Technical Improvements

2

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2.1 Introduction

Hybrid imaging with combined positron emission tomography/magnetic resonance (PET/MR) imaging is the most recent hybrid imaging modality (Drzezga et al. 2012; Quick et al. 2013). It combines excellent soft tissue contrast and high spatial image resolution of MR imaging with metabolic information provided by PET, as integrated PET/MR systems acquire PET and MR data simultaneously (Delso et al. 2011; Quick 2014; Grant et al. 2016). Beyond exact coregistration of PET and MR data, this can be applied for MR-based motion correction of PET data.

The integration of PET detectors within MR imaging systems has been a challenging task that has been solved by different vendors introducing three different PET/MR systems in the years 2010–2014 (Delso et al. 2011; Quick 2014; Grant et al. 2016; Zaidi et al. 2011). When compared to hybrid PET/computed tomography (CT), PET/MR has demonstrated comparable PET image quality and PET quantification in numerous clini-

cal comparison studies (Drzezga et al. 2012; Quick et al. 2013; Wiesmüller et al. 2013). However, due to the missing CT component, attenuation correction in PET/MR has to be based on MR images and subsequent image segmentation. This turned out to be challenging and a wealth of methodological developments have been described in the recent literature.

Ultimately, the aim of all current technical and methodological developments in PET/MR is to further improve workflow, image quality, PET quantification, and to broaden the application spectrum of PET/MR in research and clinical applications. This chapter on technical developments highlights current developments in PET/ MR attenuation correction and motion correction, introduces new hardware developments, and discusses current research efforts on artifact correction and dose reduction in PET/MR hybrid imaging.

2.2 Attenuation Correction in PET/MR

PET is a quantitative imaging technique that facilitates the determination of the amount of radioactive tracer accumulation in a tumour, lesion or organ within the human body. In this context, attenuation correction (AC) describes a physical method to account for the self-absorption of the emitted annihilation photons in tissue and

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L. Umutlu, K. Herrmann (eds.), *PET/MR Imaging: Current and Emerging Applications*, https://doi.org/10.1007/978-3-319-69641-6_2

in hardware components. Attenuation correction, thus, is a pre-requisite for accurate quantification of the PET data (Kinahan et al. 1998). More specifically, the photons that originate from a positron annihilation within the body are attenuated by the surrounding tissues and by ancillary hardware components such as the patient table before they reach the PET detectors.

In combined PET/CT systems, the attenuation properties of tissue can be derived from the complementary CT images after a fast and straightforward conversion of the photon energy levels of CT-derived Hounsfield units (HU) to linear attenuation coefficients (LAC) for PET (Kinahan et al. 1998; Carney et al. 2006). In PET/MR, however, attenuation correction is methodologically challenging (Wagenknecht et al. 2013) as MR imaging measures magnetization densities and relaxation times of hydrogen nuclei in tissue. The MR signal, thus, depends on the amount of protons and their local chemical environment in tissues. As there is no direct physical dependency of proton density and proton spin relaxation times with local electron density, which causes the photon attenuation, it is not possible to derive PET attenuation properties of tissues directly from MR imaging measurements (Wagenknecht et al. 2013). To address this issue, different concepts for attenuation correction in PET/MR have been developed (Wagenknecht et al. 2013). The most widely used method for MR-based attenuation correction relies on the segmentation of MR images into different tissue classes, based on their image-based grey scales. Following segmentation, the individual tissue compartments (e.g., background air, fat, soft tissue, lung tissue) are then assigned a predefined LAC for the corresponding tissue (Martinez-Moller et al. 2009; Schulz et al. 2011). To this day, dedicated fast MR imaging sequences, such as Dixon VIBE (Martinez-Moller et al. 2009) or a fast 3D T1-weighted gradient-echo MR sequence, are applied to obtain images of tissue distribution and subsequent segmentation (Beyer et al. 2016). This general method of tissue segmentation from MR images is widely used in all currently available PET/MR systems (Beyer et al. 2016) (Fig. 2.1).

Although the MR-based segmentation techniques for AC in general provide reproducible and straightforward results in most clinical applications, multiple initial studies directly comparing PET quantification in PET/MR with PET/CT have indicated a small but systematic underestimation of PET quantification in PET/MR studies using these MR-based AC methods (Drzezga et al. 2012; Quick et al. 2013; Wiesmüller et al. 2013; Boellaard and Quick 2015). The observed underestimation of PET quantification in PET/ MR can be attributed to three methodological challenges of MR-based AC: First, MR-based AC lacks information about the attenuating properties of bone. Second, MR-imaging based AC often shows signal truncations along the patient arms, that are then not considered in MR-based AC. Third, the use of ancillary hardware components, such as RF coils in the field-of-view (FOV) of the PET-detector during simultaneous PET and MR data acquisition cause additional attenuation of photons (Boellaard and Quick 2015).

2.3 Attenuation Correction of Bone

Cortical bone is not considered in the standard MR-based AC approaches. Bone here is classified as soft tissue, consequently, the exact magnitude of PET signal attenuation of bone might be systematically underestimated (Samarin et al. 2012; Akbarzadeh et al. 2013). Samarin et al. (Samarin et al. 2012) evaluated and quantified the amount of underestimation when bone is assigned the linear attenuation coefficient of soft tissue. It was shown, that for most soft-tissue lesions in wholebody examinations, PET quantification would be biased by a few %-points only. In brain PET/MR and when imaging individual bone lesions, however, the classification of bone as soft-tissue causes a significant and regionally variable bias of 20-30% (Samarin et al. 2012). As potential solutions for AC of bone, the use of MR sequences with ultrashort echo times (UTE) (Keereman et al. 2010; Johansson et al. 2011; Navalpakkam et al. 2013; Berker et al. 2012; Grodzki et al. 2012) or zero echo time (ZTE) have been



Fig. 2.1 Whole-body MR-based attenuation correction maps in coronal orientation. The AC maps were acquired by scanning one volunteer on all three current PET/MR systems, the Philips Ingenuity TF PET/MR (**a**), the Siemens Biograph mMR (**b**), and the GE Signa PET/MR (**c**). Note that MR-based AC in (**a**) provides three attenuation classes (background, soft tissue and lung), while MR-based AC in (**b** and **c**) provides four classes (background, fat, soft tissue, lung). At the time of this study (2014), system (**c**) additionally provided bone in the head

proposed (Wiesinger et al. 2016; Delso et al. 2015). While studies have shown that UTE-based AC provide accurate PET quantification results when imaging the brain (Johansson et al. 2011; Navalpakkam et al. 2013), their use in body imaging applications is limited (Aasheim 2015). Here, the fact that UTE and ZTE sequences tend to increase image artifacts in large FOV applications such as in body imaging (Navalpakkam et al. 2013) is a practical limitation.

A fast and practical solution for bone AC in whole-body PET/MR has recently been suggested and evaluated (Paulus et al. 2015). This method applies a CT-based 3-dimensional bonemodel of the major bones (skull, spine, pelvic bones, upper femora) to the actual MR-based AC

station based on ultrashort echo time sequences. All three AC maps are limited by field-of-view truncations along the arms. Another general limitation in AC is the substitution of major bones by the attenuation coefficients of soft tissue. The figure reflects the state of MR-based AC in the year of measurement, i.e. 2014 (Beyer et al. 2016). To date (2017) further improvements such as bone detection and MR-based truncation correction have been implemented into new product software versions of the PET/MRI systems. (Modified from Beyer et al. 2016)

data of the patient under examination and, thus, adds another compartment for the AC of bone in whole-body PET/MR exams (Fig. 2.2) (Paulus et al. 2015). This method has recently been validated in whole-body and brain PET/MR exams with promising results towards improved MR-based AC (Paulus et al. 2015; Koesters et al. 2016; Rausch et al. 2017; Oehmigen et al. 2017).

2.4 Truncation Correction

Another limitation of MR-based AC is the fact that the transaxial FOV in MR imaging is limited to about 50 cm in diameter. Beyond these dimensions, MR images show geometric distortions and



Fig. 2.2 Example for model-based addition of major bones to patient-individual MR data as shown for the pelvic region (a, b). The bone model consists of a set of MR image and bone mask pairs that are registered to subject's Dixon-sequence images for each major bone

significant signal voids (Keller et al. 2013; Brendle et al. 2015a). This frequently results in truncation artifacts along the patient arms in MR-based AC, as has been shown for all three currently available PET/MR system designs (Beyer et al. 2016). Therefore, the patient body is not completely and correctly assessed in its overall dimensions and current shape. Thus, the human tissue AC based on truncated MR images does not consider the exact amount and position of tissues that contribute to PET signal attenuation, resulting in inaccurate values for PET quantification (Delso et al. 2010a; Schramm et al. 2013). Accurate PET quantification in PET/MR, thus, requires appropriate methods for truncation correction as part of the attenuation correction strategy.

individually. Panels (\mathbf{c} and \mathbf{d}) show the result of adding bone as additional attenuation class to a whole-body MR-based attenuation map in coronal and sagittal orientation, respectively. (Modified from Paulus et al. 2015)

An appropriate method for truncation correction that is used on all three currently available PET/MR systems is the so-called MLAA (maximum likelihood estimation of attenuation and activity) algorithm (Nuyts et al. 1999, 2013). This PET-based technique derives the outer patient contours from non-AC PET data. This information is then used to complement missing attenuation information from MR imaging data that is truncated due to the limited transaxial FOV of MR imaging (Nuyts et al. 2013). However, MLAA-based contour detection is mostly limited to radiotracers that show a considerable unspecific accumulation in the human body and blood pool, thus enabling the detection of the outer patient contour from PET signals.



Fig. 2.3 Example for a MR-based attenuation map showing the typical lateral signal truncations along the subjects arms in coronal and transaxial orientation (**a**). Truncations result from the limited field-of-view in MR imaging. Image (**b**) was acquired by applying an optimized read-out gradient field provided with the HUGE-method (Blumhagen et al. 2012, 2014). This results in a field-of-view extension and enables truncation correction of the MR-based attenuation correction maps (**b**). Truncation

Another method for truncation correction based on MR data was developed by Blumhagen et al. (Blumhagen et al. 2012). The method is referred to as HUGE ((B₀ homogenization using gradient enhancement) and enlarges the fieldof-view in MR imaging beyond the conventional 50 cm diameter (Blumhagen et al. 2012). Foundation of the HUGE method is the measurement of the static magnetic field (B0) and gradient field distributions in the specific PET/ MR system. Then, an ideal, non-distorted gradient field is calculated that is applied during MR-based AC in the lateral regions of the MR imaging FOV (Blumhagen et al. 2012). Thus, the lateral MR-based field-of-view can be extended to 60 cm in left-right direction to fully cover the patient's arms. The HUGE method has been successfully evaluated for truncation correction in whole-body PET/MR examinations in the past (Blumhagen et al. 2014). Further technical refinements of the prototype sequence and the combination of HUGE with a moving table acquisition have now resulted in the product version of HUGE that provides seamless MR

correction of the arms in (c) was achieved by applying the widely established MLAA method that derives truncated regions from PET data. The difference map in (d) visualizes the quantification bias (in %) between images (a) and (b), i.e. the quantitative gain by applying HUGE truncation correction. Note that truncation correction applied along the arms has also quantitative impact on the entire body volume (red and blue areas in (d)). (Modified from Lindemann et al. 2017)

data for truncation correction in PET/MR (Lindemann et al. 2017) (Fig. 2.3).

2.5 Motion Correction

The independent and simultaneous PET and MR data acquisition in integrated PET/MR systems inherently offers the potential for motion correction and co-registration of PET and MR data (Quick 2014). This can be considered a potential advantage over PET/CT, which is currently being further explored (Tsoumpas et al. 2010; Tsoumpas et al. 2011; Wuerslin et al. 2013; Grimm et al. 2015; Baumgartner et al. 2014; Catana 2015; Manber et al. 2015; Fürst et al. 2015; Fayad et al. 2015; Gratz et al. 2017). In PET/CT the CT data is static and is acquired only once at the beginning of a typical hybrid examination. Since CT data acquisition is very fast (seconds), CT images provides a snapshot of the body anatomy and state of motion at the time of data acquisition while whole-body PET data is acquired stepwise over several minutes. In

PET/MR, the MR data is acquired simultaneous to PET data, which usually takes several minutes, both for PET and MR data. This leads to less deviation and less gross motion between both imaging modalities when compared to PET/CT hybrid imaging (Brendle et al. 2013). Moreover, real-time MR imaging and 4D MR data of breathing motion can be used to retrospectively perform motion correction of PET data, providing improved fusion of PET and MR data sets (Tsoumpas et al. 2010; 2011; Wuerslin et al. 2013; Grimm et al. 2015; Baumgartner et al. 2014; Catana 2015; Manber et al. 2015; Fürst et al. 2015; Fayad et al. 2015; Gratz et al. 2017). Motion correction strategies in PET/MR, thus, potentially lead to improved lesion visibility in the upper abdomen and liver (Fig. 2.4). Additionally, motion correction may also result in better quantification of activity in lesions and tumours as well as in cardiovascular PET/MR studies since all moving structures are depicted with sharper contours and less smeared over a larger volume, which otherwise leads to reduced standardized uptake values (SUV) of regions subject to motion (Grimm et al. 2015) (Fig. 2.4). In a recent cardiac PET/MR feasibility study, motion correction strategies have been applied to breathing and cardiac motion to assess atherosclerotic plaques in the coronary arteries (Robson et al. 2017).

2.6 Attenuation Correction of Hardware Components

The previous sections have discussed techniques, limitations, and recent solutions for MR-based AC of the patient body. An additional source of attenuation of the annihilation photons in PET/ MR is the use of ancillary hardware components, such as the patient table and radiofrequency (RF) receiver coils that are placed around the patient body for MR signal detection. These hardware components also attenuate photons before they reach the PET detector and, therefore, may cause a bias of the PET quantification, as demonstrated in earlier studies (Delso et al. 2010b; Tellmann et al. 2011). The general concept for AC of hardware components in PET/MR is to generate CT-based attenuation maps of each hardware component that has to be corrected (Quick et al. 2013; Quick 2014), as it is the current standard method on all three current PET/MR systems. Therefore, three-dimensional (3D) CT-based



Fig. 2.4 Application of motion correction in a patient with two lesions in the lung and one lesion in the spine. A coronal PET image from a PET/MR study is shown. Image (**a**) was acquired using the standard free-breathing PET protocol with an acquisition time of several minutes. Image (**b**) was acquired by applying respiratory motion correction. For motion correction the MR data was used to

derive 3-dimensional motion fields over time that were then used for non-rigid registration of the PET data to one static, motion corrected 3D image. The motion corrected data in (b) provides sharper visualization and higher contrast of the two lesions in the lung, while the non-moving lesion in the spine shows identical image features (Modified from Gratz et al. 2017) attenuation templates for rigid and stationary RF coils such as the head/neck RF coil are added to the overall patient attenuation map prior to the PET data reconstruction (Quick 2014). By automatically linking the current patient table position during a patient examination to the known position of the individual RF coil on the system's patient table, CT-template-based AC can be performed during the PET data reconstruction process (Delso et al. 2010b). This AC method provides fast and accurate results for most of the RF coils that are delivered with the current PET/ MR systems. However, the 3D attenuation templates used during reconstruction can be misaligned with the actual RF coil position or not represent the actual attenuation of the RF coils used (Paulus et al. 2012). This is an inherent limitation for flexible (non-rigid) RF surface coils, which are frequently used in whole-body imaging applications to provide excellent MRI signal from the anterior body parts. Flexible RF coils are currently not routinely considered in CT-template-based AC since their position and/ or geometry during a PET/MR examination is not known and may differ from a pre-acquired 3D AC template (Paulus et al. 2012). It has been shown in previous studies, that the flexible standard multi-channel RF surface body coils attenuate the PET signal by only few %-points (Paulus et al. 2012, 2013; Wollenweber et al. 2014; Paulus and Quick 2016). Thus, the average attenuation due to flexible RF coils in routine applications of PET/MR seems negligible. However, PET quantification may be locally biased by up to 10-20% due to increased attenuation of PET signal in the immediate vicinity of single hardware components of the RF coils (Paulus et al. 2012, 2013; Paulus and Quick 2016). As an improvement to also consider flexible RF coils in AC, it has been suggested to detect the actual position of flexible RF coils in MR images by using MR visible markers (Kartmann et al. 2013; Eldib et al. 2014) or by using residual MR signal from the RF coil housing when applying UTE sequences (Paulus et al. 2012; Eldib et al. 2015). This spatial information could then be used to align a pre-defined 3D AC template of the respective RF coil with its actual position during a PET/ MR examination as derived from MR images. The general concept for CT-based AC of hardware components in PET/MR is implemented in all currently available PET/MR systems for the range of rigid RF coils that are delivered with each PET/MR system (Quick 2014; Paulus and Quick 2016).

2.7 New Hardware Developments

The current PET/MR systems are all equipped with numerous RF coils to cover the patient from head to toe in whole-body imaging applications (Quick 2014; Beyer et al. 2016). Coverage of the entire patient body with RF surface coils is a general precondition for high quality MR imaging. In combined PET/MR, the RF coils are located in the FOV of the PET detector during simultaneous PET and MRI data acquisition. Thus, an additional design requirement for RF coil in PET/MR is, that the RF coils need to be as PET transparent as possible in order to reduce unwanted PET signal attenuation. Nevertheless, although designed PET transparent, all RF coils are subject to attenuation correction to provide accurate PET quantification as has been described in the previous section. A recent overview article by Paulus and Quick (2016) provides a summary of numerous RF coil developments for PET/MR applications and their individual impact on PET quantification (Paulus and Quick 2016).

To expand the portfolio of clinical applications of PET/MR and to improve dedicated examinations, new and specific RF coils were designed over the recent years for combined use in PET/MR. For example, new multi-channel RF head coils have been designed to improve neuro imaging and to increase the perfomance of simultaneous functional MR imaging (fMRI) with PET imaging (Sander et al. 2015). Three recent studies have described the design and implementation of bilateral breast RF coils for PET/MR breast imaging (Aklan et al. 2013; Dregely et al. 2015; Oehmigen et al. 2016). The integration of such breast RF coils requires a PET-transparent design and consideration of the ancillary RF coil



Fig. 2.5 Broadening the application spectrum of PET/ MR by integration of a breast radiofrequency (RF) coil. 16-channel breast RF coil that was designed PET transparent for use in PET/MR systems (Rapid Biomedical, Germany) (**a**). (**b**) 3-Dimensional CT-based attenuation template for attenuation correction of the RF coil housing. (**c**) Example case of patient with breast carcinoma imaged

hardware in the attenuation correction (Aklan et al. 2013; Dregely et al. 2015, 2016). Figure 2.5 provides an example of a 16-channel breast RF coil that was implemented into an integrated PET/MR system with hardware attenuation correction (Oehmigen et al. 2016).

Two recent studies describe the development of equipment for radiation therapy (RT) planning for use in PET/MR. The overall aim of this endeavour is to integrate PET/MR hybrid imaging into the concept of RT planning, which would further broaden the application spectrum of PET/ MR (Paulus et al. 2014, 2016). The developments encompass PET transparent hardware components such as a table platform with indexing system and RF coil holders for head/neck imaging as well as for body imaging (Paulus et al. 2014, 2016). All components have been evaluated for

on PET/MR with the RF breast coil. (d) Quantitative evaluation of activity concentration in the breast tumour along the red arrow (in c). The blue line plot shows the activity in the tumour after attenuation correction of the RF breast coil. The red line plot shows lower activity values because the RF breast coil here was not included in attenuation correction. (Modified from Oehmigen et al. 2016)

use in PET/MR. A systematic µmap generator ensures accurate attenuation correction of all RT equipment in the FOV of the PET detector (Paulus et al. 2014). All these recent RF coil and hardware component developments have laid the groundwork for new clinical applications of PET/ MR and further developments of dedicated RF coils are ongoing. The additional efforts in hardware component AC at the same time ensure accurate PET quantification for these exciting new applications (Paulus and Quick 2016).

2.8 Artifact Correction

The implementation of new imaging modalities and / or technical systems goes hand in hand with new types of artifacts. The complexity of integrated PET/MR hybrid imaging bears the potential for an exaggeration of new artifacts, when compared to two independent systems. Beyond the potential affection of the visual impression of either PET or MR data, artifacts in PET/MR may also have a significant effect on quantification of PET data. Artifacts in integrated PET/MR may result from the technical crosstalk between the PET and the MR components (Delso et al. 2011; Quick 2014), e.g. when both imaging centers may not be co-aligned correctly (Brendle et al. 2013). Differences in the data acquisition speed between PET and MR might lead to local misalignments and motion artifacts due to patient and organ motion (Brendle et al. 2013). In MR-based AC all deviations from the real physical photon attenuation will ultimately lead to inaccurate values in PET quantification following AC (Keereman et al. 2011; Ladefoged et al. 2014; Brendle et al. 2015). Furthermore, the administration of contrast agents before the application of MR-based AC may lead to errors in MR-based tissue segmentation due to changes in tissue contrast (Ruhlmann et al. 2016). Per definition, the signal truncations as discussed above also represent MR-based artifacts that have an influence on PET quantification (Delso et al. 2010a; Blumhagen et al. 2012, 2014). A frequent source for MR-based artifacts are dental and metal implants that are found in a large and increasing group of patients (Gunzinger et al. 2014; Ladefoged et al. 2015; Schramm et al. 2014). Apart from the safety aspects of metal implants that have to be clarified for any MR examination, all metal implants might cause signal voids or local distortions in MR images and in MR-based AC, that exceed the physical implant volume. During image segmentation, such signal voids might then be assigned with the low linear attenuation coefficients of air (Gunzinger et al. 2014; Ladefoged et al. 2015; Schramm et al. 2014).

While initial publications dealt with the description of artifacts and evaluation of their impact on PET/MR, more recent studies now report about developments to correct for artifacts. A relatively simple approach to improve the MR-based µmap, is to use inpainting to fill

signal voids arising from metal artifacts (Ladefoged et al. 2013). Thus, signal voids simulating regions with the low LAC of air are removed and the higher value LAC of the surrounding tissue is assigned (Ladefoged et al. 2013). Beyond the visual improvement of data, this may improve PET quantification as well. However, when larger metal and ceramic implants such as knee or hip joints are involved, PET quantification following µmap inpainting will still be biased due to the fact, that the real high LAC of these metallic implants is not accurately considered. Fuin et al. have suggested a method to complete signal voids in the MR-based attenuation correction data caused by implants by deriving the shape and AC values of metal implants from PET emission data (Fuin et al. 2017). In the context of metal artifact reduction in PET/MR, it has been shown that time-of-flight (TOF) PET detection with fast PET detectors allows for a significant visual reduction of artifacts in the µmap (Davison et al. 2015; Ter Voert et al. 2017), albeit PET quantification may still be biased. For the near future, it is expected that also the current breed of new artifact reducing MR imaging sequences (e.g. MAVRIC, VAT, WARP, etc.) (Sutter et al. 2012; Talbot and Weinberg 2016; Dillenseger et al. 2016; Jungmann et al. 2017) will find their implementation in dedicated PET/MR imaging protocols. In MR-only applications, such sequences have facilitated a significant reduction of the volume of distortions and signal voids around metallic implants (Sutter et al. 2012; Talbot and Weinberg 2016; Dillenseger et al. 2016; Jungmann et al. 2017). In the PET/MR regime, this could be used to further improve µmaps, and consequently, to improve PET quantification in PET/MR of patients with implants.

2.9 Dose Reduction

Integrated PET/MR hybrid imaging in selected clinical applications inherently reduces the overall patient radiation dose when compared with PET/CT by replacing ionizing CT imaging by non-ionizing MR imaging (Boellaard et al. 2010). Depending on the clinical indication, replacing CT by MR imaging in the context of PET hybrid imaging theoretically may save half of the overall radiation dose or an even higher fraction when compared with high-resolution diagnostic CT imaging (Boellaard et al. 2010). Further potential for radiotracer dose reduction in integrated PET/MR resides in the possibility of decreasing the applied activity deriving from the administered PET radiotracer. PET image quality in general is influenced by two key factors, acquisition time and injected activity, as both affect count statistics, image signal, and image noise. In PET/MR imaging, radiotracer dose reduction by injecting less tracer activity may be achieved by turning the comparatively prolonged data acquisition times into an advantage. In conventional PET/CT hybrid imaging, the PET data acquisition times typically amount to 2-3 min per bed position (Boellaard et al. 2010). In integrated PET/MR hybrid imaging, the MR examination time may be longer depending on the study protocol and clinical application field, respectively.

The higher sensitivity and larger volume coverage of new PET detectors in PET/MR systems compared to PET/CT (Delso et al. 2011) provides a third precondition for the potential to reduce the applied activity while maintaining high SNR and excellent PET image quality (Queiroz et al. 2015).

These potential advantages of PET/MR towards reducing the overall radiation dose compared to PET/CT is currently explored in selected studies. Based on the findings in controlled phantom studies (Oehmigen et al. 2014), or by simulating reduced amounts of applied activity by shortening the acquired PET list-mode data (Hartung-Knemeyer et al. 2013; Gatidis et al. 2016c), initial studies indicate that the reduction of radiotracer does not hamper diagnostic image quality in PET/MR examinations (Hartung-Knemeyer et al. 2013; Seith et al. 2017). These efforts can be considered particularly important in clinical settings for pediatric imaging or repetitive scans for therapy monitoring or surveillance (Gatidis et al. 2016a, b).

Conclusion

Today, many of the technical and methodological challenges of PET/MR imaging that were considered roadblocks to clinical PET/MRI during the early phase of implementation have been overcome. Numerous innovative solutions for attenuation correction, truncation correction, and motion correction have been suggested and scientifically evaluated during the past years. Of these, some of the most accurate and practical developments have found their way from research applications into the most recent product software applications of all PET/MR systems. Together with further hardware developments, this emerging hybrid imaging method is constantly improved and the clinical application spectrum of PET/ MR is further increased.

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