 Robust Hyperbolicity Analysis

From Theorem [1.1,](#page-5-2) we can evaluate the region that contains all potential equilibrium points. Suppose that the number of the equilibria is constant for all $\Delta \in \mathcal{U}(\gamma)$. Then, the set of potential equilibrium points associated with $\mathcal{Y}_{2ei}(\gamma)$ is evaluated by [\(1.4\)](#page-6-0) and [\(1.5\)](#page-6-0), which are defined in the proof of Theorem [1.1](#page-5-2) as

$$
\mathscr{X}_{ei}(\gamma) := \{ [x_e^\mathsf{T} \delta_e^\mathsf{T}]^\mathsf{T} \text{of } (1.4) \text{ and } (1.5) \, | \, y_{2ei} \in \mathscr{Y}_{2ei}(\gamma) \}.
$$

In this subsection, we analyze hyperbolicity of potential equilibria in $\mathscr{X}_{ei}(\gamma)$, $i =$ {1, 2,...,*N*}.

We define robust hyperbolicity for each $\mathscr{X}_{ei}(\gamma)$, $i = \{1, 2, ..., N\}$ of the feedback system (Σ, Δ) .

Definition 1.2 (*robust hyperbolicity*) For a given $\gamma > 0$, the set $\mathscr{X}_{ei}(\gamma)$ is said to be $\mathcal{U}(\gamma)$ -robustly hyperbolic if the following conditions hold.

- (D1) The set $\mathscr{X}_{ei}(\gamma)$ is connected
- (D2) The equilibrium $[x_e^T \delta_e^T]^T$ of [\(1.4\)](#page-6-0) and [\(1.5\)](#page-6-0) associated with $y_{2ei}(\Delta)$ is hyperbolic for all $\Delta \in \mathcal{U}(\gamma)$.

In the work by the authors $[26]$ $[26]$, the robust hyperbolicity is defined and its analysis method is provided. The paper $[26]$ $[26]$ assumes that the location of the unique equilibrium point x_e is not affected by the uncertainty $\Delta \in \mathcal{U}(\gamma)$. In other words, modeling errors exist only at high-frequencies and $\bar{\Delta}(0) = 0$ holds. On the other hand, in this chapter, the assumption of the steady state gain $\bar{\Delta}(0)$ is removed. In that case, the location and even existence of equilibria are uncertain as studied above.

Remark 1.3 The condition (D2) in Definition [1.2](#page-8-1) additionally implies that the dimension of the unstable manifolds at any equilibrium point $[x_e^T \delta_e^T]^T \in \mathcal{X}_{ei}(\gamma)$ of the feedback system (Σ, Δ) is constant for all $\Delta \in \mathcal{U}(\gamma)$ including the nominal case that $\Delta = 0$.

We derive a robust hyperbolicity condition for the set $\mathscr{X}_{ei}(\gamma)$. To this end, we linearize the feedback system (Σ, Δ) at an equilibrium point $[x_e^\mathsf{T} \delta_e^\mathsf{T}]^\mathsf{T} \in \mathcal{X}_{ei}(\gamma)$.

The Jacobian matrix of the function $f(y_2, \mu)$ for a fixed μ is denoted by

$$
J_f(y_{2ei}) = \frac{\partial f}{\partial y_2}\bigg|_{y_2=y_{2ei}}
$$

.

Suppose that $I - J_f(y_{2ei})D_{22}(\mu)$ is nonsingular for all $y_{2ei} \in \mathscr{Y}_{2ei}(\gamma)$, i.e., the feedback loop in Σ_L and f is well-posed. Then, the feedback system (Σ, Δ) is linearized at the equilibrium point $[x_e^T \delta_e^T]^T$, and is represented by the feedback system $(\Sigma_{\gamma_{2e}};\Delta)$ composed of the linearized system

$$
\Sigma_{y_{2ei}}: \begin{cases} \dot{x} = \hat{A}(\mu)x + \hat{B}(\mu)u_1, \\ y_1 = \hat{C}(\mu)x + \hat{D}(\mu)u_1, \end{cases}
$$

and the uncertainty $\Delta \in \mathcal{U}(\gamma)$, where

$$
\begin{bmatrix}\n\hat{A}(\mu) & \hat{B}(\mu) \\
\hat{C}(\mu) & \hat{D}(\mu)\n\end{bmatrix} = F_1 \left(\begin{bmatrix}\nA(\mu) & B_1(\mu) & B_2(\mu) \\
C_1(\mu) & D_{11}(\mu) & D_{12}(\mu) \\
\overline{C_2(\mu) & D_{21}(\mu) & D_{22}(\mu)}\n\end{bmatrix}, J_f(y_{2ei}) \right),
$$

and $F_1(X, Y)$ is the lower LFT representation as follows:

$$
F_1(X, Y) = X_{12}Y(I - X_{22}Y)^{-1}X_{21} + X_{11}.
$$

For a fixed steady state output y_{2ei} and the linearized feedback system ($\Sigma_{y_{2ei}}, \Delta$), a robust hyperbolicity condition [\[26\]](#page-15-10) is proposed based on the Nyquist stability criterion [\[27](#page-15-11)]. The proof is essentially equivalent to that of the robust stability condition [\[23,](#page-15-7) [24\]](#page-15-8) except the assumption on stability and the norm of $\Sigma_{y_{2e}}$.

Theorem 1.2 [\[26](#page-15-10)] (linear robust hyperbolicity condition) *Consider an equilibrium* x_{ei} *and its corresponding steady state output* y_{2ei} *in the feedback system* (Σ, Δ) *for a fixed* μ *. Assume that the linearized system* $\Sigma_{y_{2e}i}$ *has no neutral pole and its realization* $(\hat{A}(\mu), \hat{B}(\mu), \hat{C}(\mu))$ *is controllable and observable. Then, for a given set* $\mathscr{U}(\gamma)$ *, the set* {*x_{ei}*}*, that is, the equilibrium point x_{ei}, is* $\mathscr{U}(\gamma)$ *<i>-robustly hyperbolic if and only if*

$$
\|\Sigma_{y_{2ei}}\|_{L_{\infty}} < 1/\gamma \tag{1.7}
$$

holds.

Proof (*Sufficiency*) We denote the transfer function matrix representation of $\Sigma_{y_{2e}}$ as

$$
\bar{\Sigma}_{y_{2ei}}(s) = \hat{C}(\mu)(sI_n - \hat{A}(\mu))^{-1}\hat{B}(\mu) + \hat{D}(\mu).
$$

Since $\|\Sigma_{\gamma_{2ei}}\|_{L_{\infty}} \|\Delta\|_{H_{\infty}} < 1$ and

$$
\sup_{\text{Re}[s]=0} \rho\{\bar{\Sigma}_{y_{2ei}}(s)\bar{\Delta}(s)\} \leq \sup_{\text{Re}[s]=0} \overline{\sigma}\{\bar{\Sigma}_{y_{2ei}}(s)\bar{\Delta}(s)\}
$$

hold, there exists a positive constant ε_1 such that

$$
\rho\{\bar{\Sigma}_{y_{2ei}}(j\omega)\bar{\Delta}(j\omega)\}\leq 1-\varepsilon_1, \ \forall \omega\in\mathbb{R}.
$$

Then, for some positive constant ε_2 ,

$$
|\det\{I_p - \bar{\Sigma}_{y_{2ei}}(j\omega)\bar{\Delta}(j\omega)\}| \geq \varepsilon_2, \ \forall \omega \in \mathbb{R}
$$

holds. This implies that the linearized feedback system ($\Sigma_{\nu_{2g}}$, Δ) is well-posed and has no neutral pole.

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(*Necessity*) We suppose that [\(1.7\)](#page-9-0) does not hold, that is, there exists ω_1 such that

$$
\|\Sigma_{y_{2ei}}\|_{L_{\infty}} = \overline{\sigma}\{\Sigma_{y_{2ei}}(j\omega_1)\} \ge 1/\gamma
$$

holds to show that there exists $\Delta \in \mathcal{U}(\gamma)$ such that either a feedback system is not well-posed or it has a neutral pole. First, by the singular value decomposition, $\Sigma_{y_{2e}}(j\omega_1)$ can be represented by

$$
\bar{\Sigma}_{y_{2ei}}(j\omega_1) = U\Sigma_g V^*, \quad \Sigma_g = \begin{bmatrix} \sigma_1 & 0 \\ & \ddots & \\ 0 & 0 \end{bmatrix},
$$

where $U \in \mathbb{C}^{p \times p}$, $V \in \mathbb{C}^{q \times q}$ are unitary matrices and $\sigma_1 = ||\Sigma_{\gamma_{2e}}||_{L_{\infty}}$. Since all of the diagonal elements of Σ_g other than the (1, 1) element are not necessary in the following discussion, their descriptions are omitted. Next, we choose $\overline{\Delta}(s) \in RH_{\infty}$ such that

$$
\bar{\Delta}(j\omega_1) = V\Sigma_d U^*, \quad \Sigma_d = \begin{bmatrix} 1/\sigma_1 & 0 & \dots & 0 \\ 0 & 0 & & \\ \vdots & & \ddots & \vdots \\ 0 & & \dots & 0 \end{bmatrix}
$$

holds. Since $1/\sigma_1 \leq \gamma$ holds, $\overline{\Delta}(s) \in \mathcal{U}(\gamma)$. In addition, by using $E =$ diag{ $1, 0, \ldots, 0$ } we have

$$
\begin{aligned} \det\{I_p - \bar{\Sigma}_{y_{2ei}}(j\omega_1)\bar{\Delta}(j\omega_1)\} &= \det\{I_\ell - U\Sigma_g V^* V \Sigma_d U^*\} \\ &= |\det(U)|^2 \det\{I_\ell - E\} = 0. \end{aligned}
$$

If $\omega_1 = \infty$, the feedback system $(\Sigma_{y_{2e i}}, \Delta)$ is not well-posed. Else if $\omega_1 \in \mathbb{R}$, $\det\{I_p - \Sigma_{\gamma_{2e i}}(j\omega)\Delta(j\omega)\}\$ passes the origin of the complex plane and the feedback system ($\Sigma_{\gamma_{2ei}}, \Delta$) has the neutral pole $s = j\omega_1$. Then, the equilibrium is not $\mathcal{U}(\gamma)$ robustly hyperbolic. This completes the proof of Theorem [1.2.](#page-9-1)

By Theorem [1.2,](#page-9-1) we can solve the problem of robust hyperbolicity analysis for systems with dynamic uncertainties as well as the robust stability theorem [\[23\]](#page-15-7). The theorem is a natural extension of the robust stability theorem [\[23](#page-15-7)]. In the above, we use the L_{∞} norm to describe the condition of the theorem. The L_{∞} norm can be defined for any hyperbolic linear time-invariant system, and is equivalent to the H_{∞} norm for stable systems. Then, the condition of the theorem is reduced to the well-known small-gain theorem [\[28](#page-15-12)].

Remark 1.4 (Computation of L_{∞} *<i>norm*). To determine $\mathcal{U}(\gamma)$ -robust hyperbolicity of an equilibrium of an uncertain system, we need to compute the L_{∞} norm of a linear system. Some efficient L_{∞} norm computational algorithms are presented: for example, the Hamiltonian matrix approach [\[29](#page-15-13)] and the Riccati equation and linear matrix inequality approaches [\[30](#page-15-14), [31\]](#page-15-15).

*Remark 1.5 (Implication of L*_∞ *norm*). By simple calculations [\[23\]](#page-15-7), we can show that the L_{∞} norm of the linearized system $\Sigma_{\gamma_{2e i}}$ is equivalent to the conditional L_2 gain [\[32](#page-15-16), [33](#page-15-17)]

$$
\sup_{u \in L_{2\text{cond}} \setminus \{0\}} \frac{\| \Sigma_{y_{2ei}} u \|_{L_2}}{\| u \|_{L_2}}, \quad L_{2\text{cond}} := \{ w \in L_2 \mid \tilde{\Sigma}_{y_{2ei}} w \in L_2 \},
$$

where $\|\cdot\|_{L_2}$ is the L_2 norm of a signal and $\tilde{\Sigma}_{\nu_{2e_i}}$ is the operator representation of $\Sigma_{y_{2e}}$. The conditional L_2 gain can be defined even for unstable and nonlinear systems. This fact implies that it is possible to extend Theorem [1.2](#page-9-1) as a condition of linear systems for keeping the instability independently of uncertainties to that of nonlinear systems.

From Theorems [1.1](#page-5-2) and [1.2,](#page-9-1) we derive the robust hyperbolicity condition for the nonlinear feedback system (Σ, Δ) with uncertainty-dependent equilibria.

Theorem 1.3 *For a given set* $\mathcal{U}(\gamma)$ *, the set* $\mathcal{X}_{ei}(\gamma)$ *is* $\mathcal{U}(\gamma)$ *-robustly hyperbolic if the set* $\mathcal{X}_{2e}(\gamma)$ *is connected and the following conditions are satisfied for all* $y_{2ei} \in \mathscr{X}_{2ei}(\gamma)$.

- (C1) *The linearized system* $\Sigma_{\gamma_{2e}i}$ *has no neutral pole.*
- (C2) *Realization* $(\hat{A}(\mu), \hat{B}(\mu), \hat{C}(\mu))$ *is controllable and observable.*
- (C3) *Inequality* [\(1.7\)](#page-9-0) *holds.*

We can numerically check (C1)–(C3) by partitioning $\mathscr{X}_{ei}(\gamma)$. To check (C3), we transform the linearized system ($\Sigma_{\gamma_{2}i}$, Δ) into another feedback form composed of the linear system Σ_L and the uncertainty diag $\{J_f(y_{2ei}), \Delta\}$. The uncertainty part has block-diagonal structure and is included in the set diag $\{J_f(\mathscr{X}_{ei}(\gamma)), \mathscr{U}(\gamma)\}\)$. Then, we evaluate the hyperbolicity of the linear feedback system $(\Sigma_L, \text{diag}\{J_f(y_{2ei}), \Delta\})$ by computing the structured singular value [\[34](#page-15-18)] of Σ*^L* instead of the *L*[∞] norm. Obviously, when the norm of $J_f(y_{2ei})$ is sufficiently small, the theorem is corresponding to the robust stability theorem [\[23\]](#page-15-7) and the robust instability theorem [\[26,](#page-15-10) [35](#page-16-0)[–37\]](#page-16-1) for uncertain linear systems.

1.3.3 Robust Bifurcation Analysis

We propose a method for robust bifurcation analysis that is derived by utilizing Theorem [1.1](#page-5-2) for equilibrium analysis and Theorem [1.3](#page-11-1) for hyperbolicity analysis. In the method, $\mathcal{P}_{PB}(\gamma)$ is defined as a region that includes the potential bifurcation region $\mathscr{P}_{PB}(\gamma)$, i.e., $\mathscr{P}_{PB}(\gamma) \subseteq \mathscr{P}_{PB}(\gamma)$.

Procedure for robust bifurcation analysis: Repeat the following Steps (i) and (ii) for all parameter values $\mu \in \mathcal{P}$.

- (i) Solve the static equation [\(1.3\)](#page-5-1) for all $D_0 = \overline{\Delta}(0) \in \mathcal{U}_0(\gamma)$. If the number of the real solutions $y_{2ei}(\Delta)$ is constant for all $\Delta \in \mathcal{U}(\gamma)$ and each set $\mathcal{X}_{ei}(\gamma)$, $i = \{1, 2, ..., N\}$ is connected, then, go to Step (ii). Otherwise $\mu \in \mathcal{P}_{PB}(\gamma)$.
- (ii) Define the linearized system $\Sigma_{\gamma_{2}e^{i}}$ and evaluate the L_{∞} norm for all $\gamma_{2}e^{i} \in$ $\mathscr{Y}_{2ei}(\gamma)$, $i = \{1, 2, ..., N\}$. If all values of the L_{∞} norm are strictly less than $1/\gamma$, then, $\mu \in \mathscr{P} \backslash \mathscr{P}_{PB}(\gamma)$. Otherwise $\mu \in \mathscr{P}_{PB}(\gamma)$.

By this procedure, we can evaluate the potential bifurcation region $\mathscr{P}_{PB}(\gamma)$ more widely than the exact region. In general, to identify the type of bifurcation (saddlenode-type, Hopf-type, and so on) that occurs in $\mathcal{P}_{PB}(\gamma)$, we need additional assumptions. For example, under the assumption that $\bar{\Delta}(0) = 0$, we can show that at a saddle-node bifurcation point μ_{SN} for a nominal feedback system (Σ , 0) is *robustly* a saddle-node bifurcation point for all uncertain feedback system (Σ , Δ). We can prove this fact by showing that any uncertain feedback system (Σ , Δ) satisfies saddle-node bifurcation theorem (see e.g., Theorem [2.2](http://dx.doi.org/10.1007/978-4-431-55013-6_2) in [\[1](#page-14-0)]) as long as $\Delta(0) = 0$.

1.4 Examples of Robust Bifurcation Analysis

We illustrate a procedure of dynamic robust bifurcation analysis in the following examples for normal forms of various types of bifurcation.

1.4.1 Robustness Analysis of Saddle-Node Bifurcation

Let us consider the following normal form for saddle-node bifurcation with a dynamic uncertainty:

$$
\dot{x} = x^2 + \mu + u_1, \quad u_1 = \Delta x, \quad \Delta \in \mathcal{U}(\gamma).
$$

This uncertain model is written by the feedback form illustrated in Fig. [1.1](#page-2-0)To evaluate the potential bifurcation region, (1) first we study the existence and location of equilibria and (2) then testify the robust hyperbolicity of potential equilibria.

(1) Note that the equilibria are affected by the steady state gain $D_0 = \Delta(0) \in$ *U*₀(γ) and are determined by the intersection of $Δ_0x$ and $f(x) = x^2 + μ$. The equilibria exist at

$$
x_{ei}(D_0) = -D_0/2 \pm \sqrt{D_0^2/4 - \mu}, \ \ i = 1, \ 2
$$

for $\mu \leq D_0^2/4$, whereas no point exists for $\mu > D_0^2/4$. For any uncertainty $\Delta \in \mathcal{U}(\gamma)$, two equilibrium points encounter each other and vanish at $\mu \in [0, \gamma^2/4]$ along the parameter changing as illustrated in Fig. [1.5.](#page-13-0) This implies that the saddle-node bifurcation occurs, i.e., the number of the equilibria is varied by parameter variation, on $[0, \gamma^2/4]$ as long as $\Delta \in \mathcal{U}(\gamma)$.

Fig. 1.5 Robust bifurcation analysis for saddle-node bifurcation ($\gamma = 0.5$, $\mu \in \mathcal{P} := [-1, 1]$): The location and existence of the equilibria are affected by the uncertainties. The hyperbolicity of equilibria can be impaired for some uncertainty in the parameter region $[-3y^2/4, 0]$ and they can disappear and saddle-node bifurcation occurs in [0, $\gamma^2/4$]

(2) We further study the robust hyperbolicity of the equilibria for bifurcation analysis. Even if the equilibria exist, bifurcation can occur by hyperbolicity being impaired. Linearize the nonlinear feedback system at the points $x = x_e$ to obtain

$$
\Sigma_{y_{2ei}}: \begin{cases} \dot{\tilde{x}} = 2x_e \tilde{x} + u_1, \\ y_1 = \tilde{x} + x_e, \end{cases}
$$

where $\tilde{x} := x - x_e$. From Theorem [1.3](#page-11-1) for a fixed μ , the equilibria x_{e1} and x_{e1} are hyperbolic for all $\Delta \in \mathcal{U}(\gamma)$ if the L_{∞} norms of the linearized systems are strictly less than $1/\gamma$ for all $D_0 \in \mathcal{U}_0(\gamma)$. Therefore, we can show that the equilibria are hyperbolic for all $\mu < -3\gamma^2/4$ and there is no bifurcation point in the parameter region, although bifurcation occurs at $\mu \in [-3\gamma^2/4, \gamma^2/4]$ as illustrated in Fig. [1.5.](#page-13-0)

1.4.2 Robustness Analysis of Hopf Bifurcation

Consider the normal form for Hopf bifurcation with a dynamic uncertainty. The uncertain system is represented by the feedback form that is illustrated in Fig. [1.1,](#page-2-0) where Σ_L , *f*, and Δ are given by

$$
\Sigma_L: \begin{cases} \n\dot{x} = \begin{bmatrix} \mu - 1 \\ 1 & \mu \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u_1 + u_2, & f(y) = -|y|_2^2 y, & \Delta \in \mathcal{U}(y). \\ \ny_2 = x \n\end{cases}
$$

When $u_1 = 0$, the differential equation composed of Σ_L and f has the unique equilibrium at the origin for any parameter $\mu \in \mathbb{R}$. The existence and location of the equilibrium are independent of the feedback-type uncertainty. We perform dynamic robust bifurcation analysis of the origin. To this end, we have the linearized system $\Sigma_{y_{2e}}$ that is the same as Σ_L to compute the L_{∞} norm

$$
\|\Sigma_{y_{2ei}}\|_{L_{\infty}} = \begin{cases} 1/|2\mu|, & 0 < |\mu| \le 1, \\ 1/(\mu^2 + 1), & |\mu| > 1. \end{cases}
$$

Then, we evaluate the potential bifurcation region for the origin by

$$
\mathscr{P}_{PB}(\gamma) \subseteq \begin{cases} [-\gamma/2, \gamma/2], & 0 < \gamma \leq 2, \\ [-\sqrt{\gamma - 1}, \sqrt{\gamma - 1}], & \gamma > 2. \end{cases}
$$

1.5 Conclusion

In this chapter, we integrated a concept of bifurcation in dynamical systems theory and that of robustness analysis in control systems theory to propose dynamic robust bifurcation analysis. In the analysis, given an uncertain system described by a model set, we obtain an outer approximation of all the possible bifurcation points.

Acknowledgments The authors gratefully acknowledge Takayuki Arai, Masayasu Suzuki, and Takayuki Ishizaki for their comments and fruitful discussion on this research.

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